## ACCOUNT OF THE OPERATIONS OF

## THE GREAT TRIGONOMETRICAL SURVEY OF INDIA

## VOLUME IVA.

## **GENERAL DESCRIPTION**

OF THE

## PRINCIPAL TRIANGULATION

OF

## THE JODHPORE AND THE EASTERN SIND MERIDIONAL SERIES

OF

# THE NORTH-WEST QUADRILATERAL,

WITH THE DETAILS OF THEIR REDUCTION AND THE FINAL RESULTS.

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#### THE EASTERN SIND MERIDIONAL SERIES-(Continued).

REDUCTION CHART OF THE JODHPORE MERIDIONAL SERIES.

DITTO THE EASTERN SIND DITTO.

The present volume forms one of that series of publications, known as the "Account of the Operations of the Great Trigonometrical Survey of India," of which the design is, as has already been stated in the second volume of the series, "to give full reports—historical and descriptive—of the nature and the general "procedure of the operations; to describe the instruments which were employed in executing the several "linear and angular measurements; to furnish complete details of the actual facts of observation and the "methods of reduction by which these facts have been combined together and duly harmonized; and lastly, "to give the results which have been determined after this final reduction of the operations."

The first volume of the series accordingly gives the details of the measurements of the several baselines on which the triangulation of India rests, together with a discussion of the instruments on which the measurements depend, and the theoretical probable errors of the results. Volume II describes the principal triangulation, the theodolites with which it was executed, the procedure adopted in observing the angles, and all necessary details of the operations carried on in the field; it further describes the processes by which preliminary results were obtained from the observations, to satisfy immediate requirements, pending the completion of the several chains of triangles; also the method of final reduction which was adopted after the chains were completed, and by which the errors at the junctions of the chains with each other and with the base-lines are eliminated with the closest possible approach to mathematical rigour. It states briefly at page 28, and explains more fully at pages 162 to 170, the reasons why the method of final reduction could only be applied to limited portions of the triangulation at a time, thus necessitating the division of the triangulation into five great sections, to be reduced in succession, as indicated at page 32. It shows how the whole of the triangulation contained in the first of these sections-known as the North-West Quadrilateral-was reduced simultaneously; and, together with Volumes III and IV, it gives all the facts of angular observation appertaining to that Quadrilateral, full details of the preliminary and the final reductions of the angles and the several trigonometrical figures, and finally, the resulting values of the lengths and azimuths of the sides of the triangles and the latitudes and longitudes of the stations.

Volume V deals with a subject of its own, the Indian Pendulum Operations, which is quite unconnected with the triangulation and therefore need not be here noticed.

Volume VI treats almost entirely of the triangulation appertaining to the South-East Quadrilateral, the second of the five great sections into which the principal triangulation of India has been divided for final reduction. It commences with a brief recapitulation of the formulæ employed in the calculations, in order

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to obviate the necessity for frequent reference to Volume II, and then gives first, a complete exposition of the Simultaneous Reduction of the six chains or series of triangles forming the South-East Quadrilateral; and afterwards, for each series, an introductory account of the operations, a descriptive list of the stations, an abstract of the observations of each angle, full details of the preliminary reductions of the angles—made to satisfy the geometrical conditions of the trigonometrical figures—the final values of the angles after having been corrected to satisfy the conditions of the Quadrilateral, and finally, the resulting values of the lengths and azimuths of the sides, and of the latitudes and longitudes of the stations of the triangulation.

In like manner Volumes VII and VIII treat of the triangulation appertaining to the North-East Quadrilateral, the third of the five great sections before alluded to; and contain full details of the observations, reductions and final results of the sixteen chains or series of triangles embraced within the limits of that Quadrilateral.

Volume IX is devoted to the Electro-Telegraphic Longitude Operations which have been carried out by the Survey of India Department; but as no attempt has yet been made in this Department, to solve the equations of condition presented by the several arcs of longitude already measured, no combination of these equations with those of the triangulation has been possible and therefore the subject of Volume IX like that of Volume V may at present be considered as distinct from that of the other volumes.

The present volume is the tenth of the series in order of publication but is numbered IVA as it forms a supplement to Volumes II, III and IV, in that it treats of the reduction of two of the chains of the North-West Quadrilateral, the Jodhpore and the Eastern Sind Meridional Series, which did not exist at the time the North-West Quadrilateral was finally reduced, and of which the execution had been postponed indefinitely, on account of their falling in a tract of country mostly desert and not so immediately requiring triangulation as other portions of India.

In order that the reader may obtain a clear conception of the triangulation of India as a whole, and the position of the two series which form the subject of this volume relatively to the other series and especially as to their position in the North-West Quadrilateral, a Skeleton Chart of the Principal Triangulation of India is given opposite this page. In this chart each line represents a chain of triangles. The chain which approximates to the meridian of 78° and extends from the extreme south of India to latitude 30°, where it terminates on the Dehra Dún Base-line at the foot of the Himalaya Mountaius, forms the back-bone of the triangulation, and is well known as the Great Meridional Arc of India, which was commenced by Colonel Lambton in Southern India, and carried upwards to the Himalayas by Colonel Everest; Colonel Lambton's portion has been revised of late years, with all the refinement which the latest and best instruments and the most approved procedure rendered possible. Of the remaining chains, some were accomplished in the earlier days of the Survey, when the instrumental equipment was generally very inferior to what it became subsequently, and when the procedure, as regards portions of the operations-more particularly the construction of towers for the principal stations in the plains-was still imperfect; other chains were executed in more modern times, with the best instruments and with the utmost possible refinement in every particular. The chains last executed are generally on a par with the Great Arc itself, while some are superior to it in accuracy. It so happened that lines of demarcation could be drawn broadly between the several chains of triangles, in such a manner as to divide the superior and the inferior chains into separate groups, each group containing a large number of interdependent chains; this circumstance was therefore availed of in designing

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Photonincographed at the Office of the Trigonometrical Branch, Survey of India, Delva Drin, April 1886.

the great sections into which the triangulation had to be divided for final reduction. The bounding chains of these sections are represented in the Skeleton Chart by thick black lines, while the intermediate and all other chains are shown by thin lines. It will be seen that there are five sections in all, of which four are quadrilateral figures, while the fifth—which lies to the south of the others—is a trigon. The four quadrilaterals meet at the point Kaliánpur,—approximately in latitude 24° and longitude 78°—which was employed by Colonel Everest as the central or reference station of the triangulation; they are therefore distinguished by the corresponding cardinal points—North-East, South-East, South-West, and North-West—with reference to the central station.

It has already been shown, in Section 7 of Chapter I of Vol. II, that the most accurate of all the chains of triangles are those which enter the North-West and the South-East Quadrilaterals; the least accurate enter the North-East and the South-West Quadrilaterals. When therefore the method for the general treatment of the principal triangulation had been elaborated and was ready to be put into practice, the Simultaneous Reductions were taken in hand in the following order, *first* the North-West Quadrilateral, *second* the South-East, *third* the North-East Quadrilateral, and *fourth* the two remaining chains of the North-West Quadrilateral—the subject of the present volume,—*fifth* the Southern Trigon (now in the press), and *sixth* the South-West Quadrilateral, of which the reduction is in course of completion.

Any description of the triangulation of this Survey and the operations connected therewith, from the observations of the angles to the deduction of the most probable and therefore final results, is naturally subdivisible under six heads; first, the general principles in accordance with which the operations have been conducted; second, the practical execution of the measurement of the augles; third, the general principles followed in the combination and adjustment of the individual angular measures, with a view to satisfying all the geometrical conditions involved, as well as the primary linear elements which are fixed by the baselines; fourth, the preliminary geometrical reduction of the individual triangles, polygons and net-works of which the chains are composed; fifth, the simultaneous reduction of each of the groups of chains, or sections, into which the triangulation has been divided for convenience; and sixth, the presentation of the most probable values of the magnitudes of the angles, of the lengths and azimuths of the sides of the triangles, and of the latitudes and longitudes of the stations of the triangulation, which are the final results of the several reductions. The first and third of these branches of the subject are of general application, and they form the principal matter of Volume II, which was intended to be introductory to all subsequent volumes relating to the triangulation. The second, fourth and sixth branches have special reference to individual series or chains of triangles. The fifth has reference to each of the sections or aggregations of chains grouped together for simultaneous reduction. In the present volume it has not been necessary to touch otherwise than lightly on the first and third divisions of the subject; but the remaining divisions, including the simultaneous reduction of each series, are dwelt on at length, and full numerical details are given for each of the chains of triangles.

For their linear and geodetic elements the Jodhpore and the Eastern Sind Meridional Series are dependent on the final elements of the Karáchi (Kurrachee) Longitudinal Series and the Sutlej and the Great Indus Series.

The present volume is divided into two parts. Part I is devoted to the final reduction of each series and Part II to the details of each series.

#### PART I.

Chapter I gives a general account of each chain of triangles, indicates their dependency on the North-West Quadrilateral for their fixed data and describes the structure of the principal stations.

Chapter II describes the procedure followed in the measurement of the horizontal angles, and the methods adopted in determining their weights; it quotes the mathematical formulæ employed in the reduction of the triangulation from Volume II, where they are demonstrated; it indicates the final adjustment of the trigonometrical determinations of height by connection with the main lines of spirit levels; and lastly, it indicates the general principles of the final reduction of each series.

Chapter III gives full details of the Simultaneous or Final Reduction of each Series separately as follows :---

First. Preliminary remarks.

Second. A synopsis of the independent partial reductions antecedent to the Final Reduction.

Third. A description of the Reduction Charts which are given at the end of the volume, and of which a careful study is essential to a clear understanding of the several processes of calculation.

Fourth. A general out-line of the formation of the Linear and Geodetic Equations of Condition, four in number for each series, which had to be satisfied, in order to produce the requisite consistency in the triangulation per se, and between it and the fixed elements on which it depended.

*Fifth.* The method of constructing the Coefficients of the Unknown Quantities in the Equations of Condition, showing the general notation which was adopted for expressing the values of these coefficients, and specifying every exception to the general form.

Sixth. A synoptical exhibition of the several Equations of Condition, showing at a glance the triangles of which the angular errors enter as unknown quantities into each of the four Equations of Condition.

Seventh. The Numerical Values of the Fixed Data on which each series is based.

*Eighth.* The Values of the Sides and Angles of the Circuit Triangles, as they stood before the Final Reduction.

Ninth. The Latitudes, Longitudes and Azimuths of the Stations on the right-hand flanks of the Circuit Triangles, as they stood before the Final Reduction.

Tenth. The Numerical Values of the Absolute Terms in the several Linear and Geodetic Equations of Condition.

*Eleventh.* The Numerical Values of the  $\mu$ s and  $\phi$ s, the geodetic summations—exhibited in the table at pages [42] and [43]—which are required in forming the Coefficients of the Unknown Quantities (the Angular Errors) in the Geodetic Equations of Condition.

Twelfth. The Numerical Values of the Coefficients, **b** and **c**, of the Unknown Quantities in the several Linear and Geodetic Equations of Condition.

Thirteenth. The Coefficients, 16 and C, of the Indeterminate Factors, in the equations in which the values of the Angular Errors are expressed in terms of those factors.

Fourteenth. The Equations between the Indeterminate Factors, showing every Significant Coefficient and Absolute Term as it stood, first on the formation of the equations, and secondly after the successive

eliminations of individual factors in the process of solution; finally, the numerical values of the Factors are given.

Fifteenth. The Values of the Errors, x, y and z, of the angles of each triangle, resulting from each Final Reduction and the subsequent apportionments of residual error.

Sixteenth. The Dispersion of the Residual Errors which were met with after the Final Reduction.

Seventeenth. A Statement of the Final Results of each reduction, shewing the numerical accuracy ultimately attained in the calculations.

Chapter IV gives the Reduction of the Non-Circuit Triangles of the two series,—viz., the triangles excluded from each Final Reduction—which was needed for the final adjustments of their angles, to satisfy the geometrical conditions of the polygonal figures to which they appertain.

#### PART II.

This part gives full details of the principal work of the two chains or series of triangles—from the observations of the principal angles to the determination of the final results, angular, linear and geodetic—series by series. The Secondary and Tertiary Triangulations which were executed pari passa with the principal triangulation for geographical and topographical purposes, are as usual relegated to the corresponding Synoptical Volume; the volumes of the Accounts of the Operations &c. being exclusively devoted to the details of the principal triangulation, excepting in so far that what has been done in the way of secondary and minor triangulation in each series, is described in the Introduction to the series.

It is now desirable to give first a summary, and afterwards a general explanation, of the information and numerical data which the present volume furnishes for each chain of triangles. Summarised they are as follows :---

1. Introduction.

2. Alphabetically arranged List of Stations.

3. Numerically arranged List of Stations.

4. The Description of Stations.

5. The Observed Angles, with the Weights of the Concluded Results.

6. The Reduction of the Polygonal Figures.

7. The Final Values of the Sides and Angles of the Triangles.

8. The computed Latitudes and Longitudes of the Stations and the Azimuths at each Station.

9. The trigonometrically determined Differences of Height of the Stations and the Absolute Height of each Station above the Mean Sea Level.

10. Astronomical Observations of the Azimuth, and their Reduction.

Plate. The Diagrams of the several Polygonal Figures contained in the series.

1. The Introduction gives a historical sketch of the progress of the whole of the operations in the field,—both principal and secondary—from year to year, mentions the Officers by whom they were conducted, and the theodolites with which the principal angles were measured, and indicates the work done by each of the Assistants.

2 and 3. It has been found convenient to indicate the Principal Stations by a system of numerals, as well as by their names. Consequently at the commencement of the details of each series two lists are given, in the first of which the stations are arranged alphabetically with the numbers opposite the names, in the second numerically with the names opposite the numbers. Roman numerals have been adopted throughout for the nomenclature of the stations, and they are progressive in order from south to north in the two chains, the first number for each series being unity.

4. The Descriptions of the Stations are based generally on those made originally by the observers and entered on the spot into the angle books, subject to such modifications as are occasionally required to take cognizance of any alterations which have been subsequently effected. They give the names of the district and the sub-division in which the station was situated at the time when its description was written. For information as to the general form and structure of the stations, reference should be made to Section 4 of Chapter I.

5. In the pages which are allotted to the observed horizontal angles, the name of the observer, the distinguishing number and the name of the maker of the theodolite, and the month and year in which the observations were taken, are specified for each station.

In the details of the measures of the angles are given the reference number of the station on which the telescope was set at the commencement of each round of measures, and the reading to which the azimuthal circle was set, after each 'change of zero'; thus the graduations of the circle to which the readings were taken, at every measure of any angle, may be readily ascertained for an investigation of the law of the graduation error, such as will be found for Troughton and Simms' 18-inch Theodolite No. 1, in Appendix No. 4 of Volume II.

In the right-hand column of the record are given M, the mean of the several groups of measures on each setting, w and  $\frac{1}{w}$ , the weight and its reciprocal of the angle as deduced from differences between individual measures and between individual groups, and C, the concluded value of the angle as thus derived from the observations only; for fuller explanations reference must be made to Section 4, Chapter VII, Volume II, to the example at page 342 of the same volume, and to Section 2 of Chapter II of this volume.

The abstracts of angles are followed by lists of the Sums of Squares of Apparent Errors of Single Observations and Single Zeros, which furnish data for the investigation of the average *e.m.s.* (theoretical error of mean square) of observation in a single measure of an angle, and the average *e.m.s.* of graduation *plus* observation in the mean of the measures on a single zero. Such determinations are made in the first instance for groups of angles measured by the same observer, with the same instrument, and under similar conditions, and then for various combinations of these groups. With data thus obtained, from series of triangles, for seven of the large theodolites which have been chiefly employed in the measurement of the principal angles, the investigation of the influences of Mixed Errors of Observation and Graduation was made which forms the subject of Section 3, Chapter VII, Volume II.

6. The Reductions of the several Polygonal Figures which are contained in each series show how the angles of which each figure is composed were made consistent and harmonious *inter se*, so as to satisfy all geometrical conditions, with due regard to the respective weights of the angles. Full explanation of the principles and the procedure of these reductions, will be found in Chapter VIII of Volume II, and the for-

mulæ are given in Section 3 of Chapter II of the present volume. The figures are numbered consecutively in each series. Diagrams of the figures are given in the Plates appertaining to each series. The small numerals within each of the observed angles correspond to the subscripts to the general symbol, x, which is employed to indicate the error of any angle, the numerical subscript denoting the angle. Thus on referring to the diagram of Figure No. 2 and to the reduction of that figure on page 71, x<sub>s</sub> is the error of the angle 3, at Station II between Stations I and III. The tabular statements of the reductions give, firstly the observed angles and the reciprocals of their weights; secondly the equations by the solution of which the geometrical conditions of the figure are satisfied,—see equations on page [12]; thirdly the equations between the 'indeterminate factors'; fourthly the values of the indeterminate factors; fifthly the values of the angular errors; and sixthly the summation of the products of the square of each error and its weight—the value of which summation is made a minimum, in order that the values to be obtained for the several angular errors may be the most probable of each of the many values by which the geometrical conditions of the figure may be satisfied. In the group of equations between the indeterminate factors, the coefficient of the pth factor in the qth line is the same as that of the qth factor in the pth line; thus if a diagonal line be drawn from the coefficient of the first term in the first line to that of the last term in the last line, the coefficients which are symmetrically disposed on opposite sides of this line will be identical with each other. Consequently only the coefficients on and above the diagonal have been given; the absence of those below is indicated by an asterisk.

8. The Tabular statement of the Triangles. The first two columns of this table give the number adopted for each triangle to designate its place in the series; this number is entered in the first column if the triangle appertains to the chains of single triangles forming the two circuits whose closing errors are eliminated by the Final Reduction; it is entered in the second column for the non-circuit triangles exterior to the chains. The triangles which enter the circuits are shown in the Reduction Charts (at the end of this volume) in firm lines, with their distinguishing numbers written in the centre; those which do not enter the circuits are shown in dotted lines, and their numbers are indicated by numerals of a smaller size than the former, commencing with 49 for the Jodhpore and 40 for the Eastern Sind Meridional Series, 48 and 39 being the numbers of the last of the circuit triangles in the respective series. The columns in the table which contain the corrections to the observed angles give, first the correction for the error of the angle, with reference merely to the triangle or polygonal figure to which it belongs, as obtained from the primary reductions; and secondly the further correction which has to be applied either for the apportionment of circuit error, should the angle appertain to one of the circuits, or for the restoration of consistency in the polygonal figure after the application of the circuit errors, should it appertain to a non-circuit triangle Finally, the corrected plane angles and the lengths of the sides are given, as computed by the rules of Plane Trigonometry, in accordance with Legendre's theorem; see Section 4 of Chapter II.

9. The Table of the Latitudes and Longitudes of the Stations and the Azimuths and Lengths of the Sides. The principles on which the calculations of the Geodetic Co-ordinates and Azimuths have been made and the method of computation, are fully explained in Sections 2 and 4 of Chapter IX of Volume II, and the formulæ are quoted in Section 5 of Chapter II of the present volume. All Azimuths are referred to the south point and are measured right round the horizon by the west.

10. The Determinations of the Differences of Height of the several stations have been obtained from the measurements of the vertical angles, as explained in Section 6 of Chapter II of this volume. It has not

been considered necessary to give the individual measures of these angles, as has been done for the horizontal angles, because this portion of the operations is less exact and important. But the mean of the whole of the measures of each vertical angle, the calculated mean value of the amount of refraction in each angle and of the coefficient of refraction, the hour of observation, the heights of the signal and of the observer's telescope above the summits of the stations, the differences of height of the said summits and the absolute heights above the mean-sea level, are given. The errors generated trigonometrically between the initial and terminal obligatory stations of each series, have been duly dispersed by the method of simple proportion over the intermediate trigonometrical values, as explained in Section 7 of Chapter II of the present volume.

It may be here stated that all trigonometrically determined heights invariably refer to the upper surfaces of the central masonry pillars at the principal stations. Spirit-leveled values on the other hand sometimes refer to the upper surface and sometimes to the basement of the pillar, whichever the leveling-staff was set upon; a description of the exact point of reference then becomes necessary.

11. Finally come the details and reductions of the Astronomical Observations which have been taken, at certain stations in each series, for the determination of the Azimuth of one of the surrounding stations, or of a referring mark, the angle between which and a contiguous station has been measured. The methods of observing and of reducing the observations are fully described in Chapter XII of Volume II. For reasons which are explained in the first section of that chapter, the results have not been used in the general reduction of the triangulation, further than to give a more exact mean value of the fundamental astronomical azimuth (at Kaliánpur) than the one obtained by the observations on the spot. At the end of the details of the determination of each azimuth, the difference between the observed value and the value obtained by calculation through the triangulation from the fundamental azimuth is given. These differences may be of much value in future investigations of the Figure of the Earth and of the influence of local attraction.

Full details regarding the Unit of the Linear Measures, the Base-lines, the Initial Elements of Latidue, Longitude and Azimuth, and the Elements of the Figure of the Earth which have been adopted in the calculations, will be met with in Volumes I and II. In this place it is only necessary to state that :--

(1). The Unit of Length is the Indian Standard 10-feet Bar A, the relations between which and the principal European Standards of Length are given at page 28 of Volume I.

(2). The adopted Elements of the Figure of the Earth—assumed to be spheroidal—are given at page [15] of this volume.

(3). The Longitudes depend on an astronomically determined value of the Longitude of the Madras Observatory, East of the Royal Observatory at Greenwich, which was deduced about the year 1815. The Longitude of the Madras Observatory has however been recently re-determined, by the Electro-Telegraphic method, by observations which were made at Greenwich, Mokattam (in Egypt), Suez, Aden, Bombay and at certain stations of the triangulation in India, and with the following preliminary results :--

|                | , h           | $\mathbf{m}$ | 8              |             |                                                 |
|----------------|---------------|--------------|----------------|-------------|-------------------------------------------------|
| Longitude of N | Aokattam 2    | 5            | 6.320 East of  | f Greenwich | Supplied by SirG. Airy, from observations taken |
| Increase for S | buez c        | 5            | 6.917          | <i></i>     | in connection with Transit of Venus in 1874.    |
| ,, A           | den o         | 49           | 42.656         | ,,          | By the exerctions of this Surror, see the       |
| ", E           | Bombay I      | 51           | 19·98 <b>3</b> | <b>)</b> )  | August Depart for 1876 77                       |
| " N            | fadras c      | 29           | 43.240         | دو          | Annual Report for 1870-77.                      |
| Longitude of   | –<br>Madras 5 | 20           | 59.416         | 33          |                                                 |

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This value of the Longitude of the Madras Observatory is equivalent to 80° 14' 51"; and as the originally adopted value, on which the longitudes of the whole of the stations of this Survey are based, is 80° 17' 21" see page 135 of Volume II—the following precept may be accepted with considerable confidence :—

# All the values of longitude in this volume require a constant correction, probably of -2' 30".

The orthography of Indian names in the present volume is in accordance with the provincial lists of spellings constructed under the immediate orders of the Government of India. The newly authorised spellings were adopted for all names and other words contained in these lists; but for words for which there was no specific authority, the spellings have been framed in accordance with the methods followed in the preparation of the published lists, reference being made in the present instance more particularly to the Gazetted Lists for Rajputana and for Bombay. As a general rule the pronunciations of the vowels are as follows:—a has a variable sound as in woman, rural, paltry;  $\dot{a}$  as in tartan; i as in bit;  $\dot{i}$  as in ravine; u as in bull;  $\dot{u}$  as in rural; o as in note; e as a in say; au as ou in cloud; ai as i in ride. Final vowels and those in well-known terminals are unaccented. When the popular spelling of a name has been accepted by Government, its correct transliteration is given in parenthesis where the name occurs for the first time.

It now only remains for me to state that the Introductory Chapters forming Part I of this volume are the work of Mr. W. H. Cole, M.A., Deputy Superintendent. The Introductions to both series were written by Major M. W. Rogers, R.E., Deputy Superintendent. The reduction of the Jodhpore Meridional Series was effected chiefly with the aid of Baboos Gunga Pershad, Gopal Chandra Sarcar and Kedar Nath, and that of the Eastern Sind with the aid of Baboos Gunga Pershad and Mizaji Lal. The volume like its predecessors has been printed at the Trigonometrical Branch Office at Dehra; Mr. Peychers and Baboo Gunga Pershad have rendered valuable service in the examination of the press proofs generally, and Mr. Peychers more particularly in regard to the numerical and mathematical details which require the utmost care in supervision through the press, and in this respect from his natural aptitude and experience his assistance has been most valuable.

DEHRA DUN, March, 1886. C. T. HAIG, COLONEL, R.E., Offg. Dy. Surveyor General, In charge Trigonometrical Surveys.

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## ERRATA ET ADDENDA.

### THE JODHPORE MERIDIONAL SERIES.

| PAGE | •                                             |     |                  |      |                      |
|------|-----------------------------------------------|-----|------------------|------|----------------------|
| IX   | line 5 from top                               | for | that all trouble | read | and that all trouble |
| XVII | "16 "                                         | "   | dhaude           | "    | dhands               |
| 24   | in some copies, third zero mean of last angle | "   | 10.22            | ,,   | 20.57                |

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## VOCABULARY OF CERTAIN NATIVE WORDS MADE USE OF IN THIS VOLUME.

| Obthography<br>Employed. | •     |              | Correct<br>Orthography. |              |             | MEANING.                                                   |  |  |  |  |  |  |
|--------------------------|-------|--------------|-------------------------|--------------|-------------|------------------------------------------------------------|--|--|--|--|--|--|
| Amír.                    |       | •••          | Amír                    | •••          |             | Title of the rulers of Sind.                               |  |  |  |  |  |  |
| Bajri                    | •••   |              | Bájri                   | •••          | •••         | A kind of grain, millet.                                   |  |  |  |  |  |  |
| Bhati Bájput             | •••   |              | Bhatti Rájpút           | •••          | •••         | A clan of Rájpúts, a warrior caste of India.               |  |  |  |  |  |  |
| Chunam ·                 |       | •••          | Chúna                   | · <b>·</b> · | •••         | Lime employed in preparing mortar.                         |  |  |  |  |  |  |
| Darbár                   |       | •••          | Darbár                  |              | •••         | Government.                                                |  |  |  |  |  |  |
| Draen                    | •••   | <del>-</del> | Dráíñ                   |              |             | Tracts of shifting sand.                                   |  |  |  |  |  |  |
| Jágír                    | ••••  |              | Jágír                   | •••          | •••         | Land given by Government as a reward for services.         |  |  |  |  |  |  |
| Jain                     |       | •••          | Jain                    | •••          |             | A sect of Hindus.                                          |  |  |  |  |  |  |
| Játs                     | ••••  |              | Játs                    | ۱            |             | Ditto.                                                     |  |  |  |  |  |  |
| Kacha                    | ••••  |              | Kachchá                 |              |             | Built of clay only; or of stone or unburnt brick and clay. |  |  |  |  |  |  |
| Mahárája                 | •••   |              | Mahárája                |              |             | A king or ruler.                                           |  |  |  |  |  |  |
| Maharáwal                | ···   | •••          | Maháráwal               | •••          | •••         | Ditto.                                                     |  |  |  |  |  |  |
| Mot                      | •••   |              | Moth                    |              |             | A kind of grain, pulse.                                    |  |  |  |  |  |  |
| Pargana                  | ,<br> | •••          | Pargana                 | •••          | •••         | A sub-division of a district.                              |  |  |  |  |  |  |
| Phog                     | •••   |              | Phog                    |              | •••         | A shrub of the Calligonum species.                         |  |  |  |  |  |  |
| Rao                      | •••   |              | Ráo                     |              | · <b></b> . | A chief.                                                   |  |  |  |  |  |  |
| Sardár                   | •••   |              | Sardár                  | •••          |             | A chief or headman.                                        |  |  |  |  |  |  |
| Tahsíl                   | •••   | •••          | Tahsil                  |              | •••         | Portion of a district subject to a Revenue Collector.      |  |  |  |  |  |  |
| Taluk }<br>Taluka }      |       | •••          | Taälluk<br>Taälluka }   |              | •••         | A sub-division of a district.                              |  |  |  |  |  |  |
| Thakur                   |       |              | Thákur                  | •            | •••         | Title of a Rájpút chief.                                   |  |  |  |  |  |  |
| Thána                    | · • • | •••          | Tháná                   |              | •••         | A small police sub-division.                               |  |  |  |  |  |  |
| Vishnu                   | •••   | •••          | Vishnu                  | · • •        |             | One of the three principal Hindu deitics.                  |  |  |  |  |  |  |

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## THE FINAL REDUCTIONS

OF THE

JODHPORE MERIDIONAL SERIES

AND OF THE

EASTERN SIND MERIDIONAL SERIES

OF THE

NORTH-WEST QUADRILATERAL.



, ,

#### CHAPTER I.

#### ACCOUNT OF THE TRIANGULATION OF THE JODHPORE AND EASTERN SIND MERIDIONAL SERIES.

## 1.

#### The Triangulation included in this Volume.

The Jodhpore and Eastern Sind Meridional Series form two of the internal chains of that section of the triangulation of India, designated the North-West Quadrilateral, which embraces all the principal triangulation between the parallels of 24° and 34° and the meridians of 67° and 78°.

These two series had not been commenced at the time, 1868, the Simultaneous Reduction of the North-West Quadrilateral was undertaken; and although they formed part of the scheme for the triangulation of India, it was considered undesirable to await their execution, for reasons which are fully stated in Section 7 of Chapter I of Vol. II of the *Account of the Operations of the Great Trigonometrical Survey of India*. It thus happens that while they are on a par with the most refined work of the Survey, they have had to be separately reduced to accord with the rest of the triangulation of the North-West Quadrilateral.

## 2.

#### The Observers and the Instruments employed on the Triangulation.

#### The Jodhpore Series, meridian 72<sup>1</sup>/<sub>2</sub>°.

This Series emanates from the side Súnda-Bonik of the Karáchi Longitudinal Series and closes on the side Kaimsir-Kanda of the Sutlej Series. It was commenced by Lieutenant (now Major) M. W. Rogers, R.E., in 1872-73, who advanced the principal chain a

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distance of 95 miles, fixing 12 stations forming a quadrilateral and two single polygons. Lieutenant Rogers having proceeded on furlough, the charge of the party was transferred to Lieutenant (now Major) J. Hill, R.E., who carried the chain of principal triangles a further distance of 90 miles by a series of consecutive polygonal figures. Captain Rogers returned from furlough and relieved Captain Hill of the charge of the party on the 20th November 1874, and during that and the following field season he succeeded in completing the Series. The chain is double throughout. It comprises 3 quadrilaterals, 8 single polygons, and 2 double polygons, and is 310 miles long. The instrument employed was Barrow's 24-inch Theodolite No. 2, of which a description will be found in Appendix No. 2 of Vol. II.

#### The Eastern Sind Series, meridian 70°.

Operations were commenced on this Series during the field season of 1875-76. While Captain Rogers was bringing the Jodhpore Meridional Series to a conclusion, he detached one of his assistants to commence the selection of stations on the meridian of 70°, starting from the Karáchi Longitudinal Series. The side Rojhra-Sandohar was selected as a base; and the neighbouring stations of Fulrár and Chánga having been destroyed, new ones were built on their sites and employed in constructing a hexagon about Sandohar. When he himself had brought the Jodhpore Series to a termination on the 3rd January 1876, he marched to the proposed northern terminus of the Eastern Sind Meridional Series to commence preliminary operations from that end. In the neighbourhood where the Series was to have closed to the north, several stations of the Great Indus Series had been washed away by the river, and Captain Rogers was obliged to adopt the side Dáowála-Máchka west of the meridian of 70° and to work on to this meridian. Only preliminary operations were carried on this season, the chain being laid out for 110 miles at its southern end and for 24 miles at the northern end. In the field season of 1876-77 the final observations were commenced and the Series was carried forward a distance of 125 miles from its southern terminus. During the next season the party was employed in Baluchistan; and the season following, war having broken out between India and Afghanistan, Captain Rogers was attached to the Force operating in the latter country from the south. Towards the end of 1879 Captain Rogers returned from Afghanistan but not in time to effect a full season's work on the Eastern Sind Meridional Series. He however advanced it 64 miles, and there then remained only so much as could be easily completed during one field season.

In April, 1880, Captain Rogers went to England on furlough, when the party proceeded to Mussooree, and during the recess season was placed temporarily under Mr. J. B. N. Hennessey, in addition to his other duties. At the end of the recess, having equipped the party for the field, Mr. Hennessey transferred it to Colonel Branfill, who met it in Sind on the 6th November, 1880. The remainder of the chain of principal triangles was then completed in about two and a half months. The Series is double throughout, comprising 3 quadrilaterals, 7 single polygons and 2 double polygons. The instrument employed by Captain Rogers was Barrow's 24-inch Theodolite No. 2, and that by Colonel Branfill was Troughton and Simms' 24-inch Theodolite No. 1.

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## [5]

## 3.

#### The Dependency of the Triangulation on the North-West Quadrilateral for the fixed data.

Both the Jodhpore and Eastern Sind Meridional Series emanate from the Karáchi Longitudinal Series; the former closing on the Sutlej Series, and the latter on the Great Indus. All these three appertain to the North-West Quadrilateral which, as already stated, had been finally reduced before the two chains were executed. The only connection between the chains, other than that through triangulation which stood finally reduced, is by a secondary series, and therefore their reduction consists of two independent operations. The fixed data for each were the length and position of the side of origin and the same elements of the closing side.

### **4**.

#### The Construction of the Principal Stations.

#### The Jodhpore Meridional Series.

The principal stations of this Series are nearly all situated on hills; they consist of circular masonry pillars from 3 to 4 feet in diameter, for the large theodolite to rest on, are generally surrounded by platforms of stones and earth, or sand, of sufficient size to support the observatory tent. Several of the stations fell on sand hills which did not afford a satisfactory foundation for the pillars; piles were then driven into the sand and the foundation laid on them, the pillars being built so that their surfaces were nearly flush with the hill top. Owing to their elevated positions the pillars rarely had to be raised to a height of more than 3 or 4 feet; they contain two or more marks the upper of which is generally flush with the surface. Over the upper mark a rectangular protecting pillar, bearing a sufficiently accurate mark for Topographical and Revenue Survey purposes—as shewn at page 74 of Vol. II of the Account of the Operations, &c.—was erected after the completion of the observations, and the station was then further protected by a pile of stones and earth.

#### The Eastern Sind Meridional Series.

The great majority of the stations of this Series are situated on sand hills and their construction is as follows:—A solid, circular pillar of masonry for the theodolite to stand on, isolated by means of an annular wall, was built up from a depth of 3 feet to the level of the hill top; in this pillar were placed two or more mark-stones vertically over one another, the upper one being in the surface of the pillar. The remaining stations are tower stations: they consist of either a solid or perforated pillar surrounded by a solid tower of sun-dried bricks set in mud for the accommodation of the observatory tent. The solid pillars have marks at the top, at the bottom and intermediately, while the perforated pillars have a mark in



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the floor and another below it in the foundation, access to the mark in the ground floor being obtained by a vaulted passage through the tower and pillar. The pillars themselves were constructed in rectangular blocks of masonry surmounting one another, each succeeding block being contracted so as to leave a plinth at its base; the uppermost block, for the theodolite to stand on, is circular,  $3\frac{1}{3}$  feet in diameter, and isolated from the tower. The upper mark-stones where the pillars were solid, were in all cases protected by rectangular pyramidal pillars erected over them after the completion of the observations, and bearing a sufficiently accurate mark for Topographical and Revenue Survey purposes.

#### CHAPTER II.

# THE MEASUREMENT OF THE ANGLES AND THE GENERAL PRINCIPLES FOLLOWED IN THE REDUCTION OF THE TRIANGULATION.

## 1.

#### The Measurement of the Horizontal Angles and their Record.

In Chapter IV of Vol. II full particulars have been given of the methods of observing both horizontal and the vertical angles which have been in practice since the year 1823. It will not be necessary therefore to do more here than briefly indicate the procedure, in order that the reader may be enabled to understand the details of the observations.

The method of observing horizontal angles was that introduced by Colonel Everest, and had for its object the giving of readings at equal intervals round the azimuthal circle, with a view to the cancellation of periodic errors of graduation. When the instrument was set up for use, and had been properly centred over the station mark and levelled, either one of the surrounding stations, or a referring mark specially set up for the purpose, was adopted as what is called the *zero-station*, or the station for which the readings of the instrument are obligatory. The telescope being directed to this station, the index was made to read 0° 0'. The remaining stations were then observed to in succession, two or more rounds of observations being taken. When these were completed the telescope was turned over in altitude and brought round in azimuth to point to the zero-station: the index would then read 180° 0'. With this zero-reading another set of observations, similar to the last, was taken. A single measure on each of the two zero-settings constitute a pair of collimated observations, the face of the vertical circle being to the left of the observer at one setting and to his right at the other. The instrument was next shifted in azimuth, so as to bring the index to another arbitrary reading while the telescope pointed to the zero-station, and observations were again taken on F. L., face left, and F. R., face right; and so on. These arbitrary shifts were through arcs of 10° for theodolites with 3 microscopes and 7° 12' for 5-microscope theodolites. In 1860, in order to secure a greater change of position of the axis in its socket, and so avoid the

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occurrence of certain constant errors which might be prejudicial in a long chain of triangles, Colonel Waugh decided that the arc between the microscopes should be added to each shift.

The system of zero-settings employed in the Jodhpore and Eastern Sind Meridional Series was as follows :---

$$\frac{0^{\circ} 0'}{180^{\circ} 0'}, \frac{79^{\circ} 12'}{259^{\circ} 12'}, \frac{158^{\circ} 24'}{338^{\circ} 24'}, \frac{237^{\circ} 36'}{57^{\circ} 36'} \text{ and } \frac{316^{\circ} 48'}{136^{\circ} 48'}.$$

The minimum number of rounds on each zero was three; but when differences shewed themselves in successive measures of an angle, greater than it was considered the instrument ought to give, the observations were repeated.

The several measures of each angle, with the name of the observer and instrument employed and the date of the observations, are given in Part II of this volume, commencing for the Jodhpore Series at page 14 and for the Eastern Sind Series at page 131. Against each single measure is a letter in italics, shewing whether the signal observed to was l, a lamp, or h, a heliotrope; sometimes a direct measurement of an angle was not obtained owing to the temporary invisibility of one of the signals, but the value of the angle was deduced from the measure of the double angle given by the omission of the signal in the round, and from a direct measure of the other angle; in this case the measure is preceded by the letter d.

Below the individual measures are their means from which M the general mean is obtained. The several measures and zero means are then treated as described in the following Section, and give C the concluded angle, together with w, its relative weight to the other

angles measured under similar circumstances, and  $\frac{I}{w}$ , the reciprocal.

### 2.

#### The Deduction of an Angle from its several Measures and its Weight.

It has been stated that the number of measures of an angle on the same zero is not always constant, but is occasionally increased at the discretion of the observer. Of old the custom was to take the general mean of all the zero-means as the most probable value of the angle resulting from the several measures; but, for reasons which are explained in Chapter VII of Vol. II, this practice has been departed from, and the following procedure has been adopted in deducing the value and the weight of each angle in the present volume.

Let d', d'', d''', &c., be the differences between the successive single measures and the mean of the measures on the zero to which they respectively belong,  $n_1$ ,  $n_2$ ,  $n_3$ , &c., the number of measures on each zero, the sum of all which is = N, and  $D_1$ ,  $D_2$ ,  $D_3$ , &c., the algebraical excess of the successive zero means, Z in number, over the arithmetical mean, M, of all the zeros.

Now put

$$o^{2} = \frac{d^{\prime 2} + d^{\prime \prime 2} + d^{\prime \prime \prime 3} + \dots}{N - 1}$$
$$g^{2} = \frac{D_{1}^{2} + D_{2}^{2} + D_{3}^{2} + \dots}{Z - 1}$$

and let

$$\mathbf{w}_1 = \frac{\mathbf{I}}{g^2 + \frac{o^2}{n_1}}, \quad \mathbf{w}_2 = \frac{\mathbf{I}}{g^2 + \frac{o^2}{n_2}}, \quad \mathbf{w}_3 = \frac{\mathbf{I}}{g^2 + \frac{o^2}{n_3}}, \dots$$

Then the resulting angle C, usually called the 'Concluded Angle',

$$= M + \frac{\mathbf{w}_1 D_1 + \mathbf{w}_2 D_2 + \mathbf{w}_3 D_3 + \dots}{\mathbf{w}_1 + \mathbf{w}_2 + \mathbf{w}_3 + \dots}$$

Here  $o^*$  and g are taken as preliminary approximations to the theoretical error of mean square of observation and graduation, o being the e.m.s. of observation and g that of graduation in a single measure of an angle; these quantities being known, the weights,  $w_1, w_2, \ldots$ , of the successive zero-means are ascertained, whereby these means are readily combined to give the value of the Concluded Angle, as in the last equation.

Let w be the weight of the angle thus deduced; then we may put,

$$w = w_1 + w_2 + w_3 + \ldots$$

and if the preliminary values of o and g, as obtained from the observations, are absolutely true, then w will be the reciprocal of the square of the *e.m.s.* of the concluded angle.

It must be here observed that the values of *e.m.s.* thus obtained immediately from the observations, cannot be considered to be in the same terms when the instruments and circumstances under which the observations are taken are different. The values are only to be regarded as preliminary, applicable in any combination of angles measured with the same instrument and under similar circumstances, but requiring to be multiplied by factors of the nature of *moduli* before they can be employed in a combination of angles measured with different instruments and under different circumstances. This subject is fully treated of in Section 5 of Chapter VII of Volume II, to which reference can be made if desired. It need not be entered on here for the angles of the Jodhpore Meridional Series having been observed with the same instrument and under the same circumstances needed no *modulus* to equalize the weights; and although on the Eastern Sind Meridional Series two instruments

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<sup>\*</sup> Strictly speaking the denominator in the expression which gives the value of o would be N-Z; but a larger denominator, as N or N-1, is preferable in the present instance, because o is combined with g which, strictly speaking, would represent the total error and not that of graduation only, if each measure were absolutely independent of all the others, which it is not. Thus, though the denominator N-1 was originally employed by an oversight, as may be here frankly acknowledged, it has been retained as more appropriate than N-Z under existing circumstances.

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were employed, one of them was used for such a small portion of the triangulation as to afford too few data for determining a *modulus*, and being both 24-inch theodolites of practically equal capabilities it was the less desirable to attempt to deduce any; hence the weights of this Series were also assumed to be in the same terms.

The record of the measures of the angles is followed by a list of the "Sums of Squares of Apparent Errors of Single Observations and of Apparent Errors of Single Zeros," furnishing the requisite data for the investigation—by which it is followed—of the average 'error of mean square,' of observation only, in a single measure, and that of graduation *plus* observation in the mean of the several measures on a single zero; these are determined for certain groups of the angles in which all the measures have been made by the same observer with the same instrument and under the same conditions, and also for groups formed by various other combinations of the conditions. With the data thus obtained for each of the series, investigations of the influence of "Mixed Errors of Observation and Graduation", similar to those which are given in Chapter VII of Vol. II, may be made.

## 3.

#### Preliminary Reductions of the Groups of Angles contained in independent Trigonometrical Figures.

So long as chains of triangles are treated as independent of one another, the angles naturally separate themselves into as many groups as there are single triangles, and combinations of triangles into single polygonal figures and net-works. Each triangle is subject to the geometrical condition that the three angles are equal to  $180^{\circ}$  plus the spherical excess, and each group of triangles to additional geometrical conditions, such as that the angles at any central point should together equal  $360^{\circ}$ , and that the value of any side as calculated through any portion of the figure back to itself should be unaltered.

The formula which has been employed for calculating the spherical excess of the triangles in this volume is

$$\epsilon = ab\sin C \times \frac{\csc 1''}{2r^2}^*$$

in which  $\epsilon$  is the spherical excess in seconds, *a*, *b* and *C* two sides of the triangle and the included angle, and *r* the radius of curvature for the oblique section of which the azimuth is  $45^{\circ}$ , that is,  $r = \frac{2\rho\nu}{\rho + \nu}$ ,  $\rho$  being the radius of curvature to the meridian and  $\nu$  the normal on the axis minor for the mean latitude of the triangle.

<sup>\*</sup> The factor  $\frac{\cos e c}{2r^2}$  has been tabulated for every degree of latitude from 5 to 36 in the Auxiliary Tables to facilitate the calculations of the Survey Department of India, Dehra Doon, 1868.

The geometrical conditions connecting groups of angles divide themselves under three heads, triangular, central and side. The first is, as before stated, that the three angles of a triangle must equal  $180^{\circ}$  + the spherical excess, the second that all the angles meeting at a point and completely surrounding it must equal  $360^{\circ}$ , or when an angle is measured as a whole and also in parts, the whole should equal the parts, and the third springs from the condition that the value of any side carried through the triangulation back on itself should reproduce itself. The excesses or deficiencies which manifest themselves in these comparisons either become the right members of the equations amongst the angular errors furnished by the conditions, or they furnish the means of obtaining them.

The number of the equations for each independent trigonometrical figure is given by the formula

$$N - 2S + 4$$

in which N is the number of angles and S the number of stations.

In order to express the equations, denote the observed angles by  $X_1, X_2, X_3, \ldots$  the corresponding angular errors by  $x_1, x_2, x_3, \ldots$  and the absolute terms of the equations by *e* with subscripts denoting the equations to which they appertain. The triangular and central equations will then take the form.

$$x_1 + x_2 + \ldots = e$$

The side equations may be expressed in either of the two following forms, it is immaterial which, so far as the accuracy of the results is concerned; but the second entails least labour in calculation, and for that reason is preferred :---

If  $a_1 = \cot X_1$ ,  $a_2 = \cot X_2$ , &c., the side equations will be represented by

$$a_1 x_1 - a_2 x_2 + a_3 x_3 - a_4 x_4 + \ldots = \frac{\operatorname{cosec} 1''}{M} \times \log \frac{\sin X_1 \cdot \sin X_3 \cdots}{\sin X_2 \cdot \sin X_4 \cdots} \cdot \ldots \cdot (1)$$

M being the modulus of common logarithms; or if

$$a_1 = ext{tabular difference of log. sin } X_1 ext{ for a change of } \mathbf{1}''$$
  
 $a_2 = \dots, \dots, ext{ log. sin } X_2 \dots, ext{ }$ 

and so on

$$a_1 x_1 - a_2 x_2 + a_3 x_3 - a_4 x_4 + \ldots = \log \cdot \frac{\sin X_1 \cdot \sin X_3 \ldots}{\sin X_2 \cdot \sin X_4 \ldots} \cdot \ldots \cdot (2)$$
  
= e

These geometrical conditions have to be satisfied in such a manner, that the angles

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shall receive the most probable of the several series of corrections which present themselves. This is done by the method of minimum squares, which is now so well known that nothing need be said regarding it further than that it requires the following expression shall be made a minimum,

$$U = \frac{x_1^3}{u_1} + \frac{x_2^2}{u_2} + \ldots + \frac{x_i^3}{u_i}$$

in which  $u_1, u_2, \ldots, u_t$  are the reciprocals of the weights,  $w_1, w_2, \ldots, w_t$ , of the observed angles.

The following equations—taken from Section 5, Chapter VIII, Vol. II—express first the geometrical conditions, secondly their relations with the indeterminate factors,  $\lambda_s$ ,  $\lambda_b$ , . . .  $\lambda_s$ , by the introduction of which U is made a minimum, and thirdly the most probable values of the angular errors in terms of the geometrical conditions and the indeterminate factors.

The geometrical equations of condition, n in number between t unknown quantities are

The equations between the indeterminate factors are

| $[aa. u] \lambda_a + [ab. u] \lambda_b +$ | • | • | • | $+ [an. u] \lambda_n = e_a$     |
|-------------------------------------------|---|---|---|---------------------------------|
| $[ab. u] \lambda_a + [bb. u] \lambda_b +$ | • | • | • | $+ [bn. u] \lambda_n = e_b$     |
| • • • • • • • •                           | • | • | ٠ | • • • • •                       |
| $[an. u] \lambda_a + [bn. u] \lambda_b +$ | • | • | • | $+ [nn. u] \lambda_{s} = e_{s}$ |

in which the brackets [ ] indicate summations, thus

$$[aa. u] = a_1a_1. u_1 + a_2a_2. u_2 + \ldots + a_ia_i. u_i.$$

The resulting values of the angular errors are

 $\begin{aligned} x_1 &= u_1 (a_1 \lambda_a + b_1 \lambda_b + \dots + n_1 \lambda_s) \\ x_2 &= u_2 (a_2 \lambda_a + b_2 \lambda_b + \dots + n_2 \lambda_s) \\ \dots &\dots &\dots &\dots \\ x_t &= u_t (a_t \lambda_a + b_t \lambda_b + \dots + n_t \lambda_s) \end{aligned}$ 

and the value of the minimum, U, is

 $\lambda_a e_a + \lambda_b e_b + \ldots + \lambda_n e_n.$ 

Abstracts of the reductions of the figures will be found in Part II for the Jodhpore

[12]



Meridional Series on pages 69 to 84 and for the Eastern Sind Meridional Series on pages 181 to 195. In these abstracts are given for each figure the observed angles with their reciprocal weights, the equations to be satisfied, the resulting equations between the indeterminate factors, the values of these factors and the values of the angular errors obtained; finally the value of the minimum-is also noted.

## 4.

#### Calculation of the Sides of the Triangles.

The values of the angular errors having thus been computed are applied to the observed angles with contrary signs; then the angles of every triangle are reduced to plane angles by the subtraction of one-third of the spherical excess of the triangle from each, and the sides of the triangles are obtained in the ordinary manner. The angular corrections furnished by the figural reductions, besides being the most probable, in so far as the conditions to which they have been subjected are concerned, render each figure or net of triangles consistent, so that the ratio of any one side to any other side is the same by whatever route it is calculated.

## 5.

#### Geodetic Elements of Stations and Sides.

The lengths of the sides of triangles and the dimensions of the Figure of the Earth being known, it will be evident that if the latitude of any one station and the azimuth of any side of the triangulation from it to a second station are given, the difference in latitude and longitude between it and the second station, and the back azimuth of the connecting side, may be computed.

Now the origin of co-ordinates which has been adopted for the Indian triangulation is Kaliánpur, Station | of the North-West Quadrilateral, the initial elements at which are

|                                  | •   |    | "                   |
|----------------------------------|-----|----|---------------------|
| Latitude North                   | 24  | 7  | 1 1 <sup>.</sup> 26 |
| Longitude E. of Greenwich        | 77  | 41 | 44 <sup>.</sup> 75  |
| Azimuth of Station 29 (Súrantál) | 190 | 27 | 5 <sup>.</sup> 10   |

as explained in Chapter XI of Vol. II.

But as the positions of all the stations of the North-West Quadrilateral are regarded as having been finally fixed in the Simultaneous Reduction of that figure, the elements of

[13]

any of them may be adopted in place of those of Kaliánpur, whenever it happens to be convenient to do so. Thus, as the Jodhpore and Eastern Sind Meridional Series are based on sides of the Karáchi Longitudinal Series, one of the Series of the North-West Quadrilateral, the elements of those sides have been adopted as the initial elements of the two series, instead of falling back on Kaliánpur.

The formulæ which have been employed on the successive calculations of latitude, longitude and reverse azimuth are given below.

If A and B be two stations on the earth's surface, and the latitude and longitude of A, and the azimuth of B at A be  $\lambda$ , L and A respectively, the distance between A and B being c, and if

 $\Delta\lambda$  denote the difference of latitude between A and B

 $\nu$  , the normal to the meridian at  $\lambda$  terminated by the minor axis,

then

$$\Delta \lambda = \begin{cases} -\frac{c}{\rho} \cos \varDelta \operatorname{cosec} \mathbf{1}'' \\ -\frac{1}{1.2} \frac{c^2}{\rho.\nu} \sin^2 \varDelta \tan \lambda \operatorname{cosec} \mathbf{1}'' \\ -\frac{3}{4} \frac{c^2}{\rho.\nu} \frac{e^2}{1-e^2} \cos^2 \varDelta \sin 2\lambda \operatorname{cosec} \mathbf{1}'' \\ +\frac{1}{1.2.3} \frac{c^3}{\rho.\nu^2} \sin^2 \varDelta \cos \varDelta (\mathbf{1}+3 \tan^2 \lambda) \operatorname{cosec} \mathbf{1}'', \end{cases}$$

$$\Delta L = \begin{cases} -\frac{c}{\nu} \frac{\sin A}{\cos \lambda} \operatorname{cosec} \mathbf{1}'' \\ +\frac{1}{1.2} \frac{c^2}{\nu^2} \frac{\sin 2A \tan \lambda}{\cos \lambda} \operatorname{cosec} \mathbf{1}'' \\ -\frac{1}{1.2.3} \frac{c^3}{\nu^3} \frac{(1+3 \tan^2 \lambda) \sin 2A \cos A}{\cos \lambda} \operatorname{cosec} \mathbf{1}'' \\ +\frac{1}{1.2.3} \frac{c^3}{\nu^3} \frac{2 \sin^3 A \tan^2 \lambda}{\cos \lambda} \operatorname{cosec} \mathbf{1}'' \end{cases}$$

[14]



and

$$B = \pi + \mathbf{A} + \begin{cases} -\frac{c}{\nu} \sin \mathbf{A} \tan \lambda \operatorname{cosec} \mathbf{i}'' \\ +\frac{\mathbf{i}}{4} \frac{c^2}{\nu^2} \left\{ \mathbf{i} + 2 \tan^2 \lambda + \frac{e^2 \cos^2 \lambda}{\mathbf{i} - e^2} \right\} \sin 2\mathbf{A} \operatorname{cosec} \mathbf{i}'' \\ -\frac{c^3}{\nu^3} \left(\frac{5}{6} + \tan^2 \lambda\right) \frac{\tan \lambda}{2} \sin 2\mathbf{A} \cos \mathbf{A} \operatorname{cosec} \mathbf{i}'' \\ +\frac{\mathbf{i}}{2 \cdot 3} \frac{c^3}{\nu^3} \sin^3 \mathbf{A} \tan \lambda \left(\mathbf{i} + 2 \tan^2 \lambda\right) \operatorname{cosec} \mathbf{i}'' \end{cases}$$

For the derivation of these formulæ, and also for the manner in which they have been arranged for calculation, see Chapter IX of Volume II, also the *Auxiliary Tables to facili*tate the calculations of the Survey Department of India.

The values of the elements of the Figure of the Earth which have been employed in the calculations are those known as "Everest's Constants, 1st set", and are :---

| Semi-axis major, | a= 20,922,932 feet,                               | $Log = 7.320\ 6225\ 4$          |
|------------------|---------------------------------------------------|---------------------------------|
| Semi-axis minor, | b= 20,853,375 feet,                               | " = 7.319 1763 4                |
| Ellipticity,     | $c = \frac{a-b}{a} = \frac{1}{300.80}$            | $= \overline{3} \cdot 52171968$ |
|                  | $e^{2} = \frac{a^{2} - b^{2}}{a^{2}} = 0.0066378$ | $= \overline{3}.82202718$       |
| . I <del>.</del> | $e^3 = 0.9933622$                                 | "  = T·997 1076 I               |

from which  $\rho$  and  $\nu$  are found by the well known formulæ.

**6.** 

#### Reduction of the Vertical Angles for the determination of Differences of Height and Co-efficients of Refraction.

The relative heights of the principal stations of this Survey are determined in all instances by measuring the reciprocal vertical angles. The heights so obtained are controlled,

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wherever possible, by connecting the stations of the triangulation with those of lines of Spirit Levels, which are executed by this Survey, and occasionally with Tidal Stations on the coasts of the Peninsula, at which direct determinations of the mean sea level have been made. The formula that was employed for many years in the calculation of differences of height, is due to Colonel Everest, and is as follows :---

If h be the difference of height of two stations A and B, D' the depression of B at A and D that of A at B, H the height of A above mean sea level, c the distance between A and B at that level, and r the radius of curvature corresponding to the mean latitude of A and B, then the angle subtended at the lower station by the excess of height of the higher, or the so-called *subtended angle*, is  $\frac{1}{3}(D-D')$  and the height of B above or below A is given by the expression

$$h = c\left(1 + \frac{H}{r}\right) \frac{\sin \frac{1}{2} (D - D')}{\cos D}$$

according as the result is *plus* or *minus*. If either of the angles is an elevation instead of a depression its value must be employed with the opposite sign to that here given.

In order to use this formula it is first necessary to correct the observed angles for the heights of the observing instrument and observed signal. A much less laborious process is to employ the uncorrected vertical angles, and then reduce the result thus obtained to the levels of the stations by an algebraical combination of the heights of the instruments and signals. This procedure is as follows:—

If  $i_a$ ,  $i_b$  be the heights in feet of the theodolites at A and B respectively  $s_a$ ,  $s_b$ , ,, signals ,, ,,  $D_a$ ,  $D_b$  the observed vertical angles, both assumed to be depressions,

and we put

$$\delta = s_a - s_b + i_a - i_b$$

then

[16]

$$h = c\left(1 + \frac{H}{r}\right) \frac{\sin \frac{1}{2} \left(D_b - D_a\right)}{\cos D_b} + \frac{\delta}{2}$$

This formula, though not absolutely rigorous, holds good for all cases that have hitherto occurred or are likely to occur in this Survey.

For r, the radius of curvature, the same formula is employed as in the calculation of spherical excess, see page [10],  $\rho$  and  $\nu$  being here taken for the mean latitude of the stations.

In the preceding formulæ it is assumed that the reciprocal angles are equally affected
by refraction, and in order that this may be as nearly the case as possible, the vertical angles are generally measured between the hours of 1 and 3 p. M., when the amount of refraction is usually a minimum.

The reciprocal angles are also employed to determine the coefficient of refraction, to be used in reducing unreciprocated vertical angles; for, putting C for the arc between the stations A and B, or the *contained arc* as it is usually called, and  $\phi_a$ ,  $\phi_b$  for the refraction at the respective stations, we have

$$C = D_a + \phi_a + D_b + \phi_b - \beta$$

in which expression

$$\beta = \frac{i_a - s_a + i_b - s_b}{c \sin 1''}.$$

Thus, the mean refraction,  $\phi$ , is given by the expression

$$\phi = \frac{1}{2} \{ C - (D_a + D_b) + \beta \}$$

and  $\frac{\phi}{C}$  gives the terrestrial refraction in decimals of contained arc—or in other words the *coefficient of refraction*—for each pair of reciprocated observations. From the several values of the coefficient thus determined, those which are deemed most suitable are selected for employment in the reduction of vertical angles to secondary points, at which reciprocal observations have not been taken.

The formula for calculating the *contained arc* is

$$C'' = \frac{c}{r} \operatorname{cosec} 1''.$$

Abstracts of the calculations of differences of height as well as the final heights for the Jodhpore Meridional Series will be found on pages 97 to 106, and for the Eastern Sind Meridional Series on pages 207 to 215. In these abstracts the stations are entered in pairs as reciprocally observed, and there are given for each station the astronomical date and mean time of observation, the mean of the observed angles, preceded by a letter shewing whether it is a depression, D, or an elevation E, and the number of observations of which it is the mean. Then follow in succession the height in feet of the signal observed to and of the instrument employed, the contained arc between each pair of stations, the terrestrial refraction expressed in seconds and also in decimals of contained arc, and the resulting difference of height of the deduced station by each deduction, the height thus deduced, and the mean of several deductions. Lastly the final values of height—determined as explained in the next section—are given followed by the height of the pillar or tower above ground level.



# 7.

### The Final Values of Height.

The tide-gauge stations on the coast and the lines of spirit-levels connected with them and traversing the continent of India afford a great system of heights, which being determined with the highest attainable accuracy are considered absolute. The reciprocal vertical angles of the chains or series of triangles of the Great Trigonometrical Survey provide another very extensive system of relative heights; but from the irregularities of refraction and other causes these relative heights are less reliable than differences obtained by spirit levelling. The two systems are connected at numerous points, and where discrepancies appear, they are treated as errors in the trigonometrical heights and eliminated from them by dispersion. After this has been done the trigonometrical heights are considered as absolute also. No lines of spirit leveling having been undertaken which cross or approach the two series under report the final heights of these series have been determined by dispersing over each the discrepancy between the relative excess in height of its terminal over its initial stations as exhibited by the triangulation and the excess determined at the time of the final reduction of the North-West Quadrilateral. The initial stations of both series lie in the Karáchi Longitudinal Series; the terminals of the Jodhpore being in the Sutlej, and of the Eastern Sind in the Great Indus Series.

# 8.

### The Determinations of Azimuth by Astronomical Observations.

It has been the practice in this Survey to determine azimuths at certain stations in the course of the execution of each chain of triangles. It used to be customary to select stations for this purpose in meridional series at about 1° apart, and in longitudinal series at shorter intervals. Of late the choice of stations has also been governed by the nature of the surrounding country, those localities only being accepted where there was reason to expect that the results would be least influenced by local attraction. These independent observations of azimuth will be valuable hereafter, in investigations of the Figure of the Earth and of local attraction. But for reasons which have already been explained at page 142 of Vol. II, it would not, as a rule, be proper to employ them in the general reduction of the triangulation. It happens however that the observations have been reduced each year *pari passi* with the preliminary reductions of the triangulation—figure by figure, or series by series—which precede the final simultaneous reductions. The observations and their reductions are therefore given in the volumes which treat of the triangulation ; as they have more in common with it than with the astronomical observations for the determinations of latitude and differential longitudes.

The observations for azimuth consist of measures of the angle between a circumpolar star, when near either elongation, and some station—either directly or through the medium



of a referring mark—which are made in accordance with the system followed in observing the horizontal angles as regards the changes of zero, but with a larger number of repetitions on each zero, as the observations are individually liable to greater error.

The time of each intersection of the star being carefully noted, the difference of the momentary azimuth,  $\delta A$ , from the value at elongation is subsequently calculated and applied to the observed angle between the referring mark and the star. Thus a series of determinations of the angle between the referring mark and the star's position at elongation is obtained, from each of which and the known value of the azimuth of the star at elongation a determination of the azimuth of the referring mark is deduced.

The formula employed for the calculation has been

$$\delta \mathcal{A}^* = \frac{(2 \sin^2 \frac{1}{2} \delta P \operatorname{cosec} 1'') \tan \mathcal{A} \cos^2 a}{1 - (2 \sin^2 a \sin^2 \frac{1}{2} \delta P) \pm (\cot P \sin \delta P)}$$

in which  $\mathcal{A}$  is the azimuth of the star at elongation, P the corresponding hour angle, a the north polar distance of the star, and  $\delta \mathcal{A}$  the difference in azimuth for the time  $\delta P$  before and after elongation. The last term of the denominator is positive when the star is below and negative when above the position of maximum elongation.

At each station where the azimuth of a referring mark is observed, the angle between the referring mark and one of the contiguous stations of the triangulation is also observed, just as any other horizontal angle; and the several measures will be found in the Abstract of the Observed Angles at the observing station.

Abstracts of the azimuthal observations made on each series will be found for the Jodhpore Meridional Series on pages 107 to 115 and for the Eastern Sind Meridional Series on pages 216 to 227, in which are given, besides all necessary information regarding the observations themselves, such details of the calculations as will enable them to be followed up to the final result, *viz.*, the difference between the Astronomical and Geodetical azimuths. Sometimes the whole of the observations on a pair of zeros could not be completed on one night; in such cases the remainder were taken on a subsequent night, and the change of the star's place was duly allowed for in the reductions.

# 9.

#### The Final Reduction of the Triangulation. Preliminary Sketch.

So far the triangulation has only been made to fulfil those geometrical conditions, which apply to single triangles, polygonal figures and net-works, or all such conditions as

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<sup>\*</sup> The values of the portions of the formula enclosed in brackets within the limits of  $\delta P = 30^{\circ}$  and  $a = 10^{\circ}$  have been calculated and are given in the *Auxiliary Tables*, and as  $\tan A \cos^2 a$  may be treated as a constant for each elongation, the calculation of  $\delta A$  is easily performed.

exist until a chain closes on a side of known length and position or two or more chains unite together to form a circuit; it now becomes necessary to apply such conditions as will make the closing points of each chain take the positions already assigned them by the general reduction of the North-West Quadrilateral.

Before proceeding to indicate the forms of equations resulting from the conditions requisite for this adjustment it may be as well to anticipate a possible objection in their application. As all errors are to be dispersed by the method of minimum squares, which assumes the independency of all the quantities under investigation, it might be imagined that we must now again revert to the observed angles, as the angles which have been corrected for figural conditions cannot be considered independent. It has however been shewn in Appendix No. 8 of Vol. II, that the observed angles may be corrected in accordance with a part only of the conditions which govern them; and that when new conditions present themselves the corrected angles may be employed for finding other corrections; so that final corrections can be obtained by employing the angles after they have received any number of partial corrections, provided that the conditions which have already been satisfied are maintained when the further corrections, required to satisfy additional conditions, are calculated.

All preliminary calculations therefore stand good, and consequently equations due to new conditions may be obtained by employing the corrected, instead of reverting to the observed, values of the angles. But when we are seeking for final corrections, we must treat the corrected angles in such a manner as to preserve all the conditions already satisfied. These have however in general been so numerous and entangled as to make an exact solution of the problem impossible. Consequently all central and side conditions of the different polygonal figures and net-works composing the chains have been excluded, by omitting from the simultaneous reductions all angles appertaining to polygonal figures and net-works over and above what were needed to form continuous chains of single triangles, and increasing the weights of the angles of the retained triangles. By this means the entanglement has been greatly diminished, and the number of figural equations reduced to one for each triangle, of the simple form

### x + y + z = 0

which permits of the elimination of one of the unknown quantities in each triangle, and thus enables all the triangular equations to be dispensed with. Thus the number of equations to be solved was eventually reduced to the number of new conditions to be satisfied or in other words to the number of what are here called circuit equations, the term having reference to all the closing errors of the chains of triangles, whether occurring internally at the ends of the circuits or externally on the base-lines.

In the present case there was not the same excuse for neglecting the central and side equations, as each reduction only involved one chain of triangles; yet as each is double throughout, the introduction of all the equations would have largely added to the labor without any corresponding advantage. Hence the original plan was followed, except that Mr. J. B. N. Hennessey, who was at the time in charge of the Computing Office, decided that

[20]



the weights of all the angles in each chain of selected triangles should be considered equal or taken as unity.

After the completion of the reductions, the angles appertaining to the portions of the polygonal figures and net-works, which had been excluded, were corrected in such a manner as to restore the consistency of each figure, without altering the values of the angles already fixed.

# 10.

### The Final Reduction of the Triangulation. Formation of the Circuit Equations.

The Final Reduction of each of the two series, the Jodhpore and Eastern Sind Meridional, was an independent operation; but the process was the same for each and may be generally described as follows:—

The triangles presented for simultaneous reduction in each case consist only of a single chain, and are numbered consecutively from south to north. The angle opposite the flank side of each triangle is known as X, that opposite the side of continuation as Y and that opposite the base as Z, each being further distinguished by a subscript, which is the number of the triangle: x, y and z with corresponding subscripts are the symbols employed to represent the errors of the angles, or, in other words, the unknown fallible quantities of which the most probable values that will satisfy the equations have to be found. These equations are respectively termed *Linear* and *Geodetic*, the former taking cognizance of the errors in the sides of the triangles, which are met with at the termination of the chain, and the latter expressing the errors in latitude, longitude and azimuth at the closing station.

It is unnecessary here to repeat the deduction of the analytical expressions for the circuit equations. This has already been demonstrated in Volumes II, VI and VII of the *Account of the Operations of the Great Trigonometrical Survey of India*, to which reference can be made if necessary; it will be sufficient now to give the expressions themselves.

### I. Linear Equations.

Denoting for brevity the tabular difference (t. d.) of log sin Y for 1'' by  $\beta$ , and of log sin Z by  $\gamma$ , and by E the error in the logarithmic value of the closing side of the chain, then

$$E = \beta_1 y_1 - \gamma_1 z_1 + \beta_2 y_2 - \gamma_2 z_2 + \ldots + \beta_m y_m - \gamma_m z_m$$

*m* being the number of triangles in the chain. As in this equation E as well  $\beta$  and  $\gamma$  represent quantities in the 7th place of decimals, it is convenient to treat them as if both sides of the equation were multiplied by 10<sup>7</sup>, by which means E,  $\beta$  and  $\gamma$  become respectively the number of units in the 7th place of decimals.

[21]

If we employ brackets to denote summation the equation may be briefly written

$$E = \prod_{1}^{m} \left[ \beta y - \gamma z \right].$$



### II. Geodetic Equations.

The diagram in the margin represents the commencement of a chain of triangles in which station | is assumed to be the origin of geodetic co-ordinates, and  $2, 3, \ldots$  stations on the most direct route—indicated by the dotted line running parallel to the sides on one flank of the chain—which connects | with any station in advance. The side c is the side of origin of the chain, and its azimuth at | the fundamental azimuth of the chain.

The following symbols are required to denote the differences of latitude, longitude and azimuth, the length of side, and the forward and back azimuths from station to station along the right flank of the chain :—

For the side 1 to 2;  $\Delta \lambda_1, \Delta L_1, \Delta A_1, c_1, A_1 \text{ and } B_1$ , , , n to n + 1;  $\Delta \lambda_n, \Delta L_n, \Delta A_n, c_n, A_n \text{ and } B_n$ .

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The errors in latitude, longitude and azimuth at the closing station, the (n + 1)th, are denoted by  $d\lambda_{n+1}$ ,  $dL_{n+1}$ ,  $dB_n$ .

Now writing  $\mu$  and  $\phi$  for certain functions of  $\Delta\lambda$ ,  $\Delta L$ ,  $\Delta A$  and A as exhibited in the *Table of Substitutions* which follows, we have a general expression for each of the geodetic equations in which E represents the error in latitude, longitude or azimuth, as the case may be, at the closing station, and  $\beta$  and  $\gamma$  have the same signification as in the linear equation, while a stands for t.d. log sin X for a change of 1'':—

$$E = + (\mu_1 \beta_1 - \phi_1) y_1 + (-\mu_1 \gamma_1 - \phi_1) z_1 + \{(\mu_2 - \mu_1) a_2 + \mu_2 \beta_2 + \phi_1\} y_2 + \{(\mu_2 - \mu_1) a_2 - \mu_1 \gamma_2 + \phi_2\} z_2 + \{(\mu_3 - \mu_2) a_3 + \mu_3 \beta_3 + \phi_2\} y_3 + \{(\mu_3 - \mu_2) a_3 - \mu_2 \gamma_3 + \phi_3\} z_3 + (\mu_3 \beta_4 - \phi_3) y_4 + (-\mu_3 \gamma_4 - \phi_3) z_4 + \cdots$$

in which the  $\mu$  s and  $\phi$  s take their subscripts from the flank numbers of the stations and  $\alpha$   $\beta$  and  $\gamma$  from the triangles.

The general forms for the coefficients of y and z are :—

*First.*—If the pth triangle have no side in the line of traverse, but only an angle at the station l,

$$(\mu_i \beta_p - \phi_i) y_p + (-\mu_i \gamma_p - \phi_i) z_p.$$

Secondly.—If the qth triangle have a side in the traverse between the stations l and l + 1,

 $\{(\mu_{l+1} - \mu_l) a_q + \mu_{l+1} \beta_q + \phi_l\} y_q + \{(\mu_{l+1} - \mu_l) a_q - \mu_l \gamma_q + \phi_{l+1}\} z_q.$ 

Exceptions will appear to present themselves at the commencement and end of chains owing to the non-existence of some of the coefficients. In all instances however it will be found that  $\phi_l$  enters the coefficients of all the errors at station l, and  $\mu_l$  enters the coefficients of the other angles of the same triangles, with a *plus* sign if looking from station l the angle is the left-hand one of the triangle, and a *minus* sign if the right-hand.

The substitutions for  $\mu$  and  $\phi$  to render the general equation applicable to either latitude, longitude or azimuth are given in the following table.

|                        | Tetitude                                                                                             | Longitude                                                                                        | A rimuth.                                                                                                |
|------------------------|------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------|
| For <i>E</i>           | $d\lambda_{n+1}$                                                                                     | $\int dL_{n+1}$                                                                                  | $dB_{*}$                                                                                                 |
| ,, μ                   | <i>_</i> μ <sup>μ</sup>                                                                              | L <sup>µ</sup> .                                                                                 | <sub>A</sub> μ                                                                                           |
| " <b>φ</b>             | <sub>λ</sub> φ                                                                                       | $_{L}\phi$                                                                                       | д¢                                                                                                       |
| ,, μ <sub>1</sub>      | $+ \int_{I}^{*} \left[ \frac{I}{t.d.\log \Delta \lambda} \right]$                                    | $+ \left[\frac{\mathbf{I}}{\mathbf{t}.\mathbf{d}.\log\Delta L}\right]$                           | $+ \frac{I}{I} \left[ \frac{I}{t.d.\log \Delta A} \right]$                                               |
| », µ2                  | $+ \int_{2}^{\pi} \left[ \frac{I}{t.d.\log \Delta \lambda} \right]$                                  | $+ \int_{2}^{\pi} \left[ \frac{\mathrm{I}}{\mathrm{t.d.log}\Delta L} \right]$                    | $+ \frac{I}{2} \left[ \frac{I}{t.d.\log \Delta A} \right]$                                               |
| •••                    | • • • • • • •                                                                                        | • • • • • • • •                                                                                  | • • • • • • •                                                                                            |
| », μ"                  | $+ \frac{\mathbf{I}}{\mathbf{t.d.log}\Delta\lambda_{\mathbf{s}}}$                                    | $+ \frac{1}{\text{t.d.log}\Delta L_*}$                                                           | $+\frac{1}{t.d.\log \Delta A_{*}}$                                                                       |
| "φı                    | $+ \prod_{i}^{*} \left[ \frac{\text{t.d.log } \cos A}{\text{t.d.log } \Delta \lambda} \right]$       | $+ \int_{1}^{*} \left[ \frac{\text{t.d.log sin } A}{\text{t.d.log } \Delta L} \right]$           | $\mathbf{I} + \frac{\mathbf{I}}{\left[\frac{\mathrm{t.d.}\log\sin A}{\mathrm{t.d.}\log\Delta A}\right]}$ |
| ,<br>,, φ <sub>2</sub> | $+ \frac{1}{2} \left[ \frac{\text{t.d.log } \cos \varDelta}{\text{t.d.log } \Delta \lambda} \right]$ | $+ \int_{2}^{*} \left[ \frac{\text{t.d.log sin } \mathcal{A}}{\text{t.d.log } \Delta L} \right]$ | $1 + \frac{1}{2} \left[ \frac{\text{t.d.}\log \sin A}{\text{t.d.}\log \Delta A} \right]$                 |
| • •                    | • • • • • • • •                                                                                      |                                                                                                  | • • • • • •                                                                                              |
| », φ <sub>n</sub>      | $+\frac{\text{t.d.}\log\cos A_{*}}{\text{t.d.}\log\Delta\lambda_{*}}$                                | $+ \frac{\text{t.d.log } \sin A_n}{\text{t.d.log } \Delta L_n}$                                  | $I + \frac{\text{t.d.log} \sin A_{\pi}}{\text{t.d.log} \Delta A_{\pi}}$                                  |

Table of Substitutions for  $\mu$  and  $\phi$ .

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The values of the absolute terms, E, for the geodetic equations are the differences between the values of latitude, longitude and azimuth at the closing station, as obtained by the calculation along the traverse, and the final values as given by the Reduction of the North-West Quadrilateral; and if the subscripts f and v denote the *final* and *traverse* values at the closing station

$$E_{\lambda} = \lambda_{v} - \lambda_{f}$$
$$E_{L} = L_{v} - L_{f}$$
$$E_{A} = B_{v} - B_{f}$$

When the linear and geodetic equations have been obtained in the manner here described, it will be found that the numerical values of the coefficients are much larger in the former than in the latter, and that those in latitude and longitude are least of all. Although this cannot produce any effect on the final results it may increase the labour of the calculations. It has therefore been sometimes thought desirable to introduce factors which roughly equalize the coefficients. Such factors were employed for the Eastern Sind Series; they were

| for tl | ne azimuth equation              | ••• | ••• | 1   |
|--------|----------------------------------|-----|-----|-----|
| "      | latitude and longitude equations | ••• | ••• | 10  |
| ,,     | linear equation                  | ••• | ••• | 0.1 |

# 11.

# Final Reduction of the Triangulation. The Solution of the Equations between the Indeterminate Factors.

If we assume that the number of triangles entering the reduction is t and that they furnish n circuit equations, the latter may now be briefly written in order thus :—

in which equations the left-hand subscript in 'old face' type corresponds to the number of the equation and the right-hand subscript in ordinary type gives the number of the triangle.

Since the weights of the angles are all taken as equal, the minimum which governs the solution of the foregoing equations will, when x has been eliminated from it, become

$$U = \{(y_1 + z_1)^2 + y_1^2 + z_1^2\} + \dots + \{(y_i + z_i)^2 + y_i^2 + z_i^2\}$$

[24]



The symbols employed for the indeterminate factors are  $_1\Lambda$ ,  $_2\Lambda$ ,  $_3\Lambda$ , &c., and the equations between them are\*

$${}^{t}_{1} \begin{bmatrix} \mathbf{1} \mathbf{b} & \mathbf{1} \mathbf{3} \mathbf{i} + \mathbf{1} \mathbf{c} & \mathbf{0} \end{bmatrix}_{1} \Lambda + {}^{t}_{1} \begin{bmatrix} \mathbf{1} \mathbf{b} & \mathbf{1} \mathbf{3} \mathbf{i} + \mathbf{1} \mathbf{c} & \mathbf{0} \end{bmatrix}_{2} \Lambda + \dots + {}^{t}_{1} \begin{bmatrix} \mathbf{1} \mathbf{b} & \mathbf{1} \mathbf{3} \mathbf{i} + \mathbf{1} \mathbf{c} & \mathbf{0} \end{bmatrix}_{n} \Lambda = {}_{1} E$$

$${}^{t}_{1} \begin{bmatrix} \mathbf{0} & \mathbf{1} \mathbf{3} + \mathbf{1} \mathbf{c} & \mathbf{0} \end{bmatrix}_{1} \Lambda + {}^{t}_{1} \begin{bmatrix} \mathbf{0} & \mathbf{1} \mathbf{3} + \mathbf{0} \mathbf{c} \end{bmatrix}_{2} \Lambda + \dots + {}^{t}_{1} \begin{bmatrix} \mathbf{0} & \mathbf{1} \mathbf{3} + \mathbf{0} \mathbf{c} \end{bmatrix}_{n} \Lambda = {}_{2} E$$

$${}^{t}_{1} \begin{bmatrix} \mathbf{0} & \mathbf{1} \mathbf{3} + \mathbf{0} \mathbf{c} \end{bmatrix}_{n} \Lambda + {}^{t}_{1} \begin{bmatrix} \mathbf{0} & \mathbf{1} \mathbf{3} + \mathbf{0} \mathbf{c} \end{bmatrix}_{2} \Lambda + \dots + {}^{t}_{1} \begin{bmatrix} \mathbf{0} & \mathbf{1} \mathbf{3} + \mathbf{0} \mathbf{c} \end{bmatrix}_{n} \Lambda = {}_{2} E$$

$${}^{t}_{1} \begin{bmatrix} \mathbf{0} & \mathbf{1} \mathbf{3} + \mathbf{0} \mathbf{c} \end{bmatrix}_{n} \Lambda + {}^{t}_{1} \begin{bmatrix} \mathbf{0} & \mathbf{1} \mathbf{3} + \mathbf{0} \mathbf{c} \end{bmatrix}_{n} \Lambda + {}^{t}_{n} \begin{bmatrix} \mathbf{0} & \mathbf{1} \mathbf{3} + \mathbf{0} \mathbf{c} \end{bmatrix}_{n} \Lambda = {}_{n} E$$

in which

$$\mathfrak{B} = \frac{\mathbf{I}}{3} (2\mathfrak{b} - \mathfrak{c}) \text{ and } \mathfrak{C} = \frac{\mathbf{I}}{3} (2\mathfrak{c} - \mathfrak{b}).\dagger$$

These equations having been solved, the values of the angular errors are given by the formulæ

$$y_p = {}_1\mathfrak{G}_{p-1}\Lambda + {}_2\mathfrak{G}_{p-2}\Lambda + \cdot \cdot \cdot \cdot + {}_n\mathfrak{G}_{p-n}\Lambda,$$
  
$$z_p = {}_1\mathfrak{G}_{p-1}\Lambda + {}_2\mathfrak{G}_{p-2}\Lambda + \cdot \cdot \cdot + {}_n\mathfrak{G}_{p-n}\Lambda,$$
  
$$x_p = - (y_p + z_p).$$

$$\frac{2}{3} \int_{1}^{t} \left[ (\mathfrak{b}^{2} - \mathfrak{b}\mathfrak{c} + \mathfrak{c}^{2}) \right] \quad (\mathfrak{b}^{2} - \mathfrak{b}\mathfrak{c} + \mathfrak{c}^{2}) = 0$$

 $\uparrow$  As the factor  $\frac{1}{3}$  enters all the coefficients of all the equations, its omission from the actual calculations can have no effect on the final values of the angular errors x, y and x; it was accordingly omitted.



<sup>\*</sup> In these equations, although the corresponding coefficients on opposite sides of the diagonal appear to differ, their values are in reality identical in each term of the summation. Both forms, however, have been made use of as a check on the calculations; and for a like reason the diagonal coefficients have been obtained also by the formula

### CHAPTER III.

### THE DETAILS OF THE FINAL REDUCTIONS.

# 1.

### Preliminary Remarks.

The general principles followed in the reduction of the triangulation, as described in the preceding chapter, apply equally to both the Jodhpore and Eastern Sind Meridional Series; but in the present chapter which deals with the details of the reductions, it will be necessary, as the two series are entirely independent, to keep these details apart, while it will be convenient to include them in the same sections. The same preamble for each section will be made to apply to both reductions, the details themselves being headed by the name of the series to which they belong.

# 2.

### The Figural Reductions antecedent to the Final Simultaneous Reduction of each Series.

The Jodhpore Meridional Series comprises 3 quadrilaterals, 8 single polygons and 2 double polygons, containing 225 observed angles connected together by 76 *Triangular*, 12 *Central* and 15 *Side* equations of condition.

The Eastern Sind Meridional Series comprises 3 quadrilaterals, 7 single polygons and 2 double polygons, containing 198 observed angles connected together by 67 *Triangular*, 11 *Central* and 14 *Side* equations of condition.

The figural conditions and reductions are given for each series immediately after the Abstracts of the Observed Angles: a diagram of each figure is also given in the Plate following the details of each series. These together afford the means of readily following the calculations appertaining to each figure.

## 3.

### The Description of the Reduction Charts.

The respective Reduction Charts at the end of this volume exhibit the whole of the Principal Triangulation in each series. The triangulation in each case consists of polygonal figures from which only a single chain of triangles was selected for treatment simultaneously. The fixed data for the final reduction of the two series are the lengths and positions of the emanation-sides in the Karáchi Longitudinal and the termination-sides in the Sutlej and Great Indus Series, between which they respectively depend. These sides are shewn on the charts by double lines, terminated by black circles with white centres.

The so-called *circuit* triangles—the errors of whose angles are the unknown quantities in each reduction—are indicated by continuous lines. The *non-circuit* triangles, or those which are excluded from the simultaneous reduction, have their sides indicated by broken lines.

Along the flank on the right-hand side, looking north, of each chain, a dotted line runs parallel to the sides of the triangles; this is the line of the traverse.

The principal stations are indicated on the charts by small circles, with the names and the serial numbers by which it has been found convenient to distinguish them for reference in the course of the reductions. These numbers are in Roman character and are progressive from south to north.

All the principal stations which fall on the lines of traverse have an additional number in block type assigned to them, called their *traverse number*, these numbers commence from the initial station.

The circuit triangles are numbered in the Jodhpore Meridional Series from 1 to 48, commencing from the side Súnda-Bonik, and the non-circuit triangles are numbered in succession in smaller type from 49 to 76. In the Eastern Sind Meridional Series the circuit triangles are numbered from 1 to 39, commencing from the side Rojhra-Sandohar, and the non-circuit triangles are numbered from 40 to 67 in smaller type. In each of the circuit triangles one of the angles is marked y and another z; y and z are the symbols for the errors of the 'angles of continuation', while x is the symbol for the errors of the flank angles; but as x has been eliminated throughout by the substitution for it of -(y+z), it is not indicated on the charts. The addition of the number of any triangle as a subscript to either of these symbols, particularizes the angle in each instance.

The polygonal figures or net-works are distinguished by figural numbers as Fig. 1, Fig. 2, and these distinctions are continued in the diagrams and reductions of figures.

# **4**.

General Outline of the Formation of the Linear and Geodetic Equations of Condition.

### The Jodhpore Meridional Series.

The triangulation having first been made consistent so far as all figural conditions were concerned, the linear calculations were commenced from the side Súnda-Bonik of the Karáchi Longitudinal Series, and carried northwards, through the circuit triangles only, until they closed on the side Kaimsir-Kanda of the Sutlej Series. The calculations of geodetic latitudes, longitudes and azimuths were then carried along the eastern flank of the chain, commencing and terminating with the linear calculations. The errors which form the absolute terms of the equations, are the differences between the two sets of linear and geodetic values of the side Kaimsir-Kanda and at the station Kanda, as obtained by the calculations just described and as already given finally by the Simultaneous Reduction of the North-West Quadrilateral. Thus there are four equations which may be symbolized as follows, if we employ S to denote the sum of the terms on the right-hand side of the linear equation on page [21] and of the geodetic equation on page [22] with the subscript c to denote the linear,  $\lambda$  the latitudinal, L the longitudinal, and A the azimuthal equations; while E with the corresponding subscript denotes the absolute term :—

> (1)  $_{c}S = _{c}E$ , (2)  $_{\lambda}S = _{\lambda}E$ , (3)  $_{L}S = _{L}E$ , (4)  $_{A}S = _{A}E$ .

#### The Eastern Sind Meridional Series.

This series having in like manner been first made consistent so far as the figural conditions were concerned, the linear calculations were commenced from the side Rojhra-Sandohar of the Karáchi Longitudinal Series and closed on the side Dáowála-Máchka of the Great Indus Series, the geodetic calculations being carried along the eastern flank. The errors are the differences between two sets of values of the closing side Dáowála-Máchka and at the closing station Dáowála, as given by the Simultaneous Reduction of the North-West Quadrilateral and as obtained by the calculations carried through the series. The equations may be symbolized as before.



### Formation of the Coefficients of the Unknown Quantities.

On page [24] the equations of condition are represented by a form of which the following may be taken as a general illustration :—

 ${}_{\mathbf{m}}\mathbf{b}_{1} y_{1} + {}_{\mathbf{m}}\mathbf{c}_{1} z_{1} + {}_{\mathbf{m}}\mathbf{b}_{2} y_{2} + {}_{\mathbf{m}}\mathbf{c}_{2} z_{2} + \cdot \cdot \cdot = {}_{\mathbf{m}}E$ 

the left-hand subscript denoting the equation number and the right-hand subscript the number of the triangle to which the errors appertain, and b and c being the coefficient of y and z respectively.

For the *Linear* Equation we shall have generally, see page [21],

$$b_p = + \beta_p = + ext{ t.d. log sin } Y ext{ for } 1^{\prime}$$
  
 $c_p = - \gamma_p = - ext{ t.d. log sin } Z$  ,

For the Geodetic Equations we shall have, see page [23],

$$\mathbf{b}_p = + (\mu_i \ \beta_p - \phi_i),$$
  
 $\mathbf{c}_p = - (\mu_i \ \gamma_p + \phi_i),$ 

or

$$b_{p} = + \{ (\mu_{l+1} - \mu_{l}) a_{p} + \mu_{l+1} \beta_{p} + \phi_{l} \},\$$
  
$$c_{p} = + \{ (\mu_{l+1} - \mu_{l}) a_{p} - \mu_{l} \gamma_{p} + \phi_{l+1} \},\$$

the former being applicable to any, the pth, triangle when it has only the angle X in the traverse at station l, and the latter when it has the side opposite X in the traverse and lying between the stations l and l + 1.

Exceptions to the General Expressions for b and c.

### The Jodhpore Meridional Series.

Equation 1 has no exceptional coefficients; but in Equations 2, 3 and 4

$$\mathfrak{b}_{47} = - \mu_{23} a_{47} + \phi_{23}, \qquad \mathfrak{s}_{47} = - \mu_{23} (a_{47} + \gamma_{47}),$$

with the exception of  $c_{47}$  in Equation 4 in Azimuth, which needs the addition of unity to carry the calculations as far as the side Kanda-Randu, and the same equation has two extra coefficients

$$\mathfrak{b}_{48} = -1$$
 and  $\mathfrak{c}_{48} = -1$ 

to carry the calculations to the closing side Kanda-Kaimsir.

### The Eastern Sind Meridional Series.

Equation 1 has no exceptional coefficients, but in Equations 2, 3 and 4

$$b_{38} = -\mu_{19} a_{38} + \phi_{19}, \quad t_{38} = -\mu_{19} (a_{38} + \gamma_{38}),$$

with the exception of  $r_{38}$  in Equation 4 in Azimuth, which needs the addition of unity to carry the calculations as far as the side Dáowála-Kubba; and the same equation has two extra coefficients

$$b_{39} = -1$$
 and  $c_{39} = -1$ ,

to carry the calculations to the closing side Dáowála-Máchka.

# 6.

Synoptical Exhibition of the several Equations of Condition.

For the sake of brevity let us put  $_{m}k_{p}$  for  $_{m}b_{p} y_{p} + _{m}c_{p} z_{p}$  or, in other words, for the sum of the errors y and z of the angles Y and Z in any, the *p*th, triangle, respectively multiplied by their coefficients b and c in any, the *m*th, equation of condition; and further, let us put  $k \stackrel{i}{l}$  to represent the sum of the terms k for b series of triangles of which the

let us put  $_{m}k \int_{p}^{p}$  to represent the sum of the terms  $_{m}k$  for a series of triangles of which the first term is  $_{m}k_{p}$  and the last  $_{m}k_{q}$ .

The equations will then be expressed as follows :---

| The Jodhpore 1  | Meridional Series.                             | The Eastern Si  | nd Meridional Series                             |
|-----------------|------------------------------------------------|-----------------|--------------------------------------------------|
| (1). Linear.    | $_{1}k \downarrow^{48}$ = $_{1}E$ ,            | (1). Linear.    | $k \Big _{1}^{39} \ldots = k E,$                 |
| (2). Latitude.  | $_{2}k_{1}^{47}$ = $_{2}E$ ,                   | (2). Latitude.  | $_{2}k \Big _{1}^{38}$ = $_{2}E$ ,               |
| (3). Longitude. | $_{3}\mathbf{k}_{1}^{47}$ = $_{3}\mathbf{E}$ , | (3). Longitude. | $_{3}k \Big _{1}^{38}$ = $_{3}E$ ,               |
| (4). Azimuth.   | $_{4}^{k} \lim_{1}^{48} \ldots = _{4}E.$       | (4). Azimuth.   | $_{4}\mathbf{k} \Big _{1}^{39}  .  .  =  _{4}E.$ |
|                 |                                                |                 |                                                  |



[30]

# 7.

# The Numerical Values of the Fixed Data on which the Separate Beductions of the Jodhpore and Eastern Sind Meridional Series are based.

Both series emanate from the Karáchi Longitudinal Series; the Jodhpore closes on the Sutlej Series and the Eastern Sind on the Great Indus Series. The fixed data furnished by these series are given in Vols. III and IV of the *Account of the Operations &c.*; but for the geodetic elements a third place of decimals has been obtained by reference to the calculations of the North-West Quadrilateral. The data are as follows:—

### The Jodhpore Meridional Series.

Vol. III, page 47\_\_\_

Station of origin Bonik or XLI; side of origin Bonik or XLI to Súnda or XLIV.

### At Bonik.

| Latitude Nor | th        | •••     | ••• | •••            | 25°  | 3′  | 51"•496,  |
|--------------|-----------|---------|-----|----------------|------|-----|-----------|
| Longitude Ea | ast of Gr | eenwich | ••• | •••            | 72   | 54  | 21 .852,  |
| Azimuth of § | Súnda     | •••     | ••• | •••            | 55   | 4   | 15 .670,  |
| Distance     | "         | •••     | ••• | $\mathbf{Log}$ | Feet | 5.3 | 541461,0. |

Vol. IV, page 9\_\_\_\_

Closing station Kanda or XXI; closing side Kanda or XXI to Kaimsir or XIX.

### At Kanda.

| Latitude No | rth         | •••    | ••• | •••            | 29°  | 27  | 41 <sup>"</sup> · 523, |
|-------------|-------------|--------|-----|----------------|------|-----|------------------------|
| Longitude E | last of Gre | enwich | ••• | •••            | 72   | 22  | 12 · 292,              |
| Azimuth of  | Kaimsir     | •••    | ••• | •••            | 73   | 26  | 34 · 581,              |
| Distance    | "           | •••    | ••• | $\mathbf{Log}$ | Feet | 4.8 | 8021262,6.             |

### The Eastern Sind Meridional Series.

Vol. III, page 49\_\_\_\_

Station of origin Rojhra or LXXV; side of origin Rojhra or LXXV to Sandohar or LXXVIII.



### At Rojhra.

| Latitude Nor | rth          | •••   | ••• | ••• | 24°        | 57  | 26" · 278, |
|--------------|--------------|-------|-----|-----|------------|-----|------------|
| Longitude E  | ast of Green | nwich | ••• | ••• | 7 <b>0</b> | 16  | 45 .080,   |
| Azimuth of   | Sandohar     | •••   | ••• | ••• | III        | 55  | 37 .085,   |
| Distance     | "            | •••   | ••• | Log | g Feet     | 4.8 | 613162,0.  |

Vol. III, page 63\_\_\_

Closing station Dáowála or LXII; closing side Dáowála or LXII to Máchka or LIX.

### At Dáowála.

| Latitude North    | •••       | ••• | ••• | 28°    | 20' | 12 <sup>"</sup> ·867, |
|-------------------|-----------|-----|-----|--------|-----|-----------------------|
| Longitude East of | Greenwich | ••• | ••• | 69     | 52  | 57 .861,              |
| Azimuth of Mách   | ka        | ••• | ••• | 87     | I   | 26 · 701,             |
| Distance "        | •••       | ••• | Log | ; Feet | 4.2 | 780782,8.             |

# 8.

### The Sides and Angles of the Circuit Triangles.

The values of the Figurally Corrected Angles, and the logarithms of the Side-lengths, computed (in feet) with these angles in terms of the fixed sides of origins furnished by the Karáchi Longitudinal Series, are exhibited in the following table. The given angles are the corrected plane angles, obtained by deducting the sum of the spherical excess and the figural error from the observed angles. Should it be desired to trace the formation of any corrected plane angle, reference must be made to the Abstract of the Observed Angles and to the final data of the Sides and Angles of the Triangles, which are given for each Series in Part II of this volume. The final data will be found to contain three columns of angular corrections, which are respectively headed by the words 'Figure', 'Circuit' and 'Non-Circuit',---'figure' being here taken to include single triangles as well as polygons and net-works; the corrections in the first column are what have been applied, with the spherical excess, to the observed angles, in order to obtain the figurally corrected plane angles; those in the second column are what have been derived from the Simultaneous Reduction; and those in the third column are what have been computed to satisfy the geometrical conditions of figures containing noncircuit triangles, which had to be adjusted to the fixed circuit triangles; the application of the correction in the second or the third column, as the case may be, to the figurally corrected plane angle gives the finally corrected plane angle.

In order that it may be readily ascertained—without reference to the Reduction Chart whether any angle is a 'flank angle' or an 'angle of continuation', a column is inserted in the table which gives the symbolic error of the angle, either x, y, or z, but without the numerical subscript, as that may be inferred from the number of the triangle in the contiguous column. And since the stations on the right-hand flank of each chain are those at which the angles are the data for the formation of the values of the forward azimuth, and the sidelengths are the distances which were employed in the calculations of latitude, longitude and back azimuth-see the next section-these stations are indicated by numbers in block type, shewing by their sequence the order in which the geodetic calculations were performed, as well as by their Serial-numbers.

The logarithm of the side\* opposite any angle is given in the same horizontal line as the angle.

| _          | _               |                             |         |                                              |                               |                                                                                  |            |          |                   |        |                                                    |                      |                                                                                  |
|------------|-----------------|-----------------------------|---------|----------------------------------------------|-------------------------------|----------------------------------------------------------------------------------|------------|----------|-------------------|--------|----------------------------------------------------|----------------------|----------------------------------------------------------------------------------|
| umber      | Error           | Station Numbe               | rs      |                                              | Схсовв                        | Logarithm of                                                                     | umber      | Error    | Station Number    | r8     |                                                    | Excess               | Logarithm of                                                                     |
| Triangle N | <b>Symbolic</b> | Serial                      | Тътогво | Corrected Plane<br>Angle                     | Spherical ]                   | side-length in<br>Feet                                                           | Triangle N | Symbolic | Serial            | Ттате  | Corrected Plane<br>Angle                           | Spherical ]          | side-length in<br>Feet                                                           |
| 1          | y<br>x          | XLIV†<br>XLI†               | 1       | 0 / "<br>67 46 16 374<br>38 58 34 012        | "<br>1·546<br>1·545           | 5 <sup>.2</sup> 394300,3<br>5 <sup>.0</sup> 716169,6                             | 7          | y<br>x   | VI<br>VII         | 4      | •                                                  | "<br>• 988<br>• 988  | 5.0322902,7<br>5.0838972,8                                                       |
|            | Z               | I                           |         | 73 15 9.614                                  | 1.240                         | 5.32541461,0                                                                     |            | z        | VIII              |        | 73 29 39 581                                       | •988                 | 5.1381624,0                                                                      |
| 2          | "               | XLI <del>†</del><br>I<br>II | 1<br>2  | 42 1 18.916<br>32 57 38.418<br>105 1 2.666   | •896<br>•895<br>•896          | 5°0802170,3<br>4°9901710,1<br>5°2394300,3                                        | 8          | "        | VII<br>VIII<br>X  | 4<br>5 | 78 52 35 925<br>54 5 20 027<br>47 2 4 048          | •994<br>•994<br>•993 | 5°1596831,5<br>5°0763658,2<br>5°0322902,7                                        |
| 8          | "               | I<br>II<br>III              | 2       | 62 5 14 311<br>65 16 14 201<br>52 38 31 488  | 1 · 152<br>1 · 153<br>1 · 152 | 5`1 <b>262122,</b> 9<br>5`1381524,5<br>5`0802170,3                               | 9          | "        | X<br>VIII<br>XII  | 5<br>6 | 58 28 48 631<br>40 23 2 671<br>81 8 8 698          | •920<br>•919<br>•920 | 5 <sup>.0</sup> 955752,0<br>4 <sup>.</sup> 9764150,2<br>5 <sup>.</sup> 1596831,5 |
| 4          | <b>"</b>        | II<br>III<br>V              | 2<br>3  | 81 14 27 158<br>50 38 46 034<br>48 6 46 808  | 1 · 448<br>1 · 448<br>1 · 447 | 5°2492743,0<br>5°1426858,1<br>5°1262122,9                                        | 10         | "        | VIII<br>XII<br>XI | 6      | 54 17 18 · 500<br>53 27 47 · 666<br>72 14 53 · 834 | •839<br>•838<br>•839 | 5°0262998,0<br>5°0217343,0<br>5°0955752,0                                        |
| 5          | "               | V<br>III<br>VII             | 3       | 55 224.543<br>43 543.054<br>81 51 52.403     | 1 ° 406<br>1 ° 405<br>1 ° 406 | 5°1672445,4<br>5°0882237,0<br>5°2492743,0                                        | 11         | "        | XI<br>XII<br>XIII | 6      | 58 35 3·569<br>49 54 37·059<br>71 30 19°372        | •613<br>•612<br>•613 | 4·9804863,8<br>4·9330120,5<br>5·0262998,0                                        |
| 6          | 33              | III<br>VII<br>VI            | 4       | 59 58 37 349<br>52 14 10 360<br>67 47 12 291 | 1°259<br>1°259<br>1°260       | 5 <sup>.</sup> 1381654,0<br>5 <sup>.</sup> 0986603,6<br>5 <sup>.</sup> 1672445,4 | 12         | "        | XII<br>XIII<br>XV | 6<br>7 | 55 52 6.311<br>55 44 31.893<br>68 23 21.796        | •530<br>•530<br>•531 | 4`9300395,0<br>4`9293894,0<br>4`9804863,8                                        |

#### The Jodhpore Meridional Series.

Sides and Angles of the Circuit Triangles.

In calculating these values 7-place Logarithm Tables were employed, the 8th place here shewn being obtained by interpolation.
 Stations XLI and XLIV appertain to the Karáchi Longitudinal Series.

# [34]

### INTRODUCTORY.

| umber       | Tror        | Station Number        | rs       |                                                      | TC088                        | Logarithm of                                                                     | umber       | Grror       | Station Number           | <b>18</b> |                                                      | X0685                        | Longrithm of                                                                     |
|-------------|-------------|-----------------------|----------|------------------------------------------------------|------------------------------|----------------------------------------------------------------------------------|-------------|-------------|--------------------------|-----------|------------------------------------------------------|------------------------------|----------------------------------------------------------------------------------|
| Triangle Nt | Symbolic 1  | Serial                | Тъчегво  | Corrected Plane<br>Angle                             | Spherical R                  | side-length in<br>Feet                                                           | Triangle Nu | Symbolic I  | Serial                   | Traverse  | Corrected Plane<br>Angle                             | Spherical E                  | side-length in<br>Feet                                                           |
| 13          | y<br>x<br>z | XV<br>XIII<br>XVII    | 7<br>8   | o , , ,<br>41 2 28 235<br>71 51 28 531<br>67 6 3 234 | "<br>• 387<br>• 387<br>• 387 | 4`7829912,5<br>4`9435445,6<br>4`93 <sup>00</sup> 395,0                           | 27          | y<br>x<br>z | XXX<br>XXXI<br>XXXII     | 14        | 0 / 4<br>62 36 10 878<br>50 17 54 648<br>67 5 54 474 | "<br>* 232<br>* 231<br>* 232 | 4`7831059,3<br>4`7209139,3<br>4`7991134,9                                        |
| 14          | "           | XIII<br>XVII<br>XVI   | 8        | 62 58 19°023<br>66 39 51°219<br>50 21 49°758         | • 308<br>• 309<br>• 308      | 4·8462106,8<br>4·8593750,6<br>4·7829912,5                                        | 28          | "           | XXXI<br>XXXII<br>XXXV    | 14<br>15  | 54 41 13·360<br>69 27 16·907<br>55 51 29·733         | • 268<br>• 268<br>• 268      | 4 <sup>.</sup> 7769521,4<br>4 <sup>.</sup> 8367174,3<br>4 <sup>.</sup> 7831059,3 |
| 15          | "           | XVI<br>XVII<br>XVIII  | 8        | 61 47 49 370<br>51 41 39 470<br>66 30 31 160         | • 293<br>• 292<br>• 293      | 4 <sup>.</sup> 8288978,5<br>4 <sup>.</sup> 7784961,4<br>4 <sup>.</sup> 8462106,8 | 29          | "           | XXXII<br>XXXV<br>XXXIV   | 15        | 67 040.435<br>44 59 31.366<br>67 59 48.199           | •198<br>•198<br>•198         | 4 <sup>.</sup> 7738584,7<br>4 <sup>.</sup> 6592209,5<br>4 <sup>.</sup> 7769521,4 |
| 16          | "           | XVII<br>XVIII<br>XX   | 8<br>9   | 58 51 57.020<br>61 22 36.792<br>59 45 26.188         | · 312<br>· 312<br>· 312      | 4 <sup>.</sup> 8248875,5<br>4 <sup>.</sup> 8358251,7<br>4 <sup>.</sup> 8288978,5 | 30          | "           | XXXV<br>XXXIV<br>XXXVI   | 15<br>16  | 70 37 23 043<br>57 57 48 695<br>51 24 48 262         | • 285<br>• 285<br>• 284      | 4 <sup>.</sup> 8555127,5<br>4 <sup>.</sup> 8090846,2<br>4 <sup>.</sup> 7738584,7 |
| 17          | ,,          | XX<br>XVIII<br>XXII   | 9<br>10  | 65 34 7·195<br>57 22 36·487<br>57 3 16·318           | · 322<br>· 322<br>· 321      | 4 <sup>.</sup> 8602877,0<br>4 <sup>.</sup> 8264608,8<br>4 <sup>.</sup> 8248875,5 | 31          | "           | XXXIV<br>XXXVI<br>XXXVII | 16        | 68 16 58 548<br>45 48 22 079<br>65 54 39 373         | • 296<br>• 295<br>• 296      | 4 <sup>.</sup> 8631099,7<br>4 <sup>.</sup> 7505939,5<br>4 <sup>.</sup> 8555127,5 |
| 18          | "           | XVIII<br>XXII<br>XXI  | 10       | 49 1 44 · 785<br>56 13 29 · 638<br>74 44 45 · 577    | • 269<br>• 270<br>• 270      | 4.7538358,6<br>4 <sup>.</sup> 7955835,4<br>4 <sup>.</sup> 8602877,0              | 32          | "           | XXXVI<br>XXXVII<br>XXXIX | 16<br>17  | 76 14 23 798<br>60 49 55 059<br>42 55 41 143         | • 523<br>• 523<br>• 522      | 5 <sup>.01</sup> 72653,4<br>4 <sup>.</sup> 9710226,1<br>4 <sup>.</sup> 8631099,7 |
| 19          | 33          | XXII<br>XXI<br>XXIV   | 10<br>11 | 71 6 24 · 992<br>49 40 9 · 593<br>59 13 25 · 415     | ·213<br>·213<br>·213         | 4`7957041,1<br>4`7018942,9<br>4`7538358,6                                        | 33          | "           | XXXVII<br>XXXIX<br>XLI   | 17        | 62 27 53 960<br>58 40 37 235<br>58 51 28 805         | ·756<br>·755<br>·755         | 5 <sup>.0</sup> 326389,5<br>5 <sup>.0164334,0</sup><br>5 <sup>.0172653,4</sup>   |
| 20          | "           | XXI<br>XXIV<br>XXIII  | 11       | 49 15 47 618<br>51 43 55 099<br>79 0 17 283          | • 186<br>• 186<br>• 187      | 4`6832567,7<br>4`6986876,7<br>4`7957041,1                                        | 34          | "           | XLI<br>XXXIX<br>XLIII    | 17        | 44 29 21 · 242<br>83 20 2 · 847<br>52 10 35 · 91 1   | · 807<br>· 807<br>· 807      | 4*9806427,3<br>5*1321181,7<br>5*0326389,5                                        |
| 21          | "           | XXIII<br>XXIV<br>XXV  | 11       | 75 11 12.014<br>64 22 53.389<br>40 25 54.597         | • 247<br>• 246<br>• 246      | 4 <sup>.</sup> 8566384,9<br>4 <sup>.</sup> 8263767,7<br>4 <sup>.</sup> 6832567,7 | 35          | "           | XXXIX<br>XLIII<br>XLIV   | 17<br>18  | 50 7 57 125<br>77 27 33 887<br>52 24 28 988          | ·681<br>·682<br>·682         | 4`9668066,8<br>5`0712249,0<br>4`9806427,3                                        |
| 22          | <b>,</b> ,  | XXIV<br>XXV<br>XXVI   | 11<br>12 | 47 2 9°207<br>54 21 24°784<br>78 36 26°009           | • 247<br>• 247<br>• 248      | 4`7296621,8<br>4`7751913,7<br>4`8566384,9                                        | 36          | "           | XLIV<br>XLIII<br>XLV     | 18<br>19  | 61 46 57 777<br>56 5 3 506<br>62 7 58 717            | •559<br>•559<br>•560         | 4`9653924.4<br>4`9393418,5<br>4`9668066,8                                        |
| 23          | >>          | XXV<br>XXVI<br>XXVII  | 12       | 65 53 51 365<br>61 40 28 499<br>52 25 40 136         | • 230<br>• 230<br>• 230      | 4`7909997,2<br>4`7752303,5<br>4`7296621,8                                        | 37          | "           | XLIII<br>XLV<br>XLVI     | 19        | 46 42 57 515<br>57 7 5 041<br>76 9 57 444            | • 423<br>• 423<br>• 423      | 4 <sup>.</sup> 8402865,0<br>4 <sup>.</sup> 9023478,8<br>4 <sup>.</sup> 9653924,4 |
| 24          | "           | XXVI<br>XXVII<br>XXIX | 12       | 52 36 18·938<br>63 28 54·528<br>63 54 46·534         | · 238<br>· 238<br>· 239      | 4`7377397,9<br>4`7893845,2<br>4`7909997,2                                        | 38          | "           | XLVI<br>XLV<br>XLVIII    | 19        | 61 41 27 643<br>43 59 57 462<br>74 18 34 895         | •240<br>•240<br>•240         | 4 <sup>.</sup> 8014600,7<br>4 <sup>.</sup> 6985442,8<br>4 <sup>.</sup> 8402865,0 |
| 25          | "           | XXIX<br>XXVII<br>XXXI | 13<br>14 | 64 49 25 · 635<br>76 38 51 · 253<br>38 31 43 · 112   | · 333<br>· 333<br>· 333      | 4 <sup>.</sup> 8999677,4<br>4 <sup>.</sup> 9314159,3<br>4 <sup>.</sup> 7377397,9 | 39          | "           | XLV<br>XLVIII<br>XLIX    | 19<br>20  | 60 54 9 807<br>75 38 7 094<br>43 27 43 099           | • 389<br>• 389<br>• 388      | 4 <sup>.</sup> 9053616,1<br>4 <sup>.</sup> 9501573,9<br>4 <sup>.</sup> 8014600,7 |
| 26          | "           | XXVII<br>XXXI<br>XXX  | 14       | 47 29 25 249<br>64 5 47 364<br>68 24 47 387          | ·354<br>·355<br>·355         | 4`7991134,9<br>4`8855658,5<br>4`8999677,4                                        | 40          | "           | XLIX<br>XLVIII<br>L      | 20<br>21  | 54 14 25 146<br>53 12 46 377<br>72 32 48 477         | *347<br>*347<br>*348         | 4 <sup>.</sup> 8351057,4<br>4 <sup>.</sup> 8293903,2<br>4 <sup>.</sup> 9053616,1 |

### SIDES AND ANGLES OF THE CIRCUIT TRIANGLES.

| ele Number<br>olio Error |                 | Station Numbe     | rs         |                                                               | LTCess                  | Logarithm of                                                                                | amber      | Error       | Station Numbe       | 15         |                                                      | LCOBS                     | Logarithm of                                                                     |
|--------------------------|-----------------|-------------------|------------|---------------------------------------------------------------|-------------------------|---------------------------------------------------------------------------------------------|------------|-------------|---------------------|------------|------------------------------------------------------|---------------------------|----------------------------------------------------------------------------------|
| Triangle N               | <b>Bymbolic</b> | Serial            | Traverse   | Corrected Plane                                               | Spherical I             | ਤਿਤਾ side-length in<br>ਦਿ Feet<br>ਕਿ                                                        |            | Symbolic ]  | Serial              | Traverse   | Corrected Plane                                      | Spherical H               | side-length in<br>Feet                                                           |
| 41                       | y<br>x<br>z     | XLVIII<br>L<br>LI | 21         | o , , ,<br>72 28 35 · 609<br>53 42 55 · 525<br>53 48 28 · 866 | "<br>352<br>351<br>351  | 4`9075724,8<br>4`8345912,9<br>4`8351057,4                                                   | 45         | y<br>x<br>z | LIV<br>LV<br>LVII   | 2 2<br>2 3 | 0 / 4<br>45 15 20 358<br>60 2 25 646<br>74 42 13 996 | "<br>"151<br>"151<br>"151 | 4.6059389,0<br>4.6922322,3<br>4.7388607,5                                        |
| 42                       | "               | LI<br>L<br>LIII   | 2 1        | 61 I 3.915<br>42 10 17.234<br>76 48 38.851                    | ·311<br>·310<br>·311    | 4 <sup>.</sup> 8610759,6<br>4 <sup>.</sup> 7461320,9<br>4 <sup>.</sup> 9075724,8            | 46         | "           | LV<br>LVII<br>LIX   | 2 3        | 56 49 15 965<br>53 56 55 257<br>69 13 48 778         | •093<br>•093<br>•093      | 4`5578291,3<br>4`5427961,7<br>4`6059389,0                                        |
| 43                       | "               | L<br>LIII<br>LIV  | 2 1<br>2 2 | 63 22 13·301<br>44 16 54·664<br>72 20 52·035                  | · 272<br>· 272<br>· 273 | 4 <sup>.</sup> 8333217,7<br>4 <sup>.</sup> 7259946,3<br>4 <sup>.</sup> 8610759,6            | 47         | "           | LVII<br>LIX<br>XXI* | 23         | 63 2 16 479<br>80 51 26 717<br>36 6 16 804           | ·154<br>·154<br>·153      | 4 <sup>.</sup> 7375477,8<br>4 <sup>.</sup> 7819679,9<br>4 <sup>.</sup> 5578291,3 |
| 41                       | "               | LIII<br>LIV<br>LV | 2 2        | 52 22 56 280<br>47 41 58 303<br>79 55 5 417                   | *218<br>*217<br>*218    | 4 <sup>.7</sup> 388607,5<br>4 <sup>.7090919,8</sup><br>4 <sup>.8</sup> 333 <sup>217,7</sup> | <b>4</b> 8 | 33          | LIX<br>XXI*<br>XIX* |            | 73 52 44 873<br>50 13 50 356<br>55 53 24 771         | ·210<br>·210<br>·210      | 4 <sup>.</sup> 8021139,2<br>4 <sup>.</sup> 7052510,1<br>4 <sup>.</sup> 7375477,8 |

### The Eastern Sind Meridional Series.

| Sides and | <b>Angles</b> | of the | Circuit | Triangles. |
|-----------|---------------|--------|---------|------------|
|-----------|---------------|--------|---------|------------|

| umber      | Error           | Station Number         | <b>18</b> |                                                             | Crcess                    | Logarithm of                                                                     | umber      | Error       | Station Numbe      | rs       |                                                     | LCOBS                     | Logarithm of                                                                     |
|------------|-----------------|------------------------|-----------|-------------------------------------------------------------|---------------------------|----------------------------------------------------------------------------------|------------|-------------|--------------------|----------|-----------------------------------------------------|---------------------------|----------------------------------------------------------------------------------|
| Triangle N | <b>Bymbolio</b> | Serial                 | Traverse  | Corrected Plane<br>Angle                                    | Spherical I               | side-length in<br>Feet                                                           | Triangle N | Symbolic ]  | Serial             | Ттатегае | Corrected Plane<br>Angle                            | Spherical I               | side-length in<br>Feet                                                           |
| 1          | y<br>20<br>8    | LXXV†<br>LXXVIII†<br>V | 1<br>2    | 0 / /<br>60 25 36 · 142<br>68 39 56 · 059<br>50 54 27 · 799 | *<br>•689<br>•689<br>•689 | 5:0107629,1<br>5:0405510,9<br>4:9613162,0                                        | 7          | y<br>x<br>z | X<br>IX<br>XII     | 4        | 0 / 4<br>82 32 9 929<br>43 6 33 422<br>54 21 16 649 | "<br>"399<br>"398<br>"398 | 4`9775212,5<br>4`8158867,0<br>4`8911147,1                                        |
| 2          | · n             | LXXVIII†<br>V<br>IV    | 2         | 66 39 1.865<br>49 53 29.779<br>63 27 28.356                 | ·651<br>·650<br>·650      | 5 <sup>.0220231,3</sup><br>4 <sup>.</sup> 9426942,5<br>5 <sup>.0107629,1</sup>   | 8          | "           | IX<br>XII<br>XI    | 5        | 49 41 17 487<br>48 3 51 359<br>82 14 51 154         | • 407<br>• 407<br>• 407   | 4 <sup>.</sup> 8637686,8<br>4 <sup>.</sup> 8530204,8<br>4 <sup>.</sup> 9775212,5 |
| 3          | "               | IV<br>V<br>VII         | 2         | 54 30 56 859<br>51 49 21 859<br>73 39 41 282                | • 582<br>• 582<br>• 583   | 4`9506968,5<br>4`9354045,2<br>5`0220231,3                                        | 9          | "           | XI<br>XII<br>XIV   | 5        | 60 41 0.605<br>67 31 27.620<br>51 47 31.775         | · 432<br>· 432<br>· 431   | 4`9089527,3<br>4`9341636,6<br>4`8637686,8                                        |
| 4          | >>              | V<br>VII<br>VIII       | 2<br>3    | 45 29 6 · 174<br>68 56 56 · 008<br>65 33 57 · 818           | •459<br>•460<br>•459      | 4 <sup>.</sup> 8445767,8<br>4 <sup>.</sup> 9614489,2<br>4 <sup>.</sup> 9506968,5 | 10         | "           | XII<br>XIV<br>XV   | 5<br>6   | 57 3 26 471<br>62 44 33 923<br>60 11 59 606         | •445<br>•446<br>•446      | 4 <sup>.</sup> 8944242,1<br>4 <sup>.</sup> 9194326,2<br>4 <sup>.</sup> 9089527,3 |
| 5          | "               | VIII<br>VII<br>X       | 3<br>4    | 71 47 47 024<br>48 43 50 218<br>59 28 22 758                | • 320<br>• 319<br>• 320   | 4 <sup>.</sup> 8870788,9<br>4 <sup>.</sup> 7853734,8<br>4 <sup>.</sup> 8445767,8 | 11         | <b>)</b> )  | XV<br>XIV<br>XVII  | 6<br>7   | 55 49 56 225<br>64 1 50 061<br>60 8 13 714          | •416<br>•416<br>•416      | 4 <sup>.</sup> 8740090,7<br>4.9100682,1<br>4.8944242,1                           |
| 6          | "               | VII<br>X<br>IX         | 4         | 58 5 33 733<br>64 39 21 248<br>57 15 5 019                  | • 428<br>• 428<br>• 427   | 4 <sup>.</sup> 8911147,1<br>4 <sup>.</sup> 9183059,1<br>4 <sup>.</sup> 8870788,9 | 12         | "           | XIV<br>XVII<br>XVI | 7        | 56 8 31 · 166<br>57 21 1 · 570<br>66 30 27 · 264    | • 336<br>• 337<br>• 337   | 4 <sup>.</sup> 8308845,6<br>4 <sup>.</sup> 8368912,3<br>4 <sup>.</sup> 8740090,7 |

\* Stations XIX and XXI appertain to the Sutlej Series.
 † Stations LXXV and LXXVIII appertain to the Karáchi Longitudinal Series.

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# [36]

### INTRODUCTORY.

| umber       | Grror       | Station Number               | 18       |                                                       | gxcess                       | Logarithm of                                                                     | umber      | Error       | Station Number           | 18       |                                                         | Grees                        | Logarithm of                                                                     |
|-------------|-------------|------------------------------|----------|-------------------------------------------------------|------------------------------|----------------------------------------------------------------------------------|------------|-------------|--------------------------|----------|---------------------------------------------------------|------------------------------|----------------------------------------------------------------------------------|
| Triangle Nt | Symbolic 1  | Serial                       | Traverse | Corrected Plane<br>Angle                              | Spherical I                  | side-length in<br>Feet                                                           | Triangle N | Symbolic 1  | Serial                   | Traverse | Corrected Plane<br>Angle                                | Spherical I                  | side-length in<br>Feet                                                           |
| 18          | y<br>x<br>z | XVI<br>XVII<br>XIX           | 7        | 0 , "<br>77 11 24.737<br>55 32 19.563<br>47 16 15.700 | *<br>• 396<br>• 396<br>• 396 | 4`9539047,0<br>4`8810459,7<br>4`8308845,6                                        | 27         | у<br>х<br>z | XXXII<br>XXXVI<br>XXXV   | 14       | ° , *<br>53 8 56 °058<br>57 35 23 °738<br>69 15 40 °204 | *<br>* 357<br>* 358<br>* 358 | 4 <sup>.</sup> 8313370,8<br>4 <sup>.</sup> 8546028,5<br>4 <sup>.</sup> 8990466,5 |
| 14          | <b>))</b>   | XVII<br>XIX<br>XX            | 7<br>8   | 41 55 0.934<br>51 36 23.514<br>86 28 35.552           | *334<br>*335<br>*335         | 4`7795369,8<br>4`8489119,1<br>4`9539047,0                                        | 28         | "           | XXXVI<br>XXXV<br>XXXVIII | 14<br>15 | 80 54 58 440<br>44 31 54 224<br>54 33 7 336             | • 309<br>• 308<br>• 308      | 4 <sup>.</sup> 9148888,6<br>4 <sup>.</sup> 7662763,7<br>4 <sup>.</sup> 8313370,8 |
| 15          | <b>2</b> 7  | XX<br>XIX<br>XXII            | 8<br>9   | 56 58 45 571<br>69 3 7 045<br>53 58 7 384             | • 277<br>• 277<br>• 276      | 4`7952413,0<br>4`8420544,4<br>4`7795369,8                                        | 29         | "           | XXXV<br>XXXVIII<br>XL    | 15       | 67 48 44 755<br>51 2 25 685<br>61 8 49 560              | ·438<br>·438<br>·438         | 4°9390420,9<br>4°8632041,5<br>4°9148888,6                                        |
| 16          | "           | XIX<br>XXII<br>XXI           | 9        | 57 5 2.499<br>58 6 11.752<br>64 48 45.749             | •242<br>•242<br>•242         | 4`7626348,0<br>4`7675390,3<br>4`7952413,0                                        | 30         | "           | XXXVIII<br>XL<br>XLIII   | 15<br>16 | 51 45 15 170<br>59 49 40 747<br>68 25 4 083             | *434<br>*435<br>*435         | 4 <sup>.</sup> 8656802,9<br>4 <sup>.</sup> 9073853,9<br>4 <sup>.</sup> 9390420,9 |
| 17          | "           | XXII<br>XXI<br>XXIV          | 9<br>10  | 96 47 51 989<br>45 32 39 977<br>37 39 28 034          | · 307<br>· 307<br>· 306      | 4`9735696,1<br>4`8302062,6<br>4`7626348,0                                        | 31         | "           | XL<br>XLIII<br>XLII      | 16       | 51 3 12 711<br>45 24 44 366<br>83 32 2 923              | · 237<br>· 236<br>· 237      | 4 <sup>.7</sup> 592824,2<br>4 <sup>.7210395,8</sup><br>4 <sup>.8656802,9</sup>   |
| 18          | "           | XXI<br>XXIV<br>XXIII         | 10       | 53 51 39 689<br>41 47 58 259<br>84 20 22 052          | · 377<br>· 377<br>· 378      | 4 <sup>.</sup> 8828828,3<br>4 <sup>.</sup> 7995097,2<br>4 <sup>.</sup> 9735696,1 | 32         | "           | XLIII<br>XLII<br>XLV     | 16<br>17 | 90 57 38 993<br>39 4 15 346<br>49 58 5 66 1             | ·214<br>·214<br>·214<br>·214 | 4 <sup>.</sup> 8751695,0<br>4 <sup>.</sup> 6747655,0<br>4 <sup>.</sup> 7592824,2 |
| 19          | "           | XXIII<br>XXIV<br>XXVI        | 10       | 53 546.074<br>5027 6.823<br>7627 7.103                | • 292<br>• 291<br>• 292      | 4·7980356,0<br>4·7822440,8<br>4·8828828,3                                        | 33         | "           | XLII<br>XLV<br>XLIV      | 17       | 39 23 48 183<br>36 41 34 965<br>103 54 36 852           | · 173<br>· 173<br>· 174      | 4 <sup>.</sup> 6906554,1<br>4 <sup>.</sup> 6644544,3<br>4 <sup>.</sup> 8751695,0 |
| 20          | ,,          | XXIV<br>XXVI<br>XXIX         | 10<br>11 | 50 52 6.395<br>81 47 18.952<br>47 20 34.653           | · 325<br>· 325<br>· 324      | <b>4·8211916,3</b><br>4·9270230,5<br>4·7980356,0                                 | 34         | "           | XLV<br>XLIV<br>XLVI      | 17<br>18 | 47 39 45°093<br>46 16 27°476<br>86 3 47°431             | · 102<br>· 101<br>· 102      | 4`5604379,1<br>4`5506137,7<br>4`6906554,1                                        |
| 21          | <b>)</b> )  | XXVI<br>XXIX<br>XXVIII       | 11       | 64 59 12°135<br>52 4 35°885<br>62 56 11°980           | • 278<br>• 277<br>• 278      | 4 <sup>.</sup> 8287844,9<br>4 <sup>.</sup> 7685410,7<br>4 <sup>.</sup> 8211916,3 | 35         | "           | XLIV<br>XLVI<br>XLVIII   | 18       | 61 37 39 705<br>71 45 4 427<br>46 37 15 868             | °120<br>°120<br>°119         | 4`6434293,2<br>4`6765957,7<br>4`5604379,1                                        |
| 22          | "           | XXIX<br>XXVIII<br>XXXI       | 11<br>12 | 70 11 35 997<br>56 11 39 291<br>53 36 44 712          | •348<br>•348<br>•348         | 4 <sup>.</sup> 8964929,2<br>4 <sup>.</sup> 8425402,3<br>4 <sup>.</sup> 8287844,9 | 36         | "           | XLVI<br>XLVIII<br>XLIX   | 18<br>19 | 54 51 24 099<br>53 27 39 582<br>71 40 56 319            | · 106<br>· 105<br>· 106      | 4`5786147,4<br>4`5709725,7<br>4`6434293,2                                        |
| 23          | ,,          | XXVIII<br>XXXI<br>XXX<br>XXX | 12       | 55 22 29 880<br>56 34 38 848<br>68 2 51 272           | • 362<br>• 362<br>• 363      | 4 <sup>.8</sup> 445223,3<br>4 <sup>.8</sup> 506760,9<br>4 <sup>.8</sup> 964929,2 | 37         | <b>, 22</b> | XLVIII<br>XLIX<br>LI     | 19       | 60 29 15 293<br>55 24 53 341<br>64 5 51 366             | .090<br>.090                 | 4`5642379,9<br>4`5401437,5<br>4`5786147,4                                        |
| 24          | "           | XXXI<br>XXX<br>XXXIII        | 12<br>13 | 53 10 19°774<br>67 44 37°678<br>59 5 2°548            | •332<br>•333<br>•333         | 4 <sup>.</sup> 8144035,6<br>4 <sup>.</sup> 8774508,3<br>4 <sup>.</sup> 8445223,3 | 38         | "           | XLIX<br>LI<br>LXII       | 19       | 45 42 26 938<br>86 5 44 591<br>48 11 48 471             | ' 101<br>' 102<br>' 102      | 4`5466079,7<br>4`6908169,2<br>4`564 <b>23</b> 79,9                               |
| 25          | "           | XXX<br>XXXIII<br>XXXII       | 13       | 49 35 11°380<br>56 58 6°983<br>73 26 41°637           | • 223<br>• 223<br>• 224      | 4 <sup>.</sup> 7143950,9<br>4 <sup>.</sup> 7562272,9<br>4 <sup>.</sup> 8144035,6 | <b>39</b>  | "           | LI<br>LXII<br>LIX        |          | 85 58 0.530<br>58 12 4.394<br>35 49 55.076              | • 142<br>• 141<br>• 141      | 4.7780708,6<br>4.7085175,6<br>4.5466079,7                                        |
| 26          | 33          | XXXIII<br>XXXII<br>XXXVI     | 13<br>14 | 85 736·193<br>5414 3·144<br>403820·663                | • 263<br>• 263<br>• 262      | 4`8990466,5<br>4`8098613,5<br>4`7143950,9                                        |            |             |                          |          |                                                         |                              |                                                                                  |

NOTE.-Stations LIX and LXII apportain to the Great Indus Series.

## 9.

# Preliminary Latitudes, Longitudes, and Azimuths of the Stations on the Line of the Traverse.

The following table gives the Geodetic Latitudes, Longitudes, and Azimuths, which have been obtained for all the stations and sides on the line of the traverse by applying the values of the difference of latitude, longitude, and azimuth—computed by the formulæ of Section 5 of the preceding chapter—first to the elements of the station of origin which are given on pages [31] and [32] and then to the deduced elements of every subsequent station in the order of succession which is indicated by the Traverse-numbers. Each station is thus regarded, first as the 'Deduced Station B' and afterwards as the 'Fixed Station A'.

In order to ascertain the differential values given by the geodetic calculations on which the tabulated elements are built up, we have for any, the *a*th, side on the flank of the chain

> $\Delta \lambda_a = (\lambda_{a+1} - \lambda_a);$   $\Delta L_a = (L_{a+1} - L_a);$  $\Delta A_a = B_a - (\pi + A_a);$

where  $A_a$  stands for the forward azimuth at 'fixed station'  $A_a$  of 'deduced station'  $B_a$ , and  $B_a$  for the back azimuth of  $A_a$  at  $B_a$ .

The three differential values depend on the length  $c_a$  and forward azimuth  $A_a$  of the side a, and also on the latitude  $\lambda_a$ . The logarithmic length is given in the preceding section, on the same horizontal line as the angle at the serial station which enters, in the table, between the stations numbered in block type a and (a + 1). The forward azimuth of the side a may be deduced by adding all the spherical angles at a, as given in the table, to the back azimuth  $B_{a-1}$ . Thus the logarithmic length of flank-side 4 in the Jodhpore Meridional Series is  $5 \cdot 0763658,2$  which occurs in Triangle No. 8 on the same line as Serial Station VIII, entering between the flank stations 4 and 5; and the forward azimuth of this side is equal to the back azimuth of 3 at 4 and the sum of the spherical angles at 4, which occur in Triangles Nos. 5, 6, 7 and 8, the respective values of which are  $81^\circ 51' 53'' \cdot 809, 52^\circ 14' 11'' \cdot 619, 57^\circ 47' 50'' \cdot 868$  and  $78^\circ 52' 36'' \cdot 919$ , together amounting to  $270^\circ 46' 33'' \cdot 215$ .



### The Jodhpore Meridional Series.

| Geodetic | Elements | of the | Traverse | Stations. |
|----------|----------|--------|----------|-----------|

|                    | Fixed | Statio   | n A        | Deduced Station B  |            |        |                             |    |                 |                    |     |            |          |  |
|--------------------|-------|----------|------------|--------------------|------------|--------|-----------------------------|----|-----------------|--------------------|-----|------------|----------|--|
| No. in<br>Traverae | A     | zimut    | th of B    | No. in<br>Traverse | L          | atitud | e North                     | Lo | ongitu<br>f Gre | de East<br>eenwich | •   | zimut      | h of A   |  |
|                    | o     | ,        | "          |                    | 0          | ,      | "                           | 0  | ,               | "                  | 0   | ,          | "        |  |
| 1                  | 136   | 4        | 11.039     | 2                  | 25         | 15     | 28.459                      | 72 | 42              | <b>2</b> .971      | 315 | 58         | 56.892   |  |
| 2                  | 207   | 30       | 44.414     | 3                  | 25         | 35     | 48 · 287                    | 72 | 53              | 43.884             | 27  | 35         | 45.36.   |  |
| 3                  | 130   | 44       | 59.268     | 4                  | 25         | 48     | 59.547                      | 72 | 36              | 48.017             | 310 | 37         | 38.920   |  |
| 4                  | 22I   | 24       | 12.132     | 5                  | 26         | 3      | 44.632                      | 72 | 51              | 12.776             | 41  | <b>3</b> 0 | 30.400   |  |
| 5                  | I 47  | I        | 24.992     | 6                  | 26         | 16     | 51.352                      | 73 | 4 I             | 46 · 339           | 326 | 57         | 15.12    |  |
| 6                  | 207   | 19       | 57.791     | 7                  | <b>2</b> 6 | 29     | 19.000                      | 73 | 48              | 55.906             | 27  | 23         | 8.690    |  |
| 7                  | 136   | 48       | 59.639     | 8                  | 26         | 39     | 52.735                      | 72 | 37              | 53.447             | 316 | 44         | 3.258    |  |
| 8                  | 201   | 3        | 35.2CI     | 9                  | 26         | 50     | <b>2</b> 5 <sup>.</sup> 979 | 72 | 42              | 25.309             | 21  | 5          | 37 . 87; |  |
| 9                  | 146   | 25       | 11.894     | 10                 | 26         | 59     | 39.130                      | 72 | 35              | 35.330             | 326 | 22         | 6.249    |  |
| 10                 | 150   | 45       | 18.001     | 11                 | 27         | 6      | 54.046                      | 72 | 31              | 3.044              | 330 | 43         | 14.200   |  |
| 11                 | 193   | 5        | 38 · 202   | 12                 | 27         | 16     | 28·856                      | 72 | 33              | 32.681             | 13  | 6          | 46.58    |  |
| 12                 | 206   | o        | 0.421      | 13                 | 27         | 25     | 36.824                      | 73 | 38              | 32 · 258           | 26  | 2          | 18.388   |  |
| 13                 | 154   | 46       | 31 · 129   | 14                 | 27         | 38     | 21.662                      | 72 | 31              | 47 • 578           | 334 | 43         | 24.06    |  |
| 14                 | 182   | 20       | 3.732      | 15                 | 27         | 49     | 41.047                      | 72 | 32              | 18.732             | 2   | 20         | 18.230   |  |
| 15                 | 173   | 48       | 43 . 1 2 3 | 16                 | 28         | о      | 15.339                      | 72 | 31              | I · 244            | 353 | 48         | 6.84     |  |
| 16                 | 167   | 15       | 42.086     | 17                 | 28         | 15     | 18.795                      | 72 | 27              | 10.266             | 347 | 13         | 53.32    |  |
| 17                 | 222   | 18       | 14.443     | 18                 | 28         | 29     | 40.832                      | 72 | 41              | 59.428             | 42  | 25         | 16.86    |  |
| 18                 | 156   | 36       | 44 · 873   | 19                 | 28         | 42     | 51.016                      | 72 | 35              | 31.696             | 336 | 33         | 39*24    |  |
| 19                 | 200   | 42       | 51.881     | 20                 | 28         | 56     | 36.587                      | 72 | 41              | 26.683             | 20  | 45         | 43.05    |  |
| 20                 | 118   | 27       | 52.034     | 21                 | 20         | - 1    | 54.718                      | 72 | 30              | 18.013             | 298 | 22         | 27.08    |  |
| 21                 | 170   | ,<br>10  | 43.700     | 22                 | 20         | 10     | 33.811                      | 72 | 28              | 35.012             | 350 | ٥          | 53.00    |  |
|                    | ./.   | 28       | 5 · 2 20   | 23                 | 20         | 17     | 57.168                      | 72 | 24              | 44.722             | 325 | 7<br>26    | 12.22    |  |
| 22                 | • > > | <u>_</u> | 2 220      | ****               | *y<br>20   | -/     | J/ 100                      | 72 | - 4             | 12·17              | 222 | -0<br>     | aa.e.    |  |
| 23                 | 107   | 7        | 30.09      | AAI*               | <b>2</b> 9 | 47     | 41 351                      | 74 | <i>6 6</i>      | 14 171             | 547 | U          | 23 042   |  |

\* This Station appertains to the Sutlej Series.

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### The Eastern Sind Meridional Series.

## Geodetic Elements of the Traverse Stations.

|                    | Fixed a | Statio     | n A      |                    | Deduced Station B |       |          |          |              |                          |     |       |        |  |  |  |
|--------------------|---------|------------|----------|--------------------|-------------------|-------|----------|----------|--------------|--------------------------|-----|-------|--------|--|--|--|
| No. in<br>Traverse | A       | zimut      | h of B   | No. in<br>Traverse | Le                | titud | e North  | Lo<br>of | ngitu<br>Gre | de <b>East</b><br>enwich | A   | zimut | h of A |  |  |  |
|                    | 0       | ,          | "        |                    | 0                 | ,     | "        | 0        | ,            | "                        | 0   | ,     | "      |  |  |  |
| 1                  | 172     | <b>2</b> I | 13.916   | 2                  | 25                | 15    | 24 . 179 | 70       | 14           | 5.949                    | 352 | 20    | 6.395  |  |  |  |
| 2                  | 190     | 26         | 34 . 386 | 3                  | 25                | 30    | 15.294   | 70       | 17           | 7.000                    | 10  | 27    | 51.990 |  |  |  |
| 3                  | 147     | 49         | 37.011   | 4                  | 25                | 38    | 46.003   | 70       | 11           | 11.084                   | 327 | 47    | 4.321  |  |  |  |
| 4                  | 174     | 26         | 50.422   | 5                  | 25                | 40    | 22.224   | 70       | 10           | 2.202                    | 254 | 26    | 20:240 |  |  |  |
|                    | -/-     |            | 59 455   |                    | 40                | 49    | 32 234   |          | 10           | 2 /03                    | 354 | 20    | 29 349 |  |  |  |
| 0                  | 221     | 20         | 33.130   | 6                  | 25                | 59    | 48.084   | 70       | 20           | 5°343                    | 41  | 30    | 56.471 |  |  |  |
| 6                  | 157     | 32         | 53.164   | 7                  | 26                | I 2   | 12.776   | 70       | 14           | 24.431                   | 337 | 30    | 23.182 |  |  |  |
| 7                  | 192     | 27         | 0.446    | 8                  | 26                | 23    | 35.752   | 70       | 17           | 11.873                   | I 2 | 28    | 14.630 |  |  |  |
| 8                  | 155     | 55         | 36.365   | 9                  | 26                | 34    | 4.53     | 70       | 11           | 59.558                   | 335 | 53    | 17.106 |  |  |  |
| 9                  | 184     | 45         | 29.056   | 10                 | 26                | 45    | 11.871   | 70       | 13           | 1.420                    | 4   | 45    | 56.831 |  |  |  |
| 10                 | 185     | 32         | 37.641   | 11                 | 26                | 59    | 5.122    | 70       | 14           | 31.740                   | 5   | 33    | 18·444 |  |  |  |
| 11                 | 175     | 10         | 5.928    | 12                 | 27                | 10    | 31 · 893 | 70       | 13           | 26.831                   | 355 | 9     | 36.379 |  |  |  |
| 12                 | 158     | 31         | 20.755   | 13                 | 27                | 22    | 6.796    | 70       | 8            | 20.232                   | 338 | 29    | 0.404  |  |  |  |
| 13                 | 179     | 39         | 46.947   | 14                 | 27                | 32    | 45 984   | 70       | 8            | 16.314                   | 359 | 39    | 45.002 |  |  |  |
| 14                 | 178     | 48         | 28.772   | 15                 | 27                | 42    | 24.009   | 70       | 8            | 2.800                    | 358 | 48    | 22.205 |  |  |  |
| 15                 | 156     | 9          | 11.876   | 16                 | 27                | 54    | 35.662   | 70       | I            | 58.661                   | 336 | 6     | 21.000 |  |  |  |
| 16                 | 180     | 53         | 50.326   | 17                 | 28                | 2     | 23.887   | 70       | 2            | 6.027                    | 0   | 53    | 54.203 |  |  |  |
| 17                 | 125     | 12         | 20.411   | 1.8                | 28                | 6     | 22.262   | 60       | 57           | 27.418                   | 275 |       | 8.868  |  |  |  |
|                    | - 33    | • 3        | 20 411   |                    | 0                 | v     | 33 243   | , vy     | 57           | a/ 410                   | 315 | 11    | 0.000  |  |  |  |
| 18                 | 107     | 51         | 25.123   | 19                 | 28                | 12    | 34.031   | 69       | 55           | 59.856                   | 347 | 50    | 43.830 |  |  |  |
| 19                 | 160     | 39         | 0.725    | LXII*              | 28                | 20    | 12.444   | 69       | 52           | 57.889                   | 340 | 37    | 34.232 |  |  |  |

\* This Station appertains to the Great Indus Series.

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# 10.

### Numerical Values of the Absolute Terms in the Primary Equations of Condition.

The Lengths and Azimuths of the sides of the triangles, and the Latitudes and Longitudes of the Stations on the traverse flank of each chain, having been computed—as set forth in the two preceding sections—the values of the several Absolute Terms in the Primary Equations of Condition are indicated by the discrepancies between the computed values as here obtained at the junctions with the Sutlej and Great Indus Series and the corresponding values given in Volumes III and IV, and quoted in Section 7 of this Volume. The closing linear discrepancies are expressed logarithmically and the 7th place of decimals is treated as unity.

The Absolute Terms will now be particularised.

### The Jodhpore Meridional Series.

Equation 1, Linear. Between the sides Súnda-Bonik and Kaimsir-Kanda.

| Log. computed length Kaimsir-Kanda by Triangle No. 48 | •  | •  | •    | •  | •   | •    | •            | 4.8021139,2 |
|-------------------------------------------------------|----|----|------|----|-----|------|--------------|-------------|
| Log. final value; see page [31]                       | •  | •  | •    | •  | •   | •    | •            | 4.8021262,6 |
| $_{1}E = -123.4$                                      | Lo | ga | ritk | mi | c I | Erre | o <b>r -</b> | 0000123,4   |

Equations 2 to 4, Geodetic. Terminal Station, Kanda. Terminal side, Kaimsir-Kanda.

|                             | Latitude.        | Longitude.       | Azimuth.                  |  |  |
|-----------------------------|------------------|------------------|---------------------------|--|--|
|                             | o / //           | 0 1 //           | 0 / //                    |  |  |
| Computed values             | 29 27 41.351     | 72 22 12.171     | 73 26 31.365              |  |  |
| Final values; see page [31] | 29 27 41.523     | 72 22 12.292     | 73 26 34.581              |  |  |
| Errors                      | $_{2}E = -0.172$ | $_{3}E = -0.121$ | $_{4}\overline{E=-3.216}$ |  |  |

#### The Eastern Sind Meridional Series.

Equation 1, Linear. Between the sides Rojhra-Sandohar and Dáowála-Máchka.

| Log. computed length Dáowála-Mác | <b>hk</b> : | a k | ŊУ | Tri | ang | ;le | No | . 3 | 9  | •   | •   | •  | •   | •   | •   | 4.7780708,6  |
|----------------------------------|-------------|-----|----|-----|-----|-----|----|-----|----|-----|-----|----|-----|-----|-----|--------------|
| Log. final value; see page [32]  | •           | •   | •  | •   | •   | •   | •  | •   | •  | •   | •   | •  | •   | •   | •   | 4.7780782,8  |
| $_{1}E = -74.2$                  |             |     |    |     |     |     |    |     | Lo | gar | ith | mi | e E | rro | r – | - `0000074,2 |

#### NUMERICAL VALUES OF THE ABSOLUTE TERMS.

Equations 2 to 4, Geodetic. Terminal Station, Dáowála. Terminal side, Dáowála-Máchka.

| Latitude.                  | Longitude.                                                            | Azimuth.                                                                                                                                                                                     |
|----------------------------|-----------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| 0 / //                     | 0 / //                                                                | 0 / //                                                                                                                                                                                       |
| 28 20 12.444               | 69 52 57.889                                                          | 87 1 27.640                                                                                                                                                                                  |
| 28 20 12.867               | 69 52 57.861                                                          | 87 1 26.701                                                                                                                                                                                  |
| $_{2}E = -\circ \cdot 423$ | $_{3}E = +0.028$                                                      | $E = + \circ \cdot 939$                                                                                                                                                                      |
|                            | Latitude.<br>0 , "<br>28 20 12.444<br>28 20 12.867<br>$_2E = - 0.423$ | Latitude.       Longitude.         0       "       0       "         28       20       12.444       69       52       57.889         28       20       12.867       69       52       57.861 |

These absolute terms when multiplied by the equalizing factors given on page [24] become

 $_{1}E = -7.42$ ,  $_{2}E = -4.23$ ,  $_{3}E = +0.28$ ,  $_{4}E = +0.939$ .

# 11.

### Numerical Values of the $\mu s$ and $\phi s$ .

The table of substitutions at page [23] shews the general form of the factors  $\mu$  and  $\phi$ . The numerical values are tabulated in this section: they were constructed in the opposite order to that in which they are now recorded, commencing at the closing of the chain.\*

On reference to the equation on page [22] it will be observed that the  $\mu$ s are factors of the tab. log. differences of sine,  $\alpha$ ,  $\beta$  or  $\gamma$ . In the side equations it has been found convenient to multiply  $\alpha$ ,  $\beta$  and  $\gamma$  by 10<sup>7</sup>, or in other words to treat the 7th place of decimals as unity. It is convenient to do the same in the geodetic equations and to divide the  $\mu$ s by 10<sup>7</sup>, because the latter are large integral quantities containing more significant figures than are required: after division the last two places of decimals can be omitted. In the following tables  $\mu \times \frac{1}{10^7}$  is accordingly given.

<sup>\*</sup> The values of the tabular log. differences of the first terms of  $\Delta\lambda$ ,  $\Delta L$  and  $\Delta A$  in the expressions for them on pages [14] and [15] were employed for t.d. log.  $\Delta\lambda$ , t.d. log.  $\Delta L$  and t.d. log.  $\Delta A$ .

### The Jodhpore Meridional Series.

# Numerical Values of the $\mu s$ and $\phi s$ .

| o. of Station<br>in Traverse | Leti                                  | tude           | Long                           | itude      | Azir                              | nuth       |
|------------------------------|---------------------------------------|----------------|--------------------------------|------------|-----------------------------------|------------|
| No. of Sta<br>in Trave       | $_{\lambda}\mu \times \frac{1}{10^7}$ | <sub>م</sub> ھ | $_L \mu \times \frac{1}{10^7}$ | $_{L}\phi$ | $_{A}\mu \times \frac{1}{10^{7}}$ | д¢         |
| 1                            | + •00356                              | + .0077        | 00044                          | + .0866    | 00030                             | + 1 · 0394 |
| 2                            | 339                                   | 45             | 27                             | 829        | 13                                | 1.0328     |
| 3                            | 311                                   | 76             | 44                             | 763        | 20                                | 1.0320     |
| 4                            | 293                                   | 31             | 20                             | 721        | 10                                | 1.0335     |
| 5                            | 273                                   | <b>7</b> 0     | 40                             | 675        | 19                                | 1.0313     |
| 6                            | 255                                   | 45             | 27                             | 633        | 13                                | 1.0394     |
| 7                            | 237                                   | 64             | 37                             | 592        | 17                                | 1.0376     |
| 8                            | 223                                   | 36             | 22                             | 555        | 10                                | 1.0360     |
| 9                            | 208                                   | 48             | 28                             | 521        | 13                                | 1.0342     |
| 10                           | 196                                   | 30             | 19                             | 491        | 09                                | 1.0331     |
| 11                           | 195                                   | 19             | 12                             | 467        | 06                                | 1.0530     |
| 12                           | 181                                   | 26             | 16                             | 436        | 08                                | 1.0306     |
| 13                           | 169                                   | 39             | 23                             | 406        | 11                                | 1.0193     |
| 14                           | 151                                   | 2 I            | 13                             | 364        | 07                                | 1.0123     |
| 15                           | 135                                   | 23             | 14                             | 327        | 07                                | 1.0126     |
| 16                           | 121                                   | 20             | 12                             | 292        | 06                                | 1.0140     |
| 17                           | 100                                   | 12             | 07                             | 242        | 04                                | 1.0112     |
| 18                           | 080                                   | 50             | 27                             | 195        | 13                                | 1.0092     |
| 19                           | 062                                   | 34             | 18                             | 151        | 09                                | 1.0024     |
| 20                           | 043                                   | 49             | 27                             | 106        | 13                                | 1.0023     |
| 21                           | 036                                   | 21             | 11                             | 086        | 05                                | I '0042    |
| 22                           | 024                                   | 16             | 09                             | 057        | 04                                | 1.0038     |
| 23                           | 014                                   | 07             | •4                             | 032        | 02                                | 1.0019     |

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### The Eastern Sind Meridional Series.

Numerical Values of the  $\mu s$  and  $\phi s$ .

| of Station<br>Traverse | Leti                                    | tude           | Long                           | itude          | Azimuth                                  |         |  |  |  |
|------------------------|-----------------------------------------|----------------|--------------------------------|----------------|------------------------------------------|---------|--|--|--|
| No. of Sta<br>in Trave | $_{\lambda}\mu \times \frac{1}{10^{7}}$ | <sub>λ</sub> φ | $_L \mu \times \frac{1}{10^7}$ | <sub>L</sub> φ | $_{\mathbf{A}}\mu\times\frac{1}{10^{7}}$ | ₄φ      |  |  |  |
| 1                      | + .00381                                | + .0060        | 00033                          | + .0624        | 00012                                    | +1.0393 |  |  |  |
| 2                      | 256                                     | 52             | 29                             | - 597          | 13                                       | 1.0369  |  |  |  |
| 3                      | 235                                     | 60             | 33                             | 549            | 15                                       | 1.0348  |  |  |  |
| 4                      | 223                                     | 45             | 25                             | 522            | I 2                                      | 1.0332  |  |  |  |
| 5                      | 208                                     | 42             | 23                             | 488            | II                                       | 1'0323  |  |  |  |
| 6                      | 194                                     | 69             | 37                             | 456            | 17                                       | 1.0208  |  |  |  |
| 7                      | 177                                     | 54             | 30                             | 416            | 14                                       | 1.0191  |  |  |  |
| 8                      | 161                                     | 62             | 33                             | 380            | 15                                       | 1.0124  |  |  |  |
| 9                      | 146                                     | 49             | 26                             | 345            | 12                                       | 1.0120  |  |  |  |
| 10                     | 131                                     | 52             | 28                             | 309            | 13                                       | 1.0143  |  |  |  |
| 11                     | 112                                     | 56             | 30                             | 265            | 14                                       | 1.0133  |  |  |  |
| 12                     | 096                                     | 52             | 28                             | 228            | 13                                       | 1.0106  |  |  |  |
| 13                     | 080                                     | 40             | 21                             | 190            | 10                                       | 1.0080  |  |  |  |
| 14                     | 066                                     | 40             | 21                             | 155            | 10                                       | 1.0023  |  |  |  |
| 15                     | 052                                     | 40             | 21                             | 1 2 3          | 10                                       | 1.0028  |  |  |  |
| 16                     | 035                                     | 23             | 12                             | 084            | 60                                       | 1.0040  |  |  |  |
| 17                     | 025                                     | 23             | 13                             | 059            | 06                                       | 1.0038  |  |  |  |
| 18                     | 019                                     | 11             | 06                             | °45            | 03                                       | 1.0031  |  |  |  |
| 19                     | 011                                     | 07             | 04                             | 025            | 02                                       | 1.0015  |  |  |  |

# **12**.

Numerical Values of the Coefficients b and c of the Unknown Quantities y and z.

The following table gives the numerical values of the coefficients b and c of the unknown quantities y and z in each equation of condition. Should it be desired to reproduce



any one of these coefficients, as the value of  $b_p$  in the *q*th equation, it is first necessary to ascertain by reference to pages [29] and [30], whether the coefficient is one of those of an exceptional form for which symbolical expressions are there given. When not found in this list it will be understood to take one of the general forms on page [29].

#### Examples.

(1). To find the values of  $b_8$  and  $c_8$  in equation 1 of the Jodhpore Meridional Series.

This is a linear equation, and the forms of the coefficients are normal,

$$1b_8 = + \text{ t.d. } \log \sin 78^\circ 52' 35'' = + 4;$$
  
 $1c_8 = - \text{ t.d. } \log \sin 47 2 4 = -19.$ 

(2). To find the values of  $b_8$  and  $c_8$  in equation 3 of the Jodhpore Meridional Series.

The equation is longitudinal, and the forms of the coefficients are normal,

$${}_{3}b_{8} = + \{ ({}_{L}\mu_{5} - {}_{L}\mu_{4}) a_{8} + {}_{L}\mu_{5} \beta_{8} + {}_{L}\phi_{4} \}$$
  
= + \{ - 2000 \times '0000015 - 4023 \times '000004 + '0721 \}  
= + '0675;  
$${}_{3}c_{8} = + \{ ({}_{L}\mu_{5} - {}_{L}\mu_{4}) a_{8} - {}_{L}\mu_{4} \gamma_{8} + {}_{L}\phi_{5} \}$$
  
= + \{ - 2000 \times '0000015 + 2023 \times '0000019 + '0675 \}  
= + '0683.

(3). To find the values of  $b_{47}$  and  $c_{47}$  in equation 4 of the Jodhpore Meridional Series. The equation is azimuthal, and the forms of the coefficients are exceptional, see page [29],



### NUMERICAL VALUES OF THE COEFFICIENTS.

## The Jodhpore Meridional Series.

| Dircuit<br>Igle   | Coefficient | s of $y$ and $z$ | Circuit<br>ngle  | Coefficiente | of y and z      | Circuit<br>agle        | Coefficient | of y and z    | Circuit<br>Igle   | Coefficient | of $y$ and $z$ |             |
|-------------------|-------------|------------------|------------------|--------------|-----------------|------------------------|-------------|---------------|-------------------|-------------|----------------|-------------|
| No. of (<br>Trian | b           | ¢                | No. of (<br>Tria | đ            | ¢               | No. of (<br>Tria       | đ           | C             | No. of (<br>Triat | Ď           | ¢              |             |
| 1st               | Equation.   | Linear.          | 1st .            | Equation—    | -(Continued).   | 2nd .                  | Equation—   | -(Continued). | 2nd               | Equation-   | -(Continued)   | .).         |
| 1                 | + 8         | - 6              | 31               | + 9          | <del>-</del> το | 11                     | +0.0286     | - 0.0223      | 41                | +0.0004     | - 0.002        | 78          |
| 2                 | 24          | + 6              | 32               | 5            | 23              | 12                     | •0351       | .0191         | 42                | •0018       | •003           | 39          |
| 8                 | 11          | - 16             | 33               | 11           | 13              | 13                     | •0589       | ·0188         | 43                | .0022       | •003           | 34          |
| 4                 | 3           | 19               | 34               | 22           | 17              | 14                     | •0187       | ·0415         | 44                | •0022       | •002           | 25          |
| 5                 | 14          | 3                | 35               | 18           | 16              | 15                     | .0209       | ·0237         | 45                | •0032       | .00.           | 17          |
| 6                 | J 2         | 9                | 36               | 11           | 11              | 16                     | •0290       | ·0236         | <b>4</b> 6        | •0012       | •001           | 18          |
| 7                 | 19          | 6                | 37               | 19           | 5               | 17                     | •0226       | ·0280         | 47                | •0002       | •004           | 44          |
| 8                 | 4           | 19               | 38               | 11           | 6               | 18                     | •0322       | ·0147         |                   |             |                |             |
| 9                 | 12          | 3                | 39               | 12           | 23              | 19                     | ·0164       | ·0237         | 3rd E             | Equation.   | Longitud       | le.         |
| 10                | 16          | 6                | 40               | 15           | 6               | 20                     | •0351       | •0097         | 1                 | -0.0903     | - 0.083        | 39          |
| 11                | 13          | 7                | 41               | 7            | 16              | 21                     | •0098       | •0505         | 2                 | + .0856     | + .085         | 58          |
| 12                | 14          | 9                | 42               | 11           | 5               | 22                     | •0344       | •0072         | 8                 | 0859        | 078            | 85          |
| 18                | 24          | 9                | 43               | 11           | 7               | 23                     | •0155       | •0334         | 4                 | + .0787     | + .078         | 86          |
| 14                | 10          | 17               | 44               | 16           | 4               | 24                     | .0283       | .0122         | 5                 | •0786       | .078           | 85          |
| 15                | 11          | 9                | 45               | 21           | 5               | 25                     | .0181       | .0422         | 6                 | 0745        | 070            | 03          |
| 16                | · 13        | I 2              | 46               | 14           | 8               | 26                     | •0281       | •0157         | 7                 | •0759       | .070           | <b>0</b> 9` |
| 17                | 10          | 14               | 47               | 10           | 29              | 27                     | •0145       | .0122         | 8                 | + .0672     | + .008         | 83          |
| 18                | 18          | 6                | 48               | 6            | 14              | 28                     | ·0211       | •0202         | 9                 | •0674       | •06;           | 77          |
| 19                | 7           | 13               |                  |              |                 | 29                     | •0099       | •0131         | 10                | 0672        | — ·06          | 17          |
| 20                | 19          | 4                | 2nd I            | Equation.    | Latitude.       | 30                     | .0101       | •0229         | 11                | ·0668       | •••61          | 14          |
| 21                | 6           | 25               | 1                | +0.0302      | - 0.0290        | 81                     | •0089       | .0141         | 12                | + .0566     | + .000         | 02          |
| 22                | 19          | 4                | 2                | •0839        | + .0202         | 82                     | •0045       | •0291         | 13                | ·0551       | •059           | 99          |
| 23                | 10          | 17               | 8                | •0328        | — ·0588         | 33                     | •co98       | .0142         | 14                | 0577        | 05             | 18          |
| 24                | 16          | 10               | 4                | •0087        | ·0620           | 84                     | •0208       | •0182         | 15                | •0579       | •05            | 35          |
| 25                | 10          | 26               | 5                | •0446        | •0102           | 35                     | ·0148       | .0118         | 16                | + .0211     | + .05          | 39          |
| 26                | 20          | 9                | 6                | •0321        | ·0295           | 36                     | •0091       | 1800.         | 17                | .0515       | •05            | 43          |
| 27                | 11          | 9                | 7                | •0526        | •0207           | 37                     | ·0083       | ·0065         | 18                | 0524        | 04             | 80          |
| 28                | 15          | 14               | 8                | .0109        | ·0518           | <b>38</b> <sup>°</sup> | •0034       | ·0071         | 19                | + .0493     | + .050         | 02          |
| 29                | 9           | 8                | 9                | .0330        | ·0082           | <b>39</b>              | •0076       | .0105         | 20                | 0490        | 040            | 62          |
| <b>8</b> 0        | 8           | 17               | 10               | •0362        | •0198           | 40                     | •0090       | .0012         | 21                | •0474       | •04            | 36          |

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## The Jodhpore Meridional Series.

| Circuit<br>ngle | Coe     | Coefficients of y and z |       | and z     | Circuit<br>ngle | Coefficient | s of y and z  | Circuit<br>nglo | Coefficient | s of $y$ and $z$ | Circuit<br>ngle | Coefficient | s of y and z  |
|-----------------|---------|-------------------------|-------|-----------|-----------------|-------------|---------------|-----------------|-------------|------------------|-----------------|-------------|---------------|
| No. of<br>Tria  | b       | þ                       |       | ¢         | No. of<br>Tria  | ъ           | ¢             | No. of<br>Tria  | b           | c                | No. of<br>Tria  | b           | C             |
| 3rd             | Equat   | tion–                   | -(Coi | ntinued). | 3rd             | Equation–   | -(Continued). | 4th             | Equation–   | -(Continued).    | 4th             | Equation_   | -(Continued). |
| 22              | +0.0    | 0432                    | +     | 0.0436    | 41              | -0.0094     | - 0.0068      | 11              | -1.0311     | - 1.0285         | 30              | +1.0122     | + 1.0153      |
| 23              | 0       | 0452                    | -     | •0409     | 42              | •0098       | •0080         | 12              | +1.0263     | + 1.0281         | 81              | -1.0142     | - 1.0134      |
| 24              | + •     | 393                     | +     | •0415     | 43              | + .0081     | + .0020       | 13              | 1.0256      | 1.0281           | 82              | +1.0141     | + 1.0134      |
| 25              | ••      | <b>3</b> 98             |       | •0428     | 44              | 0071        | 0023          | 14              | -1.0320     | - 1.0242         | 83              | -1.0151     | - 1.0113      |
| 26              |         | <b>5391</b>             | _     | ·0352     | 45              | + .0026     | + .0043       | 15              | 1.0221      | 1.0251           | 34              | 1.0125      | 1.0111        |
| 27              | ••      | <b>3</b> 79             |       | •0352     | 46              | 0037        | 0029          | 16              | +1.0240     | + 1.0255         | 85              | +1.0086     | + 1.0092      |
| 28              | + .0    | 342                     | +     | ·0345     | 47              | + .0033     | + .0011       | 17              | 1.0242      | 1.0256           | 86              | 1.0001      | 1.0092        |
| 29              | - ·c    | 0340                    | -     | ·0316     |                 |             |               | 18              | -1.0547     | - 1.0226         | 37              | -1.0091     | - 1.0020      |
| 80              | + • • • | 319                     | +     | ·0318     | 4th 1           | Equation.   | Azimuth.      | 19              | +1.0333     | + 1.0232         | 38              | i•0084      | 1.0069        |
| 81              | — ·c    | o303                    | -     | •0280     | 1               | -1.0410     | - 1.0382      | <b>2</b> 0      | -1.0332     | - 1.0318         | <b>3</b> 9      | + 1 • 0057  | + 1.0071      |
| 32              | + .c    | 295                     | +     | ·0276     | 2               | +1.0386     | + 1.0390      | 21              | 1.0334      | 1.0205           | 40              | 1.0026      | 1.0063        |
| 83              | - ·c    | 250                     | -     | •0233     | 3               | -1.0393     | - 1.0357      | 22              | +1.0303     | + 1.0306         | 41              | -1.0046     | - 1.0033      |
| 34              | ٠c      | <b>52</b> 57            |       | •0230     | 4               | +1.0360     | + 1.0363      | 23              | -1.0314     | - 1.0193         | 42              | 1.0048      | 1.0039        |
| 85              | + •0    | 5185                    | +     | ·0198     | 5               | 1.0328      | 1.0360        | 24              | +1.0186     | + 1.0192         | 43              | + 1 • 0039  | + 1.0034      |
| 36              | ۰۰      | 5188                    |       | ·0194     | 6               | -1.0344     | - 1.0323      | 25              | 1.0182      | 1.0303           | 44              | -1.0032     | - 1.0026      |
| 87              | 0       | o186                    | _     | ·0142     | 7               | 1.0321      | 1.0326        | 26              | -1.0180     | - 1.0162         | 45              | +1.0032     | + 1.0031      |
| <b>3</b> 8      | •0      | 0171                    |       | ·0140     | 8               | + 1 • 0312  | + 1.0318      | 27              | 1.0180      | 1.0162           | <b>4</b> 6      | -1.0018     | - 1.0012      |
| 89              | + •0    | 0115                    | ÷     | ·0144     | 9               | 1.0311      | 1.0313        | <b>2</b> 8      | +1.0163     | + 1.0165         | 47              | +1.0012     | + 1.0006      |
| 40              | •0      | 0114                    |       | .01 27    | 10              | -1.0312     | - 1.0286      | 29              | -1.0195     | - 1.0120         | 48              | -1.0000     | - 1.0000      |

### NUMERICAL VALUES OF THE COEFFICIENTS.

### The Eastern Sind Meridional Series.

| Circuit<br>Igle   | Coefficient                                 | s of y and z | Circuit<br>Igle   | Coefficient | s of y and z | Circuit<br>Igle           | Coefficient | ts of y and z | Coefficiente              |         | s of $y$ and $z$ |  |
|-------------------|---------------------------------------------|--------------|-------------------|-------------|--------------|---------------------------|-------------|---------------|---------------------------|---------|------------------|--|
| No. of (<br>Trian | р                                           | C            | No. of (<br>Triar | ъ           | C C          | No. of (<br>Triar         | Ъ           | C             | No. of (<br>Triar         | Ъ       | C                |  |
| 1st               | Equation. Linear. 1st Equation—(Continued). |              |                   |             | 2nd          | 2nd Equation—(Continued). |             |               | 3rd Equation—(Continued). |         |                  |  |
| 1                 | + 12                                        | - 17         | 31                | + 17        | - 2          | 20                        | +0.0236     | - 0.0199      | 10                        | +0.0426 | + 0.0470         |  |
| 2                 | 9                                           | 10           | 82                | - I         | 17           | 21                        | ·0056       | ·0168         | 11                        | •0422   | ·0468            |  |
| 3                 | 15                                          | 6            | 83                | + 26        | + 5          | 22                        | .0111       | ·0138         | 12                        | - •0458 | 0389             |  |
| 4                 | 21                                          | 9            | 34                | 20          | - 2          | 23                        | •0082       | .0129         | 13                        | •0431   | •0359            |  |
| 5                 | 7                                           | I 2          | 85                | 12          | 20           | 24                        | ·0166       | •0099         | 14                        | + •0330 | + •0376          |  |
| 6                 | 13                                          | 14           | 36                | 14          | 7            | 25                        | •0104       | •0096         | 15                        | •0350   | •0401            |  |
| 7                 | 3                                           | 16           | 37                | 11          | 10           | 26                        | •0024       | .0183         | 16                        | 0379    | 0319             |  |
| 8                 | 18                                          | 3            | 38                | 2,1         | 19           | 27                        | •0059       | •0093         | 17                        | + .0349 | + .0311          |  |
| 9                 | 11                                          | 17           | 89                | 2           | 29           | 28                        | .0033       | •0088         | 18                        | 0321    | 0303             |  |
| 10                | 13                                          | 12           |                   |             |              | 29                        | .0003       | .0103         | 19                        | •0354   | ·0295            |  |
| 11                | 14                                          | 12           | 2nd 1             | Equation.   | Latitude.    | 80                        | •0074       | ·0041         | 20                        | + .0257 | + .0312          |  |
| 12                | 14                                          | 9            | 1                 | +0.0347     | - 0.0446     | 31                        | .0032       | .0030         | 21                        | 0295    | 0235             |  |
| 13                | 5                                           | 19           | 2                 | ·0178       | •0308        | 82                        | 0009        | •0066         | 22                        | + .0246 | + .0276          |  |
| 14                | 24                                          | I            | 8                 | •0332       | ·0206        | 33                        | + .0043     | .0010         | 23                        | 0267    | 0306             |  |
| 15                | 14                                          | 15           | 4                 | .0229       | ·0187        | 34                        | •0049       | •0006         | 24                        | + .0200 | + .0235          |  |
| 16                | 13                                          | 10           | 5                 | .0193       | ·0260        | <b>3</b> 5                | .0013       | •0049         | 25                        | 0338    | 0175             |  |
| 17                | - 2                                         | 27           | 6                 | •0245       | •0357        | <b>3</b> 6                | .0014       | .0018         | 26                        | + .0188 | + .0208          |  |
| 18                | + 15                                        | 2            | 7                 | •0074       | •0348        | 87                        | .0002       | .0018         | 27                        | 0187    | — ·0138          |  |
| 19                | 16                                          | 5            | 8                 | •0332       | •0104        | 88                        | •0005       | .0023         | 28                        | + .0142 | + .0122          |  |
| <b>2</b> 0        | 17                                          | 19           | 9                 | .0182       | •0396        |                           |             |               | 29                        | 0140    | 0098             |  |
| 21                | 10                                          | 10           | 10                | •0280       | •0195        | 3rd E                     | Equation.   | Longitude.    | <b>3</b> 0                | + .0114 | + .0111          |  |
| 22                | 8                                           | 15           | 11                | •0300       | •0196        | 1                         | +0.0633     | + 0.0626      | 81                        | 0104    | 0082             |  |
| 23                | 14                                          | 8            | 12                | .0194       | •0213        | 2                         | <u> </u>    | — ·0568       | 32                        | + •0085 | + .0029          |  |
| 24                | 16                                          | 13           | 13                | •0035       | •0390        | 8                         | •0641       | ·0580         | 33                        | 0093    | — ·0066          |  |
| 25                | 81                                          | 7            | 14                | .0413       | + .0012      | 4                         | + .0525     | + .0523       | 34                        | + •0059 | + .0060          |  |
| 26                | 1                                           | 25           | 15                | •0254       | 0205         | 5                         | •0546       | ·0577         | 35                        | — ·0052 | 0033             |  |
| 27                | 15                                          | 8            | 16                | .0141       | •0195        | 6                         | 0555        | 0487          | 36                        | + .0043 | + .0033          |  |
| 28                | 4                                           | 15           | 17                | - •0009     | •0374        | 7                         | + .0210     | + .0232       | 37                        | 0029    | - '0021          |  |
| 29                | 8                                           | 12           | 18                | + .0142     | •0078        | 8                         | 0529        | 0481          | 38                        | + .0026 | + .0008          |  |
| 80                | 16                                          | 8            | 19                | •0158       | .0118        | 9                         | •0513       | •0449         |                           |         |                  |  |

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| Circuit                | Coefficients of y and z |          | Circuit<br>1gle | Coefficient        | Coefficients of $y$ and $z$ |                | Coefficient                            | s of $y$ and $z$ | Circuit<br>ngle | Coefficients of $y$ and $z$ |               |
|------------------------|-------------------------|----------|-----------------|--------------------|-----------------------------|----------------|----------------------------------------|------------------|-----------------|-----------------------------|---------------|
| No. of<br>Tria         | ъ                       | ¢        | No. of<br>Tria  | ъ                  | C                           | No. of<br>Tria | ъ                                      | ¢                | No. of<br>Tria  | ъ                           | ¢             |
| 4th Equation. Azimuth. |                         |          | 4th .           | Equatio <b>n</b> – | -(Continued).               | 4th.           | 4th Equation—(Continued). 4th Equation |                  |                 |                             | -(Continued). |
| 1                      | +1.0279                 | + 1.0297 | 11              | +1.0191            | + 1.0214                    | 21             | -1.0132                                | - 1.0109         | 81              | -1.0020                     | - 1.0039      |
| 2                      | -1.0381                 | - 1.0256 | 12              | -1.0311            | - 1.0178                    | 22             | +1.0114                                | + 1.0128         | 32              | +1.0041                     | + 1.0038      |
| 8                      | 1.0289                  | 1.0261   | 13              | 1.0198             | 1.0164                      | 23             | -1.0124                                | - 1.0096         | <b>3</b> 3      | -1.0044                     | - 1.0031      |
| 4                      | +1.0232                 | + 1.0258 | 14              | +1.0125            | + 1.012                     | 24             | +1.0093                                | + 1.0109         | 34              | + 1 . 00 28                 | + 1.0028      |
| 5                      | 1.0248                  | 1.0263   | 15              | 1.0159             | 1.0184                      | 25             | -1.0102                                | - 1.0085         | 35              | -1.0022                     | - 1.0012      |
| 6                      | -1.0223                 | - 1.0330 | 16              | -1.0175            | - 1.0147                    | 26             | +1.0088                                | + 1.0098         | 36              | +1.0030                     | + 1.0019      |
| 7                      | +1.0236                 | + 1.0243 | 17              | +1.0190            | + 1.0173                    | 27             | -1.0088                                | - 1.0065         | 87              | -1.0014                     | - 1.0010      |
| 8                      | -1.0343                 | - 1.0319 | 18              | -1.0163            | - 1.0140                    | 28             | +1.0069                                | + 1.0073         | . 38            | +1.0013                     | + 1.0004      |
| 9                      | 1.0234                  | 1.0203   | 19              | 1.0164             | 1.0130                      | 29             | -1.0066                                | - 1.0046         | <b>3</b> 9      | -1.0000                     | - 1.0000      |
| 10                     | +1.0194                 | + 1.0215 | 20              | +1.0119            | + 1.0148                    | 30             | +1.0023                                | + 1.0023         |                 |                             |               |
|                        |                         |          |                 | 1                  |                             | 1              | 1                                      | 1                |                 |                             |               |

The Eastern Sind Meridional Series.

# 13.

### The Coefficients of the Indeterminate Factors in the Values of the Unknown Quantities.

On reference to the equations on page [12] it will be seen that the general expression for the error  $x_p$  of any angle  $X_p$  appertaining to a trigonometrical figure, is, when the weight is unity,

$$x_p = (a_p \lambda_a + b_p \lambda_b + \cdots + n_p \lambda_s)$$

so that the coefficients of  $\lambda_a, \lambda_b, \ldots, \lambda_n$ , the indeterminate factors, are the coefficients of  $x_p$  in the several absolute geometrical equations to which the indeterminate factors are respectively related. But one of the three unknown quantities appertaining to every triangle having been eliminated, as a preliminary to the simultaneous reduction of each





series, the coefficients of the Indeterminate Factors take a more complex form which is given on page [25]. The expressions are :—

$$y_p = {}_{1}\mathfrak{B}_{p} {}_{1}\Lambda + {}_{2}\mathfrak{B}_{p} {}_{2}\Lambda + \cdot \cdot \cdot + {}_{n}\mathfrak{B}_{p} {}_{n}\Lambda,$$
  
$$z_p = {}_{1}\mathfrak{O}_{p} {}_{1}\Lambda + {}_{2}\mathfrak{O}_{p} {}_{2}\Lambda + \cdot \cdot \cdot + {}_{n}\mathfrak{O}_{p} {}_{n}\Lambda,$$

where, see note to page [25],

$${}_{1}\mathfrak{B}_{p} = (2 {}_{1}\mathfrak{b}_{p} - {}_{1}\mathfrak{c}_{p}); \qquad {}_{2}\mathfrak{B}_{p} = (2 {}_{2}\mathfrak{b}_{p} - {}_{2}\mathfrak{c}_{p}); \qquad . \qquad .$$
$${}_{1}\mathfrak{C}_{p} = (2 {}_{1}\mathfrak{c}_{p} - {}_{1}\mathfrak{b}_{p}); \qquad {}_{2}\mathfrak{C}_{p} = (2 {}_{2}\mathfrak{c}_{p} - {}_{2}\mathfrak{b}_{p}); \qquad . \qquad .$$

the left-hand subscripts indicating the number of any one of the equations into which the errors y and z of any, the *p*th, triangle happen to enter.

The values of  $b_p$  and  $c_p$  for each equation into which the  $y_p$  and  $z_p$  enter, are given in the table in the preceding section.

### Examples.

### From the Jodhpore Meridional Series.

$${}_{2}\mathfrak{B}_{6} = (2 {}_{2}\mathfrak{b}_{6} - {}_{2}\mathfrak{b}_{6}) = (2 \times + 0.0351 + 0.0522) = + 0.0031$$
  
 ${}_{2}\mathfrak{G}_{6} = (2 {}_{2}\mathfrak{b}_{6} - {}_{2}\mathfrak{b}_{6}) = (5 \times - 0.0351 + 0.0351) = - 0.0011$ 

The following tables give the values of the significant coefficients  $\mathfrak{B}$  and  $\mathfrak{C}$  of the Indeterminate Factors  $_{1}\Lambda$ ,  $_{2}\Lambda$ , ... for the y and z of every triangle for each series.

| No. of Circuit<br>Triangle | 36   | Œ          | No. of Circuit<br>Triangle | 36        | Œ             | No. of Circuit<br>Triangle | 36        | Œ             | No. of Circuit<br>Triangle | 36                 | Œ             |
|----------------------------|------|------------|----------------------------|-----------|---------------|----------------------------|-----------|---------------|----------------------------|--------------------|---------------|
| 1st Equation. Linear.      |      |            | 1st 2                      | Equation— | -(Continued). | 1st ]                      | Equation— | -(Continued). | 1st ]                      | Equatio <b>n</b> — | -(Continued). |
| 1                          | + 22 | - 20       | 9                          | + 27      | - 18          | 17                         | + 34      | - 38          | 25                         | + 46               | - 62          |
| 2                          | 42   | 12         | 10                         | 38        | 28            | 18                         | 42        | 30            | 26                         | 49                 | 38            |
| 8                          | 38   | 43         | 11                         | 33        | 27            | 19                         | 27        | 33            | 27                         | 31                 | 29            |
| 4                          | 25   | <b>4</b> I | 12                         | 37        | 32            | 20                         | 42        | 27            | 28                         | 44                 | 43            |
| 5                          | 31   | 20         | 18                         | 57        | 42            | 21                         | 37        | 56            | 29                         | 26                 | 25            |
| 6                          | 33   | 30         | 14                         | 37        | 44            | 22                         | 43        | 27            | 80                         | 33                 | 42            |
| 7                          | 44   | 31         | 15                         | 31        | 29            | 28                         | 37        | 44            | 81                         | _ 28               | 29            |
| 8                          | 27   | 42         | 16                         | 38        | 37            | 24                         | 42        | 36            | 82                         | 33                 | 51            |

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## The Jodhpore Meridional Series.

| No. of Circuit<br>Triangle | 325       | Œ             | No. of Circuit<br>Triangle | 36        | Œ             | No. of Circuit<br>Triangle | 36        | C             | No. of Circuit<br>Triangle | 15         | ¢             |
|----------------------------|-----------|---------------|----------------------------|-----------|---------------|----------------------------|-----------|---------------|----------------------------|------------|---------------|
| 1st                        | Equation— | -(Continued). | 2nd                        | Equation– | -(Continued). | 2nd                        | Equation– | -(Continued). | 3rd.                       | Equation—  | -(Continued). |
| 33                         | + 35      | - 37          | 13                         | +0.1366   | – o·0965      | 43                         | +0.0028   | - 0.0090      | 24                         | +0.0321    | + 0.0437      |
| 34                         | 61        | 56            | 14                         | •0789     | .1012         | 44                         | •0069     | .0072         | 25                         | •0368      | •0458         |
| 85                         | 52        | 50            | 15                         | ·0655     | •0683         | 45                         | •0081     | •0066         | 26                         | 0430       | 0313          |
| 36                         | 33        | 33            | 16                         | ·0816     | ·0762         | 46                         | .0042     | •0048         | 27                         | •0406      | .0325         |
| 37                         | 43        | 29            | 17                         | •0732     | •0786         | 47                         | •0048     | •0090         | 28                         | + .0339    | + .0348       |
| 38                         | 28        | 23            | 18                         | ·0791     | •0616         |                            |           |               | 29                         | 0364       | 0292          |
| 39                         | 47        | 58            | 19                         | ·0565     | ·0638         | 3rd I                      | Equation. | Longitude.    | 30                         | + .0330    | + .0312       |
| 40                         | 36        | 27            | 20                         | •0799     | •0545         | 1                          | -0.0962   | - 0.0776      | 31                         | 0326       | 0257          |
| 41                         | 30        | 39            | 21                         | •0701     | •1108         | 2                          | + .0824   | + .0860       | 32                         | + .0314    | + .0257       |
| 42                         | 27        | 21            | 22                         | •0760     | •0488         | 3                          | 0933      | 0211          | 83                         | 0267       | 0319          |
| 43                         | 29        | 25            | 23                         | •0644     | •0823         | 4                          | + •0788   | + .0785       | 34                         | •0284      | .0203         |
| 44                         | 36        | - 24          | 24                         | •0721     | •0593         | 5                          | ·0787     | ·0784         | 35                         | + .0123    | + '0211       |
| 45                         | 47        | 31            | 25                         | •0789     | • 1035        | 6                          | 0787      | 0901          | 36                         | ·0182      | •0200         |
| 46                         | 36        | 30            | 26                         | .0719     | ·0595         | 7                          | •0809     | ·0659         | 87                         | 0230       | - ·0098       |
| 47                         | 49        | 68            | 27                         | •0447     | •0459         | 8                          | + .0667   | 1690. +       | 88                         | •0202      | .0109         |
| 48                         | 26        | 34            | 28                         | •0624     | ·0615         | 9                          | ·0671     | •0680         | 39                         | + •0086    | + .0173       |
|                            |           |               | 29                         | •0329     | •0361         | 10                         | 0737      | 0557          | 40                         | .0101      | ·0140         |
| 2nd 1                      | Equation. | Latitude.     | 30                         | •0431     | •0559         | 11                         | •0722     | •0560         | 41                         | 0130       | 0043          |
| 1                          | +0.0204   | - 0.0282      | 31                         | .0319     | .0321         | 12                         | + .0530   | + .0638       | 42                         | .0119      | ·0062         |
| 2                          | • 1473    | •0429         | 32                         | .0381     | ·0627         | 13                         | •0503     | •0647         | 43                         | + .0093    | + •0059       |
| 8                          | • 1 2 4 4 | • 1 504       | 33                         | •0338     | •0382         | 14                         | 0636      | 0459          | 44                         | 0089       | 0032          |
| 4                          | .0794     | .1327         | 34                         | •0598     | .0572         | 15                         | •0623     | •0491         | 45                         | + .0010    | + .0028       |
| 5                          | •0994     | •0650         | 35                         | .0414     | •0384         | 16                         | + .0483   | + .0567       | 46                         | 0045       | 0051          |
| 6                          | •0937     | .0011         | 36                         | .0263     | •0253         | 17                         | •0487     | .0221         | 47                         | + •0055    | .0011         |
| 7                          | • 1259    | ·0940         | 37                         | .0231     | .0213         | 18                         | 0568      | 0436          |                            |            |               |
| 8                          | •0736     | .1145         | 38                         | .0139     | •0176         | 19                         | + .0484   | + .0211       | 4th 1                      | Equation.  | Azimuth.      |
| 9                          | .0742     | •0494         | 39                         | •0254     | •0280         | 20                         | 0518      | 0434          | 1                          | -1.0438    | - 1.0354      |
| 10                         | •0922     | ·0758         | 40                         | •0197     | •0124         | 21                         | ·0512     | •0398         | 2                          | + 1 . 0382 | + 1.0394      |
| 11                         | •0795     | .0733         | 41                         | •0086     | .0100         | 22                         | + .0428   | + .0440       | 8                          | -1.0439    | - 1.0321      |
| 12                         | •0893     | •0733         | 42                         | .0075     | •0096         | 23                         | - •0495   | 0366          | 4                          | + 1 . 0357 | + 1.0366      |

### NUMERICAL VALUES OF THE 36 S AND CC S.

| No. of Circuit<br>Triangle | 36        | ¢             | No. of Circuit<br>Triangle | 36        | Œ             | No. of Circuit<br>Triangle | 36         | ¢             | No. of Circuit<br>Triangle | 36                                                                                                                                                                                                                                                                                     | E        |  |  |
|----------------------------|-----------|---------------|----------------------------|-----------|---------------|----------------------------|------------|---------------|----------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------|--|--|
| 4th                        | Equation— | -(Continued). | 4th                        | Equation— | -(Continued). | 4th                        | Equation—  | -(Continued). | 4th                        | $333$ $0$ $Equation$ —(Continued).           8 $-1 \cdot 0099$ $-1 \cdot 0054$ 9 $+1 \cdot 0043$ $+1 \cdot 0085$ 0 $1 \cdot 0050$ $1 \cdot 0068$ 1 $-1 \cdot 0059$ $-1 \cdot 0020$ 2 $1 \cdot 0057$ $1 \cdot 0030$ 3 $+1 \cdot 0044$ $+1 \cdot 0017$ 5 $+1 \cdot 0021$ $-1 \cdot 0012$ |          |  |  |
| 5                          | +1.0326   | + 1.0362      | 16                         | +1.02225  | + 1.0270      | 27                         | -1.0193    | - 1.0124      | 38                         | -1.0099                                                                                                                                                                                                                                                                                | - 1.0024 |  |  |
| 6                          | -1.0365   | - 1.0302      | 17                         | 1.0228    | 1.0270        | 28                         | +1.0191    | + 1.0167      | 39                         | +1.0043                                                                                                                                                                                                                                                                                | + 1.0085 |  |  |
| 7                          | 1.0376    | 1.0301        | 18                         | -1.0368   | - 1.0205      | 29                         | -1.0124    | - 1.0138      | 40                         | 1.0020                                                                                                                                                                                                                                                                                 | 1.0068   |  |  |
| 8                          | +1.0306   | + 1.0324      | 19                         | +1.0227   | + 1.0242      | 30                         | + 1 · 0151 | + 1.0154      | 41                         | -1.0029                                                                                                                                                                                                                                                                                | - 1.0030 |  |  |
| 9                          | 1.0309    | 1.0315        | 20                         | -1.0246   | - 1.0204      | 31                         | -1.0126    | - 1.0123      | 42                         | 1.0022                                                                                                                                                                                                                                                                                 | 1.0030   |  |  |
| 10                         | -1.0344   | - 1.0257      | 21                         | 1.0243    | 1.0180        | 32                         | +1.0148    | + 1.0127      | 43                         | +1.0044                                                                                                                                                                                                                                                                                | + 1.0039 |  |  |
| 11                         | 1.0332    | 1.0259        | 22                         | +1.0300   | + 1.0209      | 33                         | -1.0130    | - 1.0103      | 44                         | -1.0044                                                                                                                                                                                                                                                                                | - 1.0012 |  |  |
| 12                         | +1.0245   | + 1.0299      | 23                         | -1.0235   | - 1.0172      | 34                         | 1.0139     | 1.0032        | 45                         | +1.0033                                                                                                                                                                                                                                                                                | + 1.0012 |  |  |
| 13                         | 1.0231    | 1.0306        | 24                         | +1.0122   | + 1.0208      | 35                         | +1.0081    | + 1.0105      | 46                         | -1.0051                                                                                                                                                                                                                                                                                | - 1.0015 |  |  |
| 14                         | -1.0298   | - 1.0314      | 25                         | 1.0121    | 1.0219        | 36                         | 1.0082     | 1.0099        | 47                         | + 1 . 0028                                                                                                                                                                                                                                                                             | + 0.9995 |  |  |
| 15                         | 1.0291    | 1.0331        | 26                         | -1.0302   | - 1.0148      | 37                         | -1.0113    | - 1.0049      | 48                         |                                                                                                                                                                                                                                                                                        | - 1.0000 |  |  |

### The Jodhpore Meridional Series.

The Eastern Sind Meridional Series.

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| No. of Oircuit<br>Triangle | 36   | Œ    | No. of Circuit<br>Triangle | 36        | Œ             | No. of Circuit<br>Triangle | 36        | U             | No. of Circuit<br>Triangle | 36        | ¢             |
|----------------------------|------|------|----------------------------|-----------|---------------|----------------------------|-----------|---------------|----------------------------|-----------|---------------|
| 1st Equation. Linear.      |      |      | 1st .                      | Equation— | -(Continued). | 18t .                      | Equation— | -(Continued). | 1st .                      | Equation— | -(Continued). |
| 1                          | + 41 | - 46 | 11                         | + 40      | - 38          | 21                         | + 30      | - 30          | 31                         | + 36      | - 21          |
| 2                          | 28   | 29   | 12                         | 37        | 32            | 22                         | 31        | 38            | 32                         | 15        | 33            |
| 8                          | 36   | 27   | 13                         | 29        | 43            | 23                         | 36        | 30            | 33                         | 47        | 16            |
| 4                          | 51   | 39   | 14                         | 49        | 26            | 24                         | 45        | 42            | 34                         | 42        | 24            |
| 5                          | 26   | 31   | 15                         | 43        | 44            | 25                         | 43        | 32            | 35                         | 44        | 52            |
| 6                          | 40   | 41   | 16                         | 36        | 33            | 26                         | 27        | 51            | 36                         | 35        | 28            |
| 7                          | 22   | 35   | 17                         | 23        | 52            | 27                         | 38        | 31            | 37                         | 32        | 31            |
| 8                          | 39   | 24   | 18                         | 32        | 19            | 28                         | 23        | 34            | 38                         | 61        | 59            |
| 9                          | 39   | 45   | 19                         | 37        | 26            | 29                         | 28        | 32            | 89                         | 33        | 60            |
| 10                         | 38   | 37   | 20                         | 53        | <b>5</b> 5    | 30                         | 40        | 32            |                            |           |               |

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# The Eastern Sind Meridional Series.

| No. of Circuit<br>Triangle | 325                                               | œ        | No. of Circuit<br>Triangle | 325                                     | ¢                         | No. of Circuit<br>Triangle | 36         | Œ                         | No. of Circuit<br>Triangle | 36      | Œ        |
|----------------------------|---------------------------------------------------|----------|----------------------------|-----------------------------------------|---------------------------|----------------------------|------------|---------------------------|----------------------------|---------|----------|
| 2nd 1                      | 2nd Equation. Latitude. 2nd Equation—(Continued). |          |                            |                                         | 3rd Equation—(Continued). |                            |            | 4th Equation—(Continued). |                            |         |          |
| 1                          | +0.1140                                           | - 0.1239 | 31                         | +0.0104                                 | - 0.0092                  | 21                         | -0.0325    | - 0.0175                  | 11                         | +1.0198 | + 1.0237 |
| 2                          | ·0664                                             | •0794    | 32                         | •0048                                   | •0123                     | 22                         | + .0216    | + .0306                   | 12                         | -1.0544 | - 1.0145 |
| 8                          | •0870                                             | •0744    | 83                         | •0094                                   | •0062                     | 23                         | 0328       | 0145                      | 18                         | 1.0233  | 1.0130   |
| 4                          | •1245                                             | •0903    | 84                         | •0104                                   | •0061                     | 24                         | + ·0168    | + .0264                   | 14                         | +1.0135 | + 1.0192 |
| 5                          | •0646                                             | •0713    | 85                         | .0073                                   | .0110                     | 25                         | 0381       | 0133                      | 15                         | 1.0134  | 1.0209   |
| 6                          | •0847                                             | ••0959   | 36                         | ·0046                                   | •0050                     | 26                         | + •0168    | + .0228                   | 16                         | -1.0303 | - 1.0119 |
| 7                          | •0496                                             | •0770    | 87                         | •0028                                   | •0041                     | 27                         | 0236       | 0089                      | 17                         | +1.0142 | + 1.0189 |
| 8                          | •0768                                             | •0540    | 38                         | • • • • • • • • • • • • • • • • • • • • | •0051                     | 28                         | + .0139    | + .0163                   | 18                         | -1.0180 | - 1.0112 |
| 9                          | •0770                                             | •0979    |                            |                                         |                           | 29                         | 0183       | — ·0056                   | 19                         | 1.0193  | 1.0108   |
| 10                         | •0755                                             | •0670    | 3rd E                      | Equation.                               | Longitude.                | 80                         | + .0112    | 4 ·0108                   | 20                         | +1.0090 | + 1.0177 |
| 11                         | •0796                                             | •0692    | 1                          | +0.0288                                 | + 0.0690                  | 81                         | — ·0126    | - ·0060                   | 21                         | -1.0165 | - 1.0081 |
| 12                         | •0601                                             | •0620    | 2                          | - •0678                                 | 0213                      | 82                         | + •0091    | + •0073                   | 22                         | +1.0100 | + 1.0142 |
| 13                         | •0460                                             | ·0815    | 8                          | •0702                                   | •0519                     | 83                         | 0130       | 0039                      | 23                         | -1.0122 | - 1.0068 |
| 14                         | •0809                                             | •0379    | 4                          | + .0478                                 | + .0019                   | 34                         | + •0058    | + .0001                   | 24                         | +1.0022 | + 1.0125 |
| 15                         | .0213                                             | ·0664    | 5                          | •0515                                   | •0608                     | 85                         | 0011       | 0014                      | 25                         | -1.0132 | - 1.0027 |
| 16                         | •0477                                             | •0531    | 6                          | — ·c623                                 | 0419                      | 86                         | + •0052    | + .0033                   | 26                         | +1.0028 | + 1.0108 |
| 17                         | •0356                                             | •0739    | 7                          | + .0206                                 | + .0545                   | 87                         | 0031       | 0013                      | 27                         | -1.0111 | - 1.0043 |
| 18                         | •0368                                             | •0301    | 8                          | 0577                                    | 0433                      | 88                         | + •0044    | .0010                     | 28                         | +1.0062 | + 1.0077 |
| 19                         | •0434                                             | •0394    | 9                          | ·0577                                   | ·0385                     |                            |            |                           | 29                         | -1.0086 | - 1.0026 |
| 20                         | ·0671                                             | •0634    | 10                         | + .0382                                 | + .0214                   | 4th 1                      | Equation.  | Azimuth.                  | 80                         | +1.0023 | + 1.0023 |
| 21                         | •0280                                             | •0392    | 11                         | •0376                                   | .0214                     | 1                          | +1.0301    | + 1.0315                  | 81                         | -1.0001 | - 1.0028 |
| 22                         | •0360                                             | •0387    | 12                         | 0527                                    | 0320                      | 2                          | -1.0306    | - 1.0231                  | 82                         | +1.0044 | + 1.0035 |
| 23                         | •0293                                             | •0340    | 13                         | •0503                                   | •0287                     | 8                          | 1.0312     | 1.0333                    | 83                         | -1.0022 | - 1.0018 |
| 24                         | •0431                                             | •0364    | 14                         | + .0284                                 | + .0422                   | 4                          | +1.0313    | + 1.0381                  | 84                         | +1.0038 | + 1.0038 |
| 25                         | •0304                                             | •0296    | 15                         | •0299                                   | •0452                     | 5                          | 1.0333     | 1.0278                    | 85                         | -1.0032 | - 1.0005 |
| 26                         | ·0231                                             | •0390    | 16                         | 0439                                    | 0259                      | 6                          | -1.0286    | - 1.0182                  | <b>36</b>                  | +1.0054 | + 1.0013 |
| 27                         | .0311                                             | •0245    | 17                         | + .0321                                 | + •0405                   | 7                          | +1.0339    | + 1.0250                  | 87                         | -1.0018 | - 1.0006 |
| 28                         | °0152                                             | •0208    | 18                         | 0399                                    | 0255                      | 8                          | -1.0265    | - 1.0196                  | 88                         | +1.0030 | + 0.9996 |
| 29                         | .0106                                             | •0206    | 19                         | •0413                                   | ·0236                     | 9                          | 1.0265     | 1.0172                    | <b>3</b> 9                 | -1.0000 | - 1.0000 |
| 30                         | .0189                                             | •0156    | 20                         | + .0192                                 | + .0311                   | 10                         | + 1 • 0173 | + 1.0236                  |                            |         |          |

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# The Equations between the Indeterminate Factors, and their Solution.

In the equations between the Indeterminate Factors, the coefficients of the factors are summations of terms of the form  $(\mathfrak{b}\mathfrak{B} + \mathfrak{c}\mathfrak{C})$ , such as are exhibited in the equations on page [25].

In the equations appertaining to the Eastern Sind Meridional Series Equalizing Factors were employed, see page [24]; these factors were not applied directly to the **b**s and **c**s, as such a proceeding was unnecessary, but they were introduced at once into the coefficients themselves.

The manner in which this has been done will appear if the geometrical equations of condition on page [12] are multiplied in succession by the equalizing factors  $f_a$ ,  $f_b$ ,  $f_c$ , &c., and  $\lambda'_a$ ,  $\lambda'_b$ ,  $\lambda'_c$  are put for the corresponding Indeterminate Factors. The equations between the latter will then be

From this it appears that after the solution of the equations appertaining to the Eastern Sind Meridional Series, the resulting values of the Indeterminate Factors had to be multiplied by the corresponding equalizing factors before they could be employed in the formulæ on page [25] for obtaining the values of the errors y and z.

The coefficients of the Indeterminate Factors, and the Absolute Terms, in each of the 4 equations which were presented for simultaneous solution by either series are here given in a tabular form.

The tables following the groups of equations between the Indeterminate Factors, give the first of each group of equations between certain of the indeterminate factors which remained after the other factors had been eliminated. These are the equations which were used in obtaining the numerical values of the factors by successive substitutions backwards from the last to the first.

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## INTRODUCTORY.

# The Jodhpore Meridional Series.

| No. 1    | THE INI   |            |                |           |         |
|----------|-----------|------------|----------------|-----------|---------|
| Equation | ıΛ        | <b>2</b> Λ | <sub>3</sub> Л | 4Λ        | TERMS   |
| 1        | + 46834.0 | + 72.2865  | - 4°8070       | - 59.4742 | - 123.4 |
| 2        | + 72.2865 | + 0.1253   | + 0.0012       | + 0.1318  | - 0.12  |
| 3        | - 4.8070  | + 0.0012   | + 0.2159       | + 3.9612  | - 0.131 |
| 4        | - 59.4742 | + 0.1318   | + 3.9612       | + 99.6618 | - 3.310 |

The Equations between the Indeterminate Factors expressed in Natural Numbers.

| The ] | Eauations | between | the | Indeter | minate | Factors | after | the | Successive | Elimino | rtions |
|-------|-----------|---------|-----|---------|--------|---------|-------|-----|------------|---------|--------|
|-------|-----------|---------|-----|---------|--------|---------|-------|-----|------------|---------|--------|

| No. of<br>Equation | THE IN    | Тир Авеотлите  |          |                |          |
|--------------------|-----------|----------------|----------|----------------|----------|
|                    | Λι        | <sub>2</sub> Λ | 3        | 4 <sup>Λ</sup> | TERMS    |
| 1                  | + 46834.0 | + 72.2865      | - 4.8070 | - 59.4742      | - 123.4  |
| 2                  |           | + 0.0431       | + 0.0089 | + 0.2230       | + 0.0182 |
| 3                  |           |                | + 0.2136 | + 3.9096       | - 0.1375 |
| 4                  |           |                |          | + 26.8833      | - 0*9507 |

## The Eastern Sind Meridional Series.

The Equations between the Indeterminate Factors expressed in Natural Numbers, before the application of the Equalizing Factors.

| No. of<br>Equation | THE INI                                         | THE ABSOLUTE                                      |                                                   |                                                                 |                                         |
|--------------------|-------------------------------------------------|---------------------------------------------------|---------------------------------------------------|-----------------------------------------------------------------|-----------------------------------------|
|                    | ıΛ                                              | 2 <b>7</b>                                        | 4 <sup>4</sup>                                    | TERMS                                                           |                                         |
| 1<br>2<br>3<br>4   | + 38716.<br>+ 45.3001<br>- 8.7746<br>- 109.1557 | + 45°3001<br>+ 0°08076<br>- 0°005415<br>+ 0°07154 | - 8.7746<br>- 0.005415<br>+ 0.09630<br>+ 2.331265 | - 109 · 1557<br>+ 0 · 07 154<br>+ 2 · 33 1 265<br>+ 80 · 1 1747 | - 74·2<br>- 0·423<br>+ 0·028<br>+ 0·939 |

| No. of<br>Equation | THE IND   | Тик Авсолите |           |                |         |
|--------------------|-----------|--------------|-----------|----------------|---------|
|                    | ıΛ        | ₂Λ           | 3Д        | 4 <sup>A</sup> | TERMS   |
| I                  | + 387.16  | + 45:3001    | - 8.7746  | - 10.9156      | - 7.42  |
| 2                  | + 45.3001 | + 8.076      | - 0.2412  | + 0.7154       | - 4.3   |
| 3                  | - 8.7746  | - 0.2412     | + 9.630   | + 23.3127      | + 0.38  |
| 4                  | - 10.9156 | + 0.7154     | + 23.3127 | + 80.1175      | + 0.939 |

The Equations between the Indeterminate Factors expressed in Natural Numbers, after the application of the Equalizing Factors.

| The | Equations | between | the | Indeterminate | Factors afte | r the | Successive | Eliminations. |
|-----|-----------|---------|-----|---------------|--------------|-------|------------|---------------|
|-----|-----------|---------|-----|---------------|--------------|-------|------------|---------------|

| No. of<br>Equation | THE IND  | THE ABOLITE |          |                |          |  |  |  |
|--------------------|----------|-------------|----------|----------------|----------|--|--|--|
|                    | γ        | 27          | 3        | 4 <sup>A</sup> | TERMS    |  |  |  |
| I                  | + 387.16 | + 45°3001   | - 8.7746 | - 10.9156      | - 7.42   |  |  |  |
| 2                  |          | + 2.7756    | + 0.4852 | + 1.9926       | - 3.3618 |  |  |  |
| 3                  |          |             | + 9.3463 | + 22.7170      | + 0.6992 |  |  |  |
| 4                  |          |             |          | + 23.1632      | + 1.4430 |  |  |  |

The following table gives the values of the factors to 4 places of decimals as deduced from the solution of the equations.

| The       | Jodhp          | ore ] | Meridional | l Series | 3.       |
|-----------|----------------|-------|------------|----------|----------|
| Numerical | <b>V</b> alues | of t  | he Indeter | minate   | Factors. |

| Factor         | Numerical Value |
|----------------|-----------------|
| ıΛ             | - 0.0036        |
| ₂^             | + 0.6041        |
| <sub>з</sub> Л | + 0.0042        |
| <b>4</b> Λ     | - 0.0354        |

#### INTRODUCTORY.

## The Eastern Sind Meridional Series.

Numerical Values of the Indeterminate Factors.

| Factor         | Numerical Value | Numericsl Value<br>× Equalizing<br>Factors |
|----------------|-----------------|--------------------------------------------|
| ıΛ             | + 0.1323        | + 0.0126                                   |
| <b>2</b> Λ     | — 1·2425        | - 12.425                                   |
| <sub>3</sub> Л | <u> </u>        | — 0·766                                    |
| <b>4</b> Λ     | + 0.0623        | + 0.0623                                   |

# 15.

# The Angular Errors x, y and z.

The following table gives the values of the errors of the angles of every circuit triangle, the errors y and z having first been deduced for any, the pth, triangle by the formulæ,

 $y_{p} = {}_{1}\mathfrak{B}_{p} {}_{1}\Lambda + {}_{2}\mathfrak{B}_{p} {}_{2}\Lambda + \ldots$  $z_{p} = {}_{1}\mathfrak{C}_{p} {}_{1}\Lambda + {}_{2}\mathfrak{C}_{p} {}_{2}\Lambda + \ldots$ 

the error  $x_p$  was simply determined by finding the value of its equivalent,  $-(y_p + z_p)$ .

The Jodhpore Meridional Series.

| No. of<br>Triangle | x      | y              | z      | No. of<br>Triangle | x      | y             | z       | No. of<br>Triangle | x       | y        | z      | No. of<br>Triangle | x      | y      | z       |
|--------------------|--------|----------------|--------|--------------------|--------|---------------|---------|--------------------|---------|----------|--------|--------------------|--------|--------|---------|
|                    |        |                |        |                    | "      | "             | "       |                    | "       | "        |        |                    | N      |        |         |
| 1                  | -0.061 | 0.000          | +0.001 | 13                 | +0.103 | -0.129        | +0.022  | 25                 | +0.039  | -0.124   | +0.125 | 87                 | -0.031 | -0.100 | +0.122  |
| 2                  | + .118 | 099            | 019    | 14                 | 084    | <b>-</b> ∙050 | + 134   | 26                 | 039     | 098      | + 137  | 38                 | 021    | 057    | + .108  |
| 8                  | 075    | 026            | + •10) | 15                 | - ·063 | 036           | + .099  | 27                 | - `•064 | 049      | + •113 | 39                 | + .033 | – ·190 | + •157  |
| 4                  | + •047 | 079            | + .032 | 16                 | + .073 | - •124        | + .021  | · <b>28</b>        | + .075  | - •157   | + .082 | 40                 | + .099 | - •154 | + .052  |
| 5                  | + .093 | — ·088         | 004    | 17                 | + .001 | <b>-</b> •115 | + .024  | 29                 | — ·066  | 038      | + •104 | 41                 | 999    | - •068 | + •167  |
| 6                  | 064    | 026            | + .090 | 18                 | 039    | - •068        | + 107   | 30                 | + •047  | - •129   | + .085 | 42                 | 049    | 057    | + •106  |
| 7                  | 045    | 046            | + .001 | 19                 | + .024 | 099           | + .042  | 31                 | 072     | 046      | + •118 | 43                 | + .082 | 136    | + .049  |
| 8                  | + •043 | - •089         | + •046 | 20                 | 034    | 067           | + .101  | 82                 | + .021  | <u> </u> | + •111 | 44                 | 028    | 090    | + •118  |
| 9                  | + .090 | - •089         | 001    | 21                 | - •116 | 055           | + • 171 | 33                 | 076     | 020      | + •146 | 45                 | + .132 | 300    | + .073  |
| 10                 | - •046 | 045            | + •091 | 22                 | + .110 | - 142         | + .033  | 34                 | 055     | - ·148   | + .203 | 46                 | 049    | 092    | + •141  |
| 11                 | 054    | 032            | + •089 | 23                 | — ·086 | 059           | + •145  | 35                 | + .076  | - •198   | + .122 | 47                 | + .002 | 210    | + • 205 |
| 12                 | + .081 | <b>- •1</b> 16 | + .032 | 24                 | + .086 | - •144        | + .028  | <b>36</b> .        | + .021  | - •139   | + •068 | 48                 | 099    | 059    | + •158  |

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### ARBITRARY CORRECTIONS.

### The Eastern Sind Meridional Series.

The Angular Errors.

| No. of<br>Triangle | x       | y       | z        | No. of<br>Triangle | x      | y      | z      | No. of<br>Triangle | x      | y      | z      | No. of<br>Triangle | x       | y      | z      |
|--------------------|---------|---------|----------|--------------------|--------|--------|--------|--------------------|--------|--------|--------|--------------------|---------|--------|--------|
|                    | W       | v       | "        |                    | "      | "      | "      |                    | N      | "      | "      |                    |         | N      | "      |
| 1                  | -0.000  | -0.880  | +0.920   | 11                 | +0.042 | -0.420 | +0.402 | 21                 | -0.024 | -0.002 | +0.029 | 81                 | -0.069  | +0.323 | -0.303 |
| 2                  | - 112   | 484     | + •596   | 12                 | 025    | 303    | + •328 | 22                 | 031    | 010    | + •041 | 82                 | + .022  | + •185 | - •207 |
| 3                  | + .077  | 637     | + •560   | 13                 | - •198 | 331    | + •429 | 23                 | 044    | + .023 | - •008 | 33                 | - •239  | + •423 | - ·184 |
| 4                  | + •230  | — ·876  | + •646   | 14                 | + •171 | - •345 | + •174 | 24                 | 047    | + .082 | 032    | 34                 | - •289  | + •459 | - •170 |
| 5                  | 062     | - •450  | + • 51 2 | 15                 | + .004 | 303    | + •299 | 25                 | 033    | + •123 | 090    | 35                 | + •173  | + :408 | - •581 |
| 6                  | 079     | — ·564  | + .643   | 16                 | 032    | - 168  | + •200 | 26                 | + .010 | + •104 | - 114  | 36                 | - • 212 | + •443 | - •231 |
| 7                  | - • 223 | - • 314 | + •537   | 17                 | 181    | 113    | + •294 | 27                 | 030    | + 173  | - 143  | 37                 | + .093  | + .310 | 402    |
| 8                  | + •144  | - •482  | + •338   | 18                 | 005    | - •086 | + .001 | 28                 | 034    | + 154  | - 120  | 38                 | - 170   | + •788 | - ·618 |
| 9                  | - •130  | - •484  | + .614   | 19                 | 013    | - •104 | + •116 | 29                 | + .033 | + 173  | - •206 | 89                 | + •466  | + .354 | 820    |
| 10                 | + .034  | 424     | + .390   | 20                 | 011    | - •117 | + 128  | 30                 | - ·168 | + •324 | - 156  |                    |         |        |        |

# **16**.

# Arbitrary Corrections.

The values of the angular errors were first obtained to 4 places of decimals and then reduced to 3 places by rejecting the 4th and increasing the 3rd place if the 4th was not less than 5. This introduced certain closing errors in the Eastern Sind Meridional Series only, to eliminate which small arbitrary corrections had to be made: these are shewn in the following table:—

| THE EASTERN SIND MERIDIONAL<br>Series |            |                    |            |  |  |  |  |  |  |  |
|---------------------------------------|------------|--------------------|------------|--|--|--|--|--|--|--|
| 1                                     | y          | Z                  |            |  |  |  |  |  |  |  |
| No. of<br>Triangle                    | Correction | No. of<br>Triangle | Correction |  |  |  |  |  |  |  |
|                                       | "          |                    | "          |  |  |  |  |  |  |  |
| 37                                    | -0.001     | 9                  | +0.001     |  |  |  |  |  |  |  |
|                                       |            | 25                 | .001       |  |  |  |  |  |  |  |
|                                       |            | 31                 | .001       |  |  |  |  |  |  |  |
|                                       |            | 34                 | .001       |  |  |  |  |  |  |  |

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## The Final Results of the Simultaneous Reduction of each Series.

The errors recorded in Section 15 were severally applied with changed signs to the values of the figurally corrected angles which are given in Section 8, and corresponding corrections were obtained to the logarithmic lengths of the sides of the circuit triangles in that section. The corrections to the sides and angles were then introduced into the several geodetic calculations from which the values of latitude, longitude and azimuth for the stations on the line of the traverse had been obtained, as given in Section 9.

After all the corrections had been applied the residual differences were as follows :---

### The Jodhpore Meridional Series.

# At Kanda.

| Latitude North                     | ••• | + 0.0 | 01 |
|------------------------------------|-----|-------|----|
| Longitude East of Greenwich        | ••• | + .0  | 01 |
| Azimuth of Kaimsir                 | ••• | + .0  | 01 |
| Distance in the 7th place of logs. | ••• | + .3  |    |

### The Eastern Sind Meridional Series.

## At Dáowála.

N

| Latitude North                     | ••• | + | 0.005 |
|------------------------------------|-----|---|-------|
| Longitude East of Greenwich        | ••• | _ | .003  |
| Azimuth of Máchka                  | ••• |   | •003  |
| Distance in the 7th place of logs. | ••• | _ | • 2   |



## CHAPTER IV.

### THE NON-CIRCUIT TRIANGLES AND THEIR FINAL FIGURAL ADJUSTMENTS.

Only a single chain of triangles having been selected for the Final Reduction of the Jodhpore and Eastern Sind Meridional Series, it followed that when each reduction was completed, the remaining or *Non*-circuit triangles had to be brought into accord with the reduced or Circuit triangles, all the elements of the latter being maintained unaltered. The only conditions thus required to be satisfied were the following :--

- 1. That at any station falling within the circuit at which angles had been measured completely round the horizon, the sum of the Non-circuit angles + the sum of the Circuit angles should be equal to 360°.
- 2. That the ratios of sides common both to Circuit and Non-circuit triangles, must be the same by the latter as by the former.
- 3. That the algebraical sum of the corrections to the angles of each Non-circuit triangle should = 0.

In certain cases it happened that a *Non*-circuit triangle had two sides and the included angle already determined by the Circuit triangles, and the unknown quantities were the errors of the other two angles. Conditions 2 and 3 furnished two equations for determining these two unknown quantities, and the equations were solved as ordinary algebraical simultaneous equations.

In the pages of tabular matter which follow, are given, separately for each Series, the data of the *Non*-circuit triangles similar to those of the Circuit triangles shewn on pages [33] to [36], and in the same terms with them; these are followed by the "Final Figural Adjustments" of the groups. In connection with the sides and angles are shewn first the Figure to which each *Non*-circuit triangle belongs, secondly, the number of the triangle, and thirdly the Figural numbers of the angles employed in the Preliminary Reductions and again made use of here, as shewn on the Plates at the end of the numerical details of each Series. In the column giving the number of the station, the numerals corresponding to those stations of which the positions stand fixed by the Final Reduction are printed in Roman type, the rest in Italic type.

In the abstracts of the final adjustments, each group of triangles is designated by the figure to which it appertains and by the numbers of triangles it includes. The constants furnished by the Final Reduction are given, with a reference to the page from which they are taken; these are followed by the equations of condition which have to be satisfied. Lastly are shewn the *adopted* angular errors. They are so designated because they differ occasionally, but only in the last place of decimals, from those which actually resulted from the calculations; slight arbitrary corrections having been applied in order to make the logarithmic values of common sides agree where the number of places of decimals employed in the calculations had not sufficed to do so.

# INTRODUCTORY.

The Jodhpore Meridional Series. Sides and Angles of the Non-Circuit Triangles.

|                  |                    | 6                    |                               |                                                    |                              |                                                 |                  | _                  | <b>—</b> —           |                                 |                                                       | _                         |                                                 |
|------------------|--------------------|----------------------|-------------------------------|----------------------------------------------------|------------------------------|-------------------------------------------------|------------------|--------------------|----------------------|---------------------------------|-------------------------------------------------------|---------------------------|-------------------------------------------------|
| Number of Figure | Number of Triangle | Figural No. of Angle | Number of<br>Station          | Corrected<br>Plane Angle                           | Spherical Excess             | Logarithm<br>of Side-length<br>in Feet          | Number of Figure | Number of Triangle | Figural No. of Angle | Number of<br>Station            | Corrected<br>Plane Angle                              | Spherical Excess          | Logarithm<br>of Side-length<br>in Feet          |
| 1                | 49                 | 2+3<br>4<br>1        | XLI<br>XLIV<br>II             | 80 59 54 001<br>30 27 7 283<br>68 32 58 716        | "<br>1`368<br>1`367<br>1`367 | 5°2799380,6<br>4°9901710,8<br>5°2541461,0       | 9                | 63                 | 12<br>10<br>11       | XXXIII<br>XXXII<br>XXXIV        | 0 , "<br>40 46 35 977<br>94 26 45 334<br>44 46 38 689 | *<br>*176<br>*177<br>*176 | 4 · 6592209,2<br>4 · 8429244,1<br>4 · 6920244,3 |
| 2                | 50                 | 18<br>16<br>17       | I<br>III<br>IV                | 52 40 50 026<br>82 22 27 324<br>44 56 42 650       | 1.663<br>1.663<br>1.662      | 5 · 1895968,2<br>5 · 2852253,8<br>5 · 1381524,5 | 10               | 64                 | 5<br>4<br>6          | XXXV<br>XXXVI<br><i>XXXVIII</i> | 73 44 28 461<br>49 28 9 347<br>56 47 22 192           | ·286<br>·285<br>·285      | 4 · 8688079,7<br>4 · 7673799,7<br>4 · 8090846,2 |
| <b>3</b> 7       | 51                 | 15<br>18<br>14       | IV<br>III<br>VI               | 46 5 17 394<br>71 15 46 349<br>62 38 56 257        | 1°450<br>1°451<br>1°450      | 5°0986603,9<br>5°2174330,0<br>5°1895968,2       | "                | 65                 | 8<br>7<br>9          | XXXVIII<br>XXXVI<br>XL          | 62 5 32 · 652<br>47 20 17 · 51 1<br>70 34 9 · 837     | ·297<br>·297<br>·297      | 4 · 8405821,0<br>4 · 7607793,5<br>4 · 8688079,7 |
| 3                | 52                 | 18<br>16<br>17       | VI<br>VIII<br>LX              | 47 51 11 · 303<br>72 36 55 · 187<br>59 31 53 · 510 | .952<br>.953<br>.953         | 5·0185048,0<br>5·1281303,5<br>5·0838972,8       | "                | 66                 | 10<br>11<br>12       | XXXVI<br><i>XL</i><br>XXXIX     | 89 43 56 808<br>53 39 2 723<br>36 37 0 469            | .211<br>.211<br>.210      | 5.0649959,4<br>4.9710226,0<br>4.8405821,0       |
| "                | 53                 | 15<br>18<br>14       | IX<br>VIII<br>XI              | 57 46 11 572<br>65 7 38 556<br>57 6 9 872          | •785<br>•785<br>•784         | 5°0217343,1<br>5°0521333,3<br>5°0185048,0       | ,,               | 67                 | 33<br>31<br>32       | XL<br>XXXIX<br>XLII             | 51 44 39 °077<br>49 1 11 °968<br>79 14 8 °955         | .642<br>.641<br>.642      | 4 · 9677159,9<br>4 · 9506173,0<br>5 · 0649959,4 |
| 4                | 54                 | 18<br>16<br>17       | XI<br>XIII<br>XIV             | 53 27 43 865<br>48 51 26 240<br>77 40 49 895       | *359<br>*358<br>*359         | 4 · 8480958,8<br>4 · 8199665,6<br>4 · 9330120,5 | "                | 68                 | 30<br>28<br>29       | XLII<br>XXXIX<br>XLIV           | 88 44 4.580<br>39 17 24.751<br>51 58 30.669           | ·546<br>·546<br>·546      | 5°0712249,1<br>4°8729051,0<br>4°9677159,9       |
| <b>2</b> 7       | 55                 | 15<br>18<br>14       | XIV<br>XIII<br>XVI            | 67 5 50·466<br>49 3 52·442<br>63 50 17·092         | ·304<br>·303<br>·304         | 4 · 8593750,5<br>4 · 7732412,8<br>4 · 8480958,8 | 11               | 69                 | 5<br>4<br>6          | XLIV<br>XLV<br><i>XLVII</i>     | 42 38 49 459<br>78 6 52 563<br>59 14 17 978           | •460<br>•460<br>•460      | 4 · 8360926,4<br>4 · 9957840,1<br>4 · 9393418,5 |
| 5                | 56                 | 18<br>16<br>17       | XVI<br>XVIII<br><i>XIX</i>    | 55 56 1.754<br>62 50 44.783<br>61 13 13.463        | •239<br>•239<br>•239         | 4`7539904,9<br>4`7850382,9<br>4`7784961,4       | "                | 70                 | 8<br>7<br>9          | XLVII<br>XLV<br>XLIX            | 74 27 35 792<br>57 43 53 93 1<br>47 48 30 277         | '408<br>'407<br>'407      | 4°9501573,9<br>4°8934740,2<br>4°8360926,4       |
| <b>&gt;</b> >    | 57                 | 15<br>13<br>14       | XIX<br>XVIII<br>XXI           | 63 2 44 220<br>62 51 44 309<br>54 5 31 471         | •249<br>•249<br>•248         | 4 · 7955835,6<br>4 · 7948741,8<br>4 · 7539904,9 | 12               | 71                 | 5<br>4<br>6          | XLIX<br>L<br><i>LII</i>         | 52 24 57 952<br>43 28 52 703<br>84 6 9 345            | ·197<br>·197<br>·197      | 4 · 7306728,7<br>4 · 6693578,0<br>4 · 8293903,2 |
| 6                | 58                 | 4+5<br>3<br>6        | XXI<br>XXII<br>XXIII          | 98 55 57 389<br>37 25 48 809<br>43 38 13 802       | '221<br>'220<br>'221         | 4 · 9096312,4<br>4 · 6986876,8<br>4 · 7538358,6 | "                | 72                 | 8<br>7<br>9          |                                 | 47 18 16 005<br>84 42 51 057<br>47 58 52 938          | •224<br>•225<br>•225      | 4 · 7259946,0<br>4 · 8578758,0<br>4 · 7306728,7 |
| 7                | 59                 | 4<br>2+3<br>1        | XXIII<br>XXIV<br>XXVI         | 38 24 15 519<br>111 25 2 878<br>30 10 41 603       | '211<br>'211<br>'211         | 4°7751914,5<br>4°9508791,0<br>4°6832567,7       | 13               | 73                 | 18<br>16<br>17       | LIII<br>LV<br><i>LVI</i>        | 60 42 25 770<br>37 21 10 052<br>81 56 24 178          | .111.<br>011.<br>011.     | 4`6539847,5<br>4`4963923,8<br>4`7090919,8       |
| 8                | 60                 | 18<br>16<br>17       | XXV<br>XXVII<br><i>XXVIII</i> | 59 47 10 382<br>66 37 26 660<br>53 35 22 958       | ·276<br>·276<br>·276         | 4 · 8061403,7<br>4 · 8323548,0<br>4 · 7752303,5 | 27               | 74                 | 15<br>13<br>14       | LVI<br>LV<br>LVIII              | 62 923.151<br>60 426.534<br>57 46 10.315              | 145<br>145<br>145         | 4 · 6732240,2<br>4 · 6645148,8<br>4 · 6539847,5 |
| "                | 61                 | 15<br>13<br>14       | XXVIII<br>XXVII<br>XXX        | 73 37 41 · 976<br>53 19 40 · 432<br>53 2 37 · 592  | .311<br>.311<br>.311         | 4 · 8855658,1<br>4 · 8077523,1<br>4 · 8061403,7 | "                | 75                 | 10<br>12<br>11       | LV<br><i>LVIII</i><br>LIX       | 65 47 35 551<br>44 7 41 210<br>70 4 43 239            | .118<br>811.<br>811.      | 4 ° 6600505,3<br>4 ° 5427962,7<br>4 ° 6732240,2 |
| 9                | 62                 | 15<br>13<br>14       | XXX<br>XXXII<br><i>XXXIII</i> | 55 50 14 894<br>61 59 21 795<br>62 10 23 311       | .180<br>.180<br>.180         | 4 · 6920244,3<br>4 · 7201758,6<br>4 · 7209139,3 | "                | 76                 | 20<br>19<br>21       | LVIII<br>LIX<br>XIX             | 61 36 15 090<br>65 57 15 650<br>52 26 29 260          | ·167<br>·167<br>·167      | 4`7052511,1<br>4`7215006,6<br>4`6600505,3       |
|                  |                    |                      |                               |                                                    |                              |                                                 |                  | 1                  |                      |                                 |                                                       |                           |                                                 |

NOTES .- Stations XLI and XLIV appertain to the Karáchi Longitudinal Series. Station XIX appertains to the Sutlej Series.

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# THE NON-CIRCUIT TRIANGLES.

The Jodhpore Meridional Series. Final Figural Adjustments of the Non-Circuit Triangles.

Figure 1.

|                          | Consta                                                                         | Triangle 49.           | 85). |                                          |            |
|--------------------------|--------------------------------------------------------------------------------|------------------------|------|------------------------------------------|------------|
| XLIV to XLI<br>XLI " II  | Log. feet 5.2                                                                  | 541461,0<br>901706,7 } | 3+2  | Contained Angle.<br>80° 59′ 55″ 529      | )          |
| Equations                | to be satisfied.                                                               |                        |      | Adopted Errors.                          |            |
| $x_1 + x_3 + x_4 - 9x_5$ | $\begin{array}{cccc} \mathbf{x}_4 & = & + \\ \mathbf{x}_1 & = & + \end{array}$ | • 160<br>4• 1          |      | $x_1 = + " \cdot c$<br>$x_4 = + \cdot c$ | )39<br>[2] |



|                  |                                                                             |          |          |                                                                             |                                              | Tri                                                          | iangles 50          | D and 51.                                                        |                                                                  |                                                                      |                                                                                                            |                                                                                                      |
|------------------|-----------------------------------------------------------------------------|----------|----------|-----------------------------------------------------------------------------|----------------------------------------------|--------------------------------------------------------------|---------------------|------------------------------------------------------------------|------------------------------------------------------------------|----------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------|
|                  |                                                                             |          |          |                                                                             | C                                            | Constants                                                    | (from pa            | iges 85 an                                                       | nd 86).                                                          | Conte                                                                | ained Angle                                                                                                |                                                                                                      |
|                  |                                                                             | I<br>III | to<br>,, | III<br>VI                                                                   | Log. feet<br>"                               | 5.13<br>2.09                                                 | 81529,7<br>86612,2  | }                                                                | 16 + 13                                                          |                                                                      | 153° 38′ 17″ • 025                                                                                         |                                                                                                      |
|                  |                                                                             |          |          |                                                                             | Έ                                            | quations                                                     | to be sat           | isfied.                                                          |                                                                  |                                                                      |                                                                                                            | Factor.                                                                                              |
|                  | x <sub>16</sub><br>x <sub>13</sub><br>x <sub>16</sub><br>16 x <sub>18</sub> |          | +++      | x <sub>17</sub><br>x <sub>14</sub><br>x <sub>13</sub><br>21 x <sub>17</sub> | +<br>+<br>+                                  | x <sub>18</sub><br>x <sub>15</sub><br><br>21 x <sub>15</sub> | _                   | <br><br>10 x <sub>14</sub>                                       |                                                                  | e <sub>1</sub><br>e <sub>2</sub><br>e <sub>3</sub><br>e <sub>4</sub> | $= \frac{.000}{.000}, \\ = \frac{.000}{.238}, \\ = -3.1, $                                                 | $egin{array}{c} \lambda_1 & \ \lambda_2 & \ \lambda_3 & \ \lambda_4 & \end{array}$                   |
|                  | Ec                                                                          | quatio   | ns be    | etween                                                                      | the Factors                                  |                                                              |                     |                                                                  |                                                                  |                                                                      |                                                                                                            |                                                                                                      |
| No. of           | o. of Value of Co-efficients of                                             |          |          | Values of the Factors Adop                                                  |                                              |                                                              | Adopted             | Errors                                                           |                                                                  |                                                                      |                                                                                                            |                                                                                                      |
| е                | e                                                                           |          | λ        | )                                                                           | νς - λη                                      |                                                              | λ,                  |                                                                  |                                                                  |                                                                      |                                                                                                            |                                                                                                      |
| 1<br>2<br>3<br>4 | · 000<br>· 000<br>- · 238<br>- 3 · 1                                        |          | +3       | <br>-+<br>•                                                                 | $\begin{array}{c} +1\\ 3\\ +2\\ \end{array}$ |                                                              | 5<br>11<br><br>1238 | $\lambda_1$ :<br>$\lambda_2$ :<br>$\lambda_3$ :<br>$\lambda_4$ : | $= + \cdot 0$<br>= + $\cdot 0$<br>= - $\cdot 1$<br>= - $\cdot 0$ | 56<br>72<br>83<br>03                                                 | $ \begin{aligned} x_{18} &= -" \cdot 111 \\ x_{14} &= + \cdot 100 \\ x_{15} &= + \cdot 011 \end{aligned} $ | $\begin{array}{l} x_{16} = -" \cdot 127 \\ x_{17} = + \cdot 117 \\ x_{18} = + \cdot 010 \end{array}$ |

| I. M. M. C. O. |
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|                                                                             |                                                                                                            | Triangles 52 and 53.                                     |                                                                    |                                                                         |
|-----------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------|----------------------------------------------------------|--------------------------------------------------------------------|-------------------------------------------------------------------------|
|                                                                             |                                                                                                            | Constants (from page 86).                                | Contained Anala                                                    |                                                                         |
| VI<br>VIII                                                                  | to VIII Log. feet<br>,, XI ,,                                                                              | 5·0838982,0<br>5·0217355,9 }                             | Contained Angle.<br>16+13 137° 44' 35"'                            | 660                                                                     |
|                                                                             | Equ                                                                                                        |                                                          | Factor.                                                            |                                                                         |
| x <sub>16</sub><br>x <sub>18</sub><br>x <sub>16</sub><br>19 x <sub>18</sub> | $\begin{array}{ccccc} + & x_{17} & + \\ + & x_{14} & + \\ + & x_{18} & . \\ - & 13 x_{17} & + \end{array}$ | $x_{18}$<br>$x_{15}$<br>$x_{15}$<br>$x_{15}$<br>$x_{14}$ | $= e_1 =000,$<br>$= e_2 =000,$<br>$= e_3 =179,$<br>$= e_4 = -3.6,$ | $     \lambda_1 $ $     \lambda_2 $ $     \lambda_3 $ $     \lambda_4 $ |

• In the tables of the equations between the factors the co-efficients of the terms below the diagonal are omitted for convenience, the co-efficient of the pth term in the qth line being always the same as the co-efficient of the qth term in the pth line.

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The Jodhpore Meridional Series. Final Figural Adjustments of the Non-Circuit Triangles.

|                  | Equ      | ations bet     | ween the l   | Factors           |                       |                                                                                                                  |                                                                                                                                                                             |  |  |
|------------------|----------|----------------|--------------|-------------------|-----------------------|------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--|--|
| No. of           | Value of |                | Co-ef        | ficients of       |                       | Values of the Factors                                                                                            | Adopted Errors                                                                                                                                                              |  |  |
| e                | e        | λ <sub>1</sub> | λ            | λ <sub>3</sub>    | $\lambda_4$           |                                                                                                                  |                                                                                                                                                                             |  |  |
| 1<br>2<br>3<br>4 |          | +3             | <br>+ 3<br>* | + I<br>+ I<br>+ 2 | + 6<br>0<br><br>+ 868 | $\lambda_1 = + \cdot 056$<br>$\lambda_2 = + \cdot 047$<br>$\lambda_3 = - \cdot 141$<br>$\lambda_4 = - \cdot 005$ | $\begin{array}{ll} x_{13} = -" \cdot 094 & x_{16} = -" \cdot 085 \\ x_{14} = + \cdot 107 & x_{17} = + \cdot 115 \\ x_{15} = - \cdot 013 & x_{18} = - \cdot 030 \end{array}$ |  |  |

Figure 3-(Continued).

# Figure 4.

| Triangles 54 and 55.<br>Constants (from pages 86 and 87).<br>XII to XIII Log. feet 4.9330134,9<br>XIII ,, XVI ,, 4.8593774,0<br>16+13 97° 55' 19".565 |                                                                             |                  |                                                                            |                   |                                                       |                                                                                                   |                                                                                                   |                                                                                                      |                                                                                                                                       |  |
|-------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------|------------------|----------------------------------------------------------------------------|-------------------|-------------------------------------------------------|---------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------|--|
|                                                                                                                                                       |                                                                             |                  |                                                                            | Equa              | tions to be sat                                       | isfied.                                                                                           |                                                                                                   |                                                                                                      | Factor.                                                                                                                               |  |
|                                                                                                                                                       | x <sub>16</sub><br>x <sub>18</sub><br>x <sub>16</sub><br>16 x <sub>18</sub> | +<br>+<br>+<br>- | x <sub>17</sub><br>x <sub>14</sub><br>x <sub>18</sub><br>5 x <sub>17</sub> | +<br>+<br>+ 8     | x <sub>18</sub><br>x <sub>16</sub><br>x <sub>16</sub> | <br><br>- J I X <sub>14</sub>                                                                     | $= e_1$ $= e_2$ $= e_3$ $= e_4$                                                                   | $= \cdot 000, \\ = \cdot 000, \\ = - \cdot 222, \\ = -9 \cdot 1, $                                   | λ <sub>1</sub><br>λ <sub>3</sub><br>λ <sub>5</sub><br>λ <sub>4</sub>                                                                  |  |
|                                                                                                                                                       | Equ                                                                         | ations bet       | ween the                                                                   | Factors           |                                                       |                                                                                                   |                                                                                                   |                                                                                                      |                                                                                                                                       |  |
| No. of                                                                                                                                                | Value of                                                                    | Co-efficients of |                                                                            |                   | Values of the Factors Adopted Er                      |                                                                                                   |                                                                                                   | Errors                                                                                               |                                                                                                                                       |  |
| e                                                                                                                                                     | е                                                                           | λ                | λ                                                                          | λ <sub>3</sub>    | λ                                                     |                                                                                                   |                                                                                                   |                                                                                                      |                                                                                                                                       |  |
| 1<br>2<br>3<br>4                                                                                                                                      | ·000<br>·000<br>- ·222<br>-9·1                                              | +3               | <br>+3<br>*                                                                | + 1<br>+ 1<br>+ 2 | + 11<br>- 3<br>+ 466                                  | $\begin{array}{rcl} \lambda_1 & = \\ \lambda_2 & = \\ \lambda_3 & = \\ \lambda_4 & = \end{array}$ | $ \begin{array}{r} + & \cdot 155 \\ + & \cdot 048 \\ - & \cdot 213 \\ - & \cdot 023 \end{array} $ | $\begin{array}{l} x_{13} = -" \cdot 165 \\ x_{14} = + \cdot 301 \\ x_{16} = - \cdot 136 \end{array}$ | $ \begin{aligned} \mathbf{x}_{16} &= -" \cdot 057 \\ \mathbf{x}_{17} &= + \cdot 270 \\ \mathbf{x}_{18} &= - \cdot 213 \end{aligned} $ |  |

| Figure | 5. |
|--------|----|
|--------|----|

|                                                                              |            |                                                                                               |                    | Triangles 56                                                                                      | and 57.                    |       |                                                                      |            |                                 |                                  |
|------------------------------------------------------------------------------|------------|-----------------------------------------------------------------------------------------------|--------------------|---------------------------------------------------------------------------------------------------|----------------------------|-------|----------------------------------------------------------------------|------------|---------------------------------|----------------------------------|
|                                                                              |            |                                                                                               |                    | Constants (from                                                                                   | n page 87).                |       | •                                                                    |            |                                 |                                  |
| XVI<br>XVI                                                                   | to<br>II " | XVIII<br>XXI                                                                                  | Log. feet<br>"     | 4·7784986,6<br>4·7955865,4                                                                        | }                          | 16+13 | Con:                                                                 | taine<br>J | d Angle.<br>25° 42′ 29″ .′      | 745                              |
|                                                                              |            |                                                                                               | Equa               | tions to be satisfi                                                                               | ied.                       |       |                                                                      |            |                                 | Factor.                          |
| X <sub>16</sub><br>X <sub>13</sub><br>X <sub>16</sub><br>J 4 X <sub>18</sub> |            | $ \begin{array}{r} + & x_{17} \\ + & x_{14} \\ + & x_{18} \\ - & 1 & 1 & x_{17} \end{array} $ | +<br>+<br>+<br>+ 1 | $\begin{array}{c} \mathbf{x}_{18} \\ \mathbf{x}_{15} \\ \cdots \\ 0 \mathbf{x}_{15} \end{array} $ | <br><br>16 x <sub>14</sub> |       | e <sub>1</sub><br>e <sub>2</sub><br>e <sub>3</sub><br>e <sub>4</sub> |            | ·000,<br>·000,<br>·165,<br>4·6, | $λ_1$<br>$λ_2$<br>$λ_3$<br>$λ_4$ |

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# THE NON-CIRCUIT TRIANGLES.

# The Jodhpore Meridional Series. Final Figural Adjustments of the Non-Circuit Triangles.

Figure 5-(Continued).

|                  | Equ                         | ations betw | veen the F   | actors            |                  |                                                                                                                  | Adopted Errors                                       |  |  |
|------------------|-----------------------------|-------------|--------------|-------------------|------------------|------------------------------------------------------------------------------------------------------------------|------------------------------------------------------|--|--|
| No. of           | Value of                    |             | Co-effi      | cients of         |                  | Values of the Factors                                                                                            |                                                      |  |  |
| e                | e                           | λ           | λ            | λ <sub>3</sub>    | λ4               |                                                                                                                  |                                                      |  |  |
| 1<br>2<br>3<br>4 | .000<br>.000<br>165<br>-4.6 | +3          | <br>+ 3<br>* | + I<br>+ I<br>+ 2 | + 3 - 6<br>+ 673 | $\lambda_1 = + \cdot 046$<br>$\lambda_2 = + \cdot 026$<br>$\lambda_3 = - \cdot 119$<br>$\lambda_4 = - \cdot 007$ | $\begin{array}{llllllllllllllllllllllllllllllllllll$ |  |  |

| Tryare U |  | Figure | 6. |
|----------|--|--------|----|
|----------|--|--------|----|

|                                     |                            | Triangle 58.                 |                                                                                                       |
|-------------------------------------|----------------------------|------------------------------|-------------------------------------------------------------------------------------------------------|
|                                     |                            | Constants (from page 87      | ).<br>Contained Angle                                                                                 |
| XXII to<br>XXI "                    | XXI Log. feet<br>XXIII "   | 4·7538389,3<br>4·6986909,8 } | 4+5 98° 55′ 57″ 623                                                                                   |
|                                     | Equations to be satisf     | fied.                        | Adopted Errors.                                                                                       |
| x <sub>8</sub><br>27 x <sub>8</sub> | $+ x_6 = $<br>-22 $x_6 = $ | $+ \cdot 013 - 2 \cdot 3$    | $\begin{array}{rcl}\mathbf{x}_{8} & = & -" \cdot 041 \\ \mathbf{x}_{6} & = & + \cdot 054 \end{array}$ |



|                                     |         |              |                | Trian                      | gle 59 | ).       |     |                          |        | ,                                    |  |
|-------------------------------------|---------|--------------|----------------|----------------------------|--------|----------|-----|--------------------------|--------|--------------------------------------|--|
|                                     |         |              |                | Constants (fr              | om p   | age 88). |     | Cont                     |        | ]-                                   |  |
| XXIII<br>XXIV                       | to<br>" | XXIV<br>XXVI | Log. feet<br>" | 4·6832601,5<br>4·7751950,4 | }      | •••      | 8+2 |                          | III°   | <sup>2</sup> 5′ 3 <sup>‴ •</sup> 347 |  |
|                                     |         | Equations    | to be satisf   | ied.                       |        |          |     |                          | Adopte | d Errors.                            |  |
| x <sub>1</sub><br>26 x <sub>4</sub> |         | +<br>-36     |                | $+ \cdot 258$<br>-2.1      |        |          |     | <b>x</b> 1<br><b>x</b> 4 |        | +"·141<br>+ ·117                     |  |

| riyure o. |
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|-----------|

|                                                                             |                                                                                             | I                                                                                       | riangles 60 and    | i 61.    |       |                                                                                         |                                                         |
|-----------------------------------------------------------------------------|---------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------|--------------------|----------|-------|-----------------------------------------------------------------------------------------|---------------------------------------------------------|
|                                                                             |                                                                                             | Con                                                                                     | stants (from pa    | ıge 88). | G     |                                                                                         |                                                         |
| XXV<br>XXVII                                                                | to XXVII<br>,, XXX                                                                          | Log. feet 4.77                                                                          | 52348,0<br>55711,7 |          | 16+13 | . 119° 57′ 7″ 841                                                                       |                                                         |
|                                                                             |                                                                                             | Equation                                                                                | s to be satisfied  | l.       |       |                                                                                         | Factor.                                                 |
| x <sub>16</sub><br>x <sub>13</sub><br>x <sub>16</sub><br>12 x <sub>18</sub> | $ \begin{array}{r} + & x_{17} \\ + & x_{14} \\ + & x_{18} \\ - & 15 x_{17} \\ \end{array} $ | $ \begin{array}{c} + & x_{18} \\ + & x_{16} \\ & \cdots \\ + & 6 & x_{15} \end{array} $ | <br>- 16 x         | 14       |       | $e_1 = \cdot 000,$<br>$e_2 = \cdot 000,$<br>$e_3 = - \cdot 162,$<br>$e_4 = -9 \cdot 1,$ | λ <sub>1</sub><br>λ <sub>9</sub><br>λ <sub>8</sub><br>λ |

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# The Jodhpore Meridional Series. Final Figural Adjustments of the Non-Circuit Triangles.

|                  | Equ                                                                                   | ations bet     | ween the F     | actors            |                      |                                                                                                                                 |                                                                                                                                                                                |  |  |
|------------------|---------------------------------------------------------------------------------------|----------------|----------------|-------------------|----------------------|---------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--|--|
| No. of           | Value of                                                                              |                | Co-effi        | cients of         |                      | Values of the Factors                                                                                                           | Adopted Errors                                                                                                                                                                 |  |  |
| e                | e                                                                                     | λ <sub>1</sub> | λ <sub>s</sub> | λ <sub>8</sub>    | λ4                   |                                                                                                                                 |                                                                                                                                                                                |  |  |
| 1<br>2<br>3<br>4 | $ \begin{array}{c} \cdot 000 \\ \cdot 000 \\ - \cdot 162 \\ - 9 \cdot 1 \end{array} $ | +3             | <br>+ 3<br>*   | + 1<br>+ 1<br>+ 2 | - 3<br>- 10<br>+ 661 | $\lambda_1 = + \cdot 01 \mathfrak{l}$ $\lambda_2 = - \cdot 02 \mathfrak{l}$ $\lambda_3 = - \cdot 076$ $\lambda_4 = - \cdot 014$ | $\begin{array}{rcl} x_{18} = -"' \cdot 097 & x_{16} = -"' \cdot 065 \\ x_{16} = + \cdot 203 & x_{17} = + \cdot 221 \\ x_{15} = - \cdot 106 & x_{18} = - \cdot 156 \end{array}$ |  |  |

Figure 8-(Continued).

# Figure 9.

|                  |                                                                              |         |                                                                                            |                   | Triangles 6                            | 2 and 63.                                                                                         | <u> </u>                                                                                          |                                                                                                        |                                                                                                      |
|------------------|------------------------------------------------------------------------------|---------|--------------------------------------------------------------------------------------------|-------------------|----------------------------------------|---------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------|
|                  |                                                                              |         |                                                                                            | Co                | nstants (from pa                       | ges 88 and 89                                                                                     | )).<br>Co                                                                                         | ontained Angle.                                                                                        |                                                                                                      |
|                  | XXX<br>XXXII                                                                 | to<br>" | XXXII<br>XXXIV                                                                             | Log. feet         | 4·7209196,:<br>4·6592271,0             | <sup>2</sup> }                                                                                    | <b>13</b> +10                                                                                     | 156° 26′ 7                                                                                             | "·636                                                                                                |
|                  |                                                                              |         |                                                                                            | Equ               | ations to be sat                       | isfied.                                                                                           |                                                                                                   |                                                                                                        | Factor.                                                                                              |
|                  | X <sub>18</sub><br>X <sub>10</sub><br>X <sub>18</sub><br>J 5 X <sub>15</sub> |         | $ \begin{array}{c} + & x_{14} \\ + & x_{11} \\ + & x_{10} \\ - & 11 & x_{14} \end{array} $ | +<br>+<br>+ 2     | x <sub>15</sub><br>x <sub>19</sub><br> | <br><br>21 x <sub>11</sub>                                                                        | $ \begin{array}{cccccccccccccccccccccccccccccccccccc$                                             | $= \cdot 000, \\ = \cdot 000, \\ = - \cdot 150, \\ = -5 \cdot 5, $                                     | λ <sub>1</sub><br>λ <sub>9</sub><br>λ <sub>3</sub><br>λ <sub>4</sub>                                 |
|                  | Equ                                                                          | ations  | s between th                                                                               | ne Factors        |                                        |                                                                                                   |                                                                                                   |                                                                                                        | <u></u>                                                                                              |
| No. of           | Value of                                                                     |         | C                                                                                          | o-efficients o    | f                                      | Values of t                                                                                       | he Factors                                                                                        | Adopt                                                                                                  | ed Errors                                                                                            |
| е                | е                                                                            | >       | λ <sub>1</sub> λ <sub>3</sub>                                                              | λ <sub>8</sub>    | $\lambda_4$                            |                                                                                                   |                                                                                                   |                                                                                                        |                                                                                                      |
| 1<br>2<br>3<br>4 | $ \begin{array}{r}                                     $                     | ÷       | 3<br>+3<br>*                                                                               | + I<br>+ I<br>+ 2 | + 4<br>+ 3<br><br>+ 1363               | $\begin{array}{rcl} \lambda_1 & = \\ \lambda_2 & = \\ \lambda_3 & = \\ \lambda_4 & = \end{array}$ | $ \begin{array}{r} + & \cdot 046 \\ + & \cdot 044 \\ - & \cdot 120 \\ - & \cdot 004 \end{array} $ | $ \begin{array}{l} x_{10} = -" \cdot 076 \\ x_{11} = + \cdot 132 \\ x_{12} = - \cdot 056 \end{array} $ | $\begin{array}{l} x_{13} = -" \cdot 074 \\ x_{14} = + \cdot 093 \\ x_{15} = - \cdot 019 \end{array}$ |

# Figure 10.

|                        |       |                        |      |                        |                    | Triangles 64 to            | 68.   |                      |       |                       |      |                 |                |
|------------------------|-------|------------------------|------|------------------------|--------------------|----------------------------|-------|----------------------|-------|-----------------------|------|-----------------|----------------|
|                        |       |                        |      |                        | Con                | stants (from pa            | ige 8 | 39).<br>(            | Conta | aine                  | d An | gles.           |                |
|                        | XXXV  | to                     | XXXV | I                      | Log. feet          | 4·8090908,1                | }     | 4+7 +10              |       | •                     | 1860 | ° 32′ 24″ · 637 |                |
|                        | XXXIX | ,,<br>,,               | XLIV | <b>A</b>               | ))<br>))           | 4°9710293,0<br>5°0712328,4 | }     | 12+31+28             |       | •                     | 124  | 55 38 ·667      |                |
|                        |       |                        |      |                        | Equation           | ons to be satisfi          | ed.   |                      |       |                       |      |                 | Factor.        |
| X4                     | +     | x <sub>5</sub>         | +    | X <sub>6</sub>         |                    |                            |       | •••                  | =     | e <sub>1</sub>        | =    | •000,           | λ <sub>1</sub> |
| <b>x</b> <sub>7</sub>  | +     | x <sub>8</sub>         | +    | X <sub>9</sub>         | •••                | •••                        |       | •••                  | =     | eg                    | =    | •000,           | $\lambda_{g}$  |
| <b>x</b> <sub>10</sub> | +     | <b>x</b> <sub>11</sub> | +    | <b>X</b> 18            | •••                | •••                        |       | •••                  | =     | es                    | =    | •000,           | $\lambda_{s}$  |
| <b>x</b> <sub>31</sub> | +     | X <sub>32</sub>        | +    | X <sub>88</sub>        | •••                | •••                        |       | •••                  | =     | e4                    | =    | •000,           | λ4             |
| X <sub>28</sub>        | +     | x <sub>29</sub>        | +    | <b>X</b> 80            | •••                | •••                        |       | •••                  | =     | $\mathbf{e}_{5}$      | =    | •000,           | $\lambda_5$    |
| X4                     | +     | x <sub>7</sub>         | +    | <b>x</b> <sub>10</sub> | •••                |                            |       | •••                  | =     | e <sub>6</sub>        | =    | + •122,         | <b>λ</b> 6     |
| <b>x</b> 18            | +     | x <sub>31</sub>        | +    | x <sub>28</sub>        | •••                | •••                        |       | •••                  | =     | e <sub>7</sub>        | Ξ    | + •218,         | $\lambda_{7}$  |
| 7 x <sub>5</sub>       | — I 4 | 4 X <sub>6</sub>       | + 1  | 1 X <sub>8</sub>       | — 7 x <sub>9</sub> | + 16 x <sub>11</sub>       |       | — 29 X <sub>13</sub> | =     | <b>e</b> <sub>8</sub> | =    | - 5.7,          | λ8             |
| о x <sub>10</sub>      | - 10  | 6 x <sub>11</sub>      | + 1  | 7 X <sub>33</sub>      | $-4 x_{32}$        | + x <sub>80</sub>          |       | $-17 x_{29}$         | =     | e,                    | =    | -11.7,          | λ              |

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# The Jodhpore Meridional Series. Final Figural Adjustments of the Non-Circuit Triangles.

|                                           |                                                             | ]                | Equat  | ions b         | etweer     | the l         | Factor                       | 8                            |                                                                                                   |                                                                             |                                                                                                                                                                                                                                                                      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |  |
|-------------------------------------------|-------------------------------------------------------------|------------------|--------|----------------|------------|---------------|------------------------------|------------------------------|---------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--|--|
| No. of                                    | Value of                                                    | Co-efficients of |        |                |            |               |                              |                              |                                                                                                   |                                                                             | Values of the<br>Factors                                                                                                                                                                                                                                             | Adopted Errors                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |  |  |
| е                                         | е                                                           | λ                | λ      | λ <sub>8</sub> | λ          | $\lambda_{5}$ | λ <sub>6</sub>               | λ <sub>7</sub>               | λ <sub>8</sub>                                                                                    | λο                                                                          |                                                                                                                                                                                                                                                                      |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |  |  |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8<br>9 | $\begin{array}{r} & & & & & & \\ & & & & & & \\ & & & & & $ | +3               | <br>+3 | <br>+3         | <br><br>+3 | <br><br>+3    | + 1<br>+ 1<br>+ 1<br><br>+ 3 | <br>+ I<br>+ I<br>+ 1<br>+ 3 | $ \begin{array}{r} - & 7 \\ + & 4 \\ - & 13 \\ \dots \\ \dots \\ - & 29 \\ + & 1512 \end{array} $ | $ \begin{array}{c}\\ - 16\\ + 13\\ - 16\\ 0\\\\ - 256\\ + 851 \end{array} $ | $\lambda_{1} = - \cdot 0770$ $\lambda_{2} = - \cdot 0458$ $\lambda_{3} = - \cdot 2697$ $\lambda_{4} = + \cdot 0737$ $\lambda_{5} = - \cdot 1757$ $\lambda_{6} = + \cdot 1715$ $\lambda_{7} = + \cdot 1144$ $\lambda_{8} = - \cdot 0085$ $\lambda_{9} = - \cdot 0258$ | $\begin{array}{rcl} \mathbf{x}_{4} &= +" \cdot 095 & \mathbf{x}_{19} = +" \cdot 091 \\ \mathbf{x}_{5} &= - \cdot 137 & \mathbf{x}_{28} = - \cdot 061 \\ \mathbf{x}_{6} &= + \cdot 042 & \mathbf{x}_{29} = + \cdot 263 \\ \mathbf{x}_{7} &= + \cdot 125 & \mathbf{x}_{80} = - \cdot 202 \\ \mathbf{x}_{8} &= - \cdot 139 & \mathbf{x}_{31} = + \cdot 188 \\ \mathbf{x}_{9} &= + \cdot 014 & \mathbf{x}_{32} = + \cdot 177 \\ \mathbf{x}_{10} &= - \cdot 098 & \mathbf{x}_{33} = - \cdot 365 \\ \mathbf{x}_{11} &= + \cdot 007 \end{array}$ |  |  |

# Figure 10—(Continued).

# Figure 11.

|                  | Triangles 69 and 70.            |              |                                                     |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                                            |                                                                                                   |                                                                                            |                                                                    |                                                                    |  |  |  |  |  |
|------------------|---------------------------------|--------------|-----------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------|---------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------|--------------------------------------------------------------------|--------------------------------------------------------------------|--|--|--|--|--|
|                  |                                 |              |                                                     |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | Constants (fro                                             | m page 90).                                                                                       | Con                                                                                        | tained Angle                                                       |                                                                    |  |  |  |  |  |
|                  | XLIV<br>XLV                     | v to         | XLV<br>XLIX                                         | Log. feet                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 4`9393501,4<br>4`9501666,8                                 | }                                                                                                 | 4+7                                                                                        | 135° 50′ 47″ • 16                                                  | 7                                                                  |  |  |  |  |  |
|                  |                                 |              |                                                     | Ec                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | quations to be sat                                         | isfied.                                                                                           |                                                                                            |                                                                    | Factor.                                                            |  |  |  |  |  |
|                  | X4<br>X7<br>X4<br>23 X5         |              | $+ x_{5}$<br>+ $x_{8}$<br>+ $x_{7}$<br>- $13 x_{6}$ | +<br>+<br>+<br>+                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | x <sub>6</sub><br>x <sub>9</sub><br><br>6 x <sub>8</sub> — | <br><br>19 <b>x</b> 9                                                                             | $\begin{array}{cccc} = & e_1 & = \\ = & e_2 & = \\ = & e_3 & = \\ = & e_4 & = \end{array}$ | •000,<br>•000,<br>+ •194,<br>10•0,                                 | <b>λ</b> լ<br>λց<br>λց<br>λ₄                                       |  |  |  |  |  |
|                  | Equ                             | ations       | between                                             | the Factors                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |                                                            |                                                                                                   |                                                                                            |                                                                    |                                                                    |  |  |  |  |  |
| No. of           | Value of                        |              |                                                     | Co-efficients                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | of                                                         | Values of                                                                                         | f the Factors                                                                              | Adopted                                                            | Errors                                                             |  |  |  |  |  |
| е                | е                               | λ            | λ                                                   | <sub>3</sub> λ <sub>3</sub>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | λ4                                                         |                                                                                                   |                                                                                            |                                                                    |                                                                    |  |  |  |  |  |
| 1<br>2<br>3<br>4 | ·000<br>·000<br>+ ·194<br>-10·0 | _ <b>+</b> ; | 3<br>+<br>*                                         | $ \begin{array}{ccc}  & +1 \\  & +1 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +2 \\  & +$ | + 10<br>- 13<br><br>+ 1095                                 | $\begin{array}{rcl} \lambda_1 & = \\ \lambda_2 & = \\ \lambda_3 & = \\ \lambda_4 & = \end{array}$ | - ·017<br>- ·095<br>+ ·153<br>- ·010                                                       | $x_4 = +" \cdot 136$<br>$x_5 = - \cdot 250$<br>$x_6 = + \cdot 114$ | $x_7 = +" \cdot 058$<br>$x_8 = - \cdot 155$<br>$x_9 = + \cdot 097$ |  |  |  |  |  |

| <b>Fi</b> gure | 12. |
|----------------|-----|
|                |     |

|                         |         |                            |                  |               | Triangle                                                 | es 71 a | und 72.        | •    |   |                                                                      |        |                                    |                                                                      |  |
|-------------------------|---------|----------------------------|------------------|---------------|----------------------------------------------------------|---------|----------------|------|---|----------------------------------------------------------------------|--------|------------------------------------|----------------------------------------------------------------------|--|
|                         |         |                            |                  |               | Constants                                                | (from   | page S         | 90). |   | Co                                                                   | -+-:   | and Analo                          |                                                                      |  |
| XLIX<br>L               | to<br>" | L<br>LIV                   | Log. feet        |               | 4·8293997,4<br>4·7260047,2                               | }       |                | 4+   | 7 |                                                                      | 111.91 | 128° 11' 43" 953                   |                                                                      |  |
|                         |         |                            |                  | Eq            | quations to be                                           | satisfi | ied.           |      |   |                                                                      |        |                                    | Factor.                                                              |  |
| x4<br>x7<br>x4<br>16 x5 |         | + x<br>+ x<br>+ x<br>- 2 x | 5<br>8<br>7<br>6 | +<br>+<br>+ i | x <sub>6</sub><br>x <sub>9</sub><br><br>9 x <sub>8</sub> | <br>    | x <sub>9</sub> |      |   | e <sub>1</sub><br>e <sub>2</sub><br>e <sub>3</sub><br>e <sub>4</sub> |        | ·000,<br>·000,<br>+ ·229,<br>-7·0, | λ <sub>1</sub><br>λ <sub>3</sub><br>λ <sub>3</sub><br>λ <sub>4</sub> |  |

,

# INTRODUCTORY.

[66]

# The Jodhpore Meridional Series. Final Figural Adjustments of the Non-Circuit Triangles.

|                  | Equ                                                      | ations bet | ween the l   | Factors           |                   |                                                                                                                  |                                                      |  |  |  |
|------------------|----------------------------------------------------------|------------|--------------|-------------------|-------------------|------------------------------------------------------------------------------------------------------------------|------------------------------------------------------|--|--|--|
| No. of           | Value of                                                 |            | Co-el        | ficients of       |                   | Values of the Factors Adopted Errors                                                                             |                                                      |  |  |  |
| e                | e                                                        | λ          | λ            | λ <sub>8</sub>    | λ,                |                                                                                                                  |                                                      |  |  |  |
| 1<br>2<br>8<br>4 | $ \begin{array}{r}                                     $ | +3         | <br>+ 3<br>* | + 1<br>+ 1<br>+ 2 | + 14<br>0<br>+982 | $\lambda_1 = - \cdot 017$<br>$\lambda_3 = - \cdot 049$<br>$\lambda_3 = + \cdot 148$<br>$\lambda_4 = - \cdot 007$ | $\begin{array}{llllllllllllllllllllllllllllllllllll$ |  |  |  |

Figure 12-(Continued).

# Figure 13.

|                                      |                                                                                                                                                          |                                                         |                        |                                                                                                                                                      |                                    |                                                                                                                                           |                          | г                                                 | riangles                               | 73 to 76.                                    |                                                                                                                 |                                                                     |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                |                                                          |                                                                         |                                                                                                                                              |
|--------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------|------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------|--------------------------|---------------------------------------------------|----------------------------------------|----------------------------------------------|-----------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------|----------------------------------------------------------|-------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------|
|                                      |                                                                                                                                                          |                                                         |                        |                                                                                                                                                      |                                    |                                                                                                                                           |                          | Cons                                              | tants (fr                              | om page                                      | 91).                                                                                                            | Containe                                                            | d Ang                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | zle <b>s</b> . |                                                          |                                                                         |                                                                                                                                              |
|                                      |                                                                                                                                                          |                                                         | I to                   |                                                                                                                                                      | Log                                | g. feet                                                                                                                                   | 4.2                      | 709102                                            | 5,0 }                                  | •••                                          | 16+13+10                                                                                                        | ••••                                                                | 163                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | ° 13'          | ′ 12 <sup>#</sup> •66                                    | 3                                                                       |                                                                                                                                              |
|                                      |                                                                                                                                                          |                                                         | X n                    | XIX                                                                                                                                                  |                                    | در<br>در                                                                                                                                  | 4':<br>4'7               | 542807<br>705263                                  | 4,2<br>5,0 }                           |                                              | 11 + 19                                                                                                         | •••                                                                 | 136                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | I              | 59 · 26                                                  | 2                                                                       |                                                                                                                                              |
|                                      |                                                                                                                                                          | Equations to be satisfied.                              |                        |                                                                                                                                                      |                                    |                                                                                                                                           |                          |                                                   |                                        |                                              |                                                                                                                 |                                                                     |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                |                                                          | Factor.                                                                 |                                                                                                                                              |
| 1                                    | x <sub>16</sub><br>x <sub>13</sub><br>x <sub>10</sub><br>x <sub>19</sub><br>x <sub>16</sub><br>x <sub>11</sub><br>2 x <sub>18</sub><br>9 x <sub>10</sub> |                                                         | + + + + + + + - 3 - 21 | X <sub>17</sub><br>X <sub>14</sub><br>X <sub>11</sub><br>X <sub>90</sub><br>X <sub>18</sub><br>X <sub>19</sub><br>X <sub>17</sub><br>X <sub>19</sub> | +<br>+<br>+<br>+<br>+<br>12<br>+12 | X <sub>18</sub><br>X <sub>15</sub><br>X <sub>19</sub><br>X <sub>91</sub><br>X <sub>10</sub><br><br>2 X <sub>15</sub><br>J X <sub>90</sub> | Ξ                        | <br><br>J 3 X <sub>14</sub><br>16 X <sub>91</sub> | +                                      | <br><br>21 X <sub>12</sub><br>               | <br><br>-8 x <sub>11</sub>                                                                                      |                                                                     | e <sub>1</sub><br>e <sub>2</sub><br>e <sub>3</sub><br>e <sub>4</sub><br>e <sub>6</sub><br>e <sub>7</sub><br>e <sub>8</sub>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                | $ \begin{array}{c}                                     $ | oo,<br>oo,<br>oo,<br>53,<br>87,<br>,                                    | λ <sub>1</sub><br>λ <sub>2</sub><br>λ <sub>3</sub><br>λ <sub>4</sub><br>λ <sub>5</sub><br>λ <sub>6</sub><br>λ <sub>7</sub><br>λ <sub>8</sub> |
|                                      |                                                                                                                                                          |                                                         | F                      | quatior                                                                                                                                              | s betw                             | veen th                                                                                                                                   | e Facto                  | ors                                               |                                        |                                              |                                                                                                                 |                                                                     |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                |                                                          |                                                                         |                                                                                                                                              |
| No. of                               | Valu                                                                                                                                                     | e of                                                    |                        |                                                                                                                                                      |                                    | Co-et                                                                                                                                     | fficient                 | s of                                              |                                        |                                              | Values<br>Fact                                                                                                  | of the<br>ors                                                       |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                | Adopte                                                   | l Error                                                                 | 8                                                                                                                                            |
| е                                    | e                                                                                                                                                        |                                                         | λ <sub>1</sub>         | λg                                                                                                                                                   | λ                                  | λ,                                                                                                                                        | $\lambda_{5}$            | λ <sub>6</sub>                                    | λ <sub>7</sub>                         | λ <sub>8</sub>                               |                                                                                                                 |                                                                     |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                |                                                          |                                                                         |                                                                                                                                              |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8 |                                                                                                                                                          | · 000<br>· 000<br>· 000<br>· 153<br>· 087<br>· 3<br>· 4 | +3                     | <br>+3                                                                                                                                               | <br>+ 3                            | <br><br>+3                                                                                                                                | + 1<br>+ 1<br>+ 1<br>+ 3 | <br>+ 1<br>+ 1<br>+ 1<br><br>+ 2                  | + 9<br>- 1<br>+ 13<br><br>- 8<br>+ 971 | <br>- 12<br>- 5<br>+ 9<br><br>- 441<br>+ 899 | $\lambda_1 = +$ $\lambda_2 = +$ $\lambda_3 = +$ $\lambda_4 = +$ $\lambda_5 = -$ $\lambda_7 = -$ $\lambda_8 = -$ | •0658<br>•021<br>•0543<br>•0146<br>•0255<br>•1544<br>•0191<br>•0221 | $x_{10} = x_{11} = x_{12} = x_{13} = x_{13} = x_{14} = x_{14} = x_{15} = x$ |                | -"•170<br>- •053<br>- •117<br>023<br>- •250<br>- •227    | $x_{16} = x_{17} = x_{17} = x_{18} = x_{19} = x_{20} = x_{21} = x_{21}$ | = + ".040<br>= + .123<br>=163<br>=140<br>=230<br>= + .370                                                                                    |

The Eastern Sind Meridional Series. Sides and Angles of the Non-Circuit Triangles.

| Number of Figure | Number of Triangle | Figural No. of Angle | Number of<br>Station         | Corrected<br>Plane Angle                              | Spherical Excess          | Logarithm<br>of Side-length<br>in Feet          | Number of Figure | Number of Triangle | Figural No. of Angle   | Number of<br>Station            | Corrected<br>Plane Angle                                             | Spherical Excess          | Logarithm<br>of Side-length<br>in Feet                  |
|------------------|--------------------|----------------------|------------------------------|-------------------------------------------------------|---------------------------|-------------------------------------------------|------------------|--------------------|------------------------|---------------------------------|----------------------------------------------------------------------|---------------------------|---------------------------------------------------------|
| 1                | 40                 | 18<br>16<br>17       | LXXV<br>LXXVIII<br><i>I</i>  | 0 / #<br>46 47 48 398<br>44 57 21 029<br>88 14 50 573 | "<br>'340<br>'340<br>'340 | 4 · 8242053,0<br>4 · 8106694,6<br>4 · 9613162,0 | 7                | 54                 | 27<br>25<br><b>2</b> 6 | XXV<br>XXVIII<br>XXVIII         | 0 / #<br>70 10 <b>32</b> 086<br>53 38 48 331<br>56 10 <b>3</b> 9 583 | "<br>"353<br>"352<br>"352 | 4 · 8990234,6<br>4 · 8315552,2<br>4 · 8450351,1         |
| "                | 41                 | 15<br>18<br>14       | I<br>LXXVIII<br>II           | 39 13 53 781<br>81 16 52 656<br>59 29 13 563          | •254<br>•255<br>•255      | 4 · 6899733,5<br>4 · 8838948,2<br>4 · 8242053,0 | "                | 55                 | 24<br>22<br>23         | XXVII<br>XXVIII<br>XXX          | 51 10 5°477<br>68 17 21 288<br>60 32 33 235                          | '411<br>'412<br>'412      | 4·8506760,9<br>4·9271895,1<br>4·8990234,6               |
| <b>27</b>        | 42                 | 12<br>10<br>11       | II<br>LXXVIII<br>III         | 84 46 38 214<br>60 1 9 420<br>35 12 12 366            | ·283<br>·283<br>·283      | 4 · 9273813,9<br>4 · 8668031,5<br>4 · 6899733,5 | 8                | 56                 | 5<br>4<br>6            | XXXI<br>XXXIII<br><i>XXXIV</i>  | 43 6 11 · 886<br>84 38 57 · 694<br>52 14 50 · 420                    | ·385<br>·386<br>·386      | 4 · 8140819,1<br>4 · 9775640,0<br>4 · 8774508,3         |
| <b>37</b>        | 43                 | 9<br>7<br>8          | III<br>LXXVIII<br>IV         | 73 40 56 · 177<br>38 25 36 · 389<br>67 53 27 · 434    | ·364<br>·363<br>·363      | 4 · 9426942,1<br>4 · 7540012,5<br>4 · 9273813,9 | "                | 57                 | 7<br>8<br>9            | XXXIII<br><i>XXXIV</i><br>XXXVI | 74 10 15 058<br>52 32 46 562<br>53 16 58 380                         | .319<br>.319<br>.319      | 4 · 8933367, <b>3</b><br>4 · 8098613,0<br>4 · 8140819,1 |
| 2                | 44                 | 18<br>16<br>17       | IV<br>VII<br><i>VI</i>       | 49 24 6·365<br>61 59 19·285<br>68 36 34·350           | '421<br>'422<br>'422      | 4 · 8468089,0<br>4 · 9122897,5<br>4 · 9354045,2 | "                | 58                 | 17<br>16<br>18         | XXXIV<br>XXXVI<br>XXXVII        | 38 54 0°180<br>54 13 13 580<br>86 52 46 240                          | •246<br>•246<br>•246      | 4 · 6919156,8<br>4 · 8031478,4<br>4 · 8933367,3         |
| 33               | 45                 | 15<br>13<br>14       | VI<br>VII<br>IX              | 76 I 33°768<br>48 34 36°918<br>55 23 49°314           | '345<br>'344<br>'344      | 4 • 9183059,1<br>4 • 8063238,8<br>4 • 8468089,0 | "                | 59                 | 20<br>19<br>21         | XXXVII<br>XXXVI<br>XXXVIII      | 59 51 59 497<br>73 21 3 488<br>46 46 57 015                          | *217<br>*217<br>*217      | 4 · 7662764,0<br>4 · 8107321,9<br>4 · 6919156,8         |
| 8                | 46                 | 4+5<br>3<br>6        | IX<br>X<br>XI                | 92 47 51 · 277<br>41 12 39 · 846<br>45 59 28 · 877    | *437<br>*437<br>*437      | 5.0337260,3<br>4.8530204,9<br>4.8911147,1       | 9                | 60                 | 18<br>16<br>17         | XXXV<br>XL<br><i>XXXIX</i>      | 43 45 36 • 413<br>77 53 9 • 778<br>58 21 13 • 809                    | ·333<br>·334<br>·334      | 4°7729996,7<br>4°9233391,1<br>4′8632041,5               |
| 4                | 47                 | 18<br>16<br>17       | XI<br>XIV<br><i>XIII</i>     | 46 38 46 613<br>66 48 52 687<br>66 32 20 700          | .424<br>.425<br>.424      | 4 · 8332488,9<br>4 · 9350641,8<br>4 · 9341636,6 | "                | 61                 | 15<br>18<br>14         | XXXIX<br>XL<br>XLI              | 46 27 37 215<br>69 17 33 934<br>64 14 48 851                         | ·208<br>·209<br>·209      | 4 · 6787084,5<br>4 · 7894287,7<br>4 · 7729996,7         |
| 21               | <b>4</b> 8         | 15<br>18<br>14       | XIII<br>XIV<br>XVI           | 61 11 26 · 145<br>58 28 38 · 020<br>60 19 55 · 835    | ·315<br>·314<br>·314      | 4 · 8368912,5<br>4 · 8249342,2<br>4 · 8332488,9 | "                | 62                 | 12<br>10<br>11         | XLI<br>XL<br>XLII               | 77 3 55 831<br>40 47 31 488<br>62 8 32 681                           | ·130<br>·129<br>·129      | 4 • 7210396,2<br>4 • 5473245,7<br>4 • 6787084,5         |
| 5                | <b>4</b> 9         | 18<br>16<br>17       | XVI<br>XIX<br>XVIII          | 45 31 59 807<br>62 23 3 198<br>72 4 56 995            | .303<br>.303<br>.303      | 4 · 7561267,6<br>4 · 8501078,9<br>4 · 8810459,7 | 10               | 63                 | 4+5<br>8<br>6          | XLII<br>XLIII<br>XLIV           | 78 28 3.711<br>43 10 50 242<br>58 21 6 047                           | ·205<br>·205<br>·205      | 4 · 8203503,4<br>4 · 6644544,2<br>4 · 7592824,2         |
| <b>9</b> 7       | 50                 | 15<br>13<br>14       | XVIII<br>XIX<br>XXI          | 54 43 25 · 502<br>72 36 6 · 239<br>52 40 28 · 259     | ·251<br>·252<br>·251      | 4°7675390,0<br>4°8353101,2<br>4°7561267,6       | 11               | 64                 | 5<br>4<br>6            | XLV<br>XLVI<br><i>XLVII</i>     | 50 45 52 915<br>66 44 50 783<br>62 29 16 302                         | •080<br>•080<br>•080      | 4°4917850,0<br>4°5659412,4<br>4°5506137,7               |
| 6                | 51                 | 4+5<br>3<br>6        | XXI<br>XXII<br>XXIII         | 99 24 20.066<br>42 21 27.814<br>38 14 12.120          | ·284<br>·284<br>·283      | 4 · 9651280,5<br>4 · 7995097,3<br>4 · 7626348,0 | ,,               | 65                 | 8<br>7<br>9            | XLVII<br>XLVI<br>XLIX           | 55 49 49 308<br>80 34 52 762<br>43 35 17 930                         | .090<br>.090<br>.090      | 4 · 5709725,8<br>4 · 6473738,5<br>4 · 4917850,0         |
| 7                | 52                 | 15<br>18<br>14       | XXIII<br>XXVI<br><i>XXV</i>  | 59 41 54 086<br>70 28 51 543<br>49 49 14 371          | ·308<br>·308<br>·308      | 4 • 8353369,2<br>4 • 8734298,9<br>4 • 7822440,8 | 12               | 66                 | 15<br>13<br>14         | XLVIII<br>Li<br>L               | 63 42 36·363<br>59 11 39·448<br>57 5 44·189                          | •087<br>•087<br>•087      | 4 · 5686641,5<br>4 · 5500296,7<br>4 · 5401437,5         |
| n                | <b>53</b>          | 10<br>12<br>11       | XXVI<br><i>XXV</i><br>XXVIII | 66 17 28 775<br>50 9 4 037<br>63 33 27 188            | ·290<br>·290<br>·290      | 4 · 8450351,1<br>4 · 7685410,8<br>4 · 8353369,2 | "                | 67                 | 12<br>10<br>11         | L<br>LI<br>LIX                  | 71 50 14°245<br>64 38 43°508<br>43 31 2°247                          | •135<br>•135<br>•135      | 4 · 7085175,8<br>4 · 6867262,2<br>4 · 5686641,5         |

NOTES.-Stations LXXV and LXXVIII appertain to the Karáchi Longitudinal Series. Station LIX appertains to the Great Indus Series.

# INTRODUCTORY.

# The Eastern Sind Meridional Series. Final Figural Adjustments of the Non-Circuit Triangles.

Figure 1.

|                                                                                                                       |                                                                                                                                                         |                                                                                                                                  |                                         |                                                                                                                  |            |                                     |                                        | Triangles 4                               | 0 to 43.                                                                                                                         |                                                                |                                                                                                             |                                                                                        |                                                          |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                                                                                                       |
|-----------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------|------------------------------------------------------------------------------------------------------------------|------------|-------------------------------------|----------------------------------------|-------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------|----------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------|
|                                                                                                                       | Constants (from page 196).<br>Contained Angle.                                                                                                          |                                                                                                                                  |                                         |                                                                                                                  |            |                                     |                                        |                                           |                                                                                                                                  |                                                                |                                                                                                             |                                                                                        |                                                          |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                                                                                                       |
|                                                                                                                       | LXXV to LXXVIII Log. feet 4.961316<br>LXXVIII,, IV ,, 4.942697                                                                                          |                                                                                                                                  |                                         |                                                                                                                  |            |                                     | 4·9613162,<br>4·9426977,               | °}                                        | 16+13+10+                                                                                                                        | 7                                                              |                                                                                                             | = 224 <sup>°</sup>                                                                     | •<br>9 41′ 0″ •                                          | 162                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |                                                                                                       |
|                                                                                                                       | Equations to be satisfied. Factor.                                                                                                                      |                                                                                                                                  |                                         |                                                                                                                  |            |                                     |                                        |                                           |                                                                                                                                  |                                                                |                                                                                                             |                                                                                        | Factor.                                                  |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                                                                                                       |
| X <sub>1</sub> ,<br>X <sub>1</sub> ;<br>X <sub>1</sub> ,<br>X <sub>7</sub><br>X <sub>1</sub> ,<br>20 X <sub>1</sub> ; | $\begin{array}{c} \mathbf{s}  + \\ \mathbf{s}  + \\ \mathbf{o}  + \\ \mathbf{s}  + \\ \mathbf{s}  - \mathbf{c} \\ \mathbf{s}  - \mathbf{c} \end{array}$ | x <sub>17</sub><br>x <sub>14</sub><br>x <sub>11</sub><br>x <sub>8</sub><br>x <sub>13</sub><br>x <sub>13</sub><br>x <sub>17</sub> | +++++++++++++++++++++++++++++++++++++++ | x <sub>18</sub><br>x <sub>15</sub><br>x <sub>19</sub><br>x <sub>9</sub><br>x <sub>10</sub><br>26 x <sub>15</sub> |            | x <sub>7</sub><br>2 x <sub>14</sub> |                                        | <br><br>2 — 30 x                          | <br><br><br>11 +6 x,                                                                                                             | <br><br><br>-9 x <sub>8</sub>                                  |                                                                                                             | e <sub>1</sub><br>e <sub>3</sub><br>e <sub>4</sub><br>e <sub>5</sub><br>e <sub>6</sub> | =<br>=<br>=<br>= +<br>= -3                               | •000,<br>•000,<br>•000,<br>•000,<br>•573,<br>55*7,                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | λ <sub>1</sub><br>λ <sub>3</sub><br>λ <sub>4</sub><br>λ <sub>5</sub><br>λ <sub>6</sub>                |
|                                                                                                                       |                                                                                                                                                         | Eq                                                                                                                               | uatio                                   | ns betw                                                                                                          | een th     | e Facto                             | ors                                    |                                           |                                                                                                                                  |                                                                |                                                                                                             |                                                                                        |                                                          |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                                                                                                       |
| No. of                                                                                                                | Value o                                                                                                                                                 | f                                                                                                                                |                                         |                                                                                                                  | Co-ef      | ficients                            | s of                                   |                                           | Values of t                                                                                                                      | he Factors                                                     |                                                                                                             |                                                                                        | Adopte                                                   | ed Error                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | l                                                                                                     |
| e                                                                                                                     | е                                                                                                                                                       |                                                                                                                                  | λι                                      | λ                                                                                                                | λ          | λ                                   | $\lambda_5$                            | $\lambda_6$                               |                                                                                                                                  |                                                                |                                                                                                             |                                                                                        |                                                          |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                                                                                                       |
| 1<br>2<br>3<br>4<br>5<br>6                                                                                            | • 00<br>• 00<br>• 00<br>• 00<br>+ • 57<br>- 35 • 7                                                                                                      | 0<br>0<br>0<br>3                                                                                                                 | +3                                      | <br>+3<br>*                                                                                                      | <br><br>+3 | <br><br>+3                          | + 1<br>+ 1<br>+ 1<br>+ 1<br><b>+ 4</b> | + 20<br>+ 14<br>- 28<br>- 3<br><br>+ 2241 | $\lambda_1 = \cdot \\ \lambda_2 = \cdot \\ \lambda_3 = \cdot \\ \lambda_4 = \cdot \\ \lambda_5 = \cdot \\ \lambda_6 = \cdot \\ $ | + ·0642<br>+ ·0242<br>- ·2558<br>- ·0891<br>+ ·2074<br>- ·0200 | x <sub>7</sub><br>x <sub>8</sub><br>x <sub>9</sub><br>x <sub>10</sub><br>x <sub>11</sub><br>x <sub>12</sub> |                                                                                        | +"·118<br>+ ·091<br>- ·209<br>- ·049<br>+ ·345<br>- ·296 | $x_{13} = x_{14} = x_{14} = x_{16} = x_{16} = x_{17} = x_{18} = x$ | $= +" \cdot 232$<br>= + \cdot 265<br>= - \cdot 497<br>= + \cdot 272<br>= + \cdot 064<br>= - \cdot 336 |

# Figure 2.

|                  | Triangles 44 and 45.                                                        |               |                                                      |                                                                                      |                          |                                                                      |                         |                               |                                                                                                                                                           |                                                                                                                      |  |  |
|------------------|-----------------------------------------------------------------------------|---------------|------------------------------------------------------|--------------------------------------------------------------------------------------|--------------------------|----------------------------------------------------------------------|-------------------------|-------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------|--|--|
|                  |                                                                             |               | Conta                                                | Contained Angle.                                                                     |                          |                                                                      |                         |                               |                                                                                                                                                           |                                                                                                                      |  |  |
|                  | IV<br>VII                                                                   | to VII<br>"IX | Log. feet                                            | 4°9354<br>4°9183                                                                     | 085,1<br>152,4 }         | •••                                                                  | 16+13                   |                               | $= 110^{\circ} 33' 57'' \cdot 133$                                                                                                                        |                                                                                                                      |  |  |
|                  |                                                                             |               |                                                      | Equation                                                                             | s to be sati             | sfied.                                                               |                         |                               |                                                                                                                                                           | Factor.                                                                                                              |  |  |
|                  | x <sub>16</sub><br>x <sub>18</sub><br>x <sub>16</sub><br>18 x <sub>18</sub> | ++++          | $x_{17}$<br>$x_{14}$<br>$x_{13}$<br>$\cdot 8 x_{17}$ | $ \begin{array}{c} + & x_{18} \\ + & x_{15} \\ & \dots \\ + 5 & x_{15} \end{array} $ | _                        | <br><br>15 x <sub>14</sub>                                           | =                       | $e_1 = e_3 = e_3 = e_4 = e_4$ | · 000,<br>· 000,<br>· - 164,<br>· - 53 · 4,                                                                                                               | $λ_1$<br>$λ_3$<br>$λ_3$<br>$λ_4$                                                                                     |  |  |
|                  | Equ                                                                         | nations be    | tween the Fac                                        | ctors                                                                                |                          |                                                                      |                         |                               |                                                                                                                                                           |                                                                                                                      |  |  |
| No. of           | Value of                                                                    |               | Co-effic                                             | ients of                                                                             |                          | Valu                                                                 | es of the F             | actors                        | Adoj                                                                                                                                                      | pted Errors                                                                                                          |  |  |
| е                | е                                                                           | λ             | λ                                                    | λ <sub>8</sub>                                                                       | λ4                       |                                                                      |                         |                               |                                                                                                                                                           |                                                                                                                      |  |  |
| 1<br>2<br>3<br>4 | •000<br>•000<br>- •164<br>-53•4                                             | +3            | <br>+3<br>*                                          | + I<br>+ I<br>+ 2                                                                    | + 10<br>- 10<br><br>+638 | λ <sub>1</sub><br>λ <sub>2</sub><br>λ <sub>3</sub><br>λ <sub>4</sub> | = + ·<br>= - ·<br>= - · | 3527<br>2707<br>1230<br>0935  | $     \begin{aligned}             x_{13} &= - " \cdot 39 \\             x_{14} &= +1 \cdot 13 \\             x_{15} &= - \cdot 73         \end{aligned} $ | $\begin{array}{cccc} 4 & x_{16} = + & & 230 \\ 2 & x_{17} = + 1 & 101 \\ 8 & x_{18} = -1 & 331 \\ & & & \end{array}$ |  |  |

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The Eastern Sind Meridional Series. Final Figural Adjustments of the Non-Circuit Triangles.

Figure 3.

|                                     |                      | Triangle 46.                       |                                                       |
|-------------------------------------|----------------------|------------------------------------|-------------------------------------------------------|
|                                     |                      | Constants (from page 197).         | Contained Angle                                       |
| X to<br>IX "                        | IX Log. feet<br>XI " | 4·8911247,0<br>4·8530312,6 } 4+5   | $\dots = 92^{\circ} 47' 52'' \cdot 419$               |
|                                     | Equation             | s to be satisfied.                 | Adopted Errors.                                       |
| x <sub>3</sub><br>24 x <sub>3</sub> | $+ x_6 \\ - 20 x_6$  | $= e_1 = + .705$<br>$= e_g = -7.8$ | $ \begin{array}{cccccccccccccccccccccccccccccccccccc$ |

| Figure | 4. |
|--------|----|
|--------|----|

|                  | Triangles 47 and 48.                                                        |                    |                                                                            |                                   |                          |                                                          |                          |                                                                           |                                                                                                      |                                                                                                                  |  |  |
|------------------|-----------------------------------------------------------------------------|--------------------|----------------------------------------------------------------------------|-----------------------------------|--------------------------|----------------------------------------------------------|--------------------------|---------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------|--|--|
|                  |                                                                             |                    |                                                                            | Const                             | n page                   | age 198).<br>Contained Angle.                            |                          |                                                                           |                                                                                                      |                                                                                                                  |  |  |
|                  | XI t<br>XIV ,                                                               | o XIV<br>, XVI     | Log. feet                                                                  | 4°934179<br>4°83690               | 67 <b>,2</b><br>72,0     |                                                          | <b>16 + 13</b>           |                                                                           | $= 125^{\circ} 17' 31''$                                                                             | 836                                                                                                              |  |  |
|                  |                                                                             |                    |                                                                            | Equations                         | to be satis              | fied.                                                    |                          |                                                                           |                                                                                                      | Factor.                                                                                                          |  |  |
|                  | x <sub>16</sub><br>x <sub>13</sub><br>x <sub>16</sub><br>20 x <sub>18</sub> | +<br>+<br>+<br>- 1 | x <sub>17</sub><br>x <sub>14</sub><br>x <sub>13</sub><br>0 x <sub>17</sub> | $ + x_{18} + x_{15} + 11 x_{15} $ | _                        | <br><br>I 2 X <sub>14</sub>                              |                          | $\begin{array}{rcl} = & e_1 \\ = & e_2 \\ = & e_3 \\ = & e_4 \end{array}$ | $= \frac{.000}{.000}, \\ = \frac{.000}{.000}, \\ = -\frac{.390}{.390}, \\ = -28.9, \\ \end{bmatrix}$ | λ₁<br>λ₃<br>λ <sub>8</sub><br>λ₄                                                                                 |  |  |
|                  | Equ                                                                         | ations bet         | tween the Fac                                                              | ctors                             |                          |                                                          |                          |                                                                           |                                                                                                      |                                                                                                                  |  |  |
| No. of           | Value of                                                                    |                    | Co-effic:                                                                  | ients of                          |                          | Valu                                                     | es of the                | Factors                                                                   | Adopte                                                                                               | d Errors                                                                                                         |  |  |
| е                | е                                                                           | λ                  | λ                                                                          | λ <sub>3</sub>                    | λ4                       |                                                          |                          |                                                                           |                                                                                                      |                                                                                                                  |  |  |
| 1<br>2<br>3<br>4 | · 000<br>· 000<br>- · 390<br>- 28 · 9                                       | +3                 | <br>+ 3<br>*                                                               | + 1<br>+ 1<br>+ 2                 | + 10<br>- 1<br><br>+ 765 | $\lambda_1$<br>$\lambda_3$<br>$\lambda_3$<br>$\lambda_4$ | = +<br>= +<br>= -<br>= - | • 2650<br>• 1 1 46<br>• 3850<br>• 041 1                                   | $\begin{array}{l} x_{13} = -" \cdot 270 \\ x_{14} = + \cdot 608 \\ x_{15} = - \cdot 338 \end{array}$ | $\mathbf{x}_{16} = -" \cdot 1_{20}$<br>$\mathbf{x}_{17} = + \cdot 6_{76}$<br>$\mathbf{x}_{18} = - \cdot 5_{556}$ |  |  |

Figure 5.

|                                                                             |                                                                                           | Triang                                         | cles 49 and 50.            |                                                                                                                                                                                                  |                                                          |
|-----------------------------------------------------------------------------|-------------------------------------------------------------------------------------------|------------------------------------------------|----------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------|
|                                                                             |                                                                                           | Constants                                      | (from page 198).           | Contained Angle.                                                                                                                                                                                 |                                                          |
| XVI to<br>XIX "                                                             | XIX Log. feet<br>XXI "                                                                    | 4·8810634,6<br>4·7675582,6                     | } 16+                      | $13 \dots = 134^{\circ} 59'$                                                                                                                                                                     | 10″ • 428                                                |
|                                                                             |                                                                                           | Equations to b                                 | e satisfied.               |                                                                                                                                                                                                  | Factor.                                                  |
| X <sub>16</sub><br>X <sub>13</sub><br>X <sub>16</sub><br>21 X <sub>18</sub> | $ \begin{array}{r} + & x_{17} \\ + & x_{14} \\ + & x_{13} \\ - & 7 & x_{17} \end{array} $ | $+ x_{18} + x_{16} + x_{16} + x_{15} + x_{15}$ | <br><br>16 x <sub>14</sub> | $\begin{array}{rcrcrc} = & e_1 & = & \cdot & \circ & \circ & \circ \\ = & e_3 & = & & \cdot & \circ & \circ & \circ \\ = & e_3 & = & - & \cdot & 436, \\ = & e_4 & = & -17 \cdot 7, \end{array}$ | $\lambda_1$<br>$\lambda_2$<br>$\lambda_3$<br>$\lambda_4$ |

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The Eastern Sind Meridional Series. Final Figural Adjustments of the Non-Circuit Triangles.

|                  | Equ                                                      | ations betw | ween the F   | actors            |                          |                                                                                                                        |                                                                                                                                                                                                                                  |  |  |  |
|------------------|----------------------------------------------------------|-------------|--------------|-------------------|--------------------------|------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--|--|--|
| No. of Value of  |                                                          |             | Co-eff       | icients of        |                          | Values of the Factors                                                                                                  | Adopted Errors                                                                                                                                                                                                                   |  |  |  |
| е                | e e λ <sub>1</sub>                                       |             | λ            | λ                 | $\lambda_4$              |                                                                                                                        |                                                                                                                                                                                                                                  |  |  |  |
| 1<br>2<br>3<br>4 | $ \begin{array}{c}                                     $ | +3          | <br>+ 3<br>* | + I<br>+ I<br>+ 2 | + 14<br>- 1<br><br>+ 971 | $\lambda_{1} = + \cdot 2321 \\ \lambda_{2} = + \cdot 1251 \\ \lambda_{3} = - \cdot 3966 \\ \lambda_{4} = - \cdot 0214$ | $\begin{array}{rcl} \mathbf{x_{13}} = -"\cdot 271 & \mathbf{x_{16}} = -"\cdot 165 \\ \mathbf{x_{14}} = + \cdot 467 & \mathbf{x_{17}} = + \cdot 382 \\ \mathbf{x_{16}} = - \cdot 196 & \mathbf{x_{18}} = - \cdot 217 \end{array}$ |  |  |  |

Figure 5-(Continued).

# Figure 6.

|                                     |    |                     | Triangle 51.                               |     |                                                                  |  |  |  |  |  |  |
|-------------------------------------|----|---------------------|--------------------------------------------|-----|------------------------------------------------------------------|--|--|--|--|--|--|
| Constants (from page 199).          |    |                     |                                            |     |                                                                  |  |  |  |  |  |  |
| XXII                                | to | XXI Log. feet       | 4.7626542,1                                | U   | ontained Angle.                                                  |  |  |  |  |  |  |
| XXI                                 | "  | XXIII "             | 4.7995299,5                                | 4+5 | $= 99^{\circ} 24' 20'' \cdot 617$                                |  |  |  |  |  |  |
|                                     |    | Equations to be sat | isfied.                                    |     | Adopted Errors.                                                  |  |  |  |  |  |  |
| x <sub>3</sub><br>24 x <sub>3</sub> |    | $+ x_6 = -27 x_6 =$ | $e_1 = + \cdot 267$<br>$e_3 = - 8 \cdot 1$ |     | $\mathbf{x}_{3} = - \cdot 018$<br>$\mathbf{x}_{6} = + \cdot 285$ |  |  |  |  |  |  |



| Triangles 52 to 55.        |                   |                            |                |                                    |                    |  |  |  |  |  |  |
|----------------------------|-------------------|----------------------------|----------------|------------------------------------|--------------------|--|--|--|--|--|--|
| Constants (from page 199). |                   |                            |                |                                    |                    |  |  |  |  |  |  |
| XXIII to                   | XXVI Log. feet    | 4.7822645,1                | Conta          | $= 136^{\circ} 46' 21'' \cdot 015$ |                    |  |  |  |  |  |  |
| XXVI "<br>XXVIII "         | XXVIII "<br>XXX " | 4·7685622,2<br>4·8506972,9 | 11+25+22       | = 185 29 37 .941                   |                    |  |  |  |  |  |  |
|                            | Equa              | tions to be satisfied      |                |                                    | Factor.            |  |  |  |  |  |  |
| $x_{13} + x_{14}$          | $+ x_{15}$        | ••• •••                    | =              | $= e_1 = .000,$                    | λ                  |  |  |  |  |  |  |
| $x_{10} + x_{11}$          | $+ x_{12}$        | ••• •••                    | =              | $= e_{g} = \cdot 000,$             | $\lambda_2$        |  |  |  |  |  |  |
| $x_{25} + x_{26}$          | + x <sub>27</sub> | ••• •••                    | =              | $= e_3 = .000,$                    | λ                  |  |  |  |  |  |  |
| $x_{23} + x_{23}$          | $+ x_{24}$        | ••• •••                    | =              | $= e_4 = .000,$                    | λ                  |  |  |  |  |  |  |
| $x_{13} + x_{10}$          | •••               | ••• •••                    | =              | $= e_{s} = - \cdot 0.000,$         | λ <sub>5</sub>     |  |  |  |  |  |  |
| $x_{11} + x_{25}$          | + x <sub>22</sub> | ••• •••                    | =              | $= e_6 =080,$                      | <b>λ</b> 6         |  |  |  |  |  |  |
| $13 x_{15} - 18 x_{14}$    | $+ 18 x_{19} -$   | -11 x <sub>11</sub>        | =              | $= e_7 = -7.1$                     | $\lambda_{\gamma}$ |  |  |  |  |  |  |
| $9 x_{10} - 18 x_{12}$     | $+ 8 x_{27} -$    | $+14 x_{26} + 17 x_{5}$    | $-12 x_{23} =$ | $= e_8 = - \cdot 6,$               | λ <sub>8</sub>     |  |  |  |  |  |  |

|                                      | Equations between the Factors                                                                                                                                                                           |    |               |         |                  |                          |                                  |                                 |                                                                                                                                                                       |                                                                                                                                                                                                                                                                                                               |                                                                                                                                                                                                                                                                                                                                                                                                                                         |
|--------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----|---------------|---------|------------------|--------------------------|----------------------------------|---------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| No. of                               | No. of Value of                                                                                                                                                                                         |    |               |         | Co-e             | fficient                 | ts of                            |                                 | Values of the<br>Factors                                                                                                                                              | Adopted Errors                                                                                                                                                                                                                                                                                                |                                                                                                                                                                                                                                                                                                                                                                                                                                         |
| e                                    | e                                                                                                                                                                                                       | λ  | $\lambda_{2}$ | λ       | λ4               | $\lambda_{\mathfrak{s}}$ | λ <sub>6</sub>                   | λ <sub>7</sub>                  | λ <sub>8</sub>                                                                                                                                                        |                                                                                                                                                                                                                                                                                                               |                                                                                                                                                                                                                                                                                                                                                                                                                                         |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8 | $ \begin{array}{r}         \cdot 000 \\         \cdot 000 \\         \cdot 000 \\         \cdot 000 \\         - 009 \\         - 080 \\         -7 \cdot 1 \\         - 6 \\         \cdot 6         $ | +3 | <br>+3        | <br>+ 3 | <br><br>+ 3<br>* | + 1<br>+ 1<br><br>+ 2    | <br>+ I<br>+ I<br>+ I<br><br>+ 3 | - 5<br>+ 7<br><br>- 11<br>+ 938 | $ \begin{array}{r} & & & & \\ & - & & & \\ & - & & & \\ & + & & 5 \\ & + & & 5 \\ & + & & 5 \\ & + & & 5 \\ & + & & 5 \\ & - & & & 3^{24} \\ & + & 1098 \end{array} $ | $\begin{array}{rcl} \lambda_{1} &=& + & \cdot 0130 \\ \lambda_{2} &=& + & \cdot 0880 \\ \lambda_{3} &=& + & \cdot 0359 \\ \lambda_{4} &=& + & \cdot 0436 \\ \lambda_{5} &=& - & \cdot 0906 \\ \lambda_{6} &=& - & \cdot 1203 \\ \lambda_{7} &=& - & \cdot 0103 \\ \lambda_{8} &=& - & \cdot 0021 \end{array}$ | $ \begin{array}{rcl} \mathbf{x}_{10} = -" \cdot 021 & \mathbf{x}_{22} = -" \cdot 077 \\ \mathbf{x}_{11} = + \cdot 081 & \mathbf{x}_{23} = + \cdot 069 \\ \mathbf{x}_{12} = - \cdot 060 & \mathbf{x}_{24} = + \cdot 008 \\ \mathbf{x}_{13} = - \cdot 078 & \mathbf{x}_{25} = - \cdot 084 \\ \mathbf{x}_{14} = + \cdot 198 & \mathbf{x}_{26} = + \cdot 065 \\ \mathbf{x}_{15} = - \cdot 120 & \mathbf{x}_{27} = + \cdot 019 \end{array} $ |

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The Eastern Sind Meridional Series. Final Figural Adjustments of the Non-Circuit Triangles.

Figure 8.

|                                                                                                                                     |                                                    |                                                  |                                                 |                                                                                                 |                                               |                                                                                                                                        |                                         | Cons                                       | Triangles                       | 56 to 59.                                                                                  |                                                                                                                                 |                                                                     |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                                      |                                                                                                                                                                                |                                                                                                                  |
|-------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------|--------------------------------------------------|-------------------------------------------------|-------------------------------------------------------------------------------------------------|-----------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------|--------------------------------------------|---------------------------------|--------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------|
| Constants (from page 200).XXXItoXXXIIILog. feet $4.8774718.9$ 4+7XXXIII,,XXXVI,, $4.8098816.6$ 9+16+19XXXVI,, $4.7662962.0$ 9+16+19 |                                                    |                                                  |                                                 |                                                                                                 |                                               |                                                                                                                                        |                                         |                                            | ined A<br>= 1<br>= 1            | Angles.<br>5 <sup>8°</sup> 49<br>80 51                                                     | 213 <sup>**</sup> ·493<br>16 ·240                                                                                               |                                                                     |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                                      |                                                                                                                                                                                |                                                                                                                  |
| . 2                                                                                                                                 | X4<br>X7<br>X18<br>X19<br>X4<br>X9<br>2 X5<br>6 X7 |                                                  | +<br>+<br>+<br>+<br>+<br>+<br>+<br>+<br>-<br>16 | X <sub>5</sub><br>X8<br>X <sub>17</sub><br>X <sub>20</sub><br>X7<br>X <sub>16</sub><br>X6<br>X8 | +<br>+<br>+<br>+<br>+<br>+<br>1<br>+ 1<br>+ 2 | x <sub>6</sub><br>x <sub>9</sub><br>x <sub>18</sub><br>x <sub>21</sub><br><br>x <sub>19</sub><br>6 x <sub>8</sub><br>6 x <sub>17</sub> | Eq<br>                                  | uation<br><br><br><br><br><br><br><br><br> | to be sat                       |                                                                                            | <br><br><br>20 x <sub>21</sub>                                                                                                  |                                                                     | $e_1 = e_2 = e_3 = e_4 = e_5 = e_6 = e_7 = e_8 = e_7 = e_8 = e_7 = e_8 = e_7 = e_8 $ | =<br>=<br>=<br>=<br>=<br>+<br>=<br>+ | •000,<br>•000,<br>•000,<br>•000,<br>•036,<br>•010,<br>7•0,<br>5•6,                                                                                                             | Factor.<br>$\lambda_1$<br>$\lambda_3$<br>$\lambda_4$<br>$\lambda_5$<br>$\lambda_6$<br>$\lambda_7$<br>$\lambda_8$ |
| No. of<br>e                                                                                                                         | Value<br>e                                         | e of                                             | ]<br>λ <sub>1</sub>                             | Equati<br>A <sub>3</sub>                                                                        | ions bet<br>λ <sub>3</sub>                    | ween<br>Co-<br>λ <sub>4</sub>                                                                                                          | the Fact<br>efficient<br>λ <sub>5</sub> | tors<br>ts of<br>λ <sub>6</sub>            | λ <sub>7</sub>                  | λ <sub>8</sub>                                                                             | Values of<br>Factor                                                                                                             | the<br>s                                                            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | Ad                                   | lopted Erre                                                                                                                                                                    | ors                                                                                                              |
| 1<br>2<br>3<br>4<br>5<br>6<br>7<br>8                                                                                                | - · · · · · · · · · · · · · · · · · · ·            | 000<br>000<br>000<br>000<br>036<br>010<br>0<br>5 | +3                                              | <br>+3                                                                                          | <br>+3<br>*                                   | <br><br>+3                                                                                                                             | + I<br>+ I<br><br>+ 2                   | <br>+ 1<br>+ 1<br>+ 1<br>+ 1<br><br>+ 3    | + 6<br>0<br>0<br>- 16<br>+ 1252 | $ \begin{array}{r} - & 10 \\ + & 25 \\ - & 7 \\ + & 6 \\ - & 256 \\ + & 1538 \end{array} $ | $\lambda_1 = +$ $\lambda_2 = +$ $\lambda_3 = -$ $\lambda_4 = -$ $\lambda_5 = -$ $\lambda_6 = +$ $\lambda_7 = +$ $\lambda_8 = +$ | •0002<br>•0179<br>•0722<br>•039<br>•0463<br>•0566<br>•0076<br>•0064 | $\begin{array}{c} \mathbf{x_4} = \\ \mathbf{x_5} = \\ \mathbf{x_6} = \\ \mathbf{x_7} = \\ \mathbf{x_8} = \\ \mathbf{x_9} = \end{array}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        | -".0<br>+ .1<br>1<br>+ .0<br>+ .0    | $\begin{array}{cccc} 46 & \mathbf{x}_{16} \\ 67 & \mathbf{x}_{17} \\ 21 & \mathbf{x}_{18} \\ 10 & \mathbf{x}_{19} \\ 37 & \mathbf{x}_{20} \\ 47 & \mathbf{x}_{21} \end{array}$ | $= -" \cdot 016 = + \cdot 093 = - \cdot 077 = + \cdot 053 = + \cdot 079 = - \cdot 132$                           |

Figure 9.

|                                                                                                                                                                             |                                                                                             |                    |                                                                                               |                                                                                                      |                      | Т                            | riangles                          | 60 to 62. |                              |  |                                                                                        |                                                  |                                                                                        |
|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------|--------------------|-----------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------|----------------------|------------------------------|-----------------------------------|-----------|------------------------------|--|----------------------------------------------------------------------------------------|--------------------------------------------------|----------------------------------------------------------------------------------------|
| Constants (from pages 200 and 201).XXXV to XLLog. feet $4 \cdot 8632235,3$ Contained Angle.XL,,XLII,, $4 \cdot 7210583,2$ $16 + 13 + 10$ $= 187^{\circ} 58' 15'' \cdot 770$ |                                                                                             |                    |                                                                                               |                                                                                                      |                      |                              |                                   |           |                              |  |                                                                                        | <b>*</b> .770                                    |                                                                                        |
|                                                                                                                                                                             |                                                                                             |                    |                                                                                               |                                                                                                      |                      | Equations                    | to be sa                          | tisfied.  |                              |  |                                                                                        |                                                  | Factor.                                                                                |
| . 2                                                                                                                                                                         | x <sub>16</sub><br>x <sub>13</sub><br>x <sub>10</sub><br>x <sub>16</sub><br>x <sub>16</sub> | +<br>+<br>+<br>-1; | x <sub>17</sub><br>x <sub>14</sub><br>x <sub>11</sub><br>x <sub>13</sub><br>3 x <sub>17</sub> | $ \begin{array}{r} + & x_{1} \\ + & x_{1} \\ + & x_{1} \\ + & x_{1} \\ + & 20 \\ x_{1} \end{array} $ | 18<br>15<br>12<br>10 | <br><br>- 10 x <sub>14</sub> | <br><br>+ 5 <b>x</b> <sub>1</sub> |           | <br>. <b>x</b> <sub>11</sub> |  | e <sub>1</sub><br>e <sub>2</sub><br>e <sub>3</sub><br>e <sub>4</sub><br>e <sub>5</sub> | · 000,<br>· 000,<br>· 000,<br>+ · 102,<br>+ 6·8, | $egin{array}{c} \lambda_1 \ \lambda_2 \ \lambda_3 \ \lambda_4 \ \lambda_5 \end{array}$ |

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# INTRODUCTORY.

The Eastern Sind Meridional Series. Final Figural Adjustments of the Non-Circuit Triangles.

|                       | Equ                                                      | ations b       | etween t | he Facto       | rs                       |                                                                                |                                                                                                                                                    |                                                                                                                                                                                                                                                        |  |  |
|-----------------------|----------------------------------------------------------|----------------|----------|----------------|--------------------------|--------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--|--|
| No. of                | Value of                                                 |                | С        | o-efficier     | nts of                   |                                                                                | Values of the Factors                                                                                                                              | Adopted Errors                                                                                                                                                                                                                                         |  |  |
| е                     | e                                                        | λ <sub>1</sub> | λ        | λ <sub>3</sub> | λ,                       | λ                                                                              |                                                                                                                                                    |                                                                                                                                                                                                                                                        |  |  |
| 1<br>2<br>3<br>4<br>5 | $ \begin{array}{r}                                     $ | +3             | <br>+3   | <br>+3<br>*    | + 1<br>+ 1<br>+ 1<br>+ 3 | $ \begin{array}{c} + & 8 \\ + & 10 \\ - & 6 \\ \dots \\ + & 1256 \end{array} $ | $\lambda_1 = - \cdot 0367$<br>$\lambda_3 = - \cdot 0406$<br>$\lambda_3 = - \cdot 0091$<br>$\lambda_4 = + \cdot 0628$<br>$\lambda_5 = + \cdot 0059$ | $ \begin{array}{ll} x_{10} = +" \cdot 054 & x_{15} = +" \cdot 077 \\ x_{11} = - \cdot 074 & x_{16} = + \cdot 026 \\ x_{13} = + \cdot 020 & x_{17} = - \cdot 113 \\ x_{13} = + \cdot 022 & x_{18} = + \cdot 087 \\ x_{14} = - \cdot 099 & \end{array} $ |  |  |

Figure 9—(Continued).

| Figure | 10. |
|--------|-----|
|--------|-----|

|                                     |                          | Triangle 63.                     |                                                                                                   |
|-------------------------------------|--------------------------|----------------------------------|---------------------------------------------------------------------------------------------------|
|                                     |                          | Constants (from page 201).       | Contained Angle                                                                                   |
| XLIII to<br>XLII "                  | XLII Log. feet<br>XLIV " | 4·7593005,6<br>4·6644730,1 } 4+5 | $\dots = 78^{\circ} 28' 3'' \cdot 471$                                                            |
|                                     | Equations to be satis    | sfied.                           | Adopted Errors.                                                                                   |
| x <sub>3</sub><br>23 x <sub>3</sub> | $+ x_6 = -13 x_6 =$      | $e_1 =445$<br>$e_2 = -4.5$       | $\begin{array}{rcl} \mathbf{x_3} &=& - & \cdot 287 \\ \mathbf{x_6} &=& - & \cdot 158 \end{array}$ |

| L' 194/C 11. | Figure | 11. |  |
|--------------|--------|-----|--|
|--------------|--------|-----|--|

|                  | Triangles 04 and 00.                           |             |                                                          |                  |                            |                                                                                 |                          |                                                                                           |                                                                           |                                                      |  |  |
|------------------|------------------------------------------------|-------------|----------------------------------------------------------|------------------|----------------------------|---------------------------------------------------------------------------------|--------------------------|-------------------------------------------------------------------------------------------|---------------------------------------------------------------------------|------------------------------------------------------|--|--|
|                  | Constants (from page 201).<br>Contained Angle. |             |                                                          |                  |                            |                                                                                 |                          |                                                                                           |                                                                           |                                                      |  |  |
|                  | XLV<br>XLVI                                    | to X<br>"X  | LVI<br>LIX                                               | Log. feet        | 4·5506311,3<br>4·5709869,6 | }                                                                               | . 4                      | +7                                                                                        | 147° 19' 4                                                                | 14"· 161                                             |  |  |
|                  |                                                |             | •                                                        | Equati           | ions to be satisfi         | ed.                                                                             |                          |                                                                                           |                                                                           | Factor.                                              |  |  |
|                  | X4<br>X7<br>X4                                 | +<br>+<br>+ | - X <sub>5</sub><br>- X <sub>8</sub><br>- X <sub>7</sub> | + x<br>+ x       | 6 ····<br>9 ····           |                                                                                 |                          | $\begin{array}{ccc} \mathbf{e}_1 & = \\ \mathbf{e}_2 & = \\ \mathbf{e}_3 & = \end{array}$ | •000,<br>•000,<br>— •446,                                                 | $λ_1 \\ λ_2 \\ λ_3$                                  |  |  |
|                  | 17 x5                                          | -           | -11 x <sub>6</sub>                                       | + 14 X,          | 8 - 22 2                   | K <sub>9</sub>                                                                  | =                        | e <sub>4</sub> =                                                                          | + 29 · 8,                                                                 | $\lambda_4$                                          |  |  |
|                  | Equ                                            | ations b    | oetween t                                                | he Factors       |                            |                                                                                 |                          |                                                                                           |                                                                           |                                                      |  |  |
| No. of           | Value of                                       |             | C                                                        | o-efficients o   | f                          | Values                                                                          | of the                   | Factors                                                                                   | Ad                                                                        | opted Errors                                         |  |  |
| e                | e                                              | λ           | λ                                                        | λ <sub>3</sub>   | λ4                         |                                                                                 |                          |                                                                                           |                                                                           |                                                      |  |  |
| 1<br>2<br>3<br>4 | ·000<br>·000<br>- ·446<br>+ 29·8               | +3          | <br>+ :<br>*                                             | +1<br>3 +1<br>+2 | + 6<br>- 8<br><br>+ 1090   | $\begin{array}{c} \lambda_1 \\ \lambda_3 \\ \lambda_3 \\ \lambda_4 \end{array}$ | = +<br>= +<br>= -<br>= + | •0594<br>•1920<br>•3487<br>•0284                                                          | $     x_4 = -"' \cdot 2 \\     x_5 = + \cdot 5 \\     x_6 = - \cdot 2   $ | $\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$ |  |  |

The Eastern Sind Meridional Series. Final Figural Adjustments of the Non-Circuit Triangles.

Figure 12.

|                  |                                                                             |                            |                      |                                                                   | Triangles 6             | 6 and 67                                                             | <i>.</i> |                                                                                            |                                                                           |                                                                      |
|------------------|-----------------------------------------------------------------------------|----------------------------|----------------------|-------------------------------------------------------------------|-------------------------|----------------------------------------------------------------------|----------|--------------------------------------------------------------------------------------------|---------------------------------------------------------------------------|----------------------------------------------------------------------|
|                  |                                                                             |                            |                      | C                                                                 | Constants (fro          | om page                                                              | 202).    | Cor                                                                                        | tained Angle.                                                             |                                                                      |
|                  | XLVII<br>LI                                                                 | I to LI<br>"LIX            | Log                  | . feet 4.<br>" 4.                                                 | 5401566,3<br>7085244,3  | }.                                                                   | ••       | 18+10                                                                                      | $= 123^{\circ} 50'$                                                       | 22″ • 960                                                            |
|                  |                                                                             |                            |                      | Equatio                                                           | ns to be satis          | fied.                                                                |          |                                                                                            |                                                                           | Factor.                                                              |
|                  | x <sub>18</sub><br>x <sub>10</sub><br>x <sub>13</sub><br>10 x <sub>15</sub> | + x<br>+ x<br>+ x<br>-14 x | 14<br>11<br>10<br>14 | + x <sub>15</sub><br>+ x <sub>19</sub><br><br>+ 7 x <sub>18</sub> |                         | <br><br>22 x <sub>11</sub>                                           |          | $\begin{array}{cccc} = & e_1 & = \\ = & e_2 & = \\ = & e_3 & = \\ = & e_4 & = \end{array}$ | •000,<br>•000,<br>+ •218,<br>+60°3,                                       | λ <sub>1</sub><br>λ <sub>2</sub><br>λ <sub>3</sub><br>λ <sub>4</sub> |
|                  | Equ                                                                         | ations betwe               | en the l             | Factors                                                           |                         |                                                                      |          |                                                                                            |                                                                           |                                                                      |
| No. of           | Value of                                                                    |                            | Co-e                 | fficients of                                                      |                         | Valu                                                                 | es of t  | he Factors                                                                                 | Ad                                                                        | opted Errors                                                         |
| e                | e                                                                           | λ <sub>1</sub>             | λ                    | λ3                                                                | $\lambda_4$             |                                                                      |          |                                                                                            |                                                                           |                                                                      |
| 1<br>2<br>8<br>4 | ·000<br>·000<br>+ ·218<br>+60·3                                             | +3                         | <br>+3<br>*          | + I<br>+ I<br>+ 2                                                 | - 4<br>- 15<br><br>+829 | λ <sub>1</sub><br>λ <sub>3</sub><br>λ <sub>6</sub><br>λ <sub>4</sub> |          | + ·1861<br>+ ·4886<br>- ·2284<br>+ ·0825                                                   | $x_{10} = + \frac{w}{x_{11}} = -1 \frac{w}{x_{13}} = +1 \frac{w}{x_{13}}$ | $\begin{array}{llllllllllllllllllllllllllllllllllll$                 |

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# PART II.

# THE DETAILS OF THE OBSERVATIONS

AND

# THE FINAL RESULTS.

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# THE JODHPORE MERIDIONAL SERIES

AND OF

THE EASTERN SIND MERIDIONAL SERIES

OF THE

NORTH-WEST QUADRILATERAL.

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# JODHPORE MERIDIONAL SERIES

•

AND

# EASTERN SIND MERIDIONAL SERIES.



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# JODHPORE (JODHPUR) MERIDIONAL SERIES.

#### INTRODUCTION.

This chain of triangles is the eastern of two meridional series which were intended to fill up the space between the Gurhágarh Meridional Series in long. 75° and the Great Indus in long. 68°, and so complete the North-West Quadrilateral. From Calcutta westward to the Gurhágarh Meridional Series the meridional series were carried at intervals of one degree; but in filling up the remaining area two series  $2\frac{1}{2}$  degrees apart were considered sufficient; these series, however, were to be double throughout and to have an extended secondary triangulation between them.

On completion of the revision of the Great Arc Series from Bangalore to Bider, Lieutenant M. W. Rogers, R.E., and his establishment were transferred to Rajputana (Rájputána) to carry out this work. The Jodhpore Meridional Series emanates from the side Súnda (XLIV) to Bonik (XLI) of the Karáchi Longitudinal Series and closes on the side Kanda (XXI) to Kaimsir (XIX) of the Sutlej Series.

Lieutenant Rogers having detached Mr. Torrens to finish up the work remaining on

| Sea                                                    | ison ]         | 1872-7 <b>8.</b>      |                   |            |
|--------------------------------------------------------|----------------|-----------------------|-------------------|------------|
| P                                                      | BESO           | NNEL.                 |                   |            |
| Lieut. M. W. Rogen<br>8rd Grade.<br>Mr. W. C. Price. A | rs, R.         | E., Offg.<br>Survevor | . Dopu<br>. 1st G | ty Supt.,  |
| " C. P. Torrens,<br>" A. Bryson,<br>W. Oldham          | >><br>>><br>>> | ະ<br>ກ<br>ກ           | 8rd<br>4th        | ກ<br>ກ     |
| ,, w. Olulishi,                                        | "              | <b>3</b> 3            | Actt              | <b>)</b> 7 |

the Great Arc Series, Section 18° to 24°, proceeded with the remainder of the party by rail to Poona (Puna), where the office and heavy stores were left, and thence to Ahmedabad (Amdávád), which, owing to the destruction of several bridges on the Bombay and Baroda Railway and the consequent stoppage of traffic, was not reached until the end of November. Messrs. Price and Bryson marched

thence direct to the scene of operations, to inspect the country and commence the approximate work. Lieutenant Rogers visited Mount Abu, which it was intended to make the permanent recess quarters of the party, and marched thence vid Erinpura to aid the assistants in their selection of stations.

The country from the origin of the Series for about 60 miles is very favorable for triangulation, being generally flat with high isolated hills rising from it. The approximate series was soon sufficiently advanced to commence principal observations, and Mr. Oldham

having brought up the large theodolite (Barrow's 24-inch No. 2\*) from Ahmedabad, where it had been left in charge of the Executive Engineer, the measurement of the final angles was begun at Súnda (XLIV) of the Karáchi Longitudinal Series on the 31st January 1873 and proceeded with steadily until the beginning of April. Observations were taken at 14 principal stations, forming 15 triangles, which extended a distance of 95 miles. Lieutenant Rogers also took astronomical observations for the direct determination of azimuth at Thob (VIII), about 44 miles W.S.W. of the city of Jodhpore. The field operations were brought to a close at Dodo (x) on the 8th April 1873, and the party marched towards Ahmedabad in separate detachments, closing stations on the road, *i.e.*, building small rectangular pyramidal pillars over the upper marks to protect them from injury, and arrived at recess quarters in Poona on the 8th May.

Messrs. Price and Bryson made good progress in the approximate operations, Mr. Price having charge of the selection, and Mr. Bryson of the building of the stations. The total out-turn of approximate work for the season was the selection of 25 stations extending over a distance of 147 miles.

Mr. Torrens was employed on the Great Arc Series, Section 18° to 24°, and Mr. Oldham acted as Lieutenant Rogers' assistant in the office and observatory.

The country through which the season's operations were carried, is sandy and flat, with an elevation towards the east of about 700 feet, diminishing towards the west and the Lúni river to 300 or 400 feet. South of the Lúni small detached ranges and isolated hills are numerous: their sides are precipitous and covered with jungle, and many of them rise to a considerable height above the plain, several exceeding 2,000 feet. To the east, towards the Lúni, which flowing west across the Series turns south and skirts its western flank, the country becomes barren and sandy, with sand hills covered with low shrubs; water is scarce and brackish, and villages few and far between. The ranges disappear, and save sand hills, the country is level for 70 miles, as far as the Bálmír hills. North of the Lúni the country becomes still more sandy and desolate, and nearly all the water in the tract embraced by the Series is brackish. About 15 miles north of the Lúni and 20 miles from the east flank of the Series, is the city of Jodhpore, which lies at the foot of the hill on which the fort is situated and at its southern side: its greatest length from north to south is  $2\frac{1}{2}$  miles and its greatest breadth a of a mile. It is closed in on the north by the fort, and on the east, south and west by a high wall capable of mounting guns, and having six gateways. Jodhpore is a good specimen of a native city and is kept fairly clean: it possesses many wells and three tanks; one of the latter, which is artificial, is very fine and large, its bed and sides being of stone masonry.

The fort is built on a hill, the highest in the neighbourhood, rising 360 feet above the surrounding country. There are two roads leading up to it which unite a few yards from the gateway and turn a sharp corner before reaching the gate; both roads are well protected by guns. Besides this gate there are two others to be passed before the fort is gained—the first a small though strong one in a narrow pass between two rocks, and the second a large one approached by a steep ascent, well commanded by guns, and like the

<sup>\*</sup> For the description of this instrument vide Appendix No. 2, Volume II of the Account of the Operations, &c.

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outer one made difficult by being placed round a corner. Access to the fort from any other direction would be impossible, as the sides are sheer precipices from two to three hundred feet high. The country below is commanded on all sides by the guns of the fort, save one small eminence opposite the fort gate and within the outer line of fortification.

In October 1873, Lieutenant Rogers took furlough to England, and the charge of

Season 1873-74. PEBSONNEL. Lieut. J. Hill, R.E., Asst. Supt. 1st Grade. Mr. W. C. Price, Asst. Surveyor 1st Grade. , C. P. Torrens, , , 3rd ,, , W. Oldham, , , , 4th , the party was transferred to Lieutenant (now Major) J. Hill, R.E. Lieutenant Hill left Poona on the 1st November 1873 and marched to the first station of observation, having *en route* established his Head Quarters at Mount Abu. The country to be triangulated this season was a

sandy desert; and the difficulty of obtaining water and provisions soon began to make itself felt. By the kindness of the Jodhpore *Darbár* (Court), a *vakíl* (Agent) and staff of *sowárs* (mounted men), &c., was attached to the party as in the former season, and by their aid the difficulties of the country were successfully surmounted. Lieutenant Hill experienced delay from the cloudy and misty weather; he calculated that he lost 34 days in four months from this cause; however the work was pushed on vigorously by all concerned. The sand hills in the desert were generally flat-topped, low and of about equal altitudes, so that the advantages of a hilly country were lost and short sides were unavoidable. Observations were taken at 21 principal stations extending over a distance of 90 miles. The towns of Phalodi and Pokaran were fixed in position and height, and a considerable amount of secondary triangulation was accomplished.

The Superintendent having directed that three sets of observations for the determination of azimuth should be taken on the Series, at equal intervals between the Karáchi Longitudinal and Sutlej Series, astronomical observations were made at Jambo (xxvi) in lat. 27° 16'. Angular observations were closed at Harban (xxviii) on the 3rd April, and the party arrived at their recess quarters at Mount Abu on the 30th of that month.

During the season Mr. Price who was employed in laying out the approximate series in advance worked with great energy, and in spite of the difficult nature of the country, pushed on the work for 102 miles, selecting 21 stations.

Mr. Torrens was employed on secondary triangulation. Mr. Oldham assisted Lieutenant Hill as observatory recorder.

Captain Hill writes :--- "With the exception of the approximate work which extends "into Bickaneer (Bikaner), the field operations of the season were confined to the States of "Jodhpore and Jeysulmere (Jáisalmír). This season in the Jodhpore desert the triangulation "traversed a sandy country, but towards the close of the season the Series entered a part of "Jeysulmere where the ground is hard and strewn with dark, shining stones. The reflection "from these stones is something like the reflection from water, and for this reason vertical ob-"servations to certain of the heliotropes gave a good deal of trouble. Mirage was frequently "observable in the mornings, but, except in one or two instances, did not retard the work." "Throughout the country triangulated, and especially in Jeysulmere, water is scarce "and in general brackish. In many cases, according to the statement of the people, well water, "which is drinkable in the cold season, becomes actually poisonous in the hot weather. The "villages and wells are few and far between. The former generally consist of a collection of "circular wigwams, the inhabitants of which are a primitive, dirty and good humoured people, " but given to highway robbery and other forms of thieving. The wells are very deep, one at "the village of Akhadna near the station of Nok (xxx) in Jeysulmere, (said by the people to be "80 purush in depth) is 5 feet in diameter and 374 feet deep. The water arrived at after such a "laborious excavation was unfortunately bitter and quite unfit for use. The deepest well I "have seen is at the village of Bákri in Jodhpore; it has been bored through a rock and is 5 feet "4 inches in diameter and 450 feet in depth: its water is good. I know of no other well so "deep in Rajputana. The city of Jeysulmere, which was fixed this season, is much smaller "than that of Jodhpore, its reported number of inhabitants being 10,000; but from all I could "see and hear the place was once in a far more flourishing state; the ruins of its former great-"ness are yet to be seen. The water supply for the city is obtained from an adjoining lake; "when this fails, which is generally the case in June, good water has to be brought from a small "village, Kisamghát, which is about 3 miles distant. There are numerous wells in the city but "the water is not good. The city used to be closed in by a rampart, now useless, as the wall is "rapidly crumbling to pieces. The fort, once strong, is now in a dilapidated state and would "ill stand an assault; it contains no tanks but many wells. The Jain temples in the fort are "very fine, the carving in the stone being exquisite; in fact this may be said of most of the "houses in the city, the doors, windows and walls having more or less carving about them. "The greater number of the inhabitants who reside within the walls of the fort are Bhati "Rájputs and Jains, and are as a rule great opium eaters."

In November 1874, Captain Rogers having returned from furlough again took charge of the party and proceeded at once into the field to carry Season 1874-75. PERSONNEL. on the principal observations. These were commenced at Capt. M. W. Rogers, R.E., Offg. Dy. Supt., 3rd Capt. M. V. Aros-Grade. Mr. W. C. Price, Surveyor, 4th Grade. , C. P. Torrens, Asst. Surveyor, 3rd Grade. Nok (xxx) on the 17th December, and carried on without interruption. Work was closed at Bhulan (XLIX) on the 21st March, as the party had a long march across the desert to Mount Abu. During the season observations were taken at 25 principal stations and the Series was advanced 104 miles. The work lay chiefly in the States of Bickaneer and Jeysulmere whose darbárs afforded very great assistance to the party. Astronomical observations for the determination of azimuth were taken at Mugrala (XLIII) in lat. 28° 31'. The approximate series under Mr. Price was pushed on 64 miles and brought to a successful termination by junction with the Sutlej Series on the side Kanda (XXI) to Kaimsir (XIX), 17 stations being selected and built.

Mr. Torrens carried a minor series eastward to the city of Bickaneer, of which the height had not been fixed by the Gurhágarh Meridional Series. He effected a junction with the minor series emanating from the Gurhágarh, with very satisfactory results. He then returned to the main series, built small rectangular pyramidal pillars over the principal stations at which observations had been completed, and connected the town of Pungal and also the tri-

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junction pillar of the States of Bickaneer, Baháwalpur and Jeysulmere by a minor triangulation.

Mr. Prunty who had joined the party from the Computing Office at Dehra acted as observatory recorder.

Bickaneer is a fine city, built on a slightly elevated spot in the desert where the ground is hard, stony, and intersected by ravines. It has a wall  $3\frac{1}{2}$  miles in circuit wholly built of stone, in which are eight gates and three sally ports; the wall is from 15 to 30 feet high and in good repair, and has a ditch on three sides about 15 feet deep. There are many highly carved houses in the city and two imposing looking Jain temples. Water is plentiful from many very fine wells. The chief productions are sugarcandy and blankets, both of which are of a superior kind. The population is about 35,000. The fort of Bickaneer which contains the Mahárája's palace is about 300 yards N.E. of the city. The palace rises above the battlements which gives it an imposing appearance; it is 1,100 yards in circumference and has two gates, numerous bastions and a ditch all round.

Owing to the heavy rains of 1875 the return of men from leave and the collection of

Season 1875-76. PERSONNEL. Capt. M. W. Rogers, R.E., Dy. Supt., 3rd Grade. Mr. W. C. Price, Surveyor, 4th Grade. , C. P. Torrens, Asst. Surveyor, 3rd Grade. P. F. Prunty, , , 4th , stores for the party were much delayed and Captain Rogers did not leave Mount Abu until October 23rd. He however utilised his time by visiting Deesa and inspecting the Meteorological Observatory there and laying out a small triangulation to connect both it and the Telegraph Office with

the main triangulation of the Karáchi Longitudinal Series. After a long march the party reached the scene of operations on the 4th December. Observations were at once commenced and the 21 miles remaining to complete the Series were finished on the 3rd January 1876. After this the party marched westward to take up the Eastern Sind Series on the meridian of 70°.

Mr. Price was this year employed in selecting stations for the new series.

Mr. Torrens first took up the connection of Deesa (Dísa), on completion of which he commenced a minor series on the meridian of  $71^{\circ}$  15', starting from the Karáchi Longitudinal Series and effecting a junction in the vicinity of the town of Jeysulmere with a secondary series which had been extended to this place in the field season of 1873-74.

Mr. Prunty was employed for a month in connecting such of the Baháwalpur Revenue Survey stations as could be identified near the Series.

The Jodhpore Meridional Series is 310 miles in length, and with the exception of a small portion to the south of the river Lúni, it passes over a sandy tract of nearly utter desolation. On all sides nothing meets the eye for miles but sand-hills dotted here and there with tufts of coarse grass and stunted shrubs. These sand ridges vary from 20 to 200 feet in height and are sometimes 2 or 3 miles in length: they appear to be scattered on every side like the billows of the sea, but run generally in a N.E. and S.W. direction. The villages are few in number and consist of collections of squalid wigwams situated around spots where wells have been excavated. These are sometimes as much as 200 feet deep and often yield only brackish water; for the soil seems to be impregnated, although capriciously, with saline matter, and the water from a large number of the wells is more or less unfit for drinking purposes.

#### JODHPORE MERIDIONAL SERIES.

In the whole distance between the Lúni River and the Sutlej Series-250 miles-only one place. Phalodi, was met with which could be dignified by the name of a town, and but four which ranked as fair sized villages. There is not much difference in the degree of barrenness in the country traversed by the whole Series, but if any, the northern portion in Baháwalpur is the most sterile. There the Series passed over a length of 70 miles in which there were only three wells of drinkable water, and these were within a space of 10 miles. In Baháwalpur the sand hills grow smaller and fewer, and are replaced by long stretches of perfectly level hard clay like the beds of dried up tanks, separated by tracts of drifting sand, accumulating here and there into mounds; there is not a particle of vegetation save a few sparsely scattered Phog (Calligonum) bushes. However, for two or three months in the year the desert presents a cheerful appearance: each village has several hamlets, called *dhanis*, established where there is any hard soil capable of retaining water; in excavations made in this, water lodges for two or three months after the rains, and the inhabitants of the villages come to these to feed their flocks and herds on the freshly grown herbage, and to cultivate the few miserable fields which they have in the hollows between the sand hills. The rainfall is however very small, 4 or 5 inches; and the inhabitants have a hard struggle for life in respect to both food and water; their food they supplement with the seeds of various grasses, the principal of which is the bhurut. The grain of this grass is about the size of a pin's head and is enclosed in a prickly husk which causes a great deal of discomfort to both man and beast as it sticks in the clothes of the former and the hair of the latter and is very difficult to get rid of. Water is collected in receptacles called *tankas*, cylindrical reservoirs about 6 feet in diameter and 8 or 10 feet deep, coated with fine chunam. When full they are covered in with brushwood and mud and are not used until the well water fails or becomes brackish, as generally happens in the hot weather. When, as is often the case these tanks also fail, those who can afford it send for water 15 or 20 miles from the nearest fresh-water well, and the poorer drink the brackish water mixing it with a little dahi or curds.

Under these circumstances great care had to be taken to ensure a supply of wholesome water for the main camp and detached signal parties, and in many cases it had to be brought from upwards of 15 miles and sometimes over 20 miles, and even with all these precautions at times every one had to put up with brackish and hardly drinkable water; this was especially the case on the approximate series under Mr. Price, who, having to reconnoitre in parts concerning which no sure information could be got, had often to take with him a camel load of water and march on, not knowing when or where he might get a fresh supply. However every one bore with cheerfulness these privations when they occurred, and owing to the good arrangements for supplies &c., combined with the healthiness of the desert, there was but little sickness and the party lost but one man during the four years.

The most sterile part of the country, as mentioned above, crossed by the northern portion of the Series, is very near the district which at page  $xx_{IV}_{g}$  of the Introduction to the Jogi-Tila Meridional Series (see Synoptical Volume VI) is mentioned as having been visited by Lieutenant J. Tennant and Mr. J. W. Armstrong with a view to carrying that series south of the Sutlej. They found it impracticable without the arrangements which

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the experience of the Executive Officers of the Jodhpore Meridional Series had taught them to adopt, and moreover they experienced hindrance and opposition from the Baháwalpur Sardárs. It shows the improvement which has taken place in that country under the guardianship of Colonel Minchin, that, instead of opposition, Captain Rogers met with civility and help from every one, that all trouble as to carriage of water, provisions and materials for station building was taken off his hands, native officials vying with each other in aiding the survey operations. This was also the case, though perhaps in a lesser degree, in the States of Marwar (Márwár), Bickaneer and Jeysulmere, the darbárs of which gave great aid to the party. In fact without such assistance no series could have been taken across the desert except at an enormous expense.

The calculations of the triangulation of this Series having been carried up from the side of origin, Súnda-Bonik, of the Karáchi Longitudinal Series, to the terminal side, Kaimsir-Kanda, of the Sutlej Series, the following discrepancies were met with between the original values of the length and azimuth of the terminal side above named and those of the latitude and longitude of the terminal station Kanda, and the values of the same as derived from the Sutlej Series after the Simultaneous Reduction of the North-West Quadrilateral:---

| In | Logarithm of t | he side | in feet | ••• | ••• |   | 0.000,0123,4 = 1.8 inches per mile. |
|----|----------------|---------|---------|-----|-----|---|-------------------------------------|
| ,, | Latitude       | •••     | •••     | ••• | ••• | - | 0″.172                              |
| ,, | Longitude      | •••     | •••     | ••• | ••• | _ | 0 '121                              |
| "  | Azimuth        | •••     | •••     | ••• | ••• | - | 3 '216                              |

These discrepancies were treated as errors in the Jodhpore Meridional Series and were dispersed as described in Part I of this Volume.

The heights of the stations above mean sea level are entirely dependent on trigonometrical determinations, no line of spirit-leveling having been executed in the neighbourhood of this Series. The heights of the terminal stations, Kanda and Kaimsir of the Sutlej Series, as brought up by the Jodhpore Series, were in excess of the final values given in Volume IV of the *Account of the Operations*, §c., by 8.6 and 12.8 feet respectively. The mean difference 10.7 feet was treated as an error generated in the Jodhpore Series and was dispersed by simple proportion.

### Secondary Triangulation.

This may be divided into two classes :---

(1st). Secondary series of some length.

(2nd). Permanent marks intersected from the principal stations with the large theodolite or fixed by one or two triangles observed with a smaller instrument.

#### JODHPORE MERIDIONAL SERIES.

As already mentioned on page III, the intervals between the principal chains of triangles in this desert country were increased from 1° to  $2\frac{1}{2}$ °. This reduction in the amount of the principal required an increase in that of the secondary triangulation, otherwise a sufficient number of fixed points of reference would not be provided for topographical surveys; it was therefore decided to run a longitudinal chain of secondary triangles from the Indus to the Jodhpore Meridional Series, and also a meridional chain between it and the next intended principal series to the west, which should supply points in the southern and better inhabited portion of the country. In pursuance of this scheme the undermentioned secondary series were executed :—

The Bálmír and Jeysulmere Secondary Series. The longitudinal portion of this series, between the stations of Daichu (XIX), Jalora (XXI), and Ekka (XXIII) of the Jodhpore Meridional Series, and the city of Jeysulmere, was executed in the field season of 1873-74, and the meridional portion (which is double throughout) between the stations of Gangasára (LXV), Didáwa (LXII), and Támpi (LX) of the Karáchi Longitudinal Series, and the city of Jeysulmere, in the season of 1875-76. Both portions were executed by Mr. C. P. Torrens with a 10-inch theodolite by Troughton and Simms, and extend a distance of about 230 miles. The meridional portion passes through the district of Mallani which is well inhabited for that region, and fixes the town of Bálmír and many permanent marks. The whole chain has been treated as one series in the Synoptical Volume of this series and adjusted between the final position values of the principal stations of the Karáchi Longitudinal and Jodhpore Meridional Series.

The Bickaneer Secondary Series. This series was executed in the field season of 1874-75 by Mr. C. P. Torrens with a 10-inch theodolite, and emanates from the side Ronesar (XL) to Bithnok (XXXVIII) of the principal series, extends eastwards for about 45 miles, and closes on the side Bickaneer-Hethiári of the Bickaneer Secondary Series which extends westwards from the Gurhágarh Meridional Series (see Synoptical Volume IV). Thus the Jodhpore and Gurhágarh Meridional Series are connected by a longitudinal chain of triangles.

Mount Abu Secondary Triangulation. This was executed by No. 7 Topographical Survey Party, Rajputana Survey, under Captain G. Strahan, R.E., during the field season of 1869-70, and is based on the side Gúrá Sikkar-Súnda (XLII-XLIV) of the Karáchi Longitudinal Series. At the greater number of the stations, observations were taken with a 14-inch theodolite to luminous signals; but in a few cases, when an ascent was too steep and dangerous to carry up the large instrument, a 6-inch theodolite was employed: it will be seen that the summit of Mount Abu rises about 4,700 feet above the plain of Sirohee at the foot of the mountain. In 1876 Mr. Prunty connected the Hospital and the Survey Office at Mount Abu with the above triangulation, observations being taken with a 10-inch theodolite to luminous signals. The stations of this triangulation are in general marked with an engraved circle and dot and covered by a cairn of stones.

The remainder of the secondary triangulation was mainly executed *pari passi* with the principal series, by the measurement—with the large theodolite—of angles at the prin-

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cipal stations to the surrounding secondary stations, trijunction and Revenue Survey pillars and other prominent objects, the angles at the secondary stations being measured with smaller theodolites: in this way the positions of the following places of note were determined, the town of Erinpura, the fort of Jálor, the city of Jodhpore, the large village of Pungal and the towns of Mároth, Mírgarh and Maujgarh in Baháwalpur.

August, 1884.

MALCOLM W. ROGERS, R.E.



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#### EASTERN SIND MERIDIONAL SERIES.

#### INTRODUCTION.

The Eastern Sind is the western of the two meridional series which have been carried across the deserts of Rajputana (Rájputána) and Sind, between the Great Indus and the Gurhágarh Meridional Series.

The Series is double throughout and 240 miles in length: it originates from the side Rojhra (LXXV) to Sandohar (LXXVIII) of the Karáchi Longitudinal Series and after passing through the Thar and Párkar district of Sind, the eastern portion of the Khairpur State and the western portion of Jeysulmere (Jáisalmír), enters the Ubauro taluk of Shikárpur, its eastern flank stations being within the boundaries of the Baháwalpur State; it terminates on the side Dáowála (LXII) to Máchka (LIX) of the Great Indus Series. Operations were commenced in the field season of 1875-76, and continued the following year, but were suspended from 1877 to 1879, at first on account of the failure of the rains in 1877 which deprived the country of its natural water supply, and afterwards because Major Rogers's services were required with the Army in Southern Afghanistan. The Series was continued in 1879-80 and finally completed by Lieut.-Colonel Branfill in 1880-81.

With the exception of the last 50 miles of the Series on which Colonel Branfill used Troughton and Simms' 24-inch Theodolite No. 1, the observations were taken by Captain (now Major) Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

On the completion of the Jodhpore Meridional Series in January 1876, Captain Season 1875-76. PERSONNEL. Capt. M. W. Rogers, B.E., Offg. Dy. Supt., 8rd Grade. Mr. W. C. Price, Surveyor, 4th Grade. " C. P. Torrens, Asst. Surveyor, 3rd Grade. " P. F. Prunty " " 4th "

Unfortunately the River Indus had washed away several of the old stations about

#### EASTERN SIND MERIDIONAL SERIES.

the most convenient locality, so that Captain Rogers had to adopt a side west of the given meridian, intending to gradually work on to it and then turn southwards.

The country south of the Indus is quite flat and covered with dense tree and grass jungle and for four or five months in the year is inundated; it therefore became necessary in the 20 miles which intervene between the river and the sand hills to resort to ray-tracing and tower-building, and as this style of work was new to all the members of the party, the progress was in consequence slow. Eight stations were selected, advancing the Series to the the sand hills a distance of 24 miles. Two towers were built and 104 miles of rays cleared.

Mr. Price, who was to take up the selection of stations in the southern section, was delayed for a month owing to his camp being attacked by fever and having to go to Deesa (Dísa) for medical treatment, he then marched to the meridian of 70° on the Karáchi Longitudinal Series and commenced selecting and building. Mr. Price found the station Rojhra of the Karáchi Longitudinal Series in complete preservation, and the pillar at the station of Sandohar was also in good condition except that the upper mark was wanting. The neighbouring stations of Fulrár and Chánga were in ruins. He therefore based his work on the side Rojhra-Sandohar and rebuilt the stations Fulrár and Chánga as nearly on their old sites as possible making use of them to construct a hexagon about Sandohar. The elements for these stations given in the details of the Karáchi Longitudinal Series are therefore no longer applicable. He selected 24 stations and built eight, extending the Series 110 miles.

During this season there were no final observations taken, but the party was employed in pushing on the preliminary work in order to get a fair start for the next season.

(XXIV) on the 18th March up to which the weather had been very favourable for observations; after this, as is usual in the desert, high winds and duststorms commenced and made the observing difficult and tedious.

Twenty-six new principal stations were fixed, extending the Series 125 miles along the meridian. An azimuth was observed at Malar (XIV) to two circumpolar stars.

Mr. Price selected 21 new principal stations, advancing the Series 98 miles and completing its junction with the southernmost side of the work laid out by Captain Rogers during the previous season.

Mr. Torrens built 19 and closed 16 principal stations, and moreover did a good deal of work in identifying and fixing a number of stations of the Sind Revenue Survey. The construction of stations in the desert involved a large amount of trouble, owing to the difficulties of making good bricks and of transporting them, when made, to the sites where they were required.

The country through which the Series passed this season, in the district of Thar and

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INTRODUCTION.

Párkar, chiefly consisted of narrow sand hills sometimes of considerable height, running from south-west to north-east in perfectly parallel lines: they are higher and closer together than those in Rajputana, and their slopes are steep, cut up by ravines and covered with low thorn jungle. Travelling was thus rendered very tedious, the village tracks had to be followed and long detours made, 10 miles was a heavy march for laden camels, and much time was spent in moving from station to station. This season, for about 50 miles along the western side of the Series, the country was inundated and a vast expanse of water stretched as far as the eye could reach. The town of Umarkot, when visited was surrounded on two sides by water which came up to the base of the fort.

In the north of Thar and Párkar and the western portion of Jeysulmere a new phenomenon is met with. This is the draens or expanse of shifting sand, which occurs here and there amongst the desert sand hills and is often many miles in extent. These draens have no vegetation, and their surface is continually changing, the sand is in one place scooped out into funnel shaped hollows, and in another thrown up into beautifully rounded hills. They were only crossed, when unavoidable, and then the road had to be inspected and prepared beforehand, and five miles was a fatiguing march. It is a curious fact that in certain places in these draens there are wells of water on small pieces of hard ground, which seem to be spared by the overwhelming sand, and the water of which is invariably good. The draens are very numerous for some 75 miles north of parallel 26°. They impoverish the already sterile country, the acme of desolation being reached in eastern Khairpur and western Jeysulmere. There are no crops and the people live nearly entirely on milk in various forms; a little *bajri* and *mot* are however imported from Sind in exchange for sheep. The inhabitants say that the draens travel gradually northwards, but very slowly. Their summits rise to a considerable height, in many cases overtopping the sand hills: and it was a matter of considerable difficulty to arrange the Series so that the stations should not fall on them. In two cases this could not be avoided, and although all precautions for stability were taken in their construction, it is doubtful if they can remain for long. The villages are of the same description as those met with in other parts of the desert, and the majority of the houses are merely wigwams of brushwood; a house with mud walls is a rarity, and brick and stone are almost unknown. With the exception of Umarkot there is no place along the Series worthy of the name of a town. The villages are, nearly without exception, built on the summits of sand hills, and often at a great distance from their wells, which are in the The reason for this custom seems to be, that in the cold hollows between the hills. weather the tops of the sand hills are considerably warmer than the valleys where the cold is sometimes very great. The party experienced considerable trouble from the difficulty of procuring drinking water, especially on the eastern side of the Series, near the junction of the four States of Marwar (Márwár), Jeysulmere, Khairpur, and Thar and Párkar, where there is a tract of country 30 miles broad by 40 long without any drinkable water.

During the season of 1877-78 the operations of the Eastern Sind Meridional Series were suspended owing to the failure of the rains in Rajputana. Captain Rogers and his assistants, Messrs. Torrens and Prunty, were sent to carry on a survey across the Frontier in Beluchistan, whilst Mr. Price was sent to the Eastern Frontier Series in Burma.

#### EASTERN SIND MERIDIONAL SERIES.

During the season of 1878-79, Captain Rogers was sent as Survey Officer with the Army into Southern Afghanistan. Mr. Price remained with the party and continued the triangulation in Beluchistan, Mr. Torrens joining him after having completed some secondary triangulation to connect the main series with the Jeysulmere secondary series and reconnoitred the intended Schwán secondary series.

Having completed the operations on which he had been engaged in Southern Afgha-

nistan in connection with the military movements, Captain

Season 1879-80. PERSONNEL. Captain M. W. Rogers, R.E., Offg. Dy. Supt., Ard Grade.

Rogers returned to Sind to resume the principal and secondary triangulations which had been suspended in 1878 when war with Afghanistan was declared. On his Mr. W. C. Price, Surveyor, 4th Grade. ,, C. P. Torrens, Asst. Surveyor, 2nd Grade. return he was much delayed for want of transport, all available animals being required for the Army, and when he arrived at Hyderabad, Sind, where his principal instruments had been left in store, he was further delayed because no hammáls or bearers were to be obtained for the carriage of the large theodolite, all persons of this calling having either joined the Army or deserted the country through fear of being required to do so. Thus it was necessary to wait until bearers could be brought up from Poona (Púna) before operations could be commenced. This enforced delay was utilised in computing and projecting the series of triangles from Quetta to Kandahár the observations of which had been taken by Captain Rogers a few months before.

The amount of work remaining to be completed on the Eastern Sind Series would have been just possible to accomplish in a long field season and under a very favourable combination of circumstances, if the survey party were fresh and in full vigour after some months' residence in recess quarters: but it could hardly be expected from Captain Rogers and his party who had just returned from more than a year's continuous field service in Afghanistan and Beluchistan, and who were unable to commence their observations until late in the season.

Having obtained bearers from Poona, Captain Rogers left Hyderabad on the 7th January and marching through Sind and western Jeysulmere commenced observations at Ráviláhu (XXVI) on the 27th January; work was closed at Chauki (XXXV) on the 27th March, and the party marched to Reti on the Indus Valley Railway, and thence proceeded by rail and road to Dehra Dún. Fifty angles were observed at the stations, advancing the Series 64 miles: an azimuth was observed at Asu (xxx1) to two circumpolar stars.

The country through which the Series passed was much the same as described the last season, but draens were not met with outside the tract that lies between the meridians of 69° 15' and 79° 15' and the parallels of 26° and 27°. It was taken from the Amírs of Sind after the war of 1845 and given as a reward to the Maharáwal of Jeysulmere to whom it still belongs, it contains no towns of any size, and but three forts, two of which, Sháhgarh and Kháro, are of mud and in ruins, being rapidly buried by the desert sand; the third, Gotáru, is of brick and much larger; it contains two wells and is in fair repair, with two antiquated cannons on the ramparts.

#### INTRODUCTION.

Colonel Branfill having finished the principal triangulation in Southern India pro-

Season 1880-81. PERSONNEL. Lieut.-Col. B. R. Branfill, Dy. Supt., 2nd Grade. Mr. C. P. Torrens, Asst. Surveyor, 1st Grade.

ceeded from Bangalore to Sind, where on the 6th November he assumed charge of the Bombay Party formerly under Major Rogers, R.E.; it had been equipped for the field by Mr. Hennessey who had held temporary charge in addition to his other duties since Major Rogers' departure on furlough to Europe in April.

The southern portion of the country triangulated in this year was desert pure and simple, water having to be carried on camels many miles to each station. Then, as the boundary between the Baháwalpur desert and the valley of the Indus was approached, hills and long ridges of drift sand were met with, interspersed with stretches of low lying, alluvial flats, which are mostly dependent on rainfall for their supply of water, and are thus practically desert for the greater portion of the year: when rain does fall, grass and shrubs spring up and render these tracts good grazing ground for cattle and camels for a short time afterwards; to some of them the flood waters of the Indus find occasional access by the old river channels, the deeper parts of which contain water for several months after the subsidence of the annual inundation, and are thus natural reservoirs; they are locally called *dhauds*. Finally, the valley of the Indus was entered and the principal operations were brought to a close on two stations-Dáowála (LXII) and Máchka (LIX)-of the Great Indus Series, which had been established in the year 1859-60; this part of the country was covered with a dense growth of acacias and other trees, the clearance of the necessary rays through which was tedious and laborious.

The triangulation had already been designed and laid out by Major Rogers in 1876-77 in the form of a hexagon, a quadrilateral, and two pentagonal figures. Half the stations had been built; but three towers and as many platform stations remained to be completed, and 140 miles of line had to be cleared on the rays between the principal stations. The ray on the side, between the stations of Chauki (xxxv) and Trisingh (xxxviii) was found to have become blocked up by a moving sand hill during the interval of six months which had elapsed since the stations were last visited; but Major Rogers had fortunately anticipated that this might happen, and had taken observations at both the base stations to the forward station at the vertex of the first triangle; thus it only remained to measure the third angle, and the necessity for clearing a ray through the sand hill was avoided.

The terminal stations in the valley of the Indus, consisting of towers about 24 feet high, were found still serviceable, having been put in repair in 1876-77, but had both become deflected to some extent; it was thus necessary to enlarge the upper portions of the central shafts before the large theodolite could be plumbed over the mark-stone at the ground level.

The principal triangulation completed this season extended for a distance of 50 miles along the meridian, introducing 13 new stations. The vertical angles were observed with some trouble owing to variations in atmospheric conditions materially influencing the terrestrial refraction, which in several cases was found to be negative, to an average extent of an eighth of the contained arc, thus making signals at a distance of 10 miles appear to be as much as 14 feet below their actual position.

Observations for azimuth to circumpolar stars were taken at two stations on the

#### EASTERN SIND MERIDIONAL SERIES.

series, Vijnot (XLIV), and Dáowála (LXII) of the Great Indus Series.

Although so much of the country traversed by the Eastern Sind Meridional Series is a dreary wilderness of sand, it is not entirely devoid of interest, from the fact that it may only have become a desert in comparatively recent times, and being in a state of continual motion it is now probably spreading in the direction of the prevailing wind during the dry, hot season. That a part of the desert was not always so, appears from the existence of many ruined places and forts within its borders, and from the change of the bed of the river Indus from east to west within historic times. The westerly tendency of the river bed has been attributed to the natural "set" to the westward of a north to south flowing current in the northern hemisphere, due to the increasing velocity of diurnal rotation of the parallels which it successively crosses; but a more effective cause of change may be found in the prevalence of westerly or south-westerly over easterly or north-easterly winds, especially in the dry, hot months of March, April and May, when the sand of the river channel is transported continually to the eastward, tending to fill up the more easterly channels and to protect their eastern banks from erosion by the water of the ensuing inundation, besides going to increase the actual amount of drift sand in the desert to the eastward. However this may be, there is no doubt that many towns and villages have been deserted by the rivers which once watered them. The ruins of some of these and the traces of the river channels on which they were built are still met with, especially on the western and northern edges of the desert where the sand has not quite obliterated them; but most of them have probably been overwhelmed and lost in the ever moving flood of sand from the south-westward.

In the portion of Baháwalpur traversed by the Jodhpore Meridional Series the ruinous and nearly deserted towns of Maujgarh, Mírgarh and Mároth mark the course of the now non-existent Hurkaru river, and on the north of the Eastern Sind Series were met with the ruins of Vijnot and Sirwáhi (or Seoráe), the former of which is a collection of blackened mounds from 10 to 20 feet in height, consisting of the *débris* of bricks and pottery mixed with earth and comminuted pieces of charcoal, indicating the site of a considerable town extending over half a mile in length and nearly a quarter of a mile in width. Exclusive of suburban mounds the site now measures a mile and a half in circumference. The only tradition about Vijnot amongst the country folk is, that it was one of the five (or seven) chief cities of Sind in the early days before the Muhammadan conquest (711 A.D.). The place lies about half a mile east of the Reni nadi, an old channel of the river Indus, and about 4 miles south of the Reni station of the Indus Valley State Railway.

Sirwáhi, the site of a lofty fort close to a town which is also said to be one of the ancient fortified cities of Sind, is situated about five miles N.E. of Sabzalkot and 3 miles N.W. of the Walhár station of the Indus Valley State Railway in the Baháwalpur State. The fort is about a quarter of a mile in circumference and rises 50 feet above the great plain around it, whilst the mound on which the adjacent town stood is perhaps half to three quarters of a mile around and 20 to 30 feet high.

The calculations of the triangulation of this Series having been carried from the side of origin, Rojhra-Sandohar of the Karáchi Longitudinal Series, to the terminal side, Máchka-Dáowála of the Great Indus Series, the following discrepancies were met with



#### INTRODUCTION.

between the original values of the length and azimuth of the terminal side above named and those of the latitude and longitude of the terminal station Dáowála, and the values of the same as derived from the Great Indus Series after the Simultaneous Reduction of the North-West Quadrilateral:—

| In | Logarithm of | the side | ••• | ••• | = |   | 0.000,0074,2 = 1.1 inches per mile. |
|----|--------------|----------|-----|-----|---|---|-------------------------------------|
| ,, | Latitude     | •••      | ••• | ••• | = |   | o″·423                              |
| ,, | Longitude    | •••      | ••• | ••• | = | + | o '028                              |
| "  | Azimuth      | •••      | ••• | ••• | = | + | o '939                              |

These discrepancies were treated as errors in the Eastern Sind Meridional Series and were dispersed as described in Part I of this Volume.

The heights of the stations above mean sea level are entirely dependent on trigonometrical determinations, no line of spirit-leveling having been executed in the neighbourhood of this Series. The heights of the terminal stations, Máchka and Dáowála of the Great Indus Series, as brought up by the Eastern Sind Meridional Series, were in excess of the final values given in Volume III of the *Account of the Operations*, &c., by 5.0 and 0.3 feet respectively. The mean difference 2.7 feet was treated as an error generated in the Eastern Sind Meridional Series and was dispersed by simple proportion.

#### Secondary Triangulation.

The secondary triangulation executed in connection with the Eastern Sind Meridional Series may be divided into three portions.

(1st). Secondary Series of some length.

The Jeysulmere Secondary Series. The extension of the Jeysulmere chain of secondary triangles of the Jodhpore Series westward from the city of Jeysulmere to meet the principal triangulation of the Eastern Sind Meridional Series. This work was done by Mr. C. P. Torrens, Assistant Surveyor, 2nd Grade, in the field season of 1878-79. It is about 60 miles in length and extends from the side Asu-Maringra of the Eastern Sind Meridional Series to the side Jeysulmere-Thaiat of the Jeysulmere Minor Series, thereby establishing a secondary longitudinal series on the parallel of 27°, extending from the Jodhpore to the Eastern Sind Meridional Series.

The Sehwán Secondary Series. This series originates from the side Ramsar (xvi) to Patanawári (xviii) of the Eastern Sind Series and extends on the parallel of 26° 25' to the side Mírkhán (xii) to Bhit (x) of the Great Indus Series. It consists of 24 triangles extending over a direct distance of 154 miles. The whole of this series was the work of Mr. C. P. Torrens, in the field seasons of 1878-79, 1879-80 and 1880-81. The instrument used for the observations was a 10-inch theodolite; it gave very satisfactory results, the closing errors at the junction with the Great Indus Series being minute.

(2nd). Permanent marks intersected from the principal stations with the large theodolite or fixed by one or more triangles observed with a smaller instrument.

(3rd). In addition to these triangulations a considerable amount of secondary work was executed during the progress of the Series in order to fix all the stations of the Sind Revenue Survey which could be identified and which fell within the limits of the principal triangulation, also the boundary and junction pillars of the States of Marwar, Khairpur, Jeysulmere, Sind and Baháwalpur, and several forts which had once been important in that part of the country. Owing to the nature of the country and the innumerable sand hills, auxiliary stations had to be established in nearly every case. In the season of 1876-77 observations were taken with a 7-inch theodolite by Mr. C. P. Torrens, and in 1879-80 by Captain Rogers with the same instrument. Owing to the desert nature of the country the same dearth of intersected points prevails on this Series as was noticed on the Jodhpore Meridional Series.

MALCOLM W. ROGERS, R.E.

August, 1884.



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ALPHABETICAL LIST OF PRINCIPAL STATIONS.

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| Adori                            | •       | • ·      | •  |    |            | XI.        | Kundal                        | •          |                | •          |           |            | III.         |
|----------------------------------|---------|----------|----|----|------------|------------|-------------------------------|------------|----------------|------------|-----------|------------|--------------|
| Aukli                            | •       | •        | •  | •  | •          | LII.       | Loharan                       | •          | •              | •          |           | •          | XVI.         |
| Bhada .                          |         |          |    |    | •          | XLV.       | Loháwat                       | •          |                | •          |           |            | XXII.        |
| Bhádráian                        |         |          | •  |    | •          | <b>v</b> . | Malunga                       | •          |                |            |           |            | XV.          |
| Bhulan                           | •       | •        | •  | •  | •          | XLIX.      | Mandaula.                     |            |                | •          | •         |            | IV.          |
| Biili                            | •       |          |    | •  | •          | LVII.      | Mankasar                      | •          |                | •          |           |            | XXXVI.       |
| Bikampur                         |         |          | •  |    |            | XXXIII.    | Mansa                         | •          | •              | •          |           | -          | LIIL         |
| Bintli                           | •       | •        | •  | •  | •          | XXIX.      | Marot                         | •          | •              | •          | •         | •          | LIV.         |
| Bithnok                          | •       | •        | •  | •  | •          | XXXVIII.   | Modia                         | •          | •              | •          | •         | •          | XXXIX.       |
| Bouik                            | •       | •        | •  | •  | •          | XLI.       | Mongolia                      |            | •              |            | •         | •          | XXXI.        |
| (of the Karáchi Longit           | tudinal | Series). | •  | •  | •          |            | Mugrala                       | •          | •              | •          | •         | •          | XLIII.       |
| Borla                            | •       | •        | •  | •  | •          | IX.        | Nagar                         | •          | •              | •          | •         | •          | VI           |
| Borta                            | •       | •        | •  | •  | •          | Ι.         | Nok                           | •          | •              | •          | •         | •          | XXX          |
| Chamu                            | •       | •        | •  | •  | •          | XVII.      | Omlo                          |            | •              | •          | •         | •          | XXX.<br>XXIV |
| Daichu                           | •       | •        | •  | •  | •          | XIX.       | Pahusan                       | ۲          | •              | •          | •         | ۲          |              |
| Dhaul <b>a</b>                   | •       | •        | •  | •  | ٠          | II.        | Demolylicet                   | •          | •              | •          | •         | •          | T WITT       |
| Dodo                             | •       | •        | •  | •  | •          | Х.         | Paler Paler                   | <b>'</b> • | •              | •          | •         | <b>`•</b>  |              |
| Dugur                            | •       | •        | •  | •  | •          | XII.       |                               | •          | ·•             | •          | •         | •          |              |
| Ekka                             | •       | •        | •  | •  | •          | XXIII.     | Phogala                       | •          | ۰.             | <b>'•</b>  | <b>`•</b> | •          |              |
| Girondi                          | •       | •        | •  | •  | •          | XXXV.      | Phulasar                      | •          | •              |            | •         | ·•         | AAAIV.       |
| Habib                            | •       | •        | •  | •  | •          | XLVI.      | Randu                         | ·•         | ·•             | <b>`</b> ● | •         | •          | LIX.         |
| Harban                           |         | •        | •  | •  | •          | XXVIII.    | Ronesar                       | ••         | •              | ••         | ••        | ••         | XL.          |
| Hasan                            | •       | ÷        |    | •  | •          | LV.        | Sachu                         | ·•         | <b>'</b> •     | ••         | •         | ·•         | XLI.         |
| Jalora                           | •       | •        |    | •  |            | XXI.       | Samdari                       | ••         | •              | ·•         | ·•        | •          | VII.         |
| Jambo                            | •       | •        |    |    |            | XXVI.      | Sirad                         | •          | ••             | •          | •         | ••         | XXVII.       |
| Jodasar                          |         |          |    |    |            | XLII.      | Soma                          | <b>'</b> • | •              | ·•         | ʻ•        | ••         | L.           |
| Kaimsir                          |         | •        |    | -  |            | XIX.       | Sorau                         | ۰.         | ••             | ·•         | ·•        | ′ <b>•</b> | XX.          |
| (of the Sutlej Series).          | ·       | •        | •  | •  | •          |            | Sulkia Thalau                 | •          | ••             | •          | ·•        | ••         | XIV.         |
| Kanda<br>(of the Sutlej Series). | •       | .•       | •  | •  | . <b>•</b> | XXI.       | Sultán                        | ۰.         | ۰.             | •          | ••        | ۰.         | LVI.         |
| Karamala                         |         | •        |    | •  |            | XLVII.     | Súnda<br>(of the Karáchi Long | itudinal ( | ·.<br>Series). | ۰.         | ••        | ••         | XLIV.        |
| Ketu                             | •       | •        |    | •  | •          | XIII.      | Thob                          | •          | •              | •          | •         | •          | VIII.        |
| Khirsar                          |         | .•       | .• | .• | .•         | XLIV.      | Telu                          | •          | •              | •          | •         | •          | LI.          |
| Khirwa                           | •       | •        | •  | •  | •          | XXV.       | Uperthal                      | •          | •              | •          | •         | •          | XXXVII.      |

# NUMERICAL LIST OF PRINCIPAL STATIONS.

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|                           |               |          |          |   |    |                |                    |        |   |   |   |   | 76 11.            |
|---------------------------|---------------|----------|----------|---|----|----------------|--------------------|--------|---|---|---|---|-------------------|
| XLI<br>(of the Keréchi Le | •<br>maitudin | I Serie  | •<br>•). | ٠ | í. | Bonik.         | XXXI               | •      | ٠ | • | • | • | Mongolia.         |
| XLIV                      | , ng truu in  |          | •        | • | •  | Súnda.         | XXXII              | •      | • | • | • | • | Pabusar.          |
| (of the Karáchi La        | ongitudin     | al Serie | s).      | - |    |                | XXXIII             | ٠      | • | • | • | • | Bikampur.         |
| Ι                         | •             | •        | •        | • | •  | Borta.         | XXXIV              | •      | • | • | • | • | Phulasar.         |
| II                        | •             | •        | •        | ٠ | ٠  | Dhaula.        | XXXV               | ٠      | • | • | • | • | Girondi.          |
| III                       | ٠             | •        | •        | ٠ | •  | Kundal.        | XXXVI              | •      | • | • | • | • | Mankasar.         |
| .IV                       | •             | •        | •        | • | •  | Mandaula.      | XXXVII             | •      | • | • | • | • | Uperthal.         |
| V                         | •             | •        | •        | • | •  | Bhádrájan.     | XXXVIII            | •      | • | • | • | • | Bithnok.          |
| VI                        | •             | •        | •        | • | ٠  | Nagar.         | XXXIX              | •      | • | • | • | • | Modia.            |
| VII                       | •             | •        | •        | • | •  | Samdari.       | XL                 | •      | • | • | • | • | Ronesar.          |
| VIII                      | •             | •        | •        | • | •  | Thob.          | XLI                | •      | • | • | • | • | Sachu.            |
| IX                        | •             | . •      | •        | • | ٠  | Borla.         | XLII               | •      | • | • | • | • | Jodasar.          |
| X                         | •             | •        | •        | • | •  | Dodo.          | XLIII              | •      | • | • | • | • | Mugrala.          |
| XI                        | •             | •        | •        | • | •  | Adori.         | XLIV               | •      | • | • | • | • | Khirsar.          |
| XII                       | •             | •        | •        | • | •  | Dugur.         | XLV                | •      | • | • | • | • | Bhada.            |
| XIII                      | •             | •        | •        | • | •  | Ketu.          | XLVI               | •      | • | • | • | • | Habib.            |
| XIV                       | •             | •        | •        | • | •  | Sulkia Thalau. | XLVII              | •      | • | • | • | • | Karamala.         |
| XV                        | •             | •        | •        | • | •  | Malunga.       | XLVIII             | •      | • | • | • | • | Phogal <b>a</b> . |
| XVI                       | •             | •        | •        | • | •  | Loharan.       | XLIX               | •      | • | • | • | • | Bhulan.           |
| XVII                      | •             | •        | •        | • | •  | Chamu.         | L                  | •      | • | • | • | • | Soma.             |
| XVIII                     | •             | •        | •        | • | •  | Pelu.          | LI                 |        | • | • | • | • | Telu.             |
| XIX                       | •             | •        | •        | • | •  | Daichu.        | LII                | •      | • | • | • | • | Aukli.            |
| XX                        | •             |          |          | • |    | Sorau.         | LIII               | •      |   |   | • | • | Mansa.            |
| XXI                       | •             | •        | •        |   | •  | Jalora.        |                    |        | • |   | • | • | Marot.            |
| XXII                      | •             |          |          | • |    | Loháwat.       |                    | •      |   |   | • | • | Hasan.            |
| XXIII                     |               | •        |          | • |    | Ekka.          | LVT                | •      |   | - |   | • | Sultán.           |
| XXIV                      |               | •        |          |   |    | Omlo.          |                    | •      |   | • | - |   | Bijli             |
| XXV                       | •             | •        | •        | - |    | Khirwa.        |                    | •      | • | • |   |   | Panchkot.         |
| XXVI                      | •             | •        | •        | • | •  | Jambo.         |                    | •      | • | • | • | • | Bandu.            |
| XXVII                     | •             | •        | •        | • | •  | Sirad.         | TIX -              | •      | • | • | • | • | Kaimsir.          |
| XXVII                     | •             | •        | •        | • | •  | Harban         | (of the Sutlej Sen | ries). | • | • | • | • |                   |
| XXIX                      | •             | •        | •        | • | •  | Rintli         | XXI                | •      | • | • | ٠ | • | Kanda             |
| AAIA<br>VVV               | •             | •        | ٠        | • | •  | Nab            | (or the Sutley Ser |        |   |   |   |   |                   |
| АЛА                       | •             | •        | •        | • |    | TIOE.          | 1                  |        |   |   |   |   |                   |

#### DESCRIPTION OF PRINCIPAL STATIONS.

The Principal Stations of this Series consist of circular masonry pillars from 3 to 4 feet in diameter for the large Theodolite to rest on, and in general are surrounded by a platform of stones and earth, or sand, on which the observatory tent was pitched. In certain instances the sand hills, on which several of the stations fell, did not afford a satisfactory foundation for the pillars; and piles were driven deep down on which the foundations were laid and the pillars built so that their surfaces were nearly flush with the level of the hill top. When this was the case a platform was not always necessary. Being almost invariably on the highest accessible points the pillars rarely required to be raised more than 3 or 4 feet. They contain mark-stones placed vertically over one another, the uppermost being generally flush with the surface: over this a rectangular protecting pillar, bearing a sufficiently accurate mark for Topographical and Revenue Survey purposes—as shown at page 74 of Volume II of the "Account of the Operations, §c."—was erected after the completion of the observations.

The following descriptions have been compiled from those given by the officers who executed the Series. The orthography of such names of parganas, districts &c., as has been fixed by Government for Rajputana has been adhered to. A few details, such as the name of a village or pargana within which a station is situated, have been obtained from the returns furnished by the political authorities to whose charge the stations have been committed.

XLI.—(Of the Karáchi Longitudinal Series). Bonik Hill Station, lat. 25° 4′, long. 72° 54′—observed at in 1850 and 1873—is situated in a group of hills which are unconnected with the Aravalli range and lie 25 miles north of Mount Abu on the border of Marwar; pargana Jhara Kharul of the Sirohee territories. The station is fixed on the most prominent though not the most elevated hill of the group, being an acute peak crowned with large naked masses of granite of square outline. The platform is built upon and amongst these rocks, the upper surface of the pillar being 2 feet 9 inches below the highest one, viz., that towards the north-west angle of the platform.

The pillar, which is surrounded by a platform of the usual construction, is solid, and contains three marks, one at the surface, the others 1 foot and 3 feet below it, the last being at the level of the foundation. When visited in 1872 prior to the commencement of the Jodhpore Meridional Series, the station of 1850 was found intact. The azimuths and distances of the surrounding villages are:—Wáan 190°, at foot of hill; Barwára 325°, miles 2; Andor 356°, miles 2.5; Modoni (temple) 83°, miles 7.3.

XLIV.—(Of the Karáchi Longitudinal Series). Súnda Hill Station, lat. 24° 47', long. 72° 28' observed at in 1851 and 1873—is situated on an isolated group of hills, about 24 miles W. by N. of Mount Abu. The southern half of this group, known as the Nímbáj hills, from the town of Nímbáj, which lies at their foot, belongs to the Sirohee territories. The northern portion, including the hill of Súnda, after which the station is named, is in taluk Jálor of the Jodhpore territories. The ascent commences at the small village of Usmat on the eastern side of the hill.

The pillar, which is surrounded by a platform of the usual construction, is solid and contains three marks, one at the surface, the others 1.21 and 3.21 feet below it, the last being at the level of the foundation. When visited in 1872 prior to the commencement of the Jodhpore Meridional Series, the station of 1851 was found intact. The azimuths and distances of the surrounding villages are :---Warra 288°, miles 2.8; Víkanwa 240°, miles 4.7; Nímbáj (temple) 293°, miles 4.1; Rajiraua 155°, miles 6.0.

I. Borta Hill Station, lat. 25° 6′, long. 72° 23′—observed at in 1873—is on the highest part of a short range running N.E. and S.W., south of Borta village and 8 miles N.E. of Bhínmál, a large village. It is on the northern portion of the hill which is locally called Renáva. The road has been made from about a mile W. of the village and N.E. of the station. The station is in sub-division Bhínmál of taluk Jálor of the Jodhpore territories.

The pillar, which is surrounded by a platform of the usual construction, is solid and contains two marks, one level with the hill top on a very large stone, and the other at the surface of the pillar which is 3.10 feet high. The azimuths and distances of the circumjacent villages are :--Pádru 127°, miles 2.8; Borta 224°, miles 1.2; Ledramír 351°, miles 2.7.

II. Dhaula Hill Station, lat. 25° 15', long. 72° 42'—observed at in 1873—is situated on a small detached hill about 440 feet above the plain, the platform being on a mass of boulders on the eastern and highest portion. The hill, which is locally named Pansútia, is apparently a portion of the Ásarona hills, being the most southwesterly of all. The station derives its name from Dhaula village, in the lands of which it lies; it is in taluk Jálor of the Jodhpore territories. The large town and fort of Jálor are about 5.4 miles W.N.W. of the station.

The pillar, which is surrounded by a platform of the usual construction, contains two marks, the lower on the rock in sita, and the upper in the surface of the pillar, which is 2.75 feet high. The azimuths and distances of the circumjacent villages are :-Bhaugal 109°, miles 2.9; Dhaula 224°, mile 1.0; Narauáwa 346°, miles 1.4.

III. Kundal Hill Station, lat. 25° 29', long. 72° 22'—observed at in 1873—is on a hill locally called Waduwár and is on the peak which is the highest and most southerly, and most westerly but one, of a long range about 10 miles N. of the Sukri river, 16 miles N.W. of Jálor and 12 miles S. of Siwána village, extending in a curved line from Kanki to Mangi village. The hill on which the station is situated is about 14 miles S.W. of Kundal village from whence the ascent begins. It is in taluk Siwána of the Jodhpore territories. There is a higher hill, about 3 miles N., called Saura, or Mahádeo-ka-Bakra, which is the highest in that portion of the country.

The pillar, which is surrounded by a platform of the usual contruction, is solid and contains two marks, one on a huge boulder and flush with the surface of the hill, and the other at the surface of the pillar which is 3.33 feet high. The azimuths and distances of the circumjacent villages are :- Pádru 104°, miles 7.9; Kundal 171°, at foot of hill; Elana 301°, miles 8.5.

IV. Mandaula Hill Station, lat. 25° 25′, long. 71° 55′—observed at in 1873—is situated on a sand hill (locally called Ura) about 200 yards from the left bank of the Lúni river, and about two miles W. of the village of Mandaula. The station is in the lands of that village in taluk Maloni of the Jodhpore territories.

The pillar, which has no surrounding platform but is sunk so that its surface is level with the ground, is solid and contains two marks, one at the top and the other 3.25 feet below at the level of the foundation. The azimuths and distances of the cicumjacent villages are :--Harra 92°, mile 1; Koela 220°, miles 4; Mandaula 239°, miles 2.27.

V. Bhádrájan Hill Station, lat.  $25^{\circ}36'$ , long.  $72^{\circ}54'$ —observed at in 1873—is identical with the station of the same name of the Rajputana Topographical Survey. It is on the bastion of an old fort on the highest and most westerly peak of a small group of hills at the north-eastern foot of which lies the large village of Bhádrájan. The hill is locally called Dhumra and is in the Bhádrájan jágír, taluk Jodhpore, of the Jodhpore territories. The bastion on which the station is placed is 16 feet in diameter and the highest on the southern face of the fort.

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The pillar, which is surrounded by a platform of the usual construction, is solid and contains two marks, the lower on the rock *in sitú* and the upper in the surface of the pillar which is 3.17 feet high. The azimuths and distances of the circumjacent villages are :---Agalia 51°, miles 4.5; Ráma 186°, miles 4.1; Bhádrájan 270°, at foot of hill; and Koala 307°, miles 1.9.

VI. Nagar Hill Station, lat. 25° 47, long. 72° 12'—observed at in 1873—is situated on one of three peaks locally called Vauki Taunka, on the western portion of a long low range running east and west about 3 miles S. of Lúni river and 5 miles S.W. of Bálotra. The station derives its name from the village of Nagar which lies at the foot of the hill on the north. The hill is difficult of ascent; it is in sub-division Jasol, talúk Maloni of the Jodhpore territories.

VII. Samdari Hill Station, lat. 25° 49′, long. 72° 37′—observed at in 1873—is on a small isolated, irregularly shaped hill locally named Mátalalasi, on the north bank of the river Lúni and close to the large village of Samdari, in taluk Siwána of the Jodhpore territories.

The pillar, which is surrounded by a platform of the usual construction, is solid and contains three marks, one in the foundation, 2 feet below the ground, another flush with the hill top and the third on the surface of the pillar; the difference of height between the upper and lower marks is 3.13 feet. The azimuths and distances of the circumjacent villages are :- Devalihari 66°, miles 1.7; Mokrundi 180°, miles 2.25; Deopura 243°, miles 2.1; and Kømáwas 335°, miles 2.6.

VIII. Thob Hill Station, lat. 26° 3′, long. 72°, 25′—observed at in 1873—is on a low hill, about half a mile W. of the large village of Thob and 10 miles N. of Pachbudra village, in taluk Siwána of the Jodhpore territories. There is a well of fairly good water near the village.

The pillar, which is surrounded by a platform of the usual construction, is solid and contains two marks, one in the foundation, flush with the hill top and the other in the surface of the pillar which is 3 feet high. The azimuths and distances of the circumjacent villages are :--Havadhan Roáro 35°, miles 2.95; Thob 266°, mile 0.63; and Roáro 348°, miles 2.22.

IX. Borla Hill Station, lat. 26° 9', long. 72° 7'—observed at in 1873— derives its name from the local name of the sand hill on which it stands, and which is about 3 miles N.W. from the village of Lapúndra to the lands of which it appertains. It is in a desolate and barren country the nearest village being Lapúndra. Perao village lies to the N.E. distant 3.1 miles. The water of the villages is hardly drinkable, but a small supply for a short time may be obtained from the villagers' tanks. The station lies about 16 miles W. of Patodi in taluk Maloni of the Jodhpore territories.

The pillar, which is built on a foundation laid on wooden stakes driven into the ground which had previously been excavated to a depth of 4 feet, is solid and contains two marks, one in the foundation and the other in the surface of the pillar 3 feet above it. There is no platform.

X. Dodo Hill Station, lat. 26° 4′, long. 72° 51′—observed at in 1873—is on a flat rock to the west of higher but unsuitable rocks on the western side of a low irregular rocky hill about 20 miles south-east of Jodhpore, near the road from Jasol and Bálotra to Jodhpore. The hill is in the lands of Doda-Lonasar village in taluk Jodhpore of the Jodhpore territories. Water can be obtained up to the end of March from a tank  $\frac{1}{3}$  mile to the north.

The pillar, which is surrounded by a platform of the usual construction, solid and contains two marks, the lower on the rock *in situ* and the upper in the surface of the pillar 3.33 feet above it. The azimuths and distances of the circumjacent villages are :-Selawa 91°, miles 2.2; Lauowás 160°, miles 1.8; Kalijára 354°, miles 1.4; and Katowás 186°, miles 4.2.

XI. Adori Hill Station, lat. 26° 20′, long. 72° 23′—observed at in 1873—is on a small rocky hill about 300 feet above the level of the surrounding country and situated amongst the sand hills, between the villages of Shera and Sheráda. It is in the lands of Tína village in taluk Jodhpore of the Jodhpore territories.

The pillar, which is surrounded by a platform of the usual construction, is solid and contains two marks, the lower on the rock in sitil and the upper at the surface of the pillar which is 2.08 feet high. The azimuths and distances of the circumjacent villages are :--Shera 73°, miles 2.5; Tina 101°, miles 1.5; Sherada 263°, miles 2.0; and Soítra 328°, miles 4.0.

XII. Dugur Hill Station, lat. 26° 17', long. 72° 42'—observed at in 1873—is situated on a conical rocky hill, the northernmost of a range of isolated hills running north and south about 23 miles west of Jodhpore city. The ascent of the hill is from the village of Dugur. There is a tank of good water about  $\frac{1}{2}$  a mile from the hill. It is in taluk Jodhpore of the Jodhpore territories.



The pillar, which is surrounded by a platform of the usual construction, is solid and contains two marks, one on the rock *in situ* and the other on the surface of the pillar which is 1 foot high. The azimuths and distances of the circumjacent villages are :---Angolai 105°, miles 1.34; Batila 253°, miles 3.22; and Sironi 343°, miles 2.99.

XIII. Ketu Hill Station, lat. 26° 31′, long. 72° 33-observed at in 1873—is situated on a rocky hill, distant about 4 miles in an easterly direction from the village of Ketu, and about 3 miles in a westerly direction from the village of Belwa. It is in taluk Ketu of the Jodhpore territories. The water is good but scarce in the hot weather.

The pillar, which is surrounded by a platform of the usual construction, is solid and contains two marks, one on the rock *in situ* and the other at the surface of the pillar which is 3 feet high. Kirja village lies S. W. by W., at a distance of 10.7 miles.

XIV. Sulkia Thalau Hill Station, lat. 26° 31′, long. 72° 20′—observed at in 1873—is on the westernmost knoll of a range of sand hills, and is distant 2 miles to the N.E. from the large village of Sulkia Thalau in taluk Jodhpore of the Jodhpore territories. There is no good water near the station. The water in the village of Sulkia Thalau is brackish.

The pillar, which has no surrounding platform, but is sunk so that its surface is level with the ground, is solid and contains three marks, one at the bottom of the foundation, a second 2 feet above it, and a third in the surface of the pillar, which is 8.04 feet high. The azimuths and distances of the circumjacent villages are :--Loharan 205°, miles 10.5; and Kirja 825°, miles 8.5.

XV. Malunga Hill Station, lat. 26° 29', long. 72° 49'-observed at in 1874—is situated on a conspicuous conical-shaped rocky hill which rises to the height of 320 feet above the surrounding country. The small hamlet of Digari lies at its foot to the south-east, and the village of Malunga is distant 2.4 miles and 58° E. of S. The water at the village of Malunga is good. The station lies within the boundary of the village of Malunga, taluk Ketu of the Jodhpore territories.

XVI. Loharan Hill Station, lat. 26° 40′, long. 72° 25′—observed at in 1874—is situated on a low range of sand hills at a distance of  $\frac{1}{2}$  of a mile in a direction 22° E. of N. from the village of Loharan. It is within the boundary of the village of Loharan in taluk Ketu of the Jodhpore territories. There is no good water near the station.

The pillar, which is solid and 3 feet high, is built on a foundation 2 feet thick. There are three mark-stones, one at the bottom of the foundation, a second 2 feet above it and a third in the surface of the pillar. The sand had to be heaped up 1<sup>‡</sup> feet above the former hill top level, so as to form a platform flush with the upper surface of the pillar. The bearings and distances of the circumjacent villages are :---Kanudia W.N.W., about 4 miles; Laurta N.E., about 3 miles; and Daidu E.S.E., about 8 miles.

XVII. Chamu Hill Station, lat. 26° 40′, long. 72° 38′—observed at in 1874—is distant about 1 mile in a direction 42° E. of N. from the village of Chamu, and is situated on the highest sand hill in the vicinity of that village. It lies within the boundary of the village of Chamu in taluk Ketu of the Jodhpore territories.

The pillar, which is solid and 3 feet high, has been sunk so that its surface is level with the ground, and has been built on a circular foundation 6 feet in diameter and 1 foot in thickness, resting on wooden piles. It contains two marks, one at the surface and the other at the bottom of the pillar. Barnan village lies about 4 miles N.W.

XVIII. Pelu Hill Station, lat. 26° 49′, long. 72° 30′—observed at in 1874—is situated on a small sand hill, and is distant  $2\frac{1}{5}$  miles in a direction 30° E. of S. from the village of Pelu. It lies on the boundary between the villages of Pelu and Marla in taluk Ketu of the Jodhpore territories.

The pillar, which is solid and 3 feet high, has been sunk so that its surface is level with the ground and has been built upon a circular foundation 6 feet in diameter and 1 foot in thickness, resting on wooden piles. It contains two marks, one at the surface and the other at the bottom of the pillar. The azimuth and distance of Bákri village are 235°, miles 10°8.

XIX. Daichu Hill Station, lat.  $26^{\circ}$  49', long.  $72^{\circ}$  20'—observed at in 1874—is situated at the eastern extremity of a long range of sand hills, and lies about  $3\frac{1}{2}$  miles in a north-westerly direction from the large village of Daichu and 2 miles in a direction 7° 30' W. of N. from the village of Ságra. It is on the lands of the village of Daichu, in taluk Ketu of the Jodhpore territories.



The pillar, which is solid and 3 feet high, has been sunk so that its surface is level with the ground and has been built on a foundation 2 feet thick. It contains three mark-stones, one in the upper surface of the pillar, the second at the bottom of the pillar, and the third at the bottom of the foundation. The azimuths and distances of the circumjacent villages are :--Marla 149°, miles 4.7; and Koru 191°, miles 7.2.

XX. Sorau Hill Station, lat. 26° 50′, long. 72° 42′—observed at in 1874—is situated on the highest knoll of a rather elevated sand ridge, and is distant  $2\frac{1}{2}$  miles in a direction 68° E. of N. from the good sized village of Sorau. It is on the lands of the village of Sorau, in pargana Phalodi of the Jodhpore territories.

The pillar, which is solid and 3.08 feet high, has been sunk so that its surface is level with the ground, and has been built on a foundation 2 feet thick. It contains three mark-stones, one in the upper surface of the pillar, the second at the bottom of the pillar, and the third at the bottom of the foundation. The azimuth and distance of Bákri village are 138° 30', miles 5.5.

XXI. Jalora Hill Station, lat. 26° 58', long. 72° 25'—observed at in 1874—is situated on a rocky hill which has but a small elevation above the surrounding country. It is distant 2.7 miles in a direction 33° W. of S. from the village of Jalora, and is on the lands of that village in pargana Phalodi of the Jodhpore territories.

The pillar, which is surrounded by a platform of the usual construction, is solid and contains two marks, one in the surface and the other in the foundation 4 feet below. The azimuths and distances of the circumjacent villages are;—Koru 51°, miles 5 4; and Dhaiakor 328° 30′, miles 5 4.

XXII. Loháwat Hill Station, lat. 27° 0', long. 72° 36'—observed at in 1874—is situated on a conspicuous conical-shaped rocky hill which rises to a height of 250 feet above the rather elevated piece of country which immediately surrounds it. It lies in a direction 80° W. of N. from the Vishnui portion and 65° W. of N. from the Ját portion of the village of Loháwat, and is distant 2.4 miles from a point about half way between these parts of the village. It is within the boundary of the village of Loháwat in pargana Phalodi of the Jodhpore territories. Good water can be obtained from the village of Loháwat from a well 333 feet deep.

The pillar, which is surrounded by a platform of the usual construction, is solid, 3 feet high and contains two marks, one at its surface and the other at the bottom of the pillar. The azimuth and distance of Bákri village are 332°, miles 7.2.

XXIII. Ekka Hill Station, lat. 27° 6′, long. 72° 22′—observed at in 1874—is situated on the highest of a low group of sand hills and is distant 1·1 miles in a direction S.W. from the village of Ekka and 3·2 miles in a direction 36° W. of S. from the fort in the town of Phalodi. It is on the lands of the village of Ekka in pargana Phalodi of the Jodhpore territories.

The pillar, which is solid and 3 feet high, has been sunk so that its surface is level with the ground. It has been built on a foundation 1 foot thick which rests on piles driven into the sand. There are two mark-stones, one at the top and the other at the bottom of the pillar. The azimuth and distance of Mokheri village are 27° 30′, miles 2.4.

XXIV. Omlo Hill Station, lat. 27° 7', long. 72° 31'—observed at in 1874—is situated on a low stony hill and is distant 0.8 of a mile from the village of Omlo in a direction 31° W. of S. It is on the lands of the village of Omlo in pargana Phalodi of the Jodhpore territories.

The pillar, which is surrounded by a platform of the usual construction, is solid, 5 feet high and rests on a foundation 1 foot thick. It contains two marks, one at the top and the other at the bottom. The azimuths and distances of the circumjacent places are :--Phalodi town 100°, miles 7°3; and Kicham village 108° 15′, miles 4°1.

XXV. Khirwa Hill Station, lat. 27° 17′, long. 72° 24′—observed at in 1874—is situated on land of the village of Khirwa in pargana Báp of the Jeysulmere territories. The station is built on one of a group of sand knolls at a distance of about  $2\frac{1}{2}$  miles in a direction 65° 30′ E. of S. from the village of Khirwa.

The pillar, which is surrounded by a rough platform of sand covered with a layer of stones 1 foot thick, is solid and 8 feet high and has been sunk so that its surface is flush with the level of the platform. It has been built on a foundation 2 feet thick. It contains three mark-stones, one in the upper surface of the pillar, the second at the bottom of the pillar and the third at the bottom of the foundation. The azimuths and distances of the circumjacent places are :—Báp village of the Jeysulmere territories 180° 27', miles 6.64; Agar village of the Jodhpore territories 281°, miles 5.75; and Phalodi town of the latter territories 357° 30', miles 10.0.

XXVI. Jambo Hill Station, lat. 27° 16′, long. 72° 34′—observed at in 1874—is situated on a long sand ridge which runs in a N.E. and S.W. direction. It is distant 2.4 miles in a direction due south from the village of Jambo and is on the lands of Naneo village in pargana Phalodi of the Jodhpore territories.

The pillar, which is surrounded by a rough platform of sand covered with a layer of stones 1 foot thick, is solid and 3 feet high and has been sunk so that its surface is flush with the level of the platform. It has been built on a foundation 2 feet

thick. It contains three mark-stones, one in the upper surface of the pillar, the second at the bottom of the pillar and the third at the bottom of the foundation. The azimuths and distances of the circumjacent places are :—Phalodi town 45°, miles 13.75; Sawanti village 76° 30', miles 3; and Báp village of the Jeysulmere territories 125°, miles 12.2.

XXVII. Sirad Platform Station, lat. 27° 26', long. 72° 28'—observed at in 1874—is situated on an extensive flat, the soil of which is very hard and stony. It is on the lands of the village of Bara Sirad in pargana Nok of the Jeysulmere territories. The nearest village is Nauagaon, from which the station is distant 31 miles in a direction 50° E. of S.

The pillar, which is surrounded by a platform of the usual construction, is solid and 3.94 feet high, resting on a foundation 2 feet thick the upper surface of which is flush with the surface of the ground. There are three marks, one on the upper surface of a large stone in the bottom of the foundation, the second 7 inches above it and level with the surface of the ground, and the third in the upper surface of the pillar. The azimuths and distances of the circumjacent villages are;—Báp 54°, miles 6.0; and Sirad 169° 30′, miles 3.9.

XXVIII. Harban (or Ghatori Mál) Hill Station, lat. 27° 26', long. 72° 17'—observed at in 1874 is situated on a rocky hillock about 50 yards from which is another, surmounted by a stone pillar bearing an inscription. It is distant from Harban village 3.9 miles, in a direction 24° W. of N. It is on the lands of the village of Báp in pargana Báp of the Jeysulmere territories.

The pillar, which is surrounded by a platform of the usual construction, is solid and 3 feet high, resting on a foundation 2 feet thick. There are two mark-stones, one in the upper surface of the pillar and the other at the ground level. The azimuths and distances of the circumjacent villages are :--Sheora 211° 30', miles 8; Báp 299°, miles 8:3; and Mondáli 136° 30', miles 2:75.

XXIX. Bintli Hill Station, lat. 27° 26', long. 72° 39'-observed at in 1874—is named after some fields that are in its neighbourhood, and is built on the highest sand hill in that part of the country. The boundary between the Jodhpore and Jeysulmere states passes close to the station on its eastern side. The nearest village is Partáb Sing-ka-sirad from which the station is distant 6.3 miles in a direction 72° 30' E. of S. The station is on the lands of that village in pargana Nok of the Jeysulmere territories.

The pillar, which is surrounded by a rough platform of sand covered with a layer of stones 1 foot thick, is solid and 8 feet high and has been sunk so that its surface is flush with the level of the platform. It has been built on a foundation 2 feet thick. It contains three mark-stones, one in the upper surface of the pillar, the second at the bottom of the pillar and the third at the bottom of the foundation. The azimuths and distances of the circumjacent villages are;—Jambo in the Jodhpore territories 82°, miles 9.6; and Modia in the Jeysulmere territories 192° 30′, miles 12.0.

XXX. Nok Hill Station, lat. 27° 36', long. 72° 20'—observed at in 1874—is on the easternmost of a number of low sand knolls near the village of Nok. The knoll on which the station has been built is known as Mátá ji khejri-ka-dhúra. The station is on the lands of the village of Nok, from which it is distant 3.6 miles in a direction 45° 30' E. of N; pargana Nok of the Jeysulmere territories. The water obtained from its wells is good, and the supply never fails.

The pillar, which is surrounded by a rough platform of sand covered with a layer of stones 1 foot thick, is solid and 3 feet high, and has been sunk so that its surface is flush with the level of the platform. It has been built on a foundation 2 feet thick. It contains three mark-stones, one in the upper surface of the pillar, the second at the bottom of the pillar and the third at the bottom of the foundation. The azimuth and distance of Sheora village are 356° 30', miles 4.8.

XXXI. Mongolia Platform Station, lat. 27° 38', long. 72° 32'—observed at in 1874—is situated on a slight rise near the spot where the former hamlet of Mongolia once stood. The site of that village is still marked by a few plum and other trees. The nearest village is Girájsúr from which the station is distant 6<sup>‡</sup> miles in a direction 25° W. of S. The station is on the lands of Nok village in pargana Nok of the Jeysulmere territories.

The pillar, which is surrounded by a rough platform of sand covered with a layer of stones 1 foot thick, is solid and 3 feet high, and has been sunk so that its surface is flush with the level of the platform. It has been built on a foundation 2 feet thick and contains three mark-stones, one in the upper surface of the pillar, the second at the bottom of the pillar and the third at the bottom of the foundation. The azimuths and distances of the circumjacent villages are :-Sirad 21°, miles 11.6; Nokra 270° 30', miles 9.5; and Trijunction Pillar on Jodhpore, Bickaneer and Jeysulmere boundary 281°, miles 12.6.

XXXII. Pabusar Hill Station, lat. 27° 44', long. 72° 23'-observed at in 1874—is called after the village of that name which is distant 0.35 mile at an azimuth of 255°. It is on the northern end of a sand hill about 52.5 feet high terminating abruptly at the station. The path from Bikampur to Pabusar skirts its base. The village of Pabusar is very small and has a well of brackish water; fresh water comes from Nok. The vil-



lage of Kolasir a little larger lies about 5 miles to the E. The station is in that portion of pargana Nok which belongs to the Thakur of Bikampur in the Jeysulmere territories.

The pillar is 3 feet high having a foundation of 2 feet with three mark-stones, one at the bottom, another 1 foot above it and the upper one at the surface. No mention is made in the records of the existence of a platform.

XXXIII. Bikampur Hill Station, lat. 27° 43′, long. 72° 14′—observed at in 1874—is on the highest point of a sand ridge about 64.5 feet in height, the nearest village being Bikampur distant 4.9 miles at an azimuth of 131°. The fort, or Thakur's residence, built of white stone can be seen from the station. The water at Bikampur is brackish in the wells, a small quantity for drinking is stored in small excavations. The station is in the lands of the Thakur of Bikampur, in pargana Nok of the Jeysulmere territories.

The pillar is solid and 3 feet high exclusive of foundation, and has three mark-stones, one at the bottom, the second 9 inches above it and the third at the surface. No mention is made in the records of the existence of a platform. The bearings and distances of the circumjacent villages are :--Borono S.W., miles 8; and Charanala N.N.W., miles 8.

XXXIV. Phulasar Hill Station, lat. 27° 52′, long. 72° 22′—observed at in 1874-75—is named after a small village of Vishnu worshippers, which is distant 5.3 miles at an azimuth of 174°. There is a dry tank called Natheri about 1 mile south; and the station itself is on the highest sand hill in the vicinity. The only village seen is Phulasar. There is a well of brackish water at Phulasar but no good water nearer than Bikampur. The station is in the lands of the village of Gogaliala, belonging to the Thakur of Bikampur, in pargana Nok of the Jeysulmere territories.

The pillar, which is surrounded by a rough platform of sand and stones, is solid and 3 feet high exclusive of the foundation. It has three mark-stones, one at the base on a large stone, another 9 inches above it and the third at the surface. The approximate azimuths and distances of the circumjacent villages are ;—Charanala 81°, miles 6; and Gogaliala 47°, miles 9.

XXXV. Girondi Hill Station, lat. 27° 50′, long. 72° 32′—observed at in 1875—is on a high sand hill locally called Gadalet-ka-dhúra near the boundary of Jeysulmere. Girondi village is distant 1.72 miles at an azimuth of 336°. The station is in the lands of the village of Nok in pargana Nok, of the Jeysulmere territories. There are wells of brackish water at Girondi and drinking water can be obtained from the chunam tanks.

The pillar, which is surrounded by a rough platform of stones and sand, is 3 feet high with a foundation of 2 feet and has three mark-stones, one in the foundation, another 7 inches above it flush with the hill top and the third at the surface. The azimuths and distances of the circumjacent villages are :--Ghariala (which is visible from the station and is in the Bickaneer territories) 314°, miles 7.26; and Girajsar (approximately) 338°, miles 7.

XXXVI. Mankasar Hill Station, lat. 28° 0′, long. 72° 31′—observed at in 1875—is on a sand ridge 2 62 miles from Mankasar village which lies at an azimuth of 216°. All the villages about are small and have wells of brackish water, drinking water being obtained from tanks. Bangarsar is the nearest village for supplies. The station is on the lands of Nok village, in pargana Nok of the Jeysulmere territories.

The pillar, which is surrounded by a platform of stones and sand, is solid and 3.71 feet high with a 2 feet foundation. It contains three mark-stones, one at the bottom, another 2 feet above it flush with the hill surface and the third at the surface. The approximate azimuth and distance of Bangarsar village are 287°, miles 8 nearly.

XXXVII. Uperthal Hill Station, lat. 28° 0', long. 72° 17'-observed at in 1875-is on a very high sand hill called by the natives Uperthal from its being the highest in those parts; it is 170 feet above the plain to the east and commands a good view all round. The station is on the lands of Nok village, in pargana Nok of the Jeysulmere territories. The water at Goru is brackish.

The pillar is solid and 3.04 feet high exclusive of the foundation. It contains three mark-stones, one at the bottom, another 7 inches above it and the third at the top. The bearings and distances of the circumjacent villages are :-Goru (a Vishnu village) S.E., miles 1.16; Nargroh W., about miles 10; Phulasar S.S.E., miles 6; and Barsalpur the only large village N.N.W., miles 14.6.

XXXVIII. Bithnok Hill Station, lat. 27° 53' long. 72° 42'—observed at in 1875—is on the highest sand hill of a range running N. and S. locally called Gajath Thal a few hundred yards south of a cart track from Bithnok to Bagu village. Bithnok is a large village with good water. The station is in the lands of that village in pargana Magra of the Bickaneer territories.



XXXIX. Modia Hill Station, lat. 28° 15′, long. 72° 27′—observed at in 1875—is on a very conspicuous, high, long sand hill overlooking the country on all sides, 11.88 miles S.E. by E. of the large village of Barsalpur. There are no villages near, only dhanis, *e.i*, cold weather temporary villages; of these Modia is the nearest. The station is in the lands of the Rao of Barsalpur in pargana Nok of the Jeysulmere territories.

The pillar, which is surrounded by a paltform of sand, is solid and 4 feet in height above the ground and has three mark-stones, one in the lowest part of the foundation, the second 2 feet above it flush with the hill top and the third at the surface of the pillar. The approximate azimuths and distances of the circumjacent villages are :--Modia 29°, miles 2.82; Bhati Walla 59°, miles 5.61; and Bhim Walla 104°, miles 4.

XL. Ronesar Hill Station, lat. 28° 3′, long. 72° 44′—observed at in 1875—is on a high flat and extensive sand hill, not on the very highest point on account of the ray to Modia H. S. No villages are visible from the station. Water and supplies are scarce in the small villages around. The station is on the lands of the village of Ronesar in pargana Magra of the Bickaneer territories.

The pillar, which is surrounded by a platform of stones and sand, is solid and 3 feet high above the ground and has three mark-stones, one at the bottom of the foundation, the second 1 foot above it flush with the ground and the third on the top of the pillar. The approximate azimuths and distances of the circumjacent villages are :--Ronesar 314°, miles 6; and Angnu 180°, miles 6.

XLI. Sachu Hill Station, lat. 28° 15′, long. 72° 7′—observed at in 1875—is on a sand hill 183.9 feet high and 10.29 miles distant from the large village of Barsalpur to the N.N.W.: the cart track from thence to Sachu village runs about 1 mile S. of the hill. The station is on the lands of the village of Sachu which belongs to the Rao of Barsalpur in pargana Nok of the Jeysulmere territories. The well water at Sachu is drinkable.

The pillar, which is surrounded by a platform of stones and earth, is solid and 3.83 feet high with a foundation of 1 foot. There are three mark-stones, one at the bottom of the foundation, the second 11 inches above this flush with the hill top and the third at the surface of the pillar. Sachu village is distant 2.69 miles at an azimuth of 54°.

XLII. Jodasar Hill Station, lat. 28° 18', long. 72° 44'-observed at in 1875—is on a high sand hill called by the natives Keridi dhúra, and is 6.1 miles E. of the village of Jodasar and about 8 miles S.S.E. of Ramra village. The station is on the lands of Jodasar village which belongs to the Rao of Pungal in the Bickaneer territories. The water at Jodasar village is brackish. Good water has to be brought from Pungal which is 15 miles distant to the N.E.

The pillar, which is surrounded by a platform of stones and sand, is solid and 5.06 feet high with a foundation of 1.75 feet. It has three mark-stones, one on the top of the foundation, the second 2.64 feet above it and the third 2.42 feet above the second at the surface of the pillar.

XLIII. Mugrala Hill Station, lat. 28° 31', long. 72° 25'-observed at in 1875—is on a high sand hill called Mugrala. It is in the lands of the village of Akasar in the estate of the Rao of Pungal in the Bickaneer territories. The water at Akasar and Siasar is very brackish, at Balhar slightly better, at Rachni there is a small tank. Besides this there is no good water nearer than Bhiawala toba (tank), 24 miles distant to the N.N.W., in the Baháwalpur territories.

The pillar is solid and 5.17 feet high, with a foundation, which with the pillar contains 5 mark-stones, the first at the bottom of the foundation, the second 2 feet above it, the third 0.50 foot above the second, and flush with the hill surface, the fourth 2.50 feet above the third, and the fifth 2.67 feet above the fourth and flush with the upper surface of the pillar. The bearings and distances of the circumjacent villages are :—Akasar N.E., miles 4.8; Rachni S.W., miles 8.46; Balhar S., miles 8; and Siasar N.E., miles 10.

XLIV. Khirsar Hill Station, lat. 28° 30′, long. 72° 42′—observed at in 1875—derives its name from Khirsar village in the lands of which it lies in pargana Pungal of the Bickaneer territories. The hill slopes gently from the south and terminates abruptly to the north being there 186 feet above the adjacent plain. The path from Dattohar to Pungal runs south of the hill. The water of Khirsar village is brackish, drinking water comes from Pungal.

The pillar, which is surrounded by a platform of stones and sand, is solid and 5 15 feet high with a 1 foot foundation, and has three mark-stones, one at the top of the foundation, a second 2.54 feet above it and the third 2.60 feet above the second flush with the top of the pillar. The approximate bearings and distances of the circumjacent villages are :—Khirsar E. by S., miles 3.37; Dattohar S.W. by S., miles 10.05; Pungal E., miles 9.5; and Ramra S., miles 6 nearly.

XLV. Bhada Hill Station, lat. 28° 43', long. 72° 36'—observed at in 1875—is on the highest point of an extensive sand hill with many spurs. It is on the lands of Bhada village belonging to the Rao of Pungal



in the Bickaneer territories. The track from Pungal to Maujgarh is a little to the north. The water at Bhada is very brackish, at Bheria and Siasar slightly so.

The pillar, which is surrounded by a platform of stones and sand, is solid, 3 feet high with 1 foot foundation and has two mark-stones, one on the top of the foundation flush with the hill top and the second 3 feet above it at the surface of the pillar. The azimuths and distances of the circumjacent places are :--Bhada village 8°, miles 2.90; Siasar village (approximately) 45°, miles 8 nearly; and Bheria well 273°, miles 6.40.

XLVI. Habib Hill Station, lat. 28° 44', long. 72° 23'—observed at in 1875—is on a low flat-topped hill in the desert near no village. The station is in the lands of the village of Maujgarh (24 miles N.N.W.) in thána Maujgarh, pargana Khairpur of the Baháwalpur territories.

The pillar is solid and 5.33 feet high exclusive of a 2 feet foundation and has three marks, one on the top of the foundation flush with the hill top, the second 2.33 feet above the first and the third at the surface of the pillar 3 feet above the second. The boundary between Bickaneer and Baháwalpur runs near the station and the nearest visible boundary pillars have the following azimuths and distances :---No. 1, 299°, mile 0.89; No. 2, 270°, miles 1.13; No. 3, 242°, miles 3.23. The approximate bearings and distances of neighbouring places are :---Bhiawala toba (tank) N.N.W., miles 8; and Bhaian-kí-verah (well) S.E., miles 9.

XLVII. Karamala Hill Station, lat. 28° 45′, long. 72° 48′—observed at in 1875—is on a hill which rises gradually from the well at Karamala village, the water of which is slightly brackish. It is on the lands of that village which belongs to the Rao of Pungal in the Bickaneer territories.

The pillar, which is surrounded by a platform of stones and saud, is 3 feet high with 1 foot foundation and has two markstones, one on the top of the foundation flush with the hill surface and the second 3 feet above it at the surface of the pillar. The approximate bearings and distances of the following places are :--Alden-ki-verah (well) S., miles 6 nearly; Naishera S.S.W., miles 8; Karamala well S.W., mile 0.68; and Rakasam well E. by S., mile 0.97.

XLVIII. Phogala Hill Station, lat. 28° 51′, long. 72° 28′—observed at in 1875—is on a low sand hill called either "Tappiwala dhúra" or Phogala from the numerous Phog trees on it. It is in the desert in the lands of Bhiawala village in thána Maujgarh of the Baháwalpur state and pargana. There are a number of small tanks in the neighbourhood which dry up about January.

The pillar is solid and sunk in the ground so that its top is flush with the hill surface: it has two marks, one at the surface of the pillar and a second 4.25 feet below it, on the second lowest course of bricks. The Bickaneer and Baháwalpur boundary runs near the station, the three nearest visible boundary pillars have the following azimuths and distances :-- No. 1, 356° 51′, miles 3.78; No. 2, 348° 33′, miles 3.64; No. 3, 3° 33′, miles 4.01. Bhiawala toba (tauk) is 8 miles W., and Maujgarh 20 miles N.W.

XLIX. Bhulan Hill Station, lat.  $28^{\circ}$  57', long.  $72^{\circ}$  41'—observed at in 1875—is on a rising ground 4 miles S.S.W. of Bhulan tank and about  $\frac{1}{2}$  mile S.S.W. of Karamala small tank (both dry in February) in the heart of the desert. It is on the lands of Bhulan hamlet thána Marot; pargana Khairpur of the Baháwalpur territories.

The pillar, which is surrounded by a platform of sundried bricks and sand, is solid and 3 feet high having three marks on bricks, one at the very bottom of the foundation, one 2 feet above it flush with the surface of the hill and the third 3 feet above the second, at the surface of the pillar. Three of the pillars on the boundary of Bikaneer and Baháwalpur have azimuths and distances as follows:—No. 1, 340° 47', miles 2.39; No. 2, 316° 54', miles 2.38; and No. 3, 1° 15', miles 2.78. Mírgarh village lies 15 miles N.; Phulera 15 miles N.E.; and Sakhi in Bickaneer 14 miles E., the three nearest places at which drinkable water can be obtained.

L. Soma Hill Station, lat. 29° 2′, long. 72° 30′—observed at in 1875—is on a small mound on the highest sand hill 5 88 miles, 23° E. of S. of Soma well hamlet and about 5 miles E.S.E. of Jalalsar well hamlet and about 10 miles S. of Marot town. The path from Marot to Pungal in Bickaneer passes about a mile and a half E. of the hill. The station is in the lands of Soma hamlet; thána Marot, pargana Khairpur, in the Baháwalpur territories. The water at Soma and Jalalsar is undrinkable; all supplies of water are got from Marot.

The pillar, which is surrounded by a platform of sundried bricks and sand, is solid and 3.15 feet high with a foundation of 1.75 feet; it has three marks, one at the bottom of the foundation, another 1.75 feet above it and the third 3.15 feet above the second, at the surface of the pillar.

LI. Telu Hill Station, lat 28° 56′, long. 72° 17′—observed at in 1875—is on a sand rise of ground hardly to be called a hill, about 6 miles N. of Bhiawala tank and 7.77 miles S.E. of Maujgarh town. There are two old mud towers near Telu from which the station takes its name, distant 0.55 of a mile at an azimuth of 86° 16′. It is in thana Maujgarh, pargana and state Baháwalpur. Water is obtained from either Bhiawala or Maujgarh.

The pillar, which is surrounded by a platform of sundried bricks and sand, is solid and 5 feet high with a 2.5 feet foundation. There are three mark-stones, one at the bottom of the foundation, the second 2½ feet above it flush with the hill top and the third 5 feet above the second at the surface of the pillar. The azimuth and distance of Gidarwala village are 180° 45', miles 2.37.

LII. Aukli Hill Station, lat. 29° 4′, long. 72° 40′—observed at in 1875—is on a black looking hill with plenty of shrubs on the top, about 5 miles N.W. of Bhulan tank which dries up in January, in pargana Khairpur, thána Marot, and state Baháwalpur. Water is brought from Mírgarh.

The pillar, which is surrounded by a platform of sundried bricks and sand, is solid and 3.52 feet high having three mark-stones, one at the bottom of the pillar, a second 2.46 feet above it and flush with the hill top, and the third 1.06 feet above the second at the surface of the pillar. The azimuths and distances of the circumjacent places are :--Jamgarh 144° 58', miles 8.2; Mirgarh 177° 38', miles 7.2; and Kheniwala Thul (an old mud tower) 196° 25', miles 4.25.

LIII. Mansa Hill Station, lat. 29° 5′, long. 72° 17′—observed at in 1875—is 2 miles E. of a higher sand hill called by this same on a loose, shifting sand knoll, having no vegetation on the top, but being the best procurable. The country here is more or less a plain, with small rises and gentle slopes. The station is in the lands of Chápu village; in thána Maujgarh, pargana and state Baháwalpur. Water is obtained from Kundai wells 3 and 4 miles east and from Chápu village.

The pillar, which is surrounded by a platform of sundried bricks and sand, is solid and sunk into the hill. It is 5.08 feet high, with three mark-stones, one at the bottom, a second 2.62 feet above it and the third 2.46 feet above the second at the surface of the pillar. The approximate bearings and distances of the circumjacent places are :---Maujgarh town S.W., miles 8.2; Khirsar hamlet N.W., miles 4; and Chápu village N., miles 4.51.

LIV. Marot Station, lat. 29° 11′, long. 72° 29′—observed at in 1875—is on the fort on the highest mud bastion at the S.E. corner which is about 150 feet above the ground. The fort which is of mud, about 725 feet square is quite in ruins and the town lies partly within and partly without the walls. The bastion on which the station stands is of solid clay and is approached by a ramp. It is in pargana Khairpur of the Baháwalpur state. There are a tank and wells at this place.

The pillar is solid and has been sunk in the bastion; it is 4.25 feet deep with two marks, the lower at the bottom of the pillar and the upper 4.25 feet above it at the surface of the pillar.

LV. Hasan Hill Station, lat. 29° 14′, long. 72° 19′—observed at in 1875—is in the desert on a ridge called Hasanwala tibba the top of which is loose sand, 12.6 miles W. 20° N. of Marot town and about 6 miles N. of Chápu wells. The station is in the lands of Chápu village, thána Marot, division Khairpur, and state Baháwalpur.

The pillar, which is surrounded by a low platform of bricks and sand, is solid and 3 feet deep with 3 mark-stones, one at the bottom of the pillar, a second 2 feet above the first and a third (at the surface of the pillar) 1 foot above the second. The azimuths and distances of the circumjacent places are :-Bakshauwala hill (approximately) 180°, miles 2; Mashkiwali thul (deserted tower) 230°, miles 1 66; and Saduwala thul 297°, miles 3 nearly.

LVI. Sultán Hill Station, lat. 29° 9', long. 72° 13'-observed at in 1875—is on a sand hill locally named Sultánwala tibba, which is a mass of moving sand hills; but the station has been carefully built and it is anticipated that it may be permanent. The Marot-Baháwalpur track which is marked by pyramidal kacha pillars runs about 11 miles north; the nearest pillar—the 7th from Marot on the Revenue Survey maps—having an azimuth of 139° is distant 12 miles. The station is on the lands of Chápu and Khirsar villages in the Maujgarh thána, division and state Baháwalpur.

The pillar, which is surrounded by a platform of bricks and mud, is solid and 3 feet deep with two mark-stones, one in the foundation and the second 3 feet above it at the surface of the pillar which is flush with the surface of the hill. The bearings and distances of the circumjacent places are :—Khirsar hamlet and well S., miles 2; Chápu well E., about 5.5 miles; and Mauj-garh town S., miles 9.

LVII. Bijli Hill Station, lat. 29° 18', long. 72° 25'—observed at in 1875—is on a flat-topped sand hill called Bijli by the inhabitants and Jewunee on the Revenue Survey charts. It is in thána Marot, division Khairpur of the Baháwalpur state. It is about a mile east of the track from Marot to Khairpur. The nearest good well water is obtained from Marot.

The pillar, which is surrounded by a platform of sand and bricks, is 3 feet deep with 3 mark-stones, one at the bottom of the pillar, a second 1 foot above the first flush with the hill surface and a third 2 feet above the second and at the surface of the pillar. The bearings and distances of the following places are :---Mauri Rania temple (not visible) S.S.E., miles 3.50; Khandowala toba N.W. by N., miles 2.68; Marot town S., miles 10; and Khairpur town N., miles 21.



LVIII. Panchkot Hill Station, lat. 29° 16', long. 72° 10'—observed at in 1875—is on the highest portion of a flat-topped hill in the desert 18 miles S. of the Sutlej River, and is called after a toba or tank which is 0.65 of a mile distant at an azimuth of 345°. It is on the lands of Bhiawala toba (30 miles S.), thána Maujgarh, division and state Baháwalpur. When the tanks are dry the nearest good water is at Chápu about 12 miles S.E.

The pillar, which is surrounded by a low platform of bricks and sand, is solid and 3 feet high with 3 mark-stones, one at the bottom of the pillar, a second one foot above this flush with the hill top and a third 2 feet above the second on the surface of the pillar. Gharialwala toba lies to W., about miles 3.

LIX. Randu Hill Station, lat. 29° 19', long. 72° 18'—observed at in 1875—is on a flat-topped sand hill of the Kali Dhari range, the highest point of which is 3 miles to the east. It is in the heart of the desert, in the lands of the town of Khairpur, in division Khairpur, of the Baháwalpur state.

The pillar, which is surrounded by a platform of sand and bricks, is solid and 3 feet high with 3 mark-stones, one at the bottom of the foundation, a second 1.08 feet above it flush with the hill top and a third 1.92 feet above the second on the surface of the pillar. The bearings and distances of the following places are :--Kimsir well (good) N.W., miles 10; Naganiwala toba N., miles 2; Jamsar well (slightly brackish) N.N.E., miles 10; Ganiwala toba N.E., miles 3; Bahawala toba N.E., miles 4; Rohriwala N.E., miles 3.50; and Sera well (brackish) S.E., miles 8.

XIX.—(Of the Sutlej Series). Kaimsir Tower Station, lat. 29° 25', long. 72° 11'—observed at in 1862 and 1876—is situated in the Baháwalpur territories, and stands in the desert about 7 miles 8. of the village of Asrani. There is a well about 1<sup>±</sup> miles to the N.

The pillar is perforated, and 10.8 feet high. It has a mark-stone at level of ground floor. The station was visited in 1876 for the purpose of connecting the Jodhpore with the Sutlej Series and the mark-stone at the level of the ground was found intact.

XXI.—(Of the Sutlej Series). Kanda Tower Station, lat. 29°28', long. 72°22'—observed at in 1862 and 1875—is situated in the Baháwalpur territories, and stands in the desert about 10 miles S. E. of the town of Khairpur. There is a well about 2 miles to the W.

The pillar is perforated, and 20.4 feet high. It has a mark-stone at level of ground floor. The station was visited in 1875 for the purpose of connecting the Jodhpore with the Sutlej Series and the mark-stone on the level of the ground was found intact.

April 1878.

#### J. B. N. HENNESSEY,

In charge of Computing Office.

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### JODHPORE MERIDIONAL SERIES.

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# PRINCIPAL TRIANGULATION. OBSERVED ANGLES.

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### At XLI (Bonik)

February 1873; observed by Lieut. M. W. Rogers, R. E., with Barrow's 24-inch Theodolite No. 2.

| Angle                |                                          |                                    |                                                       | M - Mean of Groups                 |                                          |                               |                               |                                               |                                               |                                              |                                                                                                     |
|----------------------|------------------------------------------|------------------------------------|-------------------------------------------------------|------------------------------------|------------------------------------------|-------------------------------|-------------------------------|-----------------------------------------------|-----------------------------------------------|----------------------------------------------|-----------------------------------------------------------------------------------------------------|
| Angle<br>between<br> | 279° 1′                                  | 99°1′                              | <b>8</b> 58°18'                                       | 178° 18′                           | 77° 25′                                  | 257° 25′                      | 156° 37′                      | 286° 87′                                      | <b>235° 50</b> ′                              | 55 <b>°</b> 50′                              | w = Relative Weight<br>C = Concluded Angle                                                          |
| XLIV & I             | "<br>1 34 · 14<br>1 35 · 84<br>1 35 · 52 | "<br>2 36·24<br>2 36·70<br>2 36·26 | "<br>l 33 • 92<br>l 35 • 86<br>l 33 • 38<br>l 34 • 30 | *<br>2 35 48<br>2 35 24<br>2 35 56 | "<br>2 37 · 16<br>2 36 · 14<br>2 37 · 14 | l 36·48<br>l 36·92<br>l 35·92 | 2 35 22<br>2 35 74<br>2 35 42 | "<br>1 36·38<br>1 33·92<br>1 36·70<br>1 36·38 | n<br>h 35°04<br>h 36°60<br>h 35°84<br>d 35°93 | h 37 °02<br>h 35 °56<br>h 34 °78<br>h 35 °88 | $M = 35'' \cdot 76$ $w = 15 \cdot 56$ $\frac{1}{w} = 0 \cdot 06$ $C = 28^{\circ} 58' 25'' \cdot 75$ |
|                      | 35.17                                    | 36.40                              | 34°37<br>2 20°34                                      | 35°43<br>7 19°78                   | 36.81<br><br>18.94                       | 36.44<br>                     | 35°46<br><br>2 19°80          | 35.84                                         | 35.85<br><b>k</b> 18.24                       | 35.81<br>                                    | $M = 10'' \cdot 70$                                                                                 |
| I & II               | 2 20°12<br>2 19°86                       | 2 19·94<br>2 18·86                 | l 19.66<br>l 21.32                                    | 2 19·10<br>2 20·86                 | 2 18·46<br>2 19·16                       | 2 19·46<br>2 19·10            | 2 19·44<br>2 19·98            | 2 21 '94<br>2 18 '46<br>2 18 '96              | k 19.42<br>k 19.08<br>d 19.01                 | h 19.00<br>h 20.22                           | $w = 20 \cdot 02$ $\frac{1}{w} = 0 \cdot 05$                                                        |
|                      | 20.49                                    | 19.23                              | 20.44                                                 | 19.91                              | 18.82                                    | 19.85                         | 19.24                         | 20.18                                         | 18.94                                         | 19.94                                        | $C = 42^{\circ} 1' 19'' \cdot 7$                                                                    |

Norz.-Stations XLI and XLIV appertain to the Karáchi Longitudinal Series.

| At XLIV (Súnda)                                                                                                |                                                     |                                                                                       |                                                          |                                                               |                                                                         |                                                      |                                                        |                                                                        |                                                  |                                    |                                                                                                     |  |  |  |
|----------------------------------------------------------------------------------------------------------------|-----------------------------------------------------|---------------------------------------------------------------------------------------|----------------------------------------------------------|---------------------------------------------------------------|-------------------------------------------------------------------------|------------------------------------------------------|--------------------------------------------------------|------------------------------------------------------------------------|--------------------------------------------------|------------------------------------|-----------------------------------------------------------------------------------------------------|--|--|--|
| January and February 1873; observed by Lieut. M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.      |                                                     |                                                                                       |                                                          |                                                               |                                                                         |                                                      |                                                        |                                                                        |                                                  |                                    |                                                                                                     |  |  |  |
| Angle<br>between                                                                                               | 0°0′                                                | 180° 0'                                                                               | C<br>79° 18′                                             | Circle read<br>259° 13′                                       | lings, tele<br>158° 24′                                                 | scope bei<br>338° 24'                                | ng set on<br>237° 37'                                  | I<br>57°37′                                                            | 816° 48′                                         | 136 <b>° 48′</b>                   | $ \begin{array}{llllllllllllllllllllllllllllllllllll$                                               |  |  |  |
| I & II                                                                                                         | k 9.86<br>k 11'40<br>k 11'00                        | k 10°18<br>l 9°86<br>l 8°54<br>l 9°02                                                 | "<br>2 9°40<br>2 8°40<br>2 9°78                          | "<br>2 8.52<br>2 11.06<br>2 8.54<br>2 8.98                    | "<br>2 9 <sup>.</sup> 72<br>2 9 <sup>.</sup> 94<br>2 10 <sup>.</sup> 60 | n<br>h 10°62<br>h 8°90<br>h 7°32<br>h 9°76<br>h 8°30 | "<br>h 7.88<br>h 9.92<br>h 10.14<br>h 11.70<br>h 11.20 | "<br>h 7 <sup>.</sup> 80<br>h 9 <sup>.</sup> 26<br>h 8 <sup>.</sup> 58 | "<br>h 8.74<br>h 8.88<br>h 9.02                  | "<br>h 9°94<br>h 10°20<br>l 9°32   | $M = 9'' \cdot 51$ $w = 14 \cdot 98$ $\frac{1}{w} = 0 \cdot 07$                                     |  |  |  |
|                                                                                                                | 10.22                                               | 9.40                                                                                  | 9.19                                                     | . 9*28                                                        | 10.00                                                                   | 8.98                                                 | 10.12                                                  | 8.22                                                                   | 8.88                                             | 9.82                               | $C = 37^{\circ} 19' 9'' \cdot 51$                                                                   |  |  |  |
| II & XLI                                                                                                       | h 8°20<br>h 8°24<br>l 10°04<br>l 9°68               | l 8·32<br>l 10·48<br>l 8·44<br>l 8·50                                                 | 2 8.72<br>2 9.36<br>2 6.92<br>2 7.78                     | 2 8·74<br>2 6·60<br>2 7·90<br>2 9·10                          | l 8·22<br>l 7·06<br>l 8·56                                              | h 9°14<br>h 6°50<br>h 9°00<br>h 7°90                 | h 8.90<br>h 7.70<br>h 9.08                             | h 10°58<br>h 9°28<br>h 8°90<br>h 10°02                                 | h 9.32<br>h 8.20<br>h 10.36<br>h 9.00            | h 7.68<br>h 7.30<br>l 9.28         | $M = 8'' \cdot 59$ $w = 17 \cdot 96$ $\frac{1}{2} = 0 \cdot 06$                                     |  |  |  |
|                                                                                                                | 9.04                                                | 8.94                                                                                  | 8.19                                                     | 8.09                                                          | 7.95                                                                    | 8.13                                                 | 8.20                                                   | 9.70                                                                   | 9.33                                             | 8.09                               | $C = 30^{\circ} 27' 8'' \cdot 60$                                                                   |  |  |  |
| At I (Borta)<br>February 1873; observed by Lieut. M. W. Rogers, R. E., with Barrow's 24-inch Theodolite No. 2. |                                                     |                                                                                       |                                                          |                                                               |                                                                         |                                                      |                                                        |                                                                        |                                                  |                                    |                                                                                                     |  |  |  |
| Angle<br>between                                                                                               | 139 <b>°</b> 3′                                     | <b>8</b> 19 <b>°</b> 3′                                                               | C.<br>218° 13′                                           | ircle read<br>38° 14′                                         | ings, teles<br>297° 26'                                                 | соре bein<br>117°26'                                 | ng set on ]<br>16°38'                                  | [ <b>∇</b><br>196°38′                                                  | 95° 49′                                          | 275° 49′                           |                                                                                                     |  |  |  |
| IV & III                                                                                                       | "<br>1 49.60<br>1 51.92<br>1 51.76<br>1 52.10       | "<br>\$ 50.84<br>\$ 54.78<br>\$ 50.72<br>\$ 51.76<br>\$ 48.84<br>\$ 48.84<br>\$ 49.66 | n 52.94<br>h 51.26<br>h 53.48<br>h 53.62                 | "<br>h 51 · 70<br>h 52 · 66<br>h 52 · 76                      | "<br>h 51 · 80<br>h 50 · 32<br>h 52 · 20                                | "<br>h 52°06<br>h 50°76<br>h 50°82                   | "<br>  52·26<br>  50·34<br>  51·00                     | "<br>  50°14<br>  51°76<br>  49°96                                     | "<br>  49`74<br>  51`58<br>  50`60               | "<br>  51.60<br>  50.36<br>  49.32 | $M = 51'' \cdot 29$ $w = 10 \cdot 25$ $\frac{1}{w} = 0 \cdot 10$ $C = 52^{\circ} 40' 51'' \cdot 29$ |  |  |  |
|                                                                                                                | 51.32                                               | 50.48                                                                                 | 52.82                                                    | 52.37                                                         | 51.44                                                                   | 51.51                                                | 51.30                                                  | 50.05                                                                  | 50.64                                            | 50.43                              |                                                                                                     |  |  |  |
| III & II                                                                                                       | l 13.86<br>l 13.68<br>l 14.58<br>l 16.26            | l 16°60<br>l 15°98<br>l 15°98                                                         | h 15°20<br>h 14°40<br>h 14°16<br>h 14°24                 | h 14 90<br>h 15 16<br>h 13 96                                 | h 16°54<br>h 17°30<br>h 17°02                                           | h 16.82<br>h 15.76<br>h 15.60                        | l 14°94<br>l 14°72<br>l 15°80                          | l 14·78<br>l 14·82<br>l 14·44                                          | l 14.80<br>l 15.00<br>l 15.52                    | l 14·52<br>l 14·98<br>l\15·24      | $M = 15'' \cdot 28$ $w = 12 \cdot 88$ $I = 0 \cdot 08$                                              |  |  |  |
|                                                                                                                | 14.60                                               | 16.10                                                                                 | 14.20                                                    | 14.67                                                         | 16.92                                                                   | 10.00                                                | 15.12                                                  | 14.68                                                                  | 15.11                                            | 14.91                              | $     C = 62^{\circ} 5' 15'' \cdot 28 $                                                             |  |  |  |
| II & XLI                                                                                                       | l 40°94<br>l 39°88<br>l 38°36<br>l 37°64<br>l 37°66 | l 37 80<br>l 40 02<br>l 40 62<br>l 40 26                                              | h 41 °94<br>h 39 °86<br>h 37 °96<br>h 40 °66<br>h 40 °32 | h 37 · 56<br>h 37 · 10<br>h 38 · 62<br>h 40 · 96<br>h 39 · 70 | h 38°74<br>h 38°32<br>h 38°80                                           | h 38 34<br>h 39 90<br>h 40 5a<br>l 39 72             | l 40°32<br>l 40°56<br>l 40°34                          | l 38·46<br>l 40·10<br>l 39·96                                          | l 41 · 10<br>l 41 · 54<br>l 38 · 76<br>l 40 · 06 | l 39°14<br>l 39°52<br>l 39°46      | $M = 39'' \cdot 54$<br>$w = 14 \cdot 44$<br>$\frac{1}{20} = 0 \cdot 07$                             |  |  |  |
| *                                                                                                              | 38.90                                               | 39.68                                                                                 | 40.12                                                    | 38.79                                                         | 38.62                                                                   | 39.61                                                | 40.41                                                  | 39.21                                                                  | <b>4</b> 0°37                                    | 39`37                              | $\tilde{C} = 32^{\circ} 57' 39'' \cdot 54$                                                          |  |  |  |

Norz.-Stations XLI and XLIV appertain to the Karáchi Longitudinal Sezies.

|                                                                                                                                                                                                                    |                                                                                                                                                                       |                                                                                 |                                                         | At                                                                                | I (Bort                                                 | a)-(Ca                                        | ontinued                           | <i>!</i> ).                                      |                                                  |                                                               |                                                                                                    |  |  |  |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------|---------------------------------------------------------|-----------------------------------------------------------------------------------|---------------------------------------------------------|-----------------------------------------------|------------------------------------|--------------------------------------------------|--------------------------------------------------|---------------------------------------------------------------|----------------------------------------------------------------------------------------------------|--|--|--|
| Angle                                                                                                                                                                                                              |                                                                                                                                                                       |                                                                                 | M = Mean of Groups<br>w = Relative Weight               |                                                                                   |                                                         |                                               |                                    |                                                  |                                                  |                                                               |                                                                                                    |  |  |  |
|                                                                                                                                                                                                                    | 139° 3′                                                                                                                                                               | <b>\$19°</b> 3′                                                                 | <b>218° 13</b> ′                                        | 38° 14'                                                                           | <b>2</b> 97° 26′                                        | 117* 26'                                      | 16' 38'                            | 196*38′                                          | 95° 49″,                                         | 275° 49'                                                      | C = Concluded Angle                                                                                |  |  |  |
| XLI &<br>XLIV                                                                                                                                                                                                      | "<br>1 13 · 52<br>1 10 · 40<br>1 12 · 94<br>1 1 · 30<br>1 1 · 02                                                                                                      | "<br>2 10·78<br>2 9·68<br>2 8·76<br>2 10·60                                     | "<br>h 9 94<br>h 13 16<br>h 13 52<br>h 11 64<br>h 13 62 | "<br><b>h</b> 11 · 20<br><b>h</b> 13 · 52<br><b>h</b> 13 · 34<br><b>h</b> 11 · 96 | "<br>h 9.08<br>h 12.40<br>h 11.00<br>h 10.82<br>h 10.14 | "<br>h 12.44<br>h 10.10<br>h 11.40<br>l 10.72 | "<br>1 10`50<br>1 10`38<br>1 11`16 | "<br>12.38<br>29.84<br>11.88<br>211.54           | "<br>l 10°74<br>l 9°22<br>l 11°68<br>l 11°64     | "<br>111.56<br>111.74<br>10.12                                | $M = 11'' \cdot 26$ $w = 11 \cdot 21$ $\frac{1}{w} = 0 \cdot 09$                                   |  |  |  |
|                                                                                                                                                                                                                    | 11.84                                                                                                                                                                 | 9.96                                                                            | 12.38                                                   | 12.20                                                                             | 10.69                                                   | 11.12                                         | 10.08                              | 11.41                                            | 10.83                                            | 11.14                                                         | $C = 73^{\circ} 15^{\circ} 11^{\circ} 27$                                                          |  |  |  |
| At II (Dhaula)         February 1873; observed by Lieut. M. W. Rogers, R. E., with Barrow's 24-inch Theodolite No. 2.         Angle         Circle readings, telescope being set on XLI         M = Mean of Groups |                                                                                                                                                                       |                                                                                 |                                                         |                                                                                   |                                                         |                                               |                                    |                                                  |                                                  |                                                               |                                                                                                    |  |  |  |
| Angle<br>between                                                                                                                                                                                                   | Angle         Circle readings, telescope being set on XLI           between         0° 0′ 180° 0′ 79° 13′ 259° 13′ 158° 24′ 838° 24′ 237° 37′ 57° 37′ 316° 48′ 136° 4 |                                                                                 |                                                         |                                                                                   |                                                         |                                               |                                    |                                                  |                                                  |                                                               |                                                                                                    |  |  |  |
| XLI &<br>XLIV                                                                                                                                                                                                      | "<br>h 57 · 64<br>h 61 · 34<br>h 60 · 46<br>h 59 · 98<br>h 60 · 76                                                                                                    | "<br>h 58 · 70<br>h 63 · 52<br>h 60 · 58<br>h 59 · 74<br>h 60 · 96<br>h 59 · 78 | "<br>h 59°88<br>l 62°30<br>l 59°70<br>l 60°08           | "<br>2 60°80<br>2 60°88<br>2 59°70                                                | "<br>1 59.78<br>1 60.90<br>1 59.80<br>1 60.21           | "<br>2 60°64<br>2 60°32<br>2 59°56            | "<br>h 60°54<br>h 59°96<br>h 59°20 | "<br>\$ 60°16<br>\$ 58°70<br>\$ 58°28            | "<br>h 61 · 46<br>h 60 · 68<br>h 59 · 84         | "<br>k 59`70<br>k 60`56<br>k 59`78                            | $M = 60'' \cdot 15$ $w = 20 \cdot 98$ $\frac{1}{w} = 0 \cdot 05$ $C = 68^{\circ} 23' 0'' \cdot 17$ |  |  |  |
|                                                                                                                                                                                                                    | 60.04                                                                                                                                                                 | 60.22                                                                           | 60.49                                                   | 60.46                                                                             | 60.12                                                   | 60.12                                         | 59.90                              | 59.02                                            | 60.66                                            | 60.01                                                         |                                                                                                    |  |  |  |
| XLIV & I                                                                                                                                                                                                           | h 1.70<br>h 4.28<br>h 2.78<br>h 2.92                                                                                                                                  | k 4 · 14<br>k 1 · 12<br>k 2 · 82<br>k 3 · 48<br>k 2 · 98                        | h 1.80<br>l 3.96<br>l 2.68<br>l 2.18                    | l 3.62<br>l 3.96<br>l 5.26<br>l 4.22                                              | l 3.50<br>l 3.66<br>l 4.22<br>d 3.84                    | 2 4·40<br>2 3·28<br>2 3·64                    | h 4 46<br>h 3 56<br>h 3 08         | h 2°46<br>h 2°20<br>h 3°60                       | h 2.76<br>h 4.22<br>h 5.26<br>h 5.12             | h 3.00<br>h 4.44<br>h 2.30<br>h 2.74                          | $M = 3'' \cdot 42$ $w = 18 \cdot 15$ $\frac{1}{w} = 0 \cdot 06$                                    |  |  |  |
|                                                                                                                                                                                                                    | 2.93                                                                                                                                                                  | 2.91                                                                            | 2.66                                                    | 4.30                                                                              | 3.81                                                    | 3.11                                          | 3.20                               | 2.75                                             | 4*34                                             | 3.15                                                          | $C = 36^{\circ} 28' 3'' \cdot 42$                                                                  |  |  |  |
| I & III                                                                                                                                                                                                            | h 16°74<br>h 14°08<br>h 15°28<br>h 16°04                                                                                                                              | h 14°34<br>h 14°90<br>h 14°86                                                   | 2 13·34<br>2 15·16<br>2 16·26<br>2 17·58<br>2 15·04     | l 14.52<br>l 15.30<br>l 13.18<br>l 16.28<br>l 14.92                               | l 15°42<br>l 15°60<br>l 15°18                           | l 15°04<br>l 13°58<br>l 16°18<br>l 14°04      | h 16°34<br>h 16°68<br>h 16°86      | h 15.80<br>h 14.38<br>h 15.10                    | h 13 · 60<br>h 15 · 06<br>h 12 · 34<br>h 14 · 90 | h 14°58<br>h 14°76<br>h 14°72<br>h 15°34                      | $M = 15'' \cdot 12$ $w = 13 \cdot 96$ $\frac{1}{10} = 0 \cdot 07$                                  |  |  |  |
| ,                                                                                                                                                                                                                  | 15.24                                                                                                                                                                 | 14.20                                                                           | 15.48                                                   | 14.84                                                                             | 15.40                                                   | 14.21                                         | 16.63                              | 15.09                                            | 13.97                                            | 14.85                                                         | $C = 65^{\circ} 16' 15'' \cdot 11$                                                                 |  |  |  |
| 111 & V                                                                                                                                                                                                            | h 29°32<br>h 28°58<br>h 29°28                                                                                                                                         | h 31 · 16<br>h 30 · 28<br>h 29 · 42                                             | l 28·86<br>l 28·34<br>l 27·14                           | l 29°10<br>l 28°66<br>l 27°48<br>l 28°92<br>l 28°74                               | l 29°28<br>l 28°04<br>l 29°84                           | l 29°32<br>l 29°36<br>l 28°58                 | h 28°50<br>h 28°58<br>h 29°34      | h 28 · 58<br>h 30 · 48<br>h 28 · 26<br>h 28 · 14 | h 30°02<br>h 26°82<br>h 28°46<br>h 27°90         | h 27 · 78<br>h 26 · 80<br>h 28 · 44<br>h 27 · 54<br>h 28 · 36 | $M = 28'' \cdot 79$ $w = 16 \cdot 20$ $\frac{1}{w} = 0 \cdot 06$                                   |  |  |  |
|                                                                                                                                                                                                                    | 29.00                                                                                                                                                                 | 30.30                                                                           | 38.11                                                   | 28.58                                                                             | 29.05                                                   | 29.09                                         | 28.81                              | 28.87                                            | 28.30                                            | 27.78                                                         | $C = 81^{\circ} 14' 28'' \cdot 77$                                                                 |  |  |  |

NOTE.-Stations XLI and XLIV appertain to the Karáohi Longitudinal Series.

# At III (Kundal)

February and March 1873; observed by Lieut. M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle      |                                                              |                                                     | С                                        | ircle read                                                   | ings, teles                                                         | cope bein                                | g set on V                                                  | 71                                       |                                                     |                                                                      | M = Mean of Groups<br>w = Relative Weight                                                           |
|------------|--------------------------------------------------------------|-----------------------------------------------------|------------------------------------------|--------------------------------------------------------------|---------------------------------------------------------------------|------------------------------------------|-------------------------------------------------------------|------------------------------------------|-----------------------------------------------------|----------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------|
| between    | 0° 1′                                                        | 180° 1′                                             | 79° 12′                                  | 259°12′                                                      | 158° 25′                                                            | 838° 25'                                 | 237 <b>°</b> 37′                                            | 57^ 87'                                  | <b>316° 49'</b>                                     | 186° 49′                                                             | C = Concluded Angle                                                                                 |
| VI & VII   | "<br>* \$39`46<br>\$38`20<br>\$40`58<br>\$39`06              | "<br>h 37 °96<br>h 39 °26<br>h 37 °26               | "<br>  37·32<br>  38·18<br>  38·08       | "<br>1 37 98<br>1 37 86<br>1 38 86                           | "<br>1 37.10<br>1 40.80<br>1 36.02<br>1 39.72<br>1 39.12<br>1 39.50 | "<br>h 39`74<br>h 38`98<br>h 39`72       | "<br>h 38 · 60<br>h 38 · 16<br>h 37 · 36<br>d 38 · 71       | "<br>h 37 · 96<br>h 38 · 38<br>h 38 · 12 | "<br>1 39 °66<br>1 39 °22<br>1 37 °30<br>1 39 °06   | "<br>  38.42<br>  39.94<br>  38.72                                   | $M = 38'' \cdot 60$ $w = 18 \cdot 47$ $\frac{1}{w} = 0 \cdot 05$ $C = 50^{\circ} 58' 38'' \cdot 61$ |
|            | 39.33                                                        | 38.10                                               | 37.86                                    | 38.23                                                        | 38.21                                                               | 39.48                                    | 38.21                                                       | 38.12                                    | 38.81                                               | 39.03                                                                | - 07 0- 0-                                                                                          |
| VII & V    | h 45°42<br>h 43°90<br>h 46°05<br>h 44°82<br>h 44°88<br>45°02 | h 43 · 38<br>h 43 · 30<br>h 43 · 04                 | l 44.62<br>l 44.68<br>l 44.86<br>. 44.86 | l 45.56<br>l 42.82<br>l 44.68<br>l 44.68<br>d 42.81<br>43.99 | l 43 · 84<br>l 42 · 54<br>l 45 · 62<br>l 43 · 94<br>l 44 · 42       | h 44 · 52<br>h 45 · 70<br>h 44 · 88      | h 44 · 28<br>h 43 · 92<br>h 45 · 32<br>d 45 · 18<br>44 · 68 | h 43 °96<br>h 44 °54<br>h 44 °08         | l 44.98<br>l 45.44<br>l 40.10<br>l 44.32            | l 44.58<br>l 44.22<br>l 44.10                                        | $M = 44'' \cdot 44$ $w = 20 \cdot 42$ $\frac{1}{w} = 0 \cdot 05$ $C = 43^{\circ} 5' 44'' \cdot 44$  |
| <br>▼ & II | h 49°74<br>h 48°94<br>h 48°90<br>h 49°02                     | h 47°64<br>h 46°48<br>h 48°64<br>h 48°64<br>h 46°82 | l 47.62<br>l 48.02<br>l 47.24            | l 48.62<br>l 49.98<br>l 49.82<br>d 47.99                     | l 47.60<br>l 48.46<br>l 46.70                                       | h 48.86<br>h 47.00<br>h 48.52            | h 49°62<br>h 48°74<br>h 48°40<br>h 47°56                    | h 47 70<br>h 47 70<br>h 45 78            | l 46.66<br>l 47.02<br>l 46.60                       | l 48.70<br>l 46.98<br>l 47.34                                        | $M = 47'' \cdot 91$ $w = 12 \cdot 31$ $\frac{1}{2} = 0 \cdot 08$                                    |
| ,          | 49'''5                                                       | 47.40                                               | 47.63                                    | 49.10                                                        | 47 <sup>°</sup> 59                                                  | 48.13                                    | 48.58                                                       | 47.00                                    | 46.76                                               | 47.67                                                                | $\begin{bmatrix} w \\ C \end{bmatrix} = 50^{\circ} 38' 47'' \cdot 92$                               |
| II & I     | h 32 · 88<br>h 33 · 20<br>h 32 · 90                          | h 31 · 62<br>h 33 · 08<br>h 33 · 06                 | l 32.60<br>l 32.64<br>l 32.14            | l 31 · 76<br>l 32 · 26<br>l 32 · 12                          | l 33°06<br>l 32°80<br>l 33°38                                       | h 32°14<br>h 31°40<br>h 31°58            | h 31 · 40<br>h 34 · 04<br>h 33 · 12<br>h 31 · 74            | h 32 · 42<br>h 32 · 94<br>h 32 · 72      | l 33·34<br>l 33·82<br>l 33·48                       | l 32 <sup>:</sup> 00<br>l 33 <sup>:</sup> 52<br>l 32 <sup>:</sup> 66 | $M = 32'' \cdot 64$ $w = 27 \cdot 96$ $\frac{1}{2} = 0 \cdot 04$                                    |
|            | 32.99                                                        | 32.29                                               | 32.46.                                   | 32.05                                                        | 33.08                                                               | 31.21                                    | 32.28                                                       | 32.69                                    | 33.55                                               | 32.73                                                                | $\begin{bmatrix} w \\ C \\ = 52^{\circ} 38' 32'' \cdot 64 \end{bmatrix}$                            |
| 1 & IV     | h 28 · 44<br>h 30 · 68<br>h 27 · 80<br>h 28 · 62             | l 28:58<br>l 30:72<br>l 29:32                       | l 28.66<br>l 28.86<br>l 29.32            | l 29.80<br>l 28.96<br>l 28.32                                | l 28.98<br>l 31.02<br>l 27.98<br>l 29.78                            | h 29 98<br>h 30 38<br>h 27 46<br>h 30 16 | h 28°98<br>h 29°10<br>h 29°50                               | h 28°32<br>h 28°14<br>l 28°34            | l 27°90<br>l 27°02<br>l 29°24<br>l 29°34            | l 28°26<br>l 27°82<br>l 29°66                                        | $M = 28'' \cdot 98$ $w = 23 \cdot 02$ $\frac{1}{2} = 0 \cdot 03$                                    |
|            | 28.89                                                        | 29.24                                               | 28.95                                    | 29°03                                                        | 29.44                                                               | 29.49                                    | 29.19                                                       | 28.27                                    | 28.38                                               | 28.58                                                                | $\int_{0}^{w} C = 82^{\circ} 22' 28'' \cdot 98$                                                     |
| 1V & VI    | h 46°02<br>h 49°50<br>h 48°96<br>h 47°90                     | l 48 · 12<br>l 48 · 22<br>l 46 · 38                 | l 48.72<br>l 47.96<br>l 48.30            | l 46.68<br>l 48.92<br>l 48.18<br>l 47.94                     | l 47 · 76<br>l 45 · 50<br>l 46 · 26<br>l 47 · 18                    | h 46°32<br>h 47°82<br>h 47°74<br>h 49°56 | h 45 °96<br>l 49 °62<br>l 47 °38<br>l 47 °32                | h 49`06<br>h 48`40<br>l 48`08            | l 49.64<br>l 47.08<br>l 46.12<br>l 46.86<br>l 46.88 | l 48·80<br>l 47·22<br>l 47·30                                        | $M = 47'' \cdot 76$ $w = 17 \cdot 81$ $\frac{1}{w} = 0 \cdot 06$                                    |
|            | 48.10                                                        | 47.57                                               | 48.33                                    | 47 . 93                                                      | 46.67                                                               | 47.86                                    | 47.57                                                       | 48.51                                    | 47 . 32                                             | 47.77                                                                | $C = 71^{\circ} 15' 47'' 74$                                                                        |

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### At IV (Mandaula)

February 1873; observed by Lieut. M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle    |                                               |                                                     |                                                               | M = Mean of Groups                          |                                             |                                    |                                                     |                                          |                                                                   |                                                     |                                                                                                    |
|----------|-----------------------------------------------|-----------------------------------------------------|---------------------------------------------------------------|---------------------------------------------|---------------------------------------------|------------------------------------|-----------------------------------------------------|------------------------------------------|-------------------------------------------------------------------|-----------------------------------------------------|----------------------------------------------------------------------------------------------------|
| between  | 0°0′                                          | 180°0′                                              | 79° 12′                                                       | <b>2</b> 59° 1 <b>2′</b>                    | 158 <b>°</b> 25′                            | <b>3</b> 38° 25′                   | 237 <b>°</b> 37′                                    | 57° 37′                                  | <b>816° 49′</b>                                                   | 186° 49′                                            | w = Relative Weight<br>C = Concluded Angle                                                         |
| VI & III | "<br>h 19.58<br>h 19.88<br>h 19.58<br>h 19.58 | "<br>h 17 · 22<br>h 17 · 48<br>h 18 · 42<br>17 · 71 | "<br>h 19`58<br>h 20`02<br>h 17`46<br>h 17`42<br>18`62        | "<br>h 19`98<br>h 19`04<br>h 19`06<br>19`36 | "<br>h 20°06<br>h 18°72<br>l 18°60<br>19°13 | "<br>l 19.00<br>l 18.98<br>l 17.72 | "<br>1 17 · 32<br>1 18 · 12<br>1 16 · 58<br>17 · 34 | "<br>1 18 · 16<br>1 17 · 30<br>1 17 · 66 | "<br>h 19.04<br>h 20.38<br>h 16.62<br>h 17.18<br>h 16.58<br>17.96 | "<br>h 18 ° 26<br>h 16 ° 66<br>h 17 ° 07<br>17 ° 31 | $M = 18'' \cdot 34$ $w = 10 \cdot 39$ $\frac{1}{w} = 0 \cdot 10$ $C = 46^{\circ} 5' 18'' \cdot 34$ |
| III & I  | k 46.42<br>k 41.64<br>k 45.34                 | h 45 · 80<br>h 44 · 14<br>h 44 · 38                 | h 42 · 12<br>h 43 · 10<br>h 44 · 06<br>h 42 · 86<br>h 44 · 46 | h 43°10<br>h 43°32<br>h 42°54<br>h 44°28    | k 43 · 80<br>h 45 · 24<br>k 45 · 18         | l 44`54<br>l 45`34<br>l 44`94      | l 42°54<br>l 44°00<br>l 43°62                       | l 43 84<br>l 44 86<br>l 43 64            | h 43 °96<br>h 43 °48<br>h 45 °08                                  | h 43 ° 44<br>h 44 ° 54<br>h 43 ° 06                 | $M = 44'' \cdot 19$ $w = 13 \cdot 70$ $\frac{1}{w} = 0 \cdot 07$                                   |
|          | 45*47                                         | 44.77                                               | 43 32                                                         | 43.31                                       | 44.74                                       | 44 . 94                            | 43 * 39                                             | 44.11                                    | 44.17                                                             | 43.68                                               | $\tilde{C} = 44^{\circ} 56' 44'' \cdot 18$                                                         |

At V (Bhádrájan)

March 1873; observed by Lieut. M. W. Rogers, R. E., with Barrow's 24-inch Theodolite No. 2.

| Angle<br>between | 256 <sup>•</sup> 52′                                                       | 76 <b>°</b> 52′                                        | C<br>836° 3′                                | ircle read<br>156° 3'                       | ings, teles<br>55•16'                                  | scope bein<br>235° 16'                              | ng set on<br>134°28'                                | II<br>814° 28'                                                            | 218° 39′                                            | <b>33°</b> 89'                         | M = Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle                                         |
|------------------|----------------------------------------------------------------------------|--------------------------------------------------------|---------------------------------------------|---------------------------------------------|--------------------------------------------------------|-----------------------------------------------------|-----------------------------------------------------|---------------------------------------------------------------------------|-----------------------------------------------------|----------------------------------------|----------------------------------------------------------------------------------------------------------|
| 11 & 111         | "<br>h 46 · 88<br>h 47 · 28<br>h 49 · 34<br>h 48 · 58<br>48 · 02           | "<br>h 46.66<br>h 48.96<br>h 47.54<br>h 49.42<br>48.15 | *<br>l 48·32<br>l 48·22<br>l 49·36<br>48·63 | ,<br>l 49`32<br>l 49`76<br>l 47`82<br>48`97 | "<br>1 49`24<br>1 46`26<br>1 48`72<br>1 47`98<br>48`05 | "<br>1 47 · 86<br>1 49 · 34<br>1 49 · 48<br>48 · 89 | "<br>1 48 · 10<br>1 48 · 16<br>1 47 · 90<br>48 · 05 | /<br>/ 47 <sup>•</sup> 22<br>/ 47 <sup>•</sup> 92<br>/ 48 <sup>•</sup> 28 | "<br>h 48 · 96<br>h 48 · 46<br>h 47 · 24<br>48 · 22 | λ 48·74<br>λ 48·14<br>λ 47·96<br>48·28 | $M = 48'' \cdot 31$ $w = 28 \cdot 59$ $\frac{1}{w} = 0 \cdot 03$ $C = 48^{\circ} 6' \cdot 48'' \cdot 30$ |
| III & VII        | h 23 · 86<br>h 23 · 94<br>h 23 · 64<br>h 25 · 04<br>h 25 · 38<br>h 25 · 30 | h 25°00<br>h 25°12<br>h 24°26<br>h 25°60               | l 25.66<br>l 26.32<br>l 26.30               | l 25°30<br>l 26°46<br>l 26°06               | l 26.92<br>l 26.06<br>l 25.04                          | l 24·20<br>l 25·76<br>l 24·40                       | l 26°24<br>l 26°82<br>l 27°26                       | l 25°22<br>l 27°22<br>l 27°18<br>h 27°74                                  | h 25 · 72<br>h 24 · 36<br>h 26 · 20                 | h 27 · 14<br>h 25 · 76<br>h 25 · 76    | $M = 25'' \cdot 76$ $w = 12 \cdot 93$ $\frac{1}{w} = 0 \cdot 08$                                         |
|                  | 24.23                                                                      | 25.00                                                  | 26.09                                       | 25.94                                       | 26.01                                                  | 24.79                                               | 26.77                                               | 26.84                                                                     | 25.43                                               | 26.33                                  | $\begin{bmatrix} C = 55^{\circ} & 2' & 25'' & 75 \end{bmatrix}$                                          |

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# At VI (Nagar)

| Marc             | h 1873;                                                                                                                     | observed                                            | d by Lie                                      | eut. M.                                       | W. Rog                                | ers, R.I                            | E., with                                              | Barrow                                                        | 's 24-inc                               | ch Theod                                                | lolite No. 2.                                                        |  |  |  |  |
|------------------|-----------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------|-----------------------------------------------|-----------------------------------------------|---------------------------------------|-------------------------------------|-------------------------------------------------------|---------------------------------------------------------------|-----------------------------------------|---------------------------------------------------------|----------------------------------------------------------------------|--|--|--|--|
| Angle            | Angle<br>betweenCircle readings, telescope being set on IX $M = Mean of Groups$<br>$v = Relative WeightC = Concluded Angle$ |                                                     |                                               |                                               |                                       |                                     |                                                       |                                                               |                                         |                                                         |                                                                      |  |  |  |  |
| between          | 812° 10'                                                                                                                    | 132° 10′                                            | 31 <b>° 22'</b>                               | <b>2</b> 11° 22'                              | 110° 33'                              | -<br>290° 33′                       | 189° <b>45′</b>                                       | 9°45′                                                         | 268° 57′                                | 88° 58′                                                 | <ul> <li>m = Relative Weight</li> <li>C = Concluded Angle</li> </ul> |  |  |  |  |
| IX & VIII        | "<br>h 12`90<br>h 12`28<br>h 11`62                                                                                          | "<br>h 12°58<br>h 11°64<br>l 12°66                  | "<br>1 12.44<br>1 11.66<br>1 11.86            | "<br>l 11°26<br>l 11°14<br>l 12°04            | "<br>12 *88<br>13 *00<br>11 * 74      | "<br>h 12°24<br>h 12°02<br>h 11°98  | "<br>h 11 ° 14<br>h 12 ° 20<br>h 13 ° 18<br>h 11 ° 00 | "<br>h 13 ° 22<br>h 13 ° 80<br>h 13 ° 44<br>h 14 ° 70         | "<br>h 11 °94<br>h 12 ° 18<br>l 12 ° 26 | "<br>  12°78<br>  12°46<br>  10°98                      | $M = 12'' \cdot 25$ $w = 21 \cdot 48$ $\frac{1}{w} = 0 \cdot 05$     |  |  |  |  |
|                  | 12.22                                                                                                                       | 12.29                                               | 11.00                                         | τ <b>τ</b> •48                                | 12.24                                 | 12.08                               | 11.88                                                 | 13.79                                                         | 12.13                                   | 12.02                                                   | $C = 47^{\circ} 51' 12'' \cdot 26$                                   |  |  |  |  |
| VIII & VII       | h 30°92<br>h 32°30<br>h 32°90                                                                                               | l 30°88<br>l 30°26<br>l 31°28                       | l 31.64<br>l 31.52<br>l 31.34                 | l 33 · 82<br>l 31 · 86<br>l 31 · 88           | l 31 · 56<br>l 31 · 40<br>l 32 · 90   | h 32°00<br>h 32°76<br>h 32°12       | h 32 · 82<br>h 30 · 84<br>h 32 · 52                   | h 32 · 48<br>h 31 · 90<br>h 31 · 86<br>h 28 · 84<br>h 29 · 46 | h 31 · 20<br>h 31 · 08<br>h 30 · 68     | l 30°74<br>l 31°40<br>l 30°88                           | $M = 31'' \cdot 61$ $w = 16 \cdot 16$ $\frac{1}{w} = 0 \cdot 06$     |  |  |  |  |
|                  | 32.04                                                                                                                       | 30.81                                               | 31.20                                         | 32.22                                         | 31.92                                 | 32.29                               | 32.00                                                 | 30.01                                                         | 30.00                                   | 31.01                                                   | $\tilde{C} = 48^{\circ} 42' 31'' \cdot 60$                           |  |  |  |  |
| VII & III        | k 12 · 10<br>h 13 · 44<br>h 12 · 72<br>k 14 · 50                                                                            | l 14°44<br>l 13°82<br>l 13°60                       | l 12 · 84<br>l 14 · 76<br>l 14 · 30           | l 12°42<br>l 13°78<br>l 13°58                 | l 13.76<br>l 13.68<br>l 14.62         | k 12°12<br>k 14°04<br>k 13°14       | h 13 · 46<br>h 14 · 24<br>h 12 · 18<br>h 12 · 58      | h 12°96<br>h 11°76<br>h 13°52<br>h 13°96<br>h 13°20           | k 13.76<br>k 14.46<br>k 13.18           | l 12.62<br>l 13.18<br>l 13.96                           | $M = 13'' \cdot 47$ $w = 32 \cdot 90$ $\frac{1}{m} = 0 \cdot 03$     |  |  |  |  |
|                  | 13.10                                                                                                                       | 13.95                                               | 13.02                                         | 13.30                                         | 14.03                                 | 13.10                               | 13.15                                                 | 13.08                                                         | 13.80                                   | 13.25                                                   | $C = 67^{\circ} 47' 13'' 45$                                         |  |  |  |  |
| III & IV         | h 55 °98<br>h 57 ° 10<br>h 58 ° 62<br>h 57 ° 68                                                                             | h 55°76<br>h 57°92<br>l 55°38<br>l 56°84<br>h 58°20 | l 57 82<br>l 57 74<br>l 56 80                 | l 56°32<br>l 58°14<br>l 57°82                 | l 58.84<br>l 57.10<br>h 58.04         | h 57 · 88<br>h 58 · 36<br>h 57 · 40 | h 58·36<br>h 57·74<br>h 59·32                         | h 58 · 18<br>h 56 · 44<br>h 56 · 04<br>h 56 · 56<br>h 56 · 66 | h 57 · 58<br>h 58 · 24<br>h 57 · 18     | l 58·42<br>l 57·42<br>l 58·04                           | $M = 57'' \cdot 57$ $w = 20 \cdot 98$ $\frac{1}{m} = 0 \cdot 05$     |  |  |  |  |
|                  | 57:35                                                                                                                       | 56.82                                               | 57.45                                         | 57'43                                         | 57 99                                 | 57.88                               | 58.47                                                 | 56.66                                                         | 57.67                                   | 57.96                                                   | $C = 62^{\circ} 38' 57'' \cdot 54$                                   |  |  |  |  |
|                  |                                                                                                                             |                                                     |                                               |                                               | At V                                  | II (Sam                             | dari)                                                 |                                                               |                                         |                                                         |                                                                      |  |  |  |  |
| Marci            | h 1873;                                                                                                                     | observed                                            | l by Lie                                      | ut, M. 1                                      | W. Rog                                | ers, R. 1                           | E., with                                              | Barrou                                                        | 's 24-in                                | ch Theod                                                | lolite No. 2.                                                        |  |  |  |  |
| Angle<br>between | 0° 0′                                                                                                                       | 180° 0′                                             | 79° 12′                                       | Circle read<br>259° 12'                       | lings, tele<br>158° 25'               | scope beir<br>888° 25'              | ng set on<br>237° 37'                                 | V<br>57° 37′                                                  | <b>3</b> 16° 49′                        | 136° 49′                                                | M = Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle     |  |  |  |  |
| V & III<br>•     | "<br>1 52·30<br>1 53·50<br>1 55·26<br>1 53·04                                                                               | "<br>  53.64<br>  54.12<br>  54.24                  | "<br>  53.72<br>  54.52<br>  52.32<br>  53.66 | "<br>2 53 90<br>2 55 42<br>2 52 90<br>2 54 84 | "<br>h 54 °98<br>h 53 °58<br>h 53 °32 | "<br>h 53°16<br>h 53°80<br>h 52°64  | "<br>1 51 °60<br>1 52 °38<br>1 53 °98<br>1 53 °98     | "<br>  53.88<br>  52.30<br>  54.78<br>  54.02                 | "<br>l 53·48<br>l 52·96<br>l 53·38      | "<br>h 54 · 12 ·<br>h 55 · 10<br>h 54 · 90<br>h 52 · 64 | $M = 53'' \cdot 67$ $w = 25 \cdot 52$ $\frac{1}{w} = 0 \cdot 04$     |  |  |  |  |
|                  | 52.50                                                                                                                       | 54:00                                               | 60.66                                         | 61.07                                         | 62.06                                 | 69.90                               | E2 108                                                | 50.45                                                         | 62.07                                   | 64.10                                                   | $ C  = 81^{\circ} 51' 53'' \cdot 67$                                 |  |  |  |  |

54.00 53.55 54.27 53.96 53.20 52.98 53.75

53.23

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At VII (Samdari)-(Continued).

| Angle            | M - Mean of Groups                                                                     |                                                     |                                               |                                                               |                                               |                                                               |                                                       |                                    |                                          |                                                       |                                                                           |  |  |
|------------------|----------------------------------------------------------------------------------------|-----------------------------------------------------|-----------------------------------------------|---------------------------------------------------------------|-----------------------------------------------|---------------------------------------------------------------|-------------------------------------------------------|------------------------------------|------------------------------------------|-------------------------------------------------------|---------------------------------------------------------------------------|--|--|
| between          | 0°0′                                                                                   | 180° 0′                                             | 79° 12′                                       | 259° 12′                                                      | 158° 25'                                      | <b>3</b> 38° 25′                                              | <b>23</b> 7° 37′                                      | 57° 37′                            | <b>816° 49'</b>                          | 136° 49′                                              | w = Relative Weight<br>C = Concluded Angle                                |  |  |
| III & VI         | <i>l</i> 11'96<br><i>l</i> 10'40<br><i>l</i> 12'96<br><i>l</i> 12'10<br><i>l</i> 12'56 | "<br>  11 · 12<br>  10 · 98<br>  12 · 66            | "<br>l 11`02<br>l 11`64<br>l 11`44            | "<br>1 10°30<br>1 11°08<br>1 11°30<br>1 11°22                 | "<br>h 12 98<br>h 11 50<br>h 11 44<br>h 10 82 | "<br>h 11°12<br>h 11°22<br>h 11°96                            | "<br>  11 ° 16<br>  12 ° 90<br>  10 ° 98<br>  12 ° 10 | "<br>  10.88<br>  11.52<br>  10.64 | "<br>  11.92<br>  12.04<br>  11.20       | "<br>h 11°42<br>h 10°74<br>h 13°60                    | $M = 11'' \cdot 55$ $w = 37 \cdot 42$ $\frac{1}{w} = 0 \cdot 03$          |  |  |
|                  | 12.00                                                                                  | 11.29                                               | 11.32                                         | 10.08                                                         | 11.08                                         | 11.43                                                         | 11.40                                                 | 11.01                              | 11.72                                    | 11.92                                                 | $C = 52^{\circ} 14 11^{\circ} .50$                                        |  |  |
| VI & VIII        | l 51.68<br>l 51.88<br>l 50.00<br>l 50.20<br>l 50.70                                    | l 49 92<br>l 51 20<br>l 48 92<br>l 48 62<br>l 51 80 | l 50°10<br>l 51°56<br>l 50°28                 | l 51°96<br>l 51°54<br>h 51°24                                 | h 52°12<br>h 50°46<br>h 50°62                 | h 52 · 38<br>h 52 · 54<br>h 52 · 00                           | l 52.50<br>l 50.32<br>l 51.72<br>l 50.06              | l 50°36<br>l 50°26<br>l 51°14      | 2 52°24<br>2 51°02<br>2 51°48            | h 50°82<br>h 48°78<br>h 50°22<br>h 48°98              | $M = 50'' \cdot 96$ $w = 13 \cdot 14$ $\frac{1}{w} = 0 \cdot 08$          |  |  |
|                  | 50.80                                                                                  | 50.00                                               | 50.62                                         | 51.28                                                         | 51.02                                         | 52.31                                                         | 51.12                                                 | 50.20                              | 51.28                                    | 49`70                                                 | $C = 57^{\circ} 47' 50'' \cdot 94$                                        |  |  |
| VIII & X         | l 37°10<br>l 37°28<br>l 37°94                                                          | h 37°58<br>h 39°18<br>h 38°80<br>h 37°12<br>h 38°14 | h 36°58<br>h 35°92<br>h 37°12                 | h 36 · 12<br>h 38 · 12<br>h 35 · 72<br>h 36 · 64<br>h 38 · 82 | h 36°98<br>h 37°32<br>h 37°72                 | h 37 · 58<br>h 35 · 12<br>h 34 · 30<br>h 36 · 02<br>h 36 · 62 | l 36.02<br>l 36.70<br>l 36.36                         | l 37°20<br>l 36°68<br>l 36°62      | l 35 · 06<br>l 36 · 48<br>l 36 · 12      | k 36°62<br>h 38°36<br>h 37°62                         | $M = 36'' \cdot 91$ $w = 14 \cdot 01$ $\frac{1}{w} = 0 \cdot 07$          |  |  |
|                  | 37.44                                                                                  | 38.10                                               | 36.24                                         | 37.08                                                         | 37.34                                         | 35°93                                                         | 36.36                                                 | 36.83                              | 35.89                                    | 37.53                                                 | $\tilde{C} = 78^{\circ} 52' 36'' \cdot 91$                                |  |  |
| Marci            | h 1873; a                                                                              | observed                                            | by Lier                                       | ıt. M. V                                                      | At V<br>V. Roge                               | III (T)<br>rs, R. 1                                           | 10b)<br>E., with                                      | Barrow                             | o's 24-in                                | ch Theod                                              | dolite No. 2.                                                             |  |  |
| Angle<br>between | 0° 1′                                                                                  | <b>]80°1'</b>                                       | C<br>79° 13'                                  | ircle readi<br>259°13'                                        | ings, teles<br>158°25'                        | 20090 being<br>838°25'                                        | 3 set on V<br>237° 36'                                | II<br>57°36′                       | <b>8</b> 16° 49'                         | 1 <b>36° 4</b> 8′                                     | M = Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle          |  |  |
| VII & VI         | "<br>h 41 · 90<br>h 40 · 96<br>h 39 · 44<br>h 40 · 60                                  | "<br>h 40°08<br>l 39°72<br>l 40°10<br>l 37°94       | n<br>h 40°44<br>h 42°08<br>h 40°18<br>h 40°22 | "<br>1 40°98<br>1 40°74<br>1 38°98                            | "<br>h 39°22<br>h 41°16<br>h 41°62<br>h 40°04 | "<br>h 41 · 66<br>h 41 · 66<br>l 41 · 46                      | "<br>h 40.24<br>h 40.28<br>h 41.14                    | "<br>h 40°22<br>h 40°10<br>h 40°26 | "<br>h 41 ° 04<br>h 42 ° 16<br>h 40 ° 66 | "<br>h 39 · 20<br>h 40 · 60<br>h 40 · 08<br>l 39 · 36 | $M = 40'' \cdot 53$ $w = 17 \cdot 85$ $\frac{1}{w} = 0 \cdot 06$          |  |  |
|                  | 40.23                                                                                  | 39.46                                               | 40.23                                         | 40.23                                                         | 40.21                                         | 41.20                                                         | 40.22                                                 | 40.10                              | 41.50                                    | 39.81                                                 | $C = 73^{\circ} 29^{\prime} 40^{\prime\prime} \cdot 52$                   |  |  |
| VI & IX          | h 55 ° 10<br>h 54 ° 88<br>h 55 ° 64<br>h 55 ° 30                                       | 1 56.64<br>1 54.24<br>1 54.86<br>1 56.02            | h 55°40<br>h 56°74<br>h 55°98                 | 2 54 · 74<br>2 55 · 60<br>2 55 · 48                           | h 57°62<br>h 55°24<br>h 57°48<br>h 55°06      | l 56·72<br>h 55·96<br>h 55·30                                 | h 57°08<br>h 57°00<br>h 57°54                         | h 56°54<br>h 55°04<br>h 55°08      | h 56 • 46<br>h 57 • 38<br>h 57 • 84      | h 56°24<br>h 55°50<br>h 56°86<br>h 55°72              | $M = 56'' \cdot 04$ $w = 14 \cdot 86$ $\frac{1}{m} = 0 \cdot 07  \bullet$ |  |  |
|                  | 55.53                                                                                  | 55.44                                               | 56.04                                         | 55.27                                                         | 56.32                                         | 55 99                                                         | 57.31                                                 | 55.55                              | 57 . 23                                  | 56.08                                                 | $\int_{C}^{\infty} = 72^{\circ} 36' 56'' \cdot 03$                        |  |  |

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|                  | At VIII (Thob)-(Continued).                         |                                                  |                                                                                                                          |                                    |                                                     |                                                               |                                                   |                                                     |                                         |                                                                      |                                                                                      |  |  |  |
|------------------|-----------------------------------------------------|--------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------|------------------------------------|-----------------------------------------------------|---------------------------------------------------------------|---------------------------------------------------|-----------------------------------------------------|-----------------------------------------|----------------------------------------------------------------------|--------------------------------------------------------------------------------------|--|--|--|
| Angle<br>between | 0° 1′                                               | 180° 1′                                          | Ci<br>79°13′                                                                                                             | •<br>ircle readi<br>259°13′        | ngs, teles<br>158° 25'                              | cope bein <sub>(</sub><br>838° 25'                            | g set on V<br>287° 36'                            | 71 <b>1</b><br>57° 36′                              | <b>\$16° 49</b> ′                       | 136° 48′                                                             | M - Mean of Groupe<br>w = Relative Weight<br>C - Concluded Angle                     |  |  |  |
| IX & XI          | k 39°92<br>k 38°80<br>k 41°38<br>k 37°78<br>k 39°82 | "<br>k 39·82<br>l 40·82<br>l 42·20               | "<br>h 41 ° 36<br>h 39 ° 40<br>l 39 ° 84                                                                                 | "<br>  40°10<br>  38°16<br>  39°24 | "                                                   | "<br><b>b</b> 38 • 94<br><b>b</b> 38 • 50<br><b>c</b> 38 • 58 | *<br>\$ 40°02<br>\$ 37°88<br>\$ 38°52<br>\$ 37°38 | "<br>\$ 38.94<br>\$ 40.36<br>\$ 39.34               | "                                       | <b>k</b> 40°12<br><b>k</b> 38°70<br><b>k</b> 37°94<br><b>k</b> 38°54 | $M = 39'' \cdot 45$ $w = 12 \cdot 42$ $\frac{1}{w} = 0 \cdot 08$ $(1 + 1)^{1/2} = 0$ |  |  |  |
|                  | 39.24                                               | 40.92                                            | 40.30                                                                                                                    | 39.17                              | 39.25                                               | 38.67                                                         | 38.45                                             | 39.22                                               | 38.90                                   | 38.83                                                                | $C = 05^{\circ} 7 39^{\circ} 43$                                                     |  |  |  |
| XI & XII         | h 19.40<br>h 19.62<br>h 18.52                       | k 18°92<br>l 19°18<br>l 17°78                    | <b>h</b> 17 <sup>•</sup> 32<br><b>h</b> 20 <sup>•</sup> 46<br><b>l</b> 20 <sup>•</sup> 98<br><b>h</b> 21 <sup>•</sup> 76 | l 20°06<br>l 19°88<br>l 21°18      | h 18.14<br>h 18.46<br>h 19.52<br>h 19.50            | h 18°02<br>h 18°86<br>l 19°04<br>l 20°58                      | h 20°52<br>h 20°42<br>h 19°48<br>h 20°42          | h 18°42<br>h 17°44<br>l 19°50                       | <b>h</b> 17 °96<br>h 18 °76<br>h 19 °76 | <b>h</b> 18.76<br>h 19.08<br>h 19.14<br>h 18.42                      | $M = 19'' \cdot 27$ $w = \frac{7}{4} 14 \cdot 46$ $\frac{1}{4} = 0 \cdot 07$         |  |  |  |
|                  | 19.18                                               | 18.63                                            | 20.13                                                                                                                    | 20.37                              | 18.91                                               | 19.15                                                         | 20.51                                             | 18.45                                               | 18.83                                   | 18.85                                                                | $C = 54^{\circ} 17' 19'' \cdot 28$                                                   |  |  |  |
| XII & X          | h 1.76<br>h 2.02<br>h 3.46<br>l 4.36                | h 3.68<br>l 3.84<br>l 4.32                       | h 4°90<br>h 2°22<br>h 3°44<br>l 3°04                                                                                     | 2 4 44<br>2 4 46<br>2 3 60         | h 3°26<br>h 3°92<br>h 3°14                          | h 3.94<br>h 4.16<br>l 2.40                                    | k 1°36<br>k 3°12<br>k 4°24<br>k 1°44              | l 3°90<br>h 3°02<br>h 2°84                          | h 4°04<br>h 3°60<br>h 2°90              | h 4°76<br>h 2°70<br>h 2°86                                           | $M = 3'' \cdot 41$ $w = 23 \cdot 78$ $\frac{1}{2} = 0 \cdot 04$                      |  |  |  |
|                  | 2.90                                                | 3°95                                             | 3.40                                                                                                                     | 4.12                               | 3.44                                                | 3.20                                                          | 2°54                                              | 3.52                                                | 3.21                                    | 3.44                                                                 | $C = 40^{\circ} 23' 3'' \cdot 39$                                                    |  |  |  |
| X & VII          | k 20°96<br>k 21°52<br>k 21°54                       | k 21 · 38<br>l 21 · 02<br>l 21 · 98<br>l 20 · 58 | h 19°28<br>h 21°32<br>h 20°38<br>l 19°32                                                                                 | l 20°42<br>l 21°48<br>l 20°46      | h 23°44<br>h 19°32<br>h 19°06<br>h 19°58<br>h 20°58 | h 20°74<br>h 20°34<br>l 21°24                                 | h 20°96<br>h 22°00<br>h 20°18                     | l 22.38<br>h 22.42<br>h 23.06<br>h 21.22<br>h 18.62 | h 21 °04<br>h 21 °76<br>h 20 ° 16       | h 20°36<br>h 22°04<br>h 21°06                                        | $M = 20'' \cdot 93$ $w = 21 \cdot 18$ $\frac{1}{w} = 0 \cdot 05$                     |  |  |  |
|                  | 21.34                                               | 21 * 24                                          | 20.08                                                                                                                    | 20.79                              | 20.40                                               | 20.77                                                         | 21.02                                             | 21.24                                               | 20.99                                   | 21.12                                                                | $C = 54^{\circ} 5' 20'' \cdot 92$                                                    |  |  |  |

At IX (Borla)

March 1873; observed by Lieut. M. W. Rogers, R. E., with Barrow's 24-inch Theodolite No. 2.

| Angle          |                                               | M = Mean of Groups                                      |                                         |                                          |                                                    |                                    |                                    |                                    |                                           |                                               |                                                                  |
|----------------|-----------------------------------------------|---------------------------------------------------------|-----------------------------------------|------------------------------------------|----------------------------------------------------|------------------------------------|------------------------------------|------------------------------------|-------------------------------------------|-----------------------------------------------|------------------------------------------------------------------|
| between        | 0° 0′                                         | 180°0′                                                  | 79 <b>°</b> 13′                         | <b>2</b> 59° 13′                         | 158° 24'                                           | 338° 25′                           | 237° 87′                           | 57° 37′                            | 816° 48'                                  | 136° 49′                                      | C = Concluded Angle                                              |
| XI & VIII<br>• | n<br>h 10°30<br>h 12°98<br>h 13°14<br>h 13°18 | "<br><b>h</b> 12°90<br><b>h</b> 13°08<br><b>h</b> 13°86 | "<br>h 11 °60<br>h 12 ° 38<br>h 13 ° 22 | "<br>h 12 * 88<br>h 11 * 86<br>h 13 * 04 | <i>h</i> 13°26<br><i>h</i> 12°92<br><i>h</i> 11°60 | "<br>l 11°64<br>l 12°56<br>l 13°42 | "<br>  12°14<br>  12°60<br>  12°16 | "<br>1 13°16<br>1 13°46<br>1 11°88 | "<br><b>k</b> 11°16<br>k 12°12<br>k 11°46 | "<br>k 12°20<br>k 12°98<br>k 10°80<br>k 12°86 | $M = 12'' \cdot 47$ $w = 27 \cdot 76$ $\frac{1}{m} = 0 \cdot 04$ |
|                | 12'40                                         | 13.28                                                   | 12.40                                   | 12.59                                    | 12.29                                              | 12.24                              | 12.30                              | 12.83                              | 11.28                                     | 12.31                                         | $C = 57^{\circ} 46' 12'' \cdot 47$                               |

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| At IX (Borla)—(Continued). |                                          |                                            |                                          |                                                                              |                                                  |                                          |                                                       |                                                          |                                                               |                                                                    |                                                                                                          |  |  |
|----------------------------|------------------------------------------|--------------------------------------------|------------------------------------------|------------------------------------------------------------------------------|--------------------------------------------------|------------------------------------------|-------------------------------------------------------|----------------------------------------------------------|---------------------------------------------------------------|--------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------|--|--|
| Angle<br>between           | 0° 0′                                    | 180° 0'                                    | Cir<br>79°13′                            | cle readin<br>259° 13′                                                       | 158° 24'                                         | ope being<br>338°25'                     | set on 2<br>237° 37′                                  | 57°37'                                                   | 316° 48'                                                      | 136° 49′                                                           | M = Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle                                         |  |  |
| VIII & VI                  | "<br>h 55°32<br>h 55°02<br>h 54°60       | h 54°36<br>h 54°46<br>h 55°34              | "<br>h 54 * 36<br>h 55 * 34<br>h 54 * 80 | <i>h</i> 53 · 36<br><i>h</i> 53 · 34<br><i>h</i> 54 · 80<br><i>h</i> 54 · 68 | n 53 · 72<br>h 53 · 44<br>h 54 · 36<br>h 54 · 36 | "<br>  55°60<br>  54°66<br>  54°46       | "<br>2 54 · 22<br>2 53 · 88<br>2 56 · 70<br>2 54 · 36 | "<br>l 53°16<br>l 53°20<br>h 53°52<br>h 53°52<br>h 56°88 | "<br>h 54 • 58<br>h 53 • 02<br>h 53 • 44<br>h 55 • 44         | "<br>h 52 ° 02<br>h 55 ° 02<br>h 56 ° 68<br>h 55 ° 86<br>h 53 ° 58 | $M = 54'' \cdot 51$ $w = 23 \cdot 48$ $\frac{1}{w} = 0 \cdot 04$                                         |  |  |
|                            | 54.98                                    | 54.23                                      | 54.83                                    | 54.02                                                                        | 53'97                                            | 54.01                                    | 54.79                                                 | 54.00                                                    | 54.13                                                         | 54.63                                                              | $C = 59^{\circ} 31^{\circ} 54^{\circ} 48$                                                                |  |  |
|                            |                                          |                                            |                                          |                                                                              | At 2                                             | X (Dod                                   | 0)                                                    |                                                          |                                                               |                                                                    |                                                                                                          |  |  |
| April                      | 1873; <i>o</i>                           | bserved                                    | by Lieu                                  | t. M. W                                                                      | 7. Roge                                          | rs, R. I                                 | I., with                                              | Barrow                                                   | 's 24-inc                                                     | ch Theod                                                           | olite No. 2.                                                                                             |  |  |
| Angle                      |                                          |                                            | Cir                                      | rcle readi                                                                   | ngs, telesc                                      | ope being                                | set on V                                              | 711                                                      |                                                               |                                                                    | M = Mean of Groups                                                                                       |  |  |
| between                    | <b>254°</b> 30′                          | 74° 30′                                    | 333° 41′                                 | 153° 41′                                                                     | 52° 54′                                          | <b>23</b> 2° 54′                         | 132°6′                                                | <b>3</b> 12 <b>°</b> 6′                                  | <b>2</b> 11° 18′                                              | <b>31° 18′</b>                                                     | w = Relative Weight<br>C = Concluded Angle                                                               |  |  |
| VII & VIII                 | "<br>k 4.90<br>k 4.34<br>k 3.24          | "<br>h 4°44<br>h 5°54<br>h 5°62            | "<br>h 5°22<br>h 4°96<br>h 4°84          | "<br>h 5°08<br>h 4°12<br>h 6°08                                              | "<br>h 4·46<br>h 5·22<br>h 4·54                  | "<br>h 4°04<br>h 5°72<br>h 5°86          | "<br>h 5·32<br>h 4·86<br>h 5·16                       | "<br>h 4 44<br>h 5 28<br>h 4 50                          | "<br>h 5°62<br>h 4°64<br>h 6°28                               | *<br>h 6·46<br>h 4·90<br>h 5·14                                    | $M = 5'' \cdot 03$ $w = 35 \cdot 70$ $I = 0 \cdot 02$                                                    |  |  |
|                            | 4.10                                     | 5.30                                       | 5.01                                     | 5.09                                                                         | 4.24                                             | 5.31                                     | 2.11                                                  | · 4°74                                                   | 5.21                                                          | 5.20                                                               | $\begin{bmatrix} w & - & 0 & 0 \\ 0 & - & 0 & 0 \\ C & = & 47^{\circ} & 2' & 5'' \cdot 03 \end{bmatrix}$ |  |  |
| VIII & XII                 | h 49°78<br>h 49°72<br>h 50°32            | k 49°34<br>k 50°84<br>k 49°30              | h 50°44<br>h 48°06<br>h 50°54<br>h 49°86 | h 49°26<br>h 50°36<br>h 48°36                                                | h 47 · 78<br>h 48 · 32<br>h 49 · 12<br>h 50 · 64 | h 49°46<br>h 49°48<br>h 49°28            | h 49 · 40<br>h 50 · 54<br>h 49 · 96                   | h 49°20<br>h 48°80<br>h 48°46<br>h 49°64                 | h 48 · 18<br>h 48 · 42<br>h 48 · 02<br>h 50 · 00<br>h 51 · 20 | k 48 · 74<br>k 49 · 14<br>k 50 · 44                                | $M = 49'' \cdot 48$ $w = 29 \cdot 46$ $\frac{1}{m} = 0 \cdot 03$                                         |  |  |
| •                          | 49*94                                    | 49.83                                      | 49.73                                    | 49`33                                                                        | 48.96                                            | 49.41                                    | 49`97                                                 | 49*03                                                    | 49.16                                                         | 49.44                                                              | $\tilde{C} = 58^{\circ} 28' 49'' \cdot 46$                                                               |  |  |
|                            | <u>.</u>                                 |                                            | <u></u>                                  |                                                                              | At 2                                             | XI (Ad                                   | ori)                                                  |                                                          |                                                               |                                                                    |                                                                                                          |  |  |
| Ď                          | ecember :                                | 18 <b>73 ;</b> ol                          | bserved i                                | by Lieu                                                                      | t. <b>J</b> . Hi                                 | ll, R.E.                                 | , with B                                              | arrow's                                                  | 24-inch                                                       | Theodol                                                            | ite No. 2.                                                                                               |  |  |
| Angle<br>between           | 247° 55′                                 | 67° 54′                                    | Ci<br>327° 21′                           | rcle readi<br>147° 20                                                        | ngs, teles<br>46° 21'                            | cope bein;<br>226° 20'                   | g set on X<br>125° 38′                                | CIV<br>805° 37'                                          | 204° 46′                                                      | 24° 46′                                                            | M = Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle                                         |  |  |
| XIV & XIII                 | n<br>h 43 · 70<br>h 42 · 50<br>h 43 · 36 | <b>h</b> 45 • 42<br>l 45 • 56<br>l 45 • 24 | *<br>1 43 · 50<br>1 43 · 90<br>1 44 · 58 | "<br>2 44 · 36<br>2 42 · 92<br>2 44 · 42<br>2 41 · 78                        | "<br>h 45 * 32<br>h 44 * 36<br>h 45 * 56         | "<br>h 43 • 30<br>h 44 • 94<br>h 44 • 84 | "<br>7 43 · 38<br>7 41 · 82<br>7 43 · 72              | "<br>h 44 · 30<br>h 44 · 50<br>h 43 · 90                 | "<br>  43`72<br>  44`70<br>  43`96                            | "<br>2 43 • 46<br>2 43 • 42<br>2 45 • 06                           | $M = 44'' \cdot 05$ $w = 12 \cdot 57$ $\frac{1}{w} = 0 \cdot 08$                                         |  |  |
|                            | 43.19                                    | 45.41                                      | 43 99                                    | 43.12                                                                        | 45.08                                            | 44.36                                    | 42.97                                                 | 44°23                                                    | 44.13                                                         | 43 . 98                                                            | $\tilde{C} = 53^{\circ} 27' 44'' \cdot 05$                                                               |  |  |

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| At XI (Adori)-(Continued). |                                                       |                                       |                                           |                                          |                                                                |                                          |                                                          |                                                 |                                         |                                          |                                                                        |  |
|----------------------------|-------------------------------------------------------|---------------------------------------|-------------------------------------------|------------------------------------------|----------------------------------------------------------------|------------------------------------------|----------------------------------------------------------|-------------------------------------------------|-----------------------------------------|------------------------------------------|------------------------------------------------------------------------|--|
| Angle<br>between           | 247° 55′                                              | 67° 54′                               | Ci<br>827° 21′                            | rcle readi<br>147° 20'                   | ings, teles<br>46°21'                                          | cope being<br>226°20'                    | 3 set on X<br>125° 38'                                   | (IV<br>805°37'                                  | 201°46'                                 | 24° 46″ .                                | M = Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle       |  |
| XIII & XII                 | "                                                     | "<br>k 4 • 92<br>l 4 • 08<br>l 3 • 88 | "<br>  5°54<br>  6`26<br>  3`28<br>  4`12 | "<br>2 4 · 18<br>2 4 · 60<br>2 3 · 84    | "<br>h 3`28<br>h 5`14<br>h 3`24                                | "<br>\$ 4.24<br>\$ 3.72<br>\$ 4.08       | "<br>  4·22<br>  3·98<br>  4·50                          | "<br>h 5 • 36<br>h 5 • 40<br>h 3 • 86           | "<br>  5`04<br>  3`24<br>  4`32         | "<br>7 4 84<br>7 4 58<br>7 4 30          | $M = 4'' \cdot 29$ $w = 39 \cdot 20$ $\frac{1}{w} = 0 \cdot 03$        |  |
|                            | · 3·87                                                | 4.39                                  | 4.80                                      | 4.31                                     | 3.80                                                           | 4.01                                     | 4.53                                                     | 4.87                                            | 4.30                                    | 4.22                                     | $C = 58^{\circ} 35' 4'' \cdot 3^{\circ}$                               |  |
| Marc                       | h 1873;                                               | observe                               | d by Lie                                  | ut. M.                                   | W. Rog                                                         | vers, R.1                                | E., with                                                 | Barrow                                          | 's 24-inc                               | ch Theod                                 | olite No. 2.                                                           |  |
| Angle                      |                                                       |                                       | Ci                                        | rcle readi                               | ings, teles                                                    | cope bein                                | g set on X                                               | CII                                             |                                         |                                          | M = Mean of Groups<br>= Rolatize Waight                                |  |
| between                    | 0° 0′                                                 | 180° 0'                               | 79° 12′                                   | <b>2</b> 59° 12′                         | 158° 25′                                                       | <b>3</b> 38° 25′                         | 237° 36′                                                 | 57° 36′                                         | <b>316° 49'</b>                         | 136° 49′ .                               | C = Concluded Angle                                                    |  |
| XII & VIII                 | "<br>h 53 • 48<br>h 56 • 14<br>h 56 • 02<br>h 54 • 00 | "<br>h 54•52<br>h 54•84<br>h 54•18    | "<br>k 54 • 44<br>k 55 • 28<br>k 54 • 90  | n 55°94<br>h 54°94<br>h 54°94<br>h 54°98 | "<br>h 55 °96<br>h 53 °96<br>l 53 °30<br>l 55 °84<br>d 54 ° 13 | "<br>1 53 ° 64<br>1 55 ° 78<br>1 55 ° 82 | "<br>l 53.64<br>l 53.78<br>l 52.94<br>h 54.90<br>d 53.76 | "<br>h 56°62<br>h 55°50<br>h 54°50<br>h 56°86   | "<br>h 55°36<br>h 54°52<br>h 53°36      | "<br>h 54 ° 90<br>h 54 ° 28<br>h 53 ° 28 | $M = 54'' \cdot 72$ $w = 19 \cdot 29$ $\frac{1}{w} = 0 \cdot 05$       |  |
|                            | 54.91                                                 | 54.21                                 | 54.87                                     | 54`99                                    | 54.04                                                          | 55.02                                    | 53.80                                                    | 55.87                                           | 54.41                                   | 54.12                                    | $C = 72^{\circ}  14'  54'' \cdot 72$                                   |  |
| VIII & IX                  | h 11°30<br>h 11°92<br>h 11°48                         | h 10°54<br>h 10°72<br>h 10°90         | h 11.26<br>h 9.54<br>h 10.16              | h 9.72<br>h 11.36<br>h 10.10             | h 11.08<br>h 12.00<br>h 12.60<br>d 11.25                       | l 10.76<br>l 11.64<br>l 9.24<br>l 11.56  | l 10°32<br>h 11°62<br>h 10°34<br>d 10°70                 | l 11 · 12<br>l 9 · 64<br>l 10 · 52<br>l 10 · 74 | h 10°14<br>h 10°74<br>h 9°20<br>h 10°64 | h 11.08<br>h 11.10<br>h 10.38            | $M = 10'' \cdot 78$<br>$w = 27 \cdot 45$<br>$\frac{1}{2} = 0 \cdot 04$ |  |
|                            | 11.22                                                 | 10.23                                 | 10.35                                     | 10.39                                    | 11.23                                                          | 10.80                                    | 10.75                                                    | ¦10.20                                          | 10.18                                   | 10.87                                    | $C = 57^{\circ} 6' 10'' \cdot 78$                                      |  |

## At XII (Dugur)

March 1873; observed by Lieut. M. W. Rogers, R. E., with Barrow's 24-inch Theodolite No. 2.

| Angle    |                                                        | M = Mean of Groups                                                     |                              |                                       |                                |                                  |                                       |                                   |                                  |                                 |                                                                 |
|----------|--------------------------------------------------------|------------------------------------------------------------------------|------------------------------|---------------------------------------|--------------------------------|----------------------------------|---------------------------------------|-----------------------------------|----------------------------------|---------------------------------|-----------------------------------------------------------------|
| between  | 0°0′                                                   | 180° 0'                                                                | 79 <b>°</b> 13′              | 259° 13′                              | 158° 24′                       | 338° 24′                         | 237° 37′                              | 57° 37′                           | 316° <b>49'</b>                  | 136° 49′                        | c = Relative Weight<br>C = Concluded Angle                      |
| X & VIII | "<br>k 10°12<br>k 10°64<br>k 7°60<br>k 11°04<br>k 8°92 | "<br><b>h</b> 8.62<br><b>h</b> 9.34<br><b>h</b> 12.12<br><b>h</b> 9.98 | "<br>h9°28<br>h9°20<br>h9°44 | "<br>h 8 · 70<br>h 9 · 14<br>h 8 · 04 | "<br>h9·88<br>l 8·22<br>l 9·94 | "<br>2 9 98<br>2 10 22<br>2 9 28 | "<br>2 8 • 40<br>2 9 • 70<br>2 8 • 50 | "<br>2 10°28<br>2 9°38<br>2 10°70 | "<br>2 8.90<br>2 9.94<br>2 10.58 | "<br>2 8·84<br>2 9·20<br>2 8·76 | $M = 9'' \cdot 45$ $w = 21 \cdot 09$ $\frac{1}{w} = 0 \cdot 05$ |
|          | 9.66                                                   | 10.03                                                                  | 9.31                         | 8.63                                  | 9:35                           | 9.83                             | 8.87                                  | 10.13                             | 9.81                             | 8.93                            | $C = 81^{\circ} 8' 9'' \cdot 46$                                |

At XII (Dugur)—(Continued).

| Angle<br>between | 0° 0,                              | 180° 0′                               | C<br>79° 18′                       | ircle read<br>259°18'                             | ings, teles<br>158° 24'                  | 338° 24'                           | g set on 2<br>287° 37'                   | 57° 87'                            | 816° 49'                           | 186° 49′                           | M = Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle         |
|------------------|------------------------------------|---------------------------------------|------------------------------------|---------------------------------------------------|------------------------------------------|------------------------------------|------------------------------------------|------------------------------------|------------------------------------|------------------------------------|--------------------------------------------------------------------------|
| VIII & XI        | "<br>k 49°90<br>k 48°24<br>k 49°08 | "<br>\$ 50°10<br>\$ 48°72<br>\$ 48°22 | "<br>h 49°90<br>h 48°02<br>h 48°22 | "<br>• <b>h 48 • 16</b><br>h 47 • 56<br>h 49 • 44 | "<br>h 47 ° 02<br>l 48 ° 44<br>l 47 ° 76 | "<br>  47°40<br>  48°78<br>  48°40 | "<br>2 47 ° 90<br>2 48 ° 44<br>2 48 ° 40 | "<br>  47°78<br>  48°56<br>  48°02 | "<br>  49`80<br>  48`54<br>  49`94 | "<br>  48.08<br>  48.60<br>  49.18 | $M = 48'' \cdot 55$ $w = 25 \cdot 60$ $\frac{1}{-} = 0 \cdot 04$         |
|                  | 49.07                              | 49.01                                 | 48.71                              | 48.39                                             | 47.74                                    | 48.19                              | 48.25                                    | 48.12                              | 49*43                              | 48.02                              | $\begin{bmatrix} w \\ C \\ = 53^{\circ} 27' 48'' \cdot 55 \end{bmatrix}$ |

December 1873; observed by Lieut. J. Hill, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle     |                                 |                                               |                                                                     | M = Mean of Groups                                                |                                               |                                    |                                               |                                          |                                    |                                    |                                                                                                              |
|-----------|---------------------------------|-----------------------------------------------|---------------------------------------------------------------------|-------------------------------------------------------------------|-----------------------------------------------|------------------------------------|-----------------------------------------------|------------------------------------------|------------------------------------|------------------------------------|--------------------------------------------------------------------------------------------------------------|
| between   | <b>0°</b> 0′                    | 179° 59'                                      | <b>79° 11′</b>                                                      | <b>259°</b> 10′                                                   | 158° 25'                                      | 838° 25'                           | 237° 36′                                      | 57° 85'                                  | <b>8</b> 16° 47′                   | <b>136° 47′</b>                    | w = Relative Weight<br>C = Concluded Angle                                                                   |
| XI & XIII | "<br>ħ38*88<br>ħ38*68<br>ħ38*00 | "<br>k 39°30<br>k 36°60<br>k 37°24<br>k 36°90 | "<br>h 40°54<br>h 38°08<br>h 37°10<br>h 36°18<br>h 37°00<br>h 35°90 | "<br>h 37 •98<br>h 37 • 72<br>h 37 • 24                           | "<br>  37`34<br>  37`96<br>  39`58<br>  39`44 | "<br>  39.16<br>  39.46<br>  38.06 | "<br>h 36·36<br>h 36·54<br>h 38·42<br>h 37·38 | "<br>k 37 * 10<br>k 37 * 52<br>k 37 * 70 | "<br>h 38.00<br>h 37.46<br>h 37.04 | "<br>1 37 82<br>1 36 84<br>1 37 28 | $M = 37'' \cdot 80$<br>$w = 16 \cdot 61$<br>$\frac{1}{w} = 0 \cdot 06$<br>$C = 49^{\circ} 54' 37'' \cdot 79$ |
|           | 38.22                           | 37.21                                         | 37.47                                                               | 37.65                                                             | 38.28                                         | 38.89                              | 37.18                                         | 37.44                                    | 37.20                              | 37.31                              | - +> 51 57 77                                                                                                |
| XIII & XV | h 7°04<br>h 7°28<br>h 7°22      | ћ 6°72<br>ћ 8°14<br>ћ 8°78<br>ћ 8°94          | h 3.42<br>h 5.82<br>h 7.42<br>h 4.98<br>h 4.40                      | ћ б <sup>.</sup> 78<br>ћ б <sup>.</sup> 22<br>ћ 5 <sup>.</sup> 48 | l 5.00<br>l 7.60<br>l 6.20<br>l 5.80          | 1 5.66<br>1 7.34<br>1 6.66         | h 7°48<br>h 7°10<br>h 6°28                    | h 8°20<br>h 7°70<br>h 7°04               | h 8°14<br>l 7°94<br>l 8°54         | 2 7.88<br>h 8.36<br>h 6.96         | $M = 6'' \cdot 99$ $w = 8 \cdot 65$ $\frac{1}{2} = 0 \cdot 12$                                               |
|           | 7.18                            | 8.12                                          | 5.31                                                                | 6.10                                                              | 6.12                                          | 6.22                               | 6.92                                          | 7.65                                     | 8.31                               | 7.73                               | $C = 55^{\circ} 52' 6'' \cdot 98$                                                                            |

At XIII (Ketu)

December 1873; observed by Lieut. J. Hill, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle    |                                          | Circle readings, telescope being set on XII |                                    |                                    |                                               |                                    |                                    |                                    |                                |                                    |                                                                  |  |  |  |
|----------|------------------------------------------|---------------------------------------------|------------------------------------|------------------------------------|-----------------------------------------------|------------------------------------|------------------------------------|------------------------------------|--------------------------------|------------------------------------|------------------------------------------------------------------|--|--|--|
| between  | 859° 59′                                 | 179° 59′                                    | <b>79° 11′</b>                     | 259° 10′                           | 158° 23′                                      | 338° 23′                           | 237° 38′                           | 57° 38′                            | 316° 49′                       | 136° 49′                           | C = Concluded Angle                                              |  |  |  |
| XII & XI | "<br>l 21 * 28<br>l 20 * 04<br>k 21 * 68 | "<br>l 20°60<br>l 19°26<br>l 19°54          | "<br>h 20°92<br>h 20°70<br>l 20°30 | "<br>l 19°42<br>l 18°76<br>l 18°74 | "<br>h 17 98<br>h 19 90<br>h 20 92<br>h 20 58 | "<br>  20°42<br>  21°40<br>  20°04 | "<br>k 20°36<br>k 20°36<br>k 20°80 | "<br>h 19°76<br>h 19°34<br>l 19°68 | "<br>18.84<br>120.78<br>120.20 | "<br>k 19°00<br>l 20°28<br>l 19°26 | $M = 20'' \cdot 04$ $w = 19 \cdot 05$ $\frac{1}{w} = 0 \cdot 05$ |  |  |  |
|          | 21.00                                    | 19.80                                       | 10.22                              | 18.97                              | 19.85                                         | 20.03                              | 20.21                              | 19.29                              | 19'94                          | 19.21                              | $\int C = 71^{\circ} 30' 20'' \cdot 04$                          |  |  |  |

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| $\mathbf{At}$ | XIII | (Ketu) | )—( | [Continued] | ). |
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|---------------|------|--------|-----|-------------|----|

|                  |                                              |                                                                                           |                                                     |                                              |                                                    |                                  |                                                                               |                                                                     |                                                    |                                                        | ,                                                                                                   |
|------------------|----------------------------------------------|-------------------------------------------------------------------------------------------|-----------------------------------------------------|----------------------------------------------|----------------------------------------------------|----------------------------------|-------------------------------------------------------------------------------|---------------------------------------------------------------------|----------------------------------------------------|--------------------------------------------------------|-----------------------------------------------------------------------------------------------------|
| Angle<br>between | 359° 59′                                     | 179°59′                                                                                   | Ci<br>79°11′                                        | rclo readi<br>259°10'                        | ngs, teleso<br>158° 23'                            | cope being<br>338° 23'           | 3 set on X<br>237° 38′                                                        | II<br>57° 38′                                                       | <b>316° 49′</b>                                    | 136° 49′                                               | M - Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle                                    |
| XI & XIV         | l 25.66<br>h 25.88<br>h 27.84<br>h 26.66     | <i>x</i><br><i>l</i> 24.60<br><i>l</i> 26.72<br><i>l</i> 26.68<br><i>d</i> 26.63<br>26.16 | "<br>h 26.86<br>h 25.20<br>l 27.00<br>26.35         | *<br>l 27.82<br>l 26.90<br>l 27.06           | <i>h</i> 25.98<br><i>h</i> 26.20<br><i>h</i> 26.44 | 25.56<br>25.60<br>27.22<br>26.13 | <i>k</i> 26°06<br><i>k</i> 25°74<br><i>k</i> 25°58<br><i>k</i> 27°38<br>26°19 | <i>h</i> 26 · 52<br><i>h</i> 26 · 34<br><i>l</i> 25 · 74<br>26 · 20 | <i>t</i> 28.10<br><i>h</i> 26.12<br><i>h</i> 28.12 | <i>h</i> 25°90<br><i>h</i> 25°82<br><i>l</i> 27°14<br> | $M = 26'' \cdot 48$ $w = 25 \cdot 84$ $\frac{1}{w} = 0 \cdot 04$ $C = 48^{\circ} 51' 26'' \cdot 47$ |
| XIV & XVI        | h 51 · 52<br>h 52 · 58<br>h 52 · 64          | 2 53 90<br>2 51 46<br>2 52 64<br>2 53 08<br>d 53 40                                       | k 52°16<br>k 54°70<br>k 52°22<br>l 50°80<br>l 50°92 | l 52°28<br>l 52°54<br>l 52°00                | h 52°20<br>h 51°40<br>h 52°94                      | l 52.50<br>l 52.70<br>l 52.20    | h 52°94<br>h 52°74<br>h 54°58                                                 | h 52.58<br>h 52.34<br>l 51.62                                       | l 53.06<br>h 54.12<br>h 54.10                      | h 53 · 48<br>h 53 · 62<br>l 51 · 96                    | $M = 52'' \cdot 66$ $w = 18 \cdot 90$ $\frac{1}{2} = 0 \cdot 05$                                    |
|                  | 52.25                                        | 52.90                                                                                     | 52.16                                               | 52.27                                        | 52.18                                              | 52.47                            | 53.42                                                                         | 52.18                                                               | 53.26                                              | 53.02                                                  | $C = 49^{\circ} 3' 52'' \cdot 65$                                                                   |
| XVI & XVII       | k 18.40<br>k 18.86<br>k 19.08                | l 19°44<br>h 19°78<br>l 19°18                                                             | h 19°54<br>h 17°26<br>l 18°76<br>l 18°62            | l 20°94<br>l 19°36<br>l 21°18                | h 19.68<br>h 19.64<br>h 20.12                      | 2 18·38<br>2 20·12<br>2 19·88    | k 19°24<br>k 19°90<br>k 17°96                                                 | h 18.40<br>h 20.28<br>l 20.12                                       | l 18.86<br>h 18.90<br>h 19.94                      | h 18·42<br>h 18·54<br>l 18·62                          | $M = 19'' \cdot 29$<br>$w = 20 \cdot 13$<br>$\frac{1}{2} = 0 \cdot 05$                              |
|                  | 18.78                                        | 19.47                                                                                     | 18.22                                               | 20.49                                        | 19.81                                              | 19.46                            | 19.03                                                                         | 19.60                                                               | 19.23                                              | 18.23                                                  | $\overset{w}{C} = 62^{\circ} 58' 19'' \cdot 29$                                                     |
| XVII & XV        | h 27°74<br>h 30°12<br>h 29°50<br>h 28°02     | h 28.78<br>l 29.86<br>l 29.52                                                             | h 29°72<br>h 28°56<br>l 30°56                       | l 27°96<br>l 29°12<br>l 29°40                | h 27.72<br>h 28.36<br>h 28.82                      | 2 30°20<br>2 28°66<br>2 28°40    | <b>h</b> 28 · 16<br><b>h</b> 28 · 14<br><b>h</b> 28 · 78                      | h 28.48<br>h 27.86<br>l 29.64                                       | l 29°40<br>h 27°60<br>h 27°44                      | <b>h</b> 29°48<br><b>h</b> 28°40<br><b>l</b> 29°30     | $M = 28'' \cdot 83$ $w = 25 \cdot 28$ $\frac{1}{-} = 0 \cdot 04$                                    |
|                  | 28.85                                        | 29.39                                                                                     | 29.61                                               | 28.83                                        | 28.30                                              | 29.09                            | 28.36                                                                         | <b>2</b> 8.66                                                       | 28.12                                              | <b>2</b> 9°06                                          | $\begin{bmatrix} w \\ C = 71^{\circ} 51' 28'' \cdot 83 \end{bmatrix}$                               |
| XV & X11         | h 34 °08<br>h 31 °40<br>h 32 °24<br>h 30 °80 | k 31 · 72<br>l 30 · 94<br>l 31 · 94                                                       | h 30 · 98<br>h 31 · 86<br>l 31 · 86                 | 2 31 °04<br>2 33 °60<br>2 32 °88<br>2 32 °76 | h 31 °60<br>h 31 °98<br>h 33 °06                   | l 32°22<br>l 31°86<br>l 32°96    | h 33.70<br>h 32.64<br>h 32.28                                                 | h 33 · 90<br>h 33 · 14<br>l 32 · 66                                 | l 32°02<br>h 31°60<br>h 30°72                      | k 33°20<br>l 33°26<br>l 33°34                          | $M = 32'' \cdot 32$ $w = 16 \cdot 62$ $\frac{1}{m} = 0 \cdot 06$                                    |
|                  | 32.13                                        | 31.23                                                                                     | 31.22                                               | 32.57                                        | 32.51                                              | 32.35                            | 32.87                                                                         | 33.53                                                               | 31.45                                              | 33°27                                                  | $\overset{\omega}{C} = 55^{\circ} 44' 32'' \cdot 32$                                                |

At XIV (Sulkia Thalau)

December 1873; observed by Lieut. J. Hill, R. E., with Barrow's 24-inch Theodolite No. 2.

| Angle      |                                                          | M = Mean of Groups                       |                                               |                                               |                                       |                                       |                                    |                                               |                                    |          |                                                                    |
|------------|----------------------------------------------------------|------------------------------------------|-----------------------------------------------|-----------------------------------------------|---------------------------------------|---------------------------------------|------------------------------------|-----------------------------------------------|------------------------------------|----------|--------------------------------------------------------------------|
| between    | 0° 0′                                                    | 179°59′                                  | 79° 13′                                       | 259° 13′                                      | 158° 25'                              | 338° 24′                              | 237° 35′                           | 57° 34′                                       | 316° 48′                           | 136° 47′ | w = Relative Weight<br>C = Concluded Angle                         |
| XVI & XIII | "<br>h 52°12<br>h 49°98<br>h 51°70<br>h 53°32<br>h 52°82 | "<br>h 51 · 18<br>h 50 · 52<br>h 50 · 52 | "<br>h 50°54<br>h 52°70<br>h 52°96<br>h 50°40 | "<br>h 52°24<br>h 50°58<br>h 50°06<br>h 50°72 | "<br>\$ 50°20<br>\$ 50°00<br>\$ 49°80 | "<br>\$ 49°22<br>\$ 49°16<br>\$ 51°32 | "<br>h 49°50<br>h 51°06<br>h 50°66 | "<br>h 50°00<br>h 52°14<br>h 51°28<br>h 52°26 | "<br>h 49°48<br>h 50°42<br>h 50°16 | "        | $M = 50^{"} \cdot 71$ $w = 12 \cdot 78$ $\frac{1}{w} = 0 \cdot 08$ |
|            | 51.99                                                    | 50.74                                    | 51.62                                         | 50.90                                         | 50.00                                 | 49.90                                 | 50.41                              | 51.42                                         | 50°02                              | 50.10    | $C = 67^{\circ} 5' 5^{\circ'} 74$                                  |

| At XIV (Sulkia Thalau)—(Continued). |                                                   |                                               |                                       |                                          |                                        |                                                       |                                          |                                                          |                                        |                                                                          |                                                                                                           |  |  |
|-------------------------------------|---------------------------------------------------|-----------------------------------------------|---------------------------------------|------------------------------------------|----------------------------------------|-------------------------------------------------------|------------------------------------------|----------------------------------------------------------|----------------------------------------|--------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------|--|--|
| Angla                               |                                                   |                                               | Ci                                    | rcle readir                              | ngs, telesc                            | ope being                                             | set on X                                 | VI                                                       |                                        |                                                                          | M = Mean of Groups                                                                                        |  |  |
| between                             | 0° 0′                                             | 179° 59′                                      | 79° 13′                               | <b>25</b> 9° 13′                         | 158° 25′                               | 338° 24'                                              | 237° 35′                                 | 57° <b>34</b> ′                                          | 316° 48′                               | 136° 47′                                                                 | w = Relative Weight<br>C = Concluded Angle                                                                |  |  |
| XIII & XI                           | # 48 ° 96<br>h 50 ° 22<br>h 49 ° 88               | r<br>h 50°64<br>h 50.54<br>h 49°94            | "<br>h 50° 16<br>h 49° 46<br>h 48° 94 | "<br>h 50°12<br>h 50°62<br>h 50°04       | <b>h</b> 49°84<br>l 50°72<br>l 50°80   | "<br>2 48 · 62<br>h 51 · 34<br>h 49 · 30<br>h 49 · 66 | "<br>h 49°40<br>h 49°22<br>h 50°70       | "<br>h 49`56<br>h 50`10<br>h 50`02                       | "<br>h 50°38<br>h 52°08<br>h 51°92     | "<br>k 51 ° 02<br>k 51 ° 86<br>k 49 ° 98                                 | $M = 50'' \cdot 21$ $w = 19 \cdot 32$ $\frac{1}{w} = 0 \cdot 05$                                          |  |  |
|                                     | 49.69                                             | 50.32                                         | 49.22                                 | 50.30                                    | 50.42                                  | 49.73                                                 | <b>4</b> 9`77                            | 49*89                                                    | 51.40                                  | 50.02                                                                    | $C = 77^{\circ} 40' 50'' \cdot 21$                                                                        |  |  |
|                                     |                                                   |                                               |                                       |                                          | At XV                                  | / (Malu                                               | nga)                                     |                                                          |                                        |                                                                          | · · ·                                                                                                     |  |  |
| ' Jan                               | uary 18'                                          | 74; obse                                      | rved by                               | Lieut.                                   | J. Hill,                               | <b>R</b> . E.,                                        | with Ba                                  | rrow's 2                                                 | 4-inch                                 | Theodolit                                                                | e No. 2.                                                                                                  |  |  |
| Angle                               |                                                   |                                               | Ci                                    | rcle readi                               | ngs, telesc                            | ope being                                             | set on X                                 | II.                                                      |                                        |                                                                          | M = Mean of Groups                                                                                        |  |  |
| between                             | <b>3</b> 59 <b>° 56</b> ′                         | 179° 55′                                      | 79° 12′                               | <b>2</b> 59° 11′                         | 158° 25′                               | 838° 25′                                              | 237° 34′                                 | 57° 34′                                                  | <b>316° 49'</b>                        | 136° 49′                                                                 | w = Relative Weight<br>C = Concluded Angle                                                                |  |  |
| XII & XIII                          | "<br>h 20`88<br>h 21`92<br>h 22`92                | "<br>h 22.66<br>l 23.34<br>l 22.52<br>h 20.46 | "<br>l 23.66<br>l 22.58<br>l 23.00    | "<br>h 22 ° 02<br>h 20 ° 68<br>h 21 ° 56 | "<br>l 21.62<br>l 21.62<br>l 20.24     | "<br>l 23.70<br>l 23.38<br>l 22.00                    | "<br>h 23 ° 94<br>h 21 ° 96<br>l 22 ° 42 | "<br>l 22°42<br>l 22°84<br>l 24°88<br>h 21°48<br>h 22°68 | "<br>k 22°18<br>k 22°30<br>k 22°42     | "<br>h 22.88<br>h 21.96<br>d 22.88                                       | $M = 22'' \cdot 30$ $w = 15 \cdot 70$ $\frac{1}{w} = 0 \cdot 06$ $C = 68^{\circ} 22' \cdot 22'' \cdot 21$ |  |  |
|                                     | 21.01                                             | 22.25                                         | 23.08                                 | 21.42                                    | <b>31.1Q</b>                           | 23.02                                                 | 22.77                                    | 22.86                                                    | 22.30                                  | 33.18                                                                    | 0 = 00 23 22 31                                                                                           |  |  |
| XIII & XVII                         | h 29.16<br>h 29.16<br>h 26.40<br>h 28.44<br>28.29 | 29.18<br>27.88<br>28.72                       | 29.00<br>27.90<br>27.40               | \$ 28.18<br>\$ 29.72<br>\$ 29.12         | l 30'72<br>l 29'02<br>l 29'88<br>29'88 | 29.46<br>29.14<br>29.34<br>29.31                      | h 29.08<br>h 28.20<br>h 29.40<br>28.89   | l 28.64<br>l 27.68<br>l 27.22<br>l 26.84<br>27.60        | h 28.08<br>h 29.58<br>h 28.52<br>28.73 | k 28 · 10<br>k 27 · 12<br>k 30 · 06<br>k 28 · 64<br>d 29 · 41<br>28 · 67 | $M = 28'' \cdot 71$ $w = 17 \cdot 42$ $\frac{1}{w} = 0 \cdot 06$ $C = 41^{\circ} 2' 28'' \cdot 70$        |  |  |
|                                     |                                                   |                                               | <u></u>                               |                                          |                                        |                                                       |                                          |                                                          |                                        |                                                                          | l                                                                                                         |  |  |
| Ja                                  | nuary 18                                          | 3 <b>74;</b> obs                              | erved by                              | y Lieut.                                 | At XV<br>J. Hill                       | VI (Loh)<br>, <i>R.E.</i> , -                         | aran)<br>with Ba                         | rrow's 2                                                 | 4-inch                                 | Theodoli                                                                 | te No. 2.                                                                                                 |  |  |
| Angle<br>between                    | 0° 0′                                             | 180° 0′                                       | Cir<br>79°12′                         | rcle readi<br>259°12'                    | ngs, teleso<br>158°24'                 | cope being<br><b>3</b> 38° 24'                        | g set on X<br>237° 39'                   | IX<br>57°38'                                             | 316° 49′                               | 136° 49′                                                                 | M = Mean of Groups<br>m = Relative Weight<br>C = Concluded Angle                                          |  |  |
| XIX & XVIII                         | "<br>h 2·44<br>h 3·42<br>h 2·84                   | "<br>l 2.76<br>l 2.04<br>h 2.76               | "<br>h 2.82<br>h 4.16<br>h 2.36       | "<br>h 1·38<br>h 2·00<br>h 1·92          | "<br>l 1.26<br>l 1.00<br>h 2.62        | "<br><b>h</b> 2°08<br><b>h</b> 0°48<br><b>h</b> 2°02  | "<br>1 0.86<br>1 1.74<br>2 0.66          | "<br>h 0.58<br>h 1.04<br>h 1.48                          | "<br>h 0.64<br>l 2.02<br>l 2.28        | "<br>2 2 · 16<br>h 2 · 70<br>h 2 · 44                                    | $M = 1'' \cdot 97$ $w = 15 \cdot 90$ $\frac{1}{w} = 0 \cdot 06$ $C = r c^{\circ} r 6' \cdot 1'' \cdot 07$ |  |  |
|                                     | 2.90                                              | 2.23                                          | 3.11                                  | 1.22                                     | 1.03                                   | 1.23                                                  | 1.09                                     | 1.03                                                     | 1.02                                   | 2.43                                                                     | 0 - 55 50 1 97                                                                                            |  |  |

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• At XVI (Loharan)-(Continued).

|              |                                          |                                          |                                                   |                                               |                                    |                                                   |                                    |                                          |                                          | ·                                        |                                                                        |
|--------------|------------------------------------------|------------------------------------------|---------------------------------------------------|-----------------------------------------------|------------------------------------|---------------------------------------------------|------------------------------------|------------------------------------------|------------------------------------------|------------------------------------------|------------------------------------------------------------------------|
| Angle        |                                          |                                          | Cir                                               | cle readin                                    | gs, telesco                        | ope being                                         | set on X                           | IX                                       |                                          |                                          | M - Mean of Groups                                                     |
| between      | 0° 0′                                    | 180° 0'                                  | <b>79°</b> 12′                                    | 259° 12′                                      | 158° 24′                           | 338° 24′                                          | <b>237° 3</b> 9′                   | 57° 38′                                  | 316° 49′                                 | 136° 49′                                 | C = Concluded Angle                                                    |
| XVIII & XVII | *<br>* 49 * 08<br>* 48 * 48<br>* 49 * 28 | *<br>h 49°06<br>h 49°98<br>h 49°76       | "<br>\$ 51.06<br>\$ 48.84<br>\$ 50.52<br>\$ 48.66 | "<br>h 50°42<br>h 50°24<br>l 50°28<br>h 51°50 | "<br>2 50`86<br>2 49`24<br>h 49`72 | "<br>h 50°60<br>h 49°56<br>h 50°08                | "<br>  49`62<br>  48`38<br>  49`42 | "<br>h 49 ° 68<br>h 51 ° 08<br>h 49 ° 88 | "<br>h 51 · 48<br>l 50 · 66<br>l 49 · 98 | "<br>1 48 • 78<br>1 48 • 80<br>1 48 • 60 | $M = 49'' \cdot 77$ $w = 17 \cdot 70$ $\frac{1}{w} = 0 \cdot 06$       |
|              | 48.95                                    | 49.60                                    | 49°77                                             | 50.01                                         | 49 94                              | 50.08                                             | 49.14                              | 50.31                                    | 50.21                                    | 48.73                                    | $C = 61^{\circ} 47' 49'' 77$                                           |
| XVII & XIII  | h 50°92<br>h 50°86<br>h 50°24            | h 50°36<br>h 50°86<br>h 50°60            | l 49°56<br>h 51°08<br>h 49°18<br>h 50°26          | h 51°24<br>h 49°88<br>l 51°02                 | l 50°12<br>h 49°02<br>h 49°30      | h 48 · 82<br>h 50 · 04<br>h 51 · 04,<br>h 49 · 76 | l 50°68<br>l 50°36<br>l 49°96      | h 49 ° 68<br>h 49 ° 36<br>h 49 ° 24      | h 49°46<br>l 50°16<br>l 49°50            | l 49·84<br>h 49·46<br>h 50·08            | $M = 50'' \cdot 07$ $w = 31 \cdot 70$ $I = 0 \cdot 03$                 |
|              | 50.62                                    | 50.01                                    | 50.03                                             | 50.21                                         | 49.48                              | 49'92                                             | 50.33                              | 49'43                                    | 49.71                                    | 49`79                                    | $C = 50^{\circ} 21' 50'' \cdot 07$                                     |
| XIII & XIV   | h 17°78<br>h 17°72<br>h 15°96            | l 17.00<br>l 15.92<br>h 16.00<br>h 18.76 | h 17 °00<br>h 17 °50<br>h 17 °42                  | h 17 82<br>h 17 18<br>l 17 20                 | l 17°36<br>h 18°44<br>h 17°68      | h 18·18<br>h 17:12<br>h 18·12                     | l 16.72<br>l 17.18<br>l 17.22      | h 18°04<br>h 16°58<br>h 17°06            | l 16°90<br>l 18°06<br>l 18°86            | h 18°18<br>h 17°90<br>h 17°02            | $M = 17'' \cdot 43$<br>$w = 36 \cdot 30$<br>$\frac{1}{2} = 0 \cdot 03$ |
| •            | 17.15                                    | 16.93                                    | 17.31                                             | 17.40                                         | 17.83                              | 17.81                                             | 17.04                              | 17.23                                    | 17.94                                    | 17.70                                    | $C = 63^{\circ} 50' 17'' \cdot 42$                                     |

# At XVII (Chamu)

January 1874; observed by Lieut. J. Hill, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle<br>between | 0° 2′                                      | 180° 1′                                  | Ci<br>79° 7′                    | rcle readi<br>259°6′            | ngs, teles<br>158°24′           | cope being<br>838° 24'          | g set on X<br>237° 37'                   | 57° 37′                         | 316° <b>4</b> 7′                          | 136° 47′                        | M = Mean of Groups<br>m = Relative Weight<br>C = Concluded Angle |
|------------------|--------------------------------------------|------------------------------------------|---------------------------------|---------------------------------|---------------------------------|---------------------------------|------------------------------------------|---------------------------------|-------------------------------------------|---------------------------------|------------------------------------------------------------------|
| XV & XIII        | "<br>h 4°34<br>h 3°86<br>h 3°36            | h 3.92<br>h 2.76<br>h 4.78<br>h 3.36     | "<br>l 2·68<br>l 2·84<br>h 2·94 | "<br>h 5°26<br>h 4°56<br>h 3°56 | "<br>h 2°78<br>h 2°78<br>l 4°12 | "<br>2 4·56<br>2 2·84<br>2 3·18 | "<br>2 3·94<br>2 4·00<br>2 4·66          | "<br>h 4·40<br>h 2·96<br>h 3·78 | "<br>l 2.98<br>l 3.94<br>l 3.64<br>d 3.47 | "<br>h 1°74<br>h 3°14<br>h 3°70 | $M = 3'' \cdot 59$ $w = 25 \cdot 40$ $\frac{1}{w} = 0 \cdot 04$  |
|                  | 3.82                                       | 3.21                                     | 2.82                            | 4.40                            | 3.53                            | 3.23                            | 4.30                                     | 3.21                            | 3.21                                      | 2.80                            | $C = 67^{\circ} 6' 3'' \cdot 59$                                 |
| XIII & XVI       | <b>h</b> 51 ° 96<br>h 52 ° 24<br>l 51 ° 02 | h 52.90<br>h 50.74<br>h 50.42<br>h 51.24 | l 50.88<br>l 51.08<br>h 51.56   | h 52.80<br>h 52.30<br>h 51.52   | h 50°72<br>h 52°68<br>l 51°34   | l 52·38<br>l 51·40<br>l 52·08   | l 52°22<br>l 50°20<br>h 51°06<br>h 51°54 | h 50°52<br>h 51°88<br>h 50°36   | l 52.82<br>l 51.50<br>l 52.12<br>d 52.13  | h 50°60<br>h 52°52<br>h 51°36   | $M = 51'' \cdot 58$ $w = 30 \cdot 57$ $\frac{1}{2} = 0 \cdot 03$ |
| v                | 51.24                                      | 51.33                                    | 51.12                           | 52.51                           | 51.28                           | 51.92                           | 51.52                                    | 50.93                           | 52.14                                     | 51.49                           | $C = 66^{\circ} 39' 51'' \cdot 58$                               |

At XVII (Chamu)-(Continued).

| Angle       |                                          |                                    | Ci                                            | rcle readi                         | ings, teles                              | cope bein                          | g set on X                               | cv                                 |                                    |                                                               | M = Mean of Groups                                               |
|-------------|------------------------------------------|------------------------------------|-----------------------------------------------|------------------------------------|------------------------------------------|------------------------------------|------------------------------------------|------------------------------------|------------------------------------|---------------------------------------------------------------|------------------------------------------------------------------|
| between     | 0° 2′                                    | 180° 1′                            | 79°7′                                         | 259° 6′                            | 158° 24′                                 | 338° 24′                           | 237° <b>3</b> 7′                         | 57° 37′                            | 316° <b>4</b> 7′                   | 136° 47′                                                      | w = Relative Weight<br>C = Concluded Angle                       |
| XVI & XVIII | "<br>h 38 · 44<br>h 38 · 50<br>l 39 · 92 | "<br>h 39 98<br>h 40 28<br>h 38 98 | "<br>2 38·92<br>2 40·62<br>h 40·98<br>h 40·92 | "<br>h 38·98<br>h 38·42<br>h 40·16 | "<br>k 42 ° 10<br>k 40 ° 76<br>l 40 ° 30 | "<br>2 39`10<br>2 40`06<br>2 39`34 | "<br>1 39 · 58<br>1 39 · 48<br>h 41 · 14 | "<br>h 39.68<br>h 39.12<br>h 39.30 | "<br>k 38·54<br>l 39·42<br>l 38·44 | "<br>h 40°54<br>h 39°54<br>h 40°86                            | $M = 39'' \cdot 74$ $w = 15 \cdot 71$ $\frac{1}{m} = 0 \cdot 06$ |
|             | 38.95                                    | 39.75                              | 40.36                                         | 39.19                              | 41.02                                    | 39.20                              | 40.02                                    | 39`37                              | 38.80                              | 40.31                                                         | $C = 51^{\circ} 41' 39'' \cdot 74$                               |
| XVIII & XX  | h 57*86<br>l 56*90<br>h 57*88            | h 56°40<br>h 57°72<br>h 56°90      | l 57°16<br>l 55°34<br>h 55°72                 | h 57°90<br>h 58°70<br>h 57°82      | h 57°56<br>h 55°56<br>l 57°30            | l 57 38<br>l 57 26<br>l 58 50      | l 57°76<br>l 57°00<br>h 58°06            | h 57°62<br>h 57°88<br>h 58°58      | h 58 92<br>l 57 30<br>l 57 98      | h 58 · 56<br>h 58 · 34<br>h 56 · 30<br>h 57 · 64<br>h 55 · 48 | $M = 57'' \cdot 43$ $w = 16 \cdot 61$ $\frac{1}{w} = 0 \cdot 06$ |
|             | 57*55                                    | 57.01                              | 56.02                                         | 58.14                              | 56.81                                    | 57.21                              | 57.01                                    | 58.03                              | 58.02                              | 57:26                                                         | $\ddot{C} = 58^{\circ} 51' 57'' \cdot 43$                        |

At XVIII (Pelu)

January 1874; observed by Lieut. J. Hill, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle<br>between | 359° 59′                                 | 179° 59′                                 | Ci<br>79° 11′                      | rcle readir<br>259° 11′                  | 158° 20'                                              | cope being<br>338° 19'                        | ; set on X<br>237°37′                    | 57° 36′                                  | <b>3</b> 16° 47′                         | 136° 47′                                 | M = Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle                       |
|------------------|------------------------------------------|------------------------------------------|------------------------------------|------------------------------------------|-------------------------------------------------------|-----------------------------------------------|------------------------------------------|------------------------------------------|------------------------------------------|------------------------------------------|----------------------------------------------------------------------------------------|
| XXI & XXII       | "<br>2 46 • 58<br>k 44 • 78<br>k 44 • 74 | "<br>h 44 ° 34<br>h 46 ° 12<br>h 44 ° 18 | "<br>  44·38<br>  45·42<br>  45·52 | "<br>7 44 • 48<br>7 45 • 78<br>7 43 • 78 | "<br>h 44 · 34<br>h 46 · 42<br>h 44 · 52<br>h 44 · 46 | "<br>h 46.82<br>h 44.08<br>h 45.94<br>h 44.54 | "<br>k 46 · 18<br>l 45 · 04<br>l 44 · 82 | "<br>2 44 ° 06<br>2 45 ° 18<br>2 44 ° 40 | "<br>k 44 · 60<br>k 44 · 58<br>l 44 · 40 | "<br>2 45 • 52<br>2 44 • 54<br>2 44 • 86 | $M = 44'' \cdot 97$ $w = 35 \cdot 94$ $\frac{1}{w} = 0 \cdot 03$                       |
|                  | 45`37                                    | 44.88                                    | 45.11                              | 44.68                                    | 44 94                                                 | <b>4</b> 5°34                                 | 45.35                                    | 41.22                                    | 44°53                                    | <b>44</b> .97                            | $\tilde{C} = 49^{\circ}$ 1' 44" · 98                                                   |
| XXII & XX        | l 37.60<br>h 36.92<br>h 37.22            | h 37 · 70<br>h 36 · 00<br>h 36 · 58      | l 37.66<br>l 35.90<br>l 36.98      | h 35 82<br>h 37 42<br>h 36 04            | h 36°22<br>h 36°48<br>h 37°26                         | h 36°32<br>h 36°54<br>h 36°36                 | h 36°26<br>l 36°42<br>l 36°50            | l 37 °02<br>l 36 °52<br>l 36 °58         | h 36·78<br>h 37·04<br>l 38·60            | l 36°18<br>l 37°30<br>l 36°78            | $M = 36'' \cdot 77$ $w = 45 \cdot 50$ $\frac{1}{2} = 0 \cdot 02$                       |
|                  | 37 • 25                                  | 36.26                                    | <b>36</b> ·85                      | 36.43                                    | 36.62                                                 | 36.41                                         | 36.39                                    | 36.21                                    | 37.47                                    | 36.12                                    | $w = 57^{\circ} 52^{\circ}$<br>$C = 57^{\circ} 22^{\prime} 36^{\prime\prime} \cdot 77$ |
| XX & XVII        | l 36.80<br>h 38.14<br>h 37.84            | h 37°44<br>h 37°64<br>l 36°48            | l 35.84<br>l 36.74<br>h 36.46      | h 36·56<br>h 37·36<br>h 37·76            | h 36.68<br>h 36.34<br>l 35.96                         | h 37 · 68<br>h 36 · 86<br>h 38 · 12           | h 37 .90<br>l 37 .88<br>l 36 .96         | l 36.62<br>l 36.80<br>l 36.42            | 2 38·18<br>2 37·44<br>2 36·20            | l 37·28<br>l 36·38<br>l 36·18            | $M = 37'' \cdot 03$ $w = 29 \cdot 40$ $\frac{1}{2} = 0 \cdot 02$                       |
|                  | 37.59                                    | 37.19                                    | 36.32                              | 37.23                                    | 30.33                                                 | 37.55                                         | 37.58                                    | 30.01                                    | 37°27                                    | 36.01                                    | $ \frac{w}{w} = 61^{\circ} 22' 37'' \cdot 03 $                                         |

| At | XVIII | (Pelu)—( | (Continued) |
|----|-------|----------|-------------|
| At | XVIII | (Pelu)—( | (Continued) |

|                |                                          |                                                  | <u></u>                       |                               |                                     |                                     |                                     |                               |                                     |                                     |                                                                   |
|----------------|------------------------------------------|--------------------------------------------------|-------------------------------|-------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|-------------------------------|-------------------------------------|-------------------------------------|-------------------------------------------------------------------|
| Angle          |                                          |                                                  | Cir                           | cle readin                    | igs, telesc                         | ope being                           | set on X.                           | XI.                           |                                     |                                     | M = Mean of Groups<br>w = Relative Weight                         |
| between        | <b>35</b> 9° 59′                         | 179° 59′                                         | 79° 11′                       | 259° 11′                      | 158° 20′                            | 338° 19′                            | 237° 37′                            | 57° 36′                       | 816° 47′                            | 136° 47′                            | C - Concluded Angle                                               |
| XVII & VVI     | "<br>l 31 · 78<br>h 31 · 86              | "<br>h 31°12<br>h 31°08                          | "<br>1 30.80<br>1 31.92       | "<br>l 30·84<br>h 31·40       | "<br>h 32`20<br>h 31`34             | "<br>h 31°24<br>h 31°50             | "<br>l 32.08<br>l 32.26             | "<br>l 30°18<br>l 31°18       | "<br>  32`30<br>  31`62             | "<br>1 30°08<br>1 31°36             | $M = 31'' \cdot 42$                                               |
| Δ 7 11 0 Δ V I | <b>h</b> 31.00                           | 1 31 . 86                                        | 1 32.02                       | h31.40                        | 1 31.76                             | h31.08                              | 131.04                              | l 32·22<br>l 30·10            | 1 31 . 80                           | 1 30.90                             | $w = 45 \cdot 95$ $\frac{1}{w} = 0 \cdot 02$                      |
|                | 31.22                                    | 31.35                                            | 31.28                         | 31.51                         | 31.22                               | 31.22                               | 31.29                               | 30.92                         | 31.93                               | 30.78                               | $C = 66^{\circ} 30' 31'' \cdot 41$                                |
| XVI & XIX      | l ++ °64<br>h +4 °60<br>h +5 ° 12        | h 45 · 70<br>h 44 · 38<br>l 45 · 60<br>l 46 · 24 | l 45`20<br>l 45`74<br>l 43`76 | l 44°70<br>h 45°16<br>h 44°76 | h 45 · 18<br>h 44 · 42<br>h 44 · 74 | h 45 °68<br>h 45 °58<br>h 43 °82    | l 44 · 28<br>l 44 · 24<br>l 45 · 52 | l 45.60<br>l 46.64<br>l 45.52 | l 43 · 46<br>l 44 · 76<br>l 44 · 52 | l 44 · 82<br>l 44 · 20<br>l 45 · 10 | $M = 44'' \cdot 94$ $w = .31 \cdot 62$ $\frac{1}{2} = 0 \cdot 03$ |
|                | 44.79                                    | 45.48                                            | 44.90                         | 44.87                         | 44.78                               | 45.03                               | 44.68                               | 45.92                         | 44.25                               | 44.21                               | $C = 62^{\circ} 50' 44'' \cdot 95$                                |
| XIX & XXI      | l 42°56<br>l 44°74<br>h 42°84<br>h 42°94 | h 43 · 42<br>h 44 · 26<br>l 44 · 26              | l 45°22<br>l 44°94<br>l 44°42 | l 43°12<br>l 43°96<br>h 42°56 | l 43°90<br>. l 45°00<br>h 44°74     | h 44 · 16<br>h 43 · 48<br>h 44 · 34 | l 44°40<br>l 44°32<br>l 45°50       | l 46.00<br>l 44.88<br>l 45.74 | h 43 · 72<br>l 44 · 68<br>l 44 · 56 | l 45°96<br>l 46°76<br>l 45°78       | $M = 44'' \cdot 46$ $w = 10 \cdot 42$ $\frac{1}{10} = 0 \cdot 10$ |
|                | 43 . 27                                  | 43.98                                            | 44.86                         | 43.51                         | 44.55                               | 43`99                               | 44.24                               | 45.24                         | 44 . 32                             | 46.17                               | $\overset{w}{C} = 62^{\circ} 51' 44'' \cdot 46$                   |

## At XIX (Daichu)

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January 1874; observed by Lieut. J. Hill, B.E., with Barrow's 24-inch Theodolite No. 2.

| Angle       |                                          |                                          | Cir                                      | cle readi                          | ngs, telesc                              | ope being                                | set on X                           | XI                                 |                                          |                                          | M = Mean of Groups                                                             |
|-------------|------------------------------------------|------------------------------------------|------------------------------------------|------------------------------------|------------------------------------------|------------------------------------------|------------------------------------|------------------------------------|------------------------------------------|------------------------------------------|--------------------------------------------------------------------------------|
| between     | 0° 0′                                    | 180° 0′                                  | 79° 14′                                  | <b>259°</b> 14′                    | 158° 25'                                 | 338° 25′                                 | 287° 84′                           | 57° 34′                            | <b>816° 49'</b>                          | 186° 49′                                 | w = Relative Weight<br>C = Concluded Angle                                     |
| XXI & XVIII | "<br>h 44 · 10<br>h 44 · 26<br>h 45 · 74 | "<br>h 45 ° 44<br>h 45 ° 10<br>h 45 ° 44 | "<br>h 43 · 54<br>l 45 · 48<br>l 44 · 78 | "<br>2 44·24<br>2 44·06<br>2 44·90 | "<br>l 45 · 12<br>l 44 · 72<br>l 43 · 60 | "<br>l 44 · 40<br>l 43 · 98<br>l 44 · 14 | "<br>l 43·28<br>l 44·40<br>l 44·42 | "<br>l 45`52<br>l 43`86<br>l 45`34 | "<br>h 44 · 78<br>h 43 · 94<br>h 44 · 34 | "<br>h 43 · 36<br>h 44 · 98<br>h 44 · 12 | $M = 44'' \cdot 51$ $w = 37 \cdot 00$ $\frac{1}{w} = 0 \cdot 03$               |
| •           | 44.70                                    | 45.33                                    | 44.60                                    | 44 ' 40                            | 44.48                                    | 44'17                                    | 44 ' 03                            | 44'91                              | 44.35                                    | 44.12                                    | $C = 63^{\circ} 2' 44'' \cdot 51$                                              |
| XVIII & XVI | h 14 22<br>h 14 48<br>h 13 80            | h 12.90<br>h 12.98<br>h 12.90            | h 14.92<br>l 14.12<br>l 13.80            | l 14.50<br>l 13.32<br>l 13.48      | l 13°44<br>l 12°84<br>l 13°96            | l 14.84<br>l 14.62<br>l 15.24            | l 14.06<br>l 13.24<br>l 13.68      | l 12°54<br>l 12°94<br>l 13°36      | h 14°18<br>h 14°44<br>h 14°50            | h 13°34<br>h 13°74<br>h 13°18            | $M = 13'' \cdot 78$ $w = 21 \cdot 30$ $\frac{1}{2} = 0 \cdot 05$               |
|             | 14.12                                    | 12.83                                    | 14 . 28                                  | 13.29                              | 13.41                                    | 14.00                                    | 13.66                              | 12.95                              | 14.37                                    | 13.42                                    | $\begin{bmatrix} w & 0 & 0 \\ C &= 61^{\circ} & 13' & 13'' & 78 \end{bmatrix}$ |

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At XX (Sorau)

February 1874; observed by Lieut. J. Hill, R. E., with Barrow's 24-inch Theodolite No. 2.

| Angle           |                                          |                                          | Cir                                      | cle readin                    | gs, telesc                                                                | ope being                                     | set on X                           | VII                                      |                                    |                                     | M - Mean of Groups                                               |
|-----------------|------------------------------------------|------------------------------------------|------------------------------------------|-------------------------------|---------------------------------------------------------------------------|-----------------------------------------------|------------------------------------|------------------------------------------|------------------------------------|-------------------------------------|------------------------------------------------------------------|
| between         | 234° 42′                                 | 54° 41′                                  | 818° 54′                                 | 1 <b>83°</b> 53'              | 33° 3′                                                                    | 213° 3′                                       | 112° 16'                           | <b>2</b> 92° 16′                         | 191° <b>3</b> 0′                   | 11 <b>° 30′</b>                     | w = Relative Weight<br>C = Concluded Angle                       |
| XVII &<br>XVIII | h 25°04<br>h 26°38<br>l 27°46<br>h 27°98 | "<br>h 27 · 44<br>h 25 · 54<br>h 25 · 52 | n<br>h 25 · 62<br>h 26 · 72<br>h 26 · 74 | l 25.52<br>l 25.48<br>l 25.98 | "<br>l 27 <sup>•</sup> 52<br>h 27 <sup>•</sup> 20<br>h 26 <sup>•</sup> 06 | "<br>l 27.64<br>l 24.94<br>l 27.56<br>l 26.46 | "<br>l 25°78<br>l 25°16<br>l 27°12 | "<br>l 26 · 12<br>l 26 · 08<br>l 25 · 86 | "<br>l 25°60<br>l 26°84<br>l 25°74 | h 27 · 82<br>h 28 · 84<br>h 28 · 02 | $M = 26'' \cdot 48$ $w = 14 \cdot 08$ $\frac{1}{w} = 0 \cdot 07$ |
| · · · ·         | 26.72                                    | 26.12                                    | 26.36                                    | 25.66                         | 26.93                                                                     | 26.65                                         | 26.02                              | 26.02                                    | 26.06                              | 28.23                               | $C = 59^{\circ} 45' 26'' \cdot 48$                               |
| XVIII &<br>XXII | h 7°20<br>h 7°42<br>l 8°58               | h 6°20<br>h 5°86<br>h 6°92               | h 8.82<br>h 8.82<br>h 9.22               | 2 9'12<br>2 8'36<br>2 8'28    | l 8.76<br>h 7.00<br>h 7.36                                                | l 6.70<br>l 7.12<br>l 7.68                    | 1 7.98<br>1 6.58<br>1 7.06         | 2 8.40<br>2 7.74<br>2 8.30               | l 7.76<br>l 7.28<br>l 6.84         | h 8°14<br>h 6°88<br>h 7°10          | $M = 7'' \cdot 65$ $w = 15 \cdot 20$ $\frac{1}{2} = 0 \cdot 07$  |
|                 | 7.73                                     | 6.33                                     | 8.95                                     | 8.29                          | 7.21                                                                      | 7.17                                          | 7.51                               | 8.12                                     | 7 * 29                             | 7:37                                | $C = 65^{\circ} 34' 7'' \cdot 65$                                |

At XXI (Jalora)

February 1874; observed by Lieut. J. Hill, R. E., with Barrow's 24-inch Theodolite No. 2.

| Angle<br>between | 182° 14′                                                | 312°14′                                             | Cir<br>211° 27′                                     | cle reading<br>31°26'                                       | gs, telesco<br>290*39'                      | po being s<br>110°40'                           | et on XX<br>9°50′                              | III<br>189° 50′                                             | 89° 0′                                            | 269° 0′                                             | M - Mean of Groups<br>w - Relative Weight<br>C - Concluded Angle                                                                                                            |
|------------------|---------------------------------------------------------|-----------------------------------------------------|-----------------------------------------------------|-------------------------------------------------------------|---------------------------------------------|-------------------------------------------------|------------------------------------------------|-------------------------------------------------------------|---------------------------------------------------|-----------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------|
| XXIII &<br>XXIV  | "<br>h 47 · 38<br>h 47 · 66<br>h 48 · 40<br>47 · 81     | *<br>h 47 · 34<br>l 47 · 36<br>l 47 · 82<br>47 · 51 | "<br>h 48 · 48<br>h 48 · 62<br>h 47 · 68<br>48 · 26 | "<br>h 49.00<br>h 48.10<br>l 48.88<br>48.66                 | "<br>l 48·52<br>l 48·38<br>l 47·16<br>48·02 | "<br>h 48.78<br>h 48.62<br>h 48.38<br>48.59     | "<br>h 47°74<br>h 47°92<br>h 48°90<br>48°19    | "<br>h 48·26<br>l 48·86<br>l 48·58<br>48·57                 | "<br>h 46°20<br>h 47°94<br>h 46°60<br>46°91       | *<br>h 46 · 18<br>h 47 · 86<br>h 47 · 58<br>47 · 21 | $\dot{M} = 47^{*} \cdot 97$<br>$w = 22 \cdot 20$<br>$\frac{1}{w} = 0 \cdot 05$<br>$C = 49^{\circ} 15' 47'' \cdot 97$                                                        |
| XXIV &<br>XXII   | h 10°24<br>h 10°16<br>h 9°80                            | k 9.30<br>l 9.80<br>l 11.26                         | h 9.06<br>h 8.60<br>h 10.84<br>h 9.92               | k 10.64<br>k 10.92<br>l 10.10                               | 2 8.68<br>2 9.08<br>2 9.38                  | k 8.36<br>k 9.48<br>k 9.94                      | h 11 °00<br>h 8 °96<br>h 9 °06<br>l 10 °06     | h 9.62<br>l 8.76<br>l 9.30                                  | h 10°38<br>h 10°20<br>h 9°38<br>d 9°61            | h 10.82<br>h 10.54<br>h 9.24                        | $M = 9'' \cdot 77$ $w = 28 \cdot 75$ $\frac{1}{w} = 0 \cdot 03$ $(1 - 10^{\circ} 10' - 0'') = 10^{\circ}$                                                                   |
| XXII &<br>XVIII  | 10 07<br>h 45 · 48<br>h 46 · 54<br>h 45 · 48<br>45 · 83 | h 45°72<br>l 45°98<br>l 46°00<br>d 45°68<br>45°85   | h 47 °00<br>h 45 °22<br>h 45 °44<br>45 °89          | <i>h</i> 46.84<br><i>h</i> 46.12<br><i>l</i> 45.50<br>46.15 | 2 46·24<br>2 46·18<br>2 45·78<br>46·07      | 45°78<br>h 45°78<br>h 44°16<br>h 45°66<br>45°20 | h 45.28<br>h 46.16<br>h 46.72<br>46.05         | <i>h</i> 45°90<br><i>l</i> 45°42<br><i>l</i> 45°10<br>45°47 | l 46.58<br>h 45.38<br>h 46.54<br>d 45.79<br>46.07 | h 46.60<br>h 45.96<br>h 45.18<br>45.91              | $ \begin{array}{c} C = 49 \ 40 \ 9 \ 77 \\ M = 45'' \cdot 85 \\ w = 57 \ \cdot \infty0 \\ \frac{1}{w} = 0 \ \cdot 02 \\ C = 74^{\circ} 44' \ 45'' \cdot 85 \\ \end{array} $ |
| XVIII &<br>XIX   | h 31.66<br>h 31.52<br>h 31.38                           | h 32°10<br>l 32°18<br>l 31°90<br>d 31°84<br>32°01   | h 32.54<br>h 33.58<br>h 32.60<br>32.91              | h 29.80<br>h 30.24<br>h 30.18<br>l 31.72<br>30.48           | 2 30.82<br>2 32.10<br>2 32.52<br>31.81      | h 30.78<br>h 31.70<br>h 32.08                   | h 31 · 36<br>h 33 · 04<br>h 31 · 24<br>31 · 88 | <i>k</i> 32.08<br><i>l</i> 32.86<br><i>l</i> 33.30<br>32.75 | l 32.10<br>h 32.48<br>h 33.06<br>h 31.42<br>32.27 | h 32.88<br>h 32.60<br>h 31.44<br>h 31.28<br>32.05   | $M = 31'' \cdot 92$ $w = 17 \cdot 30$ $\frac{1}{w} = 0 \cdot 06$ $C = 54^{\circ} 5' 31'' \cdot 92$                                                                          |

## At XXII (Loháwat)

February 1874; observed by Lieut. J. Hill, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle           |                                          |                                    | Ci                                 | ircle readi                        | ngs, teles                                             | cope being                    | g set on X                         | x                                  |                                          |                                    | M = Mean of Groups                                               |
|-----------------|------------------------------------------|------------------------------------|------------------------------------|------------------------------------|--------------------------------------------------------|-------------------------------|------------------------------------|------------------------------------|------------------------------------------|------------------------------------|------------------------------------------------------------------|
| between         | 0° 1′                                    | 180° l'                            | 79° 13′                            | 259° 18′                           | 158° 27′                                               | <b>338°</b> 27′               | 237° 36'                           | 57° 36′                            | <b>316° 45'</b>                          | 136° <b>45</b> ′                   | $\omega$ = Relative Weight<br>C = Concluded Angle                |
| XX & XVIII      | h 17°04<br>h 15°14<br>h 17'92<br>h 16'36 | "<br>h 15`86<br>l 17`34<br>l 16`26 | "<br>l 17·52<br>l 15·78<br>l 16·90 | "<br>l 16·46<br>h 17·94<br>h 16·52 | "<br>h 17 ° 04<br>h 16 ° 30<br>h 1 5 ° 64<br>h 17 ° 62 | "<br>16.18<br>16.38<br>16.34  | "<br>l 17°68<br>l 17°66<br>l 16°04 | "<br>h 15°04<br>h 16°24<br>h 16°26 | "<br>h 17 · 26<br>l 15 · 62<br>l 16 · 28 | "<br>  17°14<br>  16°76<br>  17°64 | $M = 16'' \cdot 64$ $w = 32 \cdot 18$ $\frac{1}{w} = 0 \cdot 03$ |
|                 | 16.03                                    | 16.49                              | 16.23                              | 16.92                              | 16.62                                                  | 16.37                         | 17.13                              | 15.85                              | 16.39                                    | 17.18                              | $C = 57^{\circ} 3' 16'' \cdot 64$                                |
| XVIII & XXI     | h 29.60<br>h 30.34<br>h 29.74            | l 29·44<br>l 30·64<br>l 29·46      | l 32°10<br>l 31°42<br>l 30°78      | l 30.48<br>h 30.06<br>h 30.46      | h 28 · 76<br>h 29 · 78<br>h 30 · 34                    | l 30°64<br>l 30°32<br>l 30 60 | l 28.52<br>l 28.82<br>l 28.94      | h 29°36<br>h 29°54<br>h 30°58      | l 30°30<br>l 30°88<br>l 30°86            | l 29°78<br>l 28°88<br>l 28°96      | $M = 30'' \cdot 01$ $w = 15 \cdot 60$ $v = 0.006$                |
|                 | 29.89                                    | 29.85                              | 31.43                              | 30.33                              | 29.63                                                  | 30.22                         | 28.76                              | 29.83                              | 30.08                                    | 29.31                              | $\frac{1}{w} = 56^{\circ} 13' 30'' \cdot 01$                     |
| XXI & XXIII     | h 50°00<br>h 50°46<br>h 49°34            | l 49°30<br>l 48°78<br>l 49°34      | l 47 74<br>l 48 68<br>l 48 96      | l 49.86<br>h 48.56<br>h 48.00      | h 48 · 50<br>h 47 · 36<br>h 49 · 42<br>h 47 · 72       | l 50°00<br>l 50°64<br>l 50°52 | l 50°46<br>l 49°66<br>l 51°48      | h 49°32<br>h 48°82<br>h 50°30      | k 49°14<br>l 49°44<br>l 49°40            | l 47 84<br>l 49 10<br>l 48 44      | $M = 49'' \cdot 28$ $w = 13 \cdot 25$ $\frac{1}{2} = 0 \cdot 08$ |
|                 | 49.93                                    | 49.14                              | 48.46                              | 48.81                              | 48.25                                                  | 50.30                         | 50.23                              | 49.48                              | 49.33                                    | 48.46                              | $     C = 37^{\circ} 25' 49'' \cdot 28 $                         |
| XXIII &<br>XXIV | h 35°82<br>h 36°08<br>h 34°84            | l 36.04<br>l 35.56<br>l 36.18      | l 35 98<br>l 37 42<br>l 35 50      | l 34·80<br>h 34·32<br>h 35·92      | h 35°78<br>h 35°62<br>h 37°50                          | l 35.56<br>l 34.86<br>l 35.38 | l 35°72<br>l 34°88<br>l 35°72      | h 35°54<br>h 36°24<br>h 35°22      | h 37 °08<br>h 36 °66<br>l 36 °12         | 2 37°10<br>2 38°28<br>2 36°32      | $M = 35'' \cdot 94$ $w = 17 \cdot 20$ I                          |
|                 | 35*58                                    | 35 93                              | 36.30                              | 35.01                              | 36.30                                                  | 35.27                         | 35*44                              | 35.67                              | 36.63                                    | 37.23                              | $\overline{w} = 0.00$<br>$C = 33^{\circ} 40' 35''.94$            |

#### At XXIII (Ekka)

February 1874; observed by Lieut. J. Hill, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle         |                                    |                                          | Cir                                                      | cle readir                         | ngs, telesc                        | ope being                                | set on X                                 | XV                                 |                                                                    |                                         | M = Mean of Groups                                               |
|---------------|------------------------------------|------------------------------------------|----------------------------------------------------------|------------------------------------|------------------------------------|------------------------------------------|------------------------------------------|------------------------------------|--------------------------------------------------------------------|-----------------------------------------|------------------------------------------------------------------|
| between       | 0° 1′                              | 180° 0′                                  | 79° 13′                                                  | <b>2</b> 59° 13 <b>′</b>           | 158° 28'                           | <b>3</b> 38° 23′                         | <b>237° 35′</b>                          | 57° 35′                            | <b>3</b> 16° 49′                                                   | 136° 48′                                | w = Relative Weight<br>C = Concluded Angle                       |
| XXV &<br>XXVI | "<br>h 56°74<br>h 56°98<br>h 57°08 | "<br>h 58 ° 08<br>h 57 ° 86<br>h 57 ° 04 | "<br>l 55°62<br>l 56°52<br>l 57°42<br>h 59°02<br>h 56°36 | "<br>h 56*82<br>h 57*68<br>h 56*96 | "<br>h 56°36<br>h 57°34<br>h 56°38 | "<br>h 57 ° 60<br>h 57 ° 04<br>h 56 ° 52 | "<br>1 58 · 10<br>1 56 · 32<br>1 56 · 40 | "<br>l 56°26<br>h 55°48<br>h 56°94 | "<br>h 58 · 70<br>h 57 · 70<br>h 55 · 56<br>h 55 · 64<br>h 56 · 38 | "<br>h 55 °84<br>h 57 ° 20<br>h 55 ° 42 | $M = 56'' \cdot 86$ $w = 25 \cdot 78$ $\frac{1}{w} = 0 \cdot 04$ |
|               | 56.93                              | 57.66                                    | 56.99                                                    | 57.15                              | 56.69                              | 57.05                                    | 56.94                                    | 56.33                              | 56.80                                                              | 56.12                                   | $C = 36^{\circ} 46' 56'' \cdot 86$                               |

| Am-1-           |                                               |                                    | Circ                                                     | cle readin                         | gs, telesco                                                       | ope being                          | set on X                           | <br>XV                                                               |                                    |                                                         | M = Mean of Groups                                                                                              |
|-----------------|-----------------------------------------------|------------------------------------|----------------------------------------------------------|------------------------------------|-------------------------------------------------------------------|------------------------------------|------------------------------------|----------------------------------------------------------------------|------------------------------------|---------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------|
| ngie<br>between | 0° 1′                                         | 180° 0′                            | 79° 13′                                                  | 259° 13′                           | 158° 23′                                                          | 338° 23′                           | 237° 35′                           | 57° 85′                                                              | <b>8</b> 16° <b>4</b> 9′           | 136° 48′                                                | w = Relative Weight<br>C = Concluded Angle                                                                      |
| XXVI & XXIV     | "<br>h 17°44<br>h 16°22<br>h 15°34<br>h 17°10 | "<br>h 13°36<br>h 14°00<br>h 14°98 | "<br>l 16.94<br>l 16.84<br>h 15.18<br>h 13.82<br>h 13.80 | "<br>h 14.80<br>h 14.74<br>h 14.92 | "<br>h 14°78<br>h 13°56<br>h 14°24                                | "<br>h 15.56<br>h 16.46<br>h 16.56 | "<br>l 15.00<br>l 16.88<br>l 16.02 | "<br>l 16·46<br>h 15·64<br>h 15·86                                   | "<br>h 13.02<br>h 15.00<br>h 14.66 | "<br>h 15.82<br>h 16.00<br>h 15.34                      | $M = 15'' \cdot 31$ $w = 9 \cdot 83$ $\frac{1}{w} = 0 \cdot 10$                                                 |
|                 | 16.23                                         | 14.11                              | 15.32                                                    | 14.82                              | 14.19                                                             | 16.19                              | 15.92                              | 15.99                                                                | 14.23                              | 15.72                                                   | $C = 38^{\circ} 24' 15'' \cdot 32$                                                                              |
| XXIV & XXII     | h 2°34<br>h 4°92<br>h 3°94<br>h 2°14          | h 4.78<br>h 4.94<br>h 4.64         | l 4.94<br>l 5.04<br>h 3.70<br>h 4.40<br>h 3.22           | h 5°18<br>h 4°26<br>h 5°06         | h 3 <sup>.</sup> 22<br>h 4 <sup>.</sup> 18<br>h 4 <sup>.</sup> 10 | h 3.02<br>h 2.36<br>h 2.40         | l 4·22<br>l 3·04<br>l 2·76         | l 2°54<br>l 3°30<br>h 3°04                                           | h 3·38<br>h 4·34<br>h 3·54         | h 3.36<br>h 3.52<br>h 2.18                              | $M = 3'' \cdot 67$ $w = 14 \cdot 06$ $\frac{1}{w} = 0 \cdot 07$                                                 |
|                 | 3`34                                          | 4.79                               | 4.36                                                     | 4.83                               | 3.83                                                              | 2.29                               | 3'34                               | 2.96                                                                 | 3.75                               | 3.03                                                    | $C = 35^{\circ} 22' 3'' \cdot 67$                                                                               |
| XXII & XXI      | h 14.18<br>h 12.48<br>h 15.22<br>h 14.90      | h 13°58<br>h 13°44<br>h 13°18      | l 12°76<br>h 13°88<br>h 14°54<br>h 14°98                 | h 13°34<br>h 14°58<br>h 14°04      | h 14.64<br>h 13.48<br>h 13.92                                     | h 14°18<br>h 15°30<br>h 14°80      | l 13°90<br>l 12°78<br>l 12°76      | l 14 <sup>.</sup> 84<br>l 13 <sup>.</sup> 84<br>h 13 <sup>.</sup> 62 | h 15.64<br>h 14.94<br>h 13.98      | h 12.88<br>h 13 <sup>.</sup> 22<br>h 14 <sup>.</sup> 42 | $M = 14'' \cdot 00$ $w = 22 \cdot 64$ $\frac{1}{2} = 0.101$                                                     |
|                 | 14.30                                         | 13.40                              | 14.04                                                    | 13.99                              | 14.01                                                             | 14.76                              | 13.12                              | 14.10                                                                | 14.85                              | 13.21                                                   | $\begin{vmatrix} \bar{w} & - & 0 & 0 \\ \bar{w} & - & 0 & 0 \\ C &= 43^{\circ} 38' & 14'' & 0 \\ \end{vmatrix}$ |

## At XXIV (Omlo)

February 1874; observed by Lieut. J. Hill, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle       |                                                  |                                           | Cir                                              | cle readin                               | gs, telesco                        | ope being                          | set on XX                          | <b>II</b>                                |                                                      |                                    | M = Mean of Groups                                                       |
|-------------|--------------------------------------------------|-------------------------------------------|--------------------------------------------------|------------------------------------------|------------------------------------|------------------------------------|------------------------------------|------------------------------------------|------------------------------------------------------|------------------------------------|--------------------------------------------------------------------------|
| between     | 0° 1′                                            | 180° 1′                                   | 79° 13′                                          | <b>25</b> 9° 1 <b>3′</b>                 | 1 <b>5</b> 8° 26′                  | <b>338° 26′</b>                    | 237° 34′                           | 57° 84′                                  | <b>3</b> 16° <b>4</b> 8′                             | 136° 48′                           | C = Concluded Angle                                                      |
| XXII & XXI  | "<br>h 25°02<br>h 25°68<br>l 26°84               | "<br>h 26 ° 06.<br>h 25 ° 32<br>h 26 ° 14 | "<br>h 26·32<br>h 26·62<br>h 24·50<br>h 25·64    | "<br>l 26·20<br>l 24·94<br>h 25·70       | "<br>h 26·30<br>h 25·62<br>h 26·40 | "<br>h 25°62<br>h 26°48<br>l 24°88 | "<br>l 24·78<br>l 25·16<br>l 25·96 | "<br>h 25 ° 32<br>h 25 ° 96<br>h 24 ° 80 | "<br>h 26 °00<br>h 24 ° 30<br>h 24 ° 98<br>l 25 ° 64 | "<br>h 25°52<br>l 25°60<br>l 26°08 | $M = 25'' \cdot 65$ $w = 54 \cdot 31$ $\frac{1}{m} = 0 \cdot 02$         |
|             | 25.85                                            | 25.84                                     | 25.77                                            | 25.61                                    | 26.11                              | 25.66                              | 25.30                              | 25.36                                    | 25.23                                                | 25.73                              | $\tilde{C} = 59^{\circ} 13' 25'' \cdot 64$                               |
| XXI & XXIII | h 54 ° 90<br>h 55 ° 32<br>l 56 ° 22<br>d 54 ° 66 | h 54°94<br>h 55°44<br>h 54°76             | h 54 ° 84<br>h 53 ° 50<br>h 54 ° 48<br>d 53 ° 53 | l 56°22<br>l 54°06<br>h 54°98<br>h 54°16 | h 55°34<br>h 55°26<br>h 55°90      | h 55°58<br>h 56°54<br>l 55°86      | 2 55°58<br>2 55°68<br>2 54°78      | h 55°30<br>h 55°50<br>h 54°52            | h 56°30<br>h 56°52<br>h 54°76                        | h 56 °00<br>h 55 °82<br>h 54 °00   | $M = 55'' \cdot 24$ $w = 25 \cdot 11$ $\frac{1}{2} = 0 \cdot 04$         |
|             | 55.28                                            | 55.02                                     | 54.09                                            | 54.85                                    | 55.20                              | 55-99                              | 55°35                              | 55.11                                    | 55.86                                                | 55°27                              | $\begin{bmatrix} w \\ C \\ = 51^{\circ} 43' 55'' \cdot 23 \end{bmatrix}$ |

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| $\mathbf{At}$ | XXIV | (Omlo)-( | (Continued). |
|---------------|------|----------|--------------|
|---------------|------|----------|--------------|

| Angle<br>between | 0° 1′                                                  | 180° 1′                                             | Ciro<br>79° 18′                                        | cle readin<br>259° 13′                              | gs, telesco<br>158° 26'                   | ope being<br>338° 26'                               | set on X<br>237° 34'                        | XII<br>57°34′                                | 816° 48′                                    | 136° 48′                                                | M = Mean of Groups<br>$\infty$ = Relative Weight<br>C = Concluded Angle                             |
|------------------|--------------------------------------------------------|-----------------------------------------------------|--------------------------------------------------------|-----------------------------------------------------|-------------------------------------------|-----------------------------------------------------|---------------------------------------------|----------------------------------------------|---------------------------------------------|---------------------------------------------------------|-----------------------------------------------------------------------------------------------------|
| XXIII &<br>XXV   | "<br>h 55°22<br>h 55°40<br>l 54°92<br>d 54°36<br>54°98 | "<br>h 54 · 20<br>h 54 · 62<br>h 54 · 16<br>54 · 33 | "<br>h 54.96<br>h 54.82<br>h 55.44<br>d 54.33<br>54.89 | "<br>1 54 · 30<br>1 52 · 94<br>1 53 · 26<br>53 · 50 | ,,<br>h 53 · 58<br>h 53 · 12<br>h 52 · 98 | "<br>h 52 * 88<br>h 53 * 14<br>l 52 * 34<br>52 * 79 | "<br>2 53 82<br>2 53 30<br>2 54 78<br>53 97 | "<br>h 52°98<br>h 54°56<br>h 54°42<br>53°99  | "<br>h 55`58<br>h 54`20<br>h 55`64<br>55`14 | "<br>h 53.08<br>l 53.48<br>l 52.80<br>53.12             | $M = 53'' \cdot 99$ $w = 13 \cdot 06$ $\frac{1}{w} = 0 \cdot 08$ $C = 64^{\circ} 22' 53'' \cdot 99$ |
| XXV &<br>XXVI    | k 10°46<br>k 9°98<br>k 7°74<br>l 7°78<br>8°99          | h 8.86<br>h 8.70<br>h 8.98<br>8.85                  | h 7.32<br>h 10.18<br>h 9.60<br>h 9.58<br>9.17          | l 8·24<br>l 9·04<br>l 8·12<br>8·47                  | h 9°20<br>h 9°78<br>h 9°68<br>9°55        | h 9.40<br>h 10.20<br>l 8.26                         | l 10°46<br>l 9°90<br>l 8°32<br>9°56         | h 7°74<br>h 9°96<br>h 9°56<br>h 9°54<br>9°20 | k 10°54<br>h 10°48<br>k 8°82<br>9°95        | <b>h</b> 8.18<br><b>l</b> 7.46<br><b>l</b> 7.86<br>7.83 | $M = 9'' \cdot 09$ $w = 17 \cdot 77$ $\frac{1}{w} = 0 \cdot 06$ $C = 47^{\circ} 2' 9'' \cdot 09$    |

# At XXV (Khirwa)

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March 1874; observed by Lieut. J. Hill, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle             |                                     |                                                                                                                                              |                                     | M = Mean of Groups                  |                                          |                                                  |                                     |                               |                                          |                                          |                                                                                          |
|-------------------|-------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------|-------------------------------------|------------------------------------------|--------------------------------------------------|-------------------------------------|-------------------------------|------------------------------------------|------------------------------------------|------------------------------------------------------------------------------------------|
| between           | <b>234°</b> 19′                     | <b>54°</b> 18′                                                                                                                               | <b>3</b> 13° <b>3</b> 2′            | 133° 32′                            | 82° <b>43</b> ′                          | <b>212° 43'</b>                                  | 111° 56′                            | <b>291° 56′</b>               | 191° <b>9′</b>                           | 11°9′                                    | w = Relative Weight $C = Concluded Angle$                                                |
| XXVIII &<br>XXVII | "<br>h 9°90<br>h 9°38<br>l 9°52     | <sup>4</sup><br><sup>1</sup><br><sup>1</sup><br><sup>1</sup><br><sup>1</sup><br><sup>1</sup><br><sup>1</sup><br><sup>1</sup><br><sup>1</sup> | "<br>h 10.66<br>h 8.90<br>h 10.22   | "<br>h 10°06<br>h 9°22<br>h 11°22   | *<br>h 10°98<br>h 10°46<br>h 10°40       | "<br>h 10°28<br>h 9°42<br>h 10°80                | "<br>k 10°04<br>k 8°58<br>l 9°42    | l 10°30<br>h 11°08<br>h 9°20  | ,<br>k 12 · 46<br>k 11 · 26<br>k 10 · 60 | "<br>h 11 ° 02<br>h 11 ° 36<br>h 11 ° 42 | $M = 10^{\prime\prime} \cdot 16$ $w = 12 \cdot 37$ $\frac{1}{20} = 0 \cdot 08$           |
|                   | 9.60                                | 8.85                                                                                                                                         | 9.93                                | 10.12                               | 10.01                                    | 10.12                                            | 9.35                                | 10.19                         | 11.44                                    | 11.32                                    | $\begin{bmatrix} w \\ C = 59^{\circ} 47' 10'' \cdot 15 \end{bmatrix}$                    |
| XXVII &<br>XXVI   | k 50°62<br>k 51°04<br>k 51°38       | h 52.68<br>h 52.20<br>h 53.20                                                                                                                | h 53°22<br>h 51°94<br>h 51°84       | h 51°16<br>h 52°50<br>l 51°92       | h 52°08<br>h 52°02<br>h 53°26            | h 52°26<br>h 52°78<br>h 52°70                    | k 50°98<br>k 51°06<br>l 49°94       | l 51°56<br>h 52°90<br>h 53°22 | h 51°78<br>h 51°80<br>h 51°48            | h 52°56<br>h 51°34<br>l 52°88            | $M = 52'' \cdot 01$ $w = 17 \cdot 20$                                                    |
|                   | 51.01                               | 52.69                                                                                                                                        | 52.33                               | 51.86                               | 52.45                                    | 52.58                                            | 50.66                               | 52.26                         | 51.69                                    | 52.26                                    | $\begin{bmatrix} \bar{w} = 0.06 \\ \bar{w} = 65^{\circ} 53' 52'' \cdot 01 \end{bmatrix}$ |
| XXVI &<br>XXIV    | h 26 ° 06<br>h 24 ° 80<br>h 25 ° 70 | l 25.68<br>k 24.44<br>k 24.94                                                                                                                | h 24 · 32<br>h 25 · 88<br>h 25 · 98 | h 24 · 16<br>h 23 · 94<br>h 25 · 24 | h 23·36<br>h 25·62<br>h 24·52<br>h 25·88 | h 26 · 34<br>h 24 · 12<br>h 25 · 00<br>h 25 · 12 | h 24 · 10<br>h 25 · 20<br>l 25 · 82 | l 24°92<br>h 23°80<br>h 25°08 | h 25°36<br>h 25°80<br>h 23°62<br>l 25°96 | <b>h</b> 25°52<br>h 27°06<br>h 25°28     | $M = 25'' \cdot 11$ $w = 27 \cdot 41$ $\frac{1}{2} = 0 \cdot 04$                         |
|                   | 25.52                               | 25.02                                                                                                                                        | 25.39                               | <b>2</b> 4°45                       | 24.85                                    | 25.14                                            | 25.04                               | 24.60                         | 25.19                                    | <b>2</b> 5°95                            | $C = 54^{\circ} 21' 25'' \cdot 11$                                                       |

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|                  |                                    |                                       |                                    | At XX                  | KV (Kh                                                               | irwa)—                             | (Continu                                              | ued).                         |                                                    |                                    |                                                                                                                                                 |
|------------------|------------------------------------|---------------------------------------|------------------------------------|------------------------|----------------------------------------------------------------------|------------------------------------|-------------------------------------------------------|-------------------------------|----------------------------------------------------|------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------|
| Angle<br>between | 234° 19'                           | 54° 18'                               | Circle<br>813° 32′                 | e readings<br>133° 32' | s, telescor<br>82°43'                                                | be being a<br>212° 43'             | set on XX<br>111°56′                                  | VIII<br>291° 56′              | 191° 9′                                            | 11° 9′                             | $ \begin{array}{ll} \underline{M} & - & \text{Mean of Groups} \\ w & - & \text{Relative Weight} \\ C & - & \text{Concluded Angle} \end{array} $ |
| XXIV &<br>XXIII  | "<br>h 53°96<br>h 53°72<br>h 54°28 | "<br>\$ 53*84<br>\$ 53*80<br>\$ 53*96 | n<br>h 55 82<br>h 54 80<br>h 54 06 | *                      | <i>k</i> 53.64<br><i>h</i> 56.10<br><i>h</i> 53.54<br><i>h</i> 55.66 | "<br>h 55°00<br>h 55°62<br>h 54°80 | "<br>h 54 · 86<br>h 53 · 30<br>h 54 · 84<br>l 54 · 82 | l 55°72<br>h 54°80<br>h 55°48 | <i>h</i> 55°70<br><i>h</i> 54°36<br><i>h</i> 55°80 | *<br>h 55°14<br>h 54°62<br>h 53°94 | $M = 54'' \cdot 72$ $w = 29 \cdot 34$ $\frac{1}{2} = 0 \cdot 03$                                                                                |
|                  | 53.99                              | 54°20                                 | 54.89                              | 54.58                  | 54.74                                                                | 55.14                              | 54.45                                                 | 55.33                         | 55.39                                              | 54°57                              | $\int_{0}^{w} C = 40^{\circ} 25' 54'' \cdot 72$                                                                                                 |

At XXVI (Jambo)

February and March 1874; observed by Lieut. J. Hill, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle            |                                                                          |                                                    |                                                             | M - Mean of Groups                                  |                                                                |                                                |                                                 |                                                                          |                                                |                                                     |                                                                                                              |
|------------------|--------------------------------------------------------------------------|----------------------------------------------------|-------------------------------------------------------------|-----------------------------------------------------|----------------------------------------------------------------|------------------------------------------------|-------------------------------------------------|--------------------------------------------------------------------------|------------------------------------------------|-----------------------------------------------------|--------------------------------------------------------------------------------------------------------------|
| between          | 0° 0′                                                                    | 179° 59′                                           | <b>79°</b> 11′                                              | 259° 11′                                            | 158° 26'                                                       | <b>33</b> 8° 26'                               | 237° 38′                                        | 57° 38′                                                                  | 316° 47'                                       | 136° 47                                             | $\omega = \text{Relative Weight}$<br>C = Concluded Angle                                                     |
| XXIV &<br>XXIII  | "<br>k 42 ° 62<br>k 43 ° 68<br>k 42 ° 20<br>42 ° 83                      | "<br>h 42.64<br>h 40.50<br>h 42.70<br>41.95        | "<br>h 40°34<br>h 41°30<br>h 41°60<br>41°08                 | "<br>h 42 · 20<br>h 42 · 10<br>h 42 · 98<br>42 · 43 | "<br>h 40.74<br>h 41.86<br>h 41.54<br>41.38                    | h 43 · 38<br>h 43 · 34<br>h 43 · 58<br>43 · 43 | "<br>h 43 °68<br>h 44 °02<br>h 43 °04<br>43 °58 | "<br>h 43`62<br>h 42`14<br>k 42`14<br>42`63                              | "<br>h 42`46<br>h 42`92<br>h 42`70<br>42`69    | "<br>h 41 · 86<br>h 42 · 88<br>h 40 · 94<br>41 · 89 | $M = 42'' \cdot 39$<br>$w = 12 \cdot 70$<br>$\frac{1}{w} = 0 \cdot 08$<br>$C = 30^{\circ} 10' 42'' \cdot 39$ |
| XXIII &<br>XXV   | l 43.84<br>h 44.16<br>h 43.66<br>43.89                                   | h 45°22<br>h 44°14<br>h 43°12<br>44°16             | h 43.88<br>h 45.22<br>h 45.52<br>44.87                      | h 44°06<br>h 43°38<br>h 44°60<br>44°01              | h 44 · 26<br>h 44 · 14<br>h 44 · 74<br>44 · 38                 | h 44 · 38<br>h 45 · 70<br>h 45 · 72<br>45 · 27 | h 42 · 28<br>h 42 · 46<br>h 43 · 86<br>42 · 87  | h 42 ° 96<br>h 43 ° 42<br>h 43 ° 72<br>43 ° 37                           | h 43 ° 90<br>h 43 ° 22<br>h 44 ° 28<br>43 ° 80 | h 43 °76<br>h 43 °28<br>h 44 °64<br>43 °89          | $M = 44'' \cdot 05$<br>$w = 17 \cdot 20$<br>$\frac{1}{w} = 0 \cdot 06$<br>$C = 48^{\circ} 25' 44'' \cdot 05$ |
| XXV &<br>XXVII   | h 27 · 42<br>h 29 · 12<br>h 27 · 18<br>d 29 · 29<br>d 28 · 67<br>28 · 34 | h 30° 36<br>h 28°04<br>h 29°66<br>h 30°64<br>29°68 | λ 29 · 52<br>h 29 · 62<br>h 27 · 48<br>h 27 · 72<br>28 · 58 | h 28·34<br>h 29·24<br>h 27·94<br>28·51              | 27.56<br>28.08<br>28.22<br>27.95                               | 28.84<br>29.12<br>27.88<br>28.61               | h 27 · 34<br>h 28 · 56<br>h 26 · 62<br>27 · 51  | h 29 · 34<br>h 26 · 82<br>h 30 · 04<br>l 26 · 90<br>d 29 · 45<br>28 · 51 | h 29°54<br>h 29°16<br>h 28°50<br>29°07         | h 27°14<br>l 27°86<br>l 27°58                       | $M = 28'' \cdot 43$<br>$w = 15 \cdot 28$<br>$\frac{1}{w} = 0 \cdot 07$<br>$C = 61^{\circ} 40' 28'' \cdot 44$ |
| XXVII &<br>R. M. | k 9.78<br>k 8.90<br>k 8.54<br>d 10.45<br>d 9.83                          | k 10.70<br>k 9.22<br>k 9.02                        | h 9.32<br>h 10.28<br>h 10.92                                | h 9.66<br>h 9.52<br>h 9.06                          | l 9 <sup>.70</sup><br>l 9 <sup>.20</sup><br>l 8 <sup>.54</sup> | l 9°20<br>l 9°46<br>l 9°76                     | h 10°46<br>h 9°88<br>h 11°74                    | h 9°24<br>h 10°62<br>h 9°26<br>d 10°88                                   | h 9°84<br>h 9°46<br>h 8°16                     | 2 9.80<br>2 10.14<br>2 8.40                         | $M = 9'' \cdot 66$ $w = 26 \cdot 93$ $\frac{1}{w} = 0 \cdot 04$ $C = 3^{\circ} 10' 0'' \cdot 66$             |
|                  | 9.20                                                                     | 9.62                                               | 10.12                                                       | 9.41                                                | 9.12                                                           | 9.42                                           | 10.69                                           | 10.00                                                                    | 9.12                                           | <b>9</b> °45                                        | C = 3 19 9'00                                                                                                |

Norg.-R.M. denotes Referring Mark.

#### PRINCIPAL TRIANGULATION. OBSERVED ANGLES.

| $\mathbf{At}$ | XXVI | (Jambo) | )—( | (Continued | ). |
|---------------|------|---------|-----|------------|----|
|---------------|------|---------|-----|------------|----|

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| Angle<br>between | 0° 0′                             | 179° 59′ | Circ<br>79°11′                   | ele reading<br>259° 11'           | g <b>s</b> , telesco<br>158°26'          | pe being<br>838° 26'            | set on X<br>237° 38' | XIV<br>57°38'                    | 316° 47′                         | 186° 47′                         | M = Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle |
|------------------|-----------------------------------|----------|----------------------------------|-----------------------------------|------------------------------------------|---------------------------------|----------------------|----------------------------------|----------------------------------|----------------------------------|------------------------------------------------------------------|
| R.M. &<br>XXIX   | "<br>k 10°04<br>k 9°74<br>k 11°94 | "        | "<br>h 10°18<br>h 8°68<br>h 8°78 | "<br>h 9.20<br>h 10.08<br>h 10.28 | "<br>111.18<br>111.10<br>111.30<br>18.76 | "<br>l 9°14<br>l 9°10<br>l 8°92 | "                    | "<br>h 9°60<br>h 10°14<br>h 8°26 | "<br>k 10°64<br>k 8°84<br>k 9°82 | "<br>h 8·72<br>h 10·44<br>h 9·20 | $M = 9'' \cdot 84$ $w = 19 \cdot 28$ $\frac{1}{40} = 0 \cdot 05$ |
|                  | 10.22                             | 10.42    | 9.51                             | 9.85                              | 10.20                                    | 9.02                            | 10,10                | 9`33                             | 9.77                             | 9*45                             | $C' = 49^{\circ} 17' 9'' \cdot 85$                               |

At XXVII (Sirad)

March 1874; observed by Lieut. J. Hill, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle<br>between | 0° 0′                                               | 180° 0′                                                | Cir<br>79° 13′                                                                           | cle readir<br>259°13'                                                            | igs, telesc<br>158° 26'                             | ope being<br>338°25'                           | set on X2<br>237° 37'                           | LIX<br>57° 37′                              | <b>816° 47'</b>                                | 136 <sup>°</sup> 47′                                                                         | M - Mean of Groups<br>w - Relative Weight<br>C - Concluded Angle                                                       |
|------------------|-----------------------------------------------------|--------------------------------------------------------|------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------|-----------------------------------------------------|------------------------------------------------|-------------------------------------------------|---------------------------------------------|------------------------------------------------|----------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------|
| XXIX &<br>XXVI   | "<br>h 54 · 84<br>h 54 · 46<br>h 55 · 22<br>54 · 84 | "<br>2 55.68<br>2 54.16<br>2 53.58<br>2 53.90<br>54.33 | "<br>2 53 84<br>h 54 70<br>h 55 12<br>h 56 70<br>55 09                                   | $     "     h 55 \cdot 40     h 55 \cdot 66     h 55 \cdot 20           55 · 42$ | "<br>h 55 · 32<br>h 55 · 58<br>h 54 · 14<br>55 · 01 | "<br>\$ 54.30<br>\$ 53.96<br>\$ 55.70<br>54.65 | "<br>h 53 °74<br>h 53 °40<br>h 54 °10<br>53 °75 | "<br>h 55°02<br>h 54°76<br>h 53°54<br>54°44 | "<br>\$ 53.80<br>\$ 55.08<br>\$ 54.10<br>54.33 | "<br><b>h</b> 53 ° 90<br><b>l</b> 56 ° 14<br><b>l</b> 53 ° 96<br><b>l</b> 53 ° 86<br>54 ° 47 | $M = 54^{\circ} \cdot 63$<br>$w = 25 \cdot 84$<br>$\frac{1}{w} = 0 \cdot 04$<br>$C = 63^{\circ} 28' 54'' \cdot 63$     |
| XXVI &<br>XXV    | h 41 ° 44<br>h 41 ° 58<br>h 40 ° 10                 | h 39.34<br>h 39.72<br>h 41.16                          | l 41 · 30<br>h 39 · 62<br>h 40 · 16                                                      | h 39 · 42<br>h 40 · 36<br>h 39 · 18                                              | h 41 · 36<br>h 39 · 48<br>h 40 · 04                 | l 41 · 26<br>h 40 · 50<br>h 41 · 46            | h 41 · 84<br>h 40 · 46<br>h 40 · 02             | h 40°90<br>h 40°46<br>h 41°32               | h 40°18<br>h 40°56<br>h 40°04                  | h 40°02<br>l 40'16<br>l 40'24                                                                | $M = 40'' \cdot 45$ $w = 29 \cdot 40$ $\frac{1}{w} = 0 \cdot 03$                                                       |
| XXV &<br>XXVIII  | h 26.52<br>h 26.76<br>h 27.44                       | h 26.82<br>h 25.98<br>h 28.12<br>h 25.18               | 1 27 96<br>h 25 74<br>h 24 90<br>h 24 74<br>h 26 58                                      | 39 05<br>h 27 30<br>h 25 62<br>h 26 14                                           | 40 29<br>h 26 44<br>h 28 08<br>h 27 78              | 41 07<br>2 27 • 46<br>h 27 • 52<br>h 26 • 26   | h 26°58<br>h 27°66<br>h 28°20                   | 40 89<br>h 26 96<br>h 28 10<br>h 27 24      | 40 20<br>h 28 20<br>h 26 96<br>h 26 84         | 40 14<br>h 27.60<br>l 28.22<br>l 27.26<br>l 27.16                                            | $C = 52^{\circ} 25^{\circ} 40^{\circ} \cdot 45$ $M = 27^{\circ} \cdot 01$ $w = 20 \cdot 82$ $\frac{1}{w} = 0 \cdot 05$ |
|                  | 26.91                                               | 26.23                                                  | 25.98                                                                                    | 26.35                                                                            | 27.43                                               | 27.08                                          | 27.48                                           | 27 * 43                                     | 27.33                                          | 27.56                                                                                        | $C = 60^{\circ} 37^{\circ} 20^{\circ} 99$                                                                              |
| XXVIII &<br>XXX  | h 41 · 88<br>h 40 · 38<br>h 41 · 40                 | h 40°12<br>h 39°42<br>h 40°82<br>h 40°06               | l 39 <sup>.84</sup><br>h 40 <sup>.84</sup><br>h 42 <sup>.00</sup><br>h 41 <sup>.68</sup> | h 40°84<br>h 40°76<br>h 39°86                                                    | k 40°60<br>h 39°82<br>h 40°24                       | l 41 °00<br>h 41 ° 44<br>h 41 ° 18             | h 41 · 26<br>h 40 · 48<br>h 41 · 10             | h 39°48<br>h 39°60<br>h 41°54<br>h 42°22    | h 41 °02<br>h 41 ° 20<br>h 40 ° 40             | l 40°00<br>l 40°48<br>l 39°76                                                                | $M = 40'' \cdot 69$ $w = 31 \cdot 20$ $\frac{1}{2} = 0 \cdot 03$                                                       |
|                  | 41 . 52                                             | 40'11                                                  | 41.09                                                                                    | 40°49                                                                            | 40°22                                               | 41.51                                          | 40°95                                           | 40.21                                       | 40.87                                          | <b>4</b> 0°08                                                                                | $C = 53^{\circ} 19' 40'' \cdot 69$                                                                                     |

| At XXVII (Sirad)—(Continued). |                                          |                                    |                                                                         |                                          |                                    |                                       |                                          |                                                       |                                    |                                          |                                                                       |  |
|-------------------------------|------------------------------------------|------------------------------------|-------------------------------------------------------------------------|------------------------------------------|------------------------------------|---------------------------------------|------------------------------------------|-------------------------------------------------------|------------------------------------|------------------------------------------|-----------------------------------------------------------------------|--|
| Angle<br>between              | 0° 0′                                    | 180° 0′                            | M = Mean of Groups<br>$\varpi = Relative Weight$<br>C = Concluded Angle |                                          |                                    |                                       |                                          |                                                       |                                    |                                          |                                                                       |  |
| XXX &<br>XXXI                 | "<br>h 25°66<br>h 24°40<br>hl26°02       | "<br>h 25°24<br>h 26°44<br>h 25°20 | "<br>l 25.58<br>h 25.90<br>h 25.24<br>h 27.56                           | "<br>h 25 · 38<br>h 25 · 30<br>h 26 · 46 | "<br>h 25°16<br>h 26°28<br>h 25°70 | "<br>\$ 25.70<br>\$ 26.64<br>\$ 25.22 | "<br>h 24 °94<br>h 25 ° 26<br>h 25 ° 60  | "<br>h 25 · 70<br>h 24 · 94<br>h 24 · 02<br>h 24 · 82 | "<br>h 25°12<br>h 25°64<br>h 25°86 | "<br>26°14<br>26°34<br>227°16            | $M = 25'' \cdot 66$ $w = 31 \cdot 82$ $\frac{1}{w} = 0 \cdot 03$      |  |
|                               | 25.36                                    | 25.63                              | 26.02                                                                   | 25.21                                    | 25.71                              | 25.85                                 | 25.27                                    | 24.87                                                 | 25.24                              | 26.22                                    | $C = 47^{\circ} 29' 25'' \cdot 66$                                    |  |
| XXXI &<br>XXIX                | h 50°70<br>h 50°30<br>h 50°30<br>h 51°26 | h 52°48<br>h 51°00<br>h 50°98      | l 50°48<br>h 52°96<br>h 52°66<br>h 52°74                                | h 51°50<br>h 52°98<br>h 51°48            | h 51°50<br>h 51°76<br>h 52°26      | l 50°26<br>l 51°16<br>h 51°50         | h 53°24<br>h 50°86<br>h 50°80<br>h 53°28 | h 52°32<br>h 52°20<br>h 52°26                         | h 51°00<br>h 51°04<br>h 51°98      | l 51.52<br>l 51.84<br>l 50.30<br>l 51.04 | $M = 51'' \cdot 60$ $w = 21 \cdot 68$ $\frac{1}{-} = 0 \cdot 05$      |  |
|                               | 50.64                                    | 51.49                              | 52.21                                                                   | 51.99                                    | 51.84                              | 50.92                                 | 52.05                                    | 52.26                                                 | 51.34                              | 51.17                                    | $\begin{bmatrix} w \\ C = 76^{\circ} 38' 51'' \cdot 60 \end{bmatrix}$ |  |

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At XXVIII (Harban)

April 1874; observed by Lieut. J. Hill, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle          |                                          |                                     |                                                       | M = Mean of Groups                                    |                                               |                                    |                                                          |                                     |                                                |                                    |                                                                                                              |
|----------------|------------------------------------------|-------------------------------------|-------------------------------------------------------|-------------------------------------------------------|-----------------------------------------------|------------------------------------|----------------------------------------------------------|-------------------------------------|------------------------------------------------|------------------------------------|--------------------------------------------------------------------------------------------------------------|
| between        | 0° 2′                                    | 180°1′                              | <b>79° 13′</b>                                        | <b>2</b> 59° 18′                                      | 158° 27′                                      | <b>33</b> 8° 27'                   | 237° 37′                                                 | 57° 36′                             | <b>316° 49'</b>                                | 136° 48′                           | C = Concluded Augle                                                                                          |
| XXX &<br>XXVII | "<br>h 42 ° 00<br>h 40 ° 96<br>h 42 ° 44 | "<br>h 43°28<br>h 42°74<br>h 41°76  | "<br>h 42 · 78<br>h 40 · 72<br>h 42 · 46<br>h 41 · 32 | "<br>h 42 · 86<br>h 40 · 40<br>h 40 · 60<br>h 42 · 82 | "<br>h 40°84<br>h 43°00<br>h 42°66<br>l 42°14 | "<br>  43°08<br>  42°54<br>  42°12 | "<br>l 43°28<br>l 39°82<br>h 42°86<br>h 42°80<br>h 40°20 | "<br>h 43`02<br>h 42`12<br>h 42`42  | "<br>h 42.66<br>h 40.60<br>hl 42.14<br>l 41.38 | "<br>  42.56<br>  42.06<br>  41.82 | $M = 42'' \cdot 08$ $w = 27 \cdot 59$ $\frac{1}{w} = 0 \cdot 04$ $G = 72'' \cdot 05'' \cdot 05'' \cdot 05''$ |
|                | 41.80                                    | 42.29                               | 41.82                                                 | 41.62                                                 | 42.10                                         | 42.58                              | 41.28                                                    | 42.22                               | 41.20                                          | 42.15                              | $C = 73 \ 37 \ 42 \ 00$                                                                                      |
| XXVII &<br>XXV | h 23 ° 74<br>h 23 ° 00<br>h 22 ° 82      | h 23 · 32<br>h 23 · 44<br>h 25 · 08 | h 24 °00<br>h 23 °46<br>h 22 °22                      | h 22 °94<br>h 23 °78<br>h 23 °26                      | h 22.62<br>h 21.86<br>hl23.72<br>l 24.84      | l 24.06<br>l 24.34<br>l 23.98      | l 24.82<br>h 22.70<br>h 24.38<br>h 23.48                 | h 24 · 12<br>h 23 · 96<br>h 22 · 42 | h 24 °00<br>h 23 °48<br>l 22 °22               | l 23°02<br>l 23°44<br>l 22°94      | $M = 23'' \cdot 48$ $w = 34 \cdot 34$ $\frac{I}{-} = 0 \cdot 03$                                             |
|                | 23.19                                    | 23.95                               | 23.23                                                 | 23.33                                                 | <b>23°2</b> 6.                                | 24.13                              | 23.85                                                    | 23.20                               | 23.23                                          | 23.13                              | $C = 53^{\circ} 35' 23'' \cdot 48$                                                                           |

At XXIX (Bintli)

March 1874; observed by Lieut. J. Hill, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle           |                                          | Circle readings, telescope being set on XXVI          |                                          |                                          |                                          |                               |                                                       |                                                      |                                          |                                          |                                                                  |  |  |  |  |
|-----------------|------------------------------------------|-------------------------------------------------------|------------------------------------------|------------------------------------------|------------------------------------------|-------------------------------|-------------------------------------------------------|------------------------------------------------------|------------------------------------------|------------------------------------------|------------------------------------------------------------------|--|--|--|--|
| between         | 0° 1′                                    | 180° 1′                                               | 79° 14′                                  | 259° 14'                                 | 158° 24′                                 | 838° 24'                      | 237° 36′                                              | 57° 35′                                              | 316° 51′                                 | 136 <b>°</b> 50′                         | C = Concluded Angle                                              |  |  |  |  |
| XXVI &<br>XXVII | "<br>h 46 • 42<br>h 45 • 78<br>h 45 • 22 | "<br>h 45 ° 06<br>h 47 ° 18<br>l 45 ° 78<br>l 46 ° 82 | "<br>l 47 • 46<br>l 46 • 80<br>l 46 • 90 | "<br>l 46 · 16<br>l 46 · 70<br>l 47 · 74 | n<br>h 46 · 16<br>h 47 · 48<br>h 46 · 90 | n 45 58<br>h 46 90<br>h 46 72 | "<br>h 45 · 56<br>h 45 · 18<br>h 45 · 14<br>h 46 · 92 | "<br>h 47 °60<br>h 45 ° 20<br>h 45 ° 54<br>h 44 ° 90 | "<br>h 46 · 94<br>h 46 · 72<br>h 45 · 50 | ,<br>h 47 * 28<br>h 46 * 48<br>h 47 * 36 | $M = 46'' \cdot 4I$ $w = 23 \cdot 99$ $\frac{I}{w} = 0 \cdot c4$ |  |  |  |  |
|                 | 45.81                                    | 46.31                                                 | +7.02                                    | 46.87                                    | 46.85                                    | 46.40                         | 45.70                                                 | 45.81                                                | 46.39                                    | 47.04                                    | $\tilde{C} = 63^{\circ} 54' 46'' \cdot 40$                       |  |  |  |  |

| At XXIX (Bintli)—(Continued).                                                   |                                                                                                                    |                                                               |                                                                                   |                                                                |                                                       |                                                         |                                    |                                                  |                                               |                                                               |                                                                                                           |  |  |
|---------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------|-----------------------------------------------------------------------------------|----------------------------------------------------------------|-------------------------------------------------------|---------------------------------------------------------|------------------------------------|--------------------------------------------------|-----------------------------------------------|---------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------|--|--|
| Angle                                                                           |                                                                                                                    |                                                               | Circ                                                                              | ele reading                                                    | gs, telesco                                           | pe being                                                | set on X                           | XVI                                              |                                               |                                                               | M = Mean of Groups                                                                                        |  |  |
| between                                                                         | 0° 1′                                                                                                              | 180° 1′                                                       | 79° 14′                                                                           | <b>25</b> 9° 14′                                               | 158° 24′                                              | 338° 24′                                                | 237° 36′                           | 57° 35′                                          | <b>3</b> 16°51′                               | 136° 50′                                                      | w = Relative Weight<br>C = Concluded Angle                                                                |  |  |
| XXVII &<br>XXXI                                                                 | "<br>h 27°20<br>h 27°22<br>h 27°28                                                                                 | "<br>k 26*88<br>l 25*84<br>l 26*40                            | "<br>l 26·24<br>l 27·16<br>l 25·70                                                | "<br>l 25`78<br>l 26`48<br>l 26`44                             | "<br>h 27 · 84<br>h 28 · 64<br>h 26 · 02<br>h 25 · 86 | "<br>h 25°82<br>h 26°70<br>h 26°82                      | "<br>h 25°78<br>h 27°02<br>h 26°84 | "<br>h 24°52<br>h 25°58<br>h 24°60<br>h 25°48    | "<br>h 24.60<br>h 26.48<br>h 24.46<br>h 25.60 | "<br>h 26°04<br>h 25°10<br>h 26°26                            | $M = 26'' \cdot 24$ $w = 16 \cdot 18$ $\frac{1}{w} = 0 \cdot 06$                                          |  |  |
|                                                                                 | 27.23                                                                                                              | 26.37                                                         | 26.37.                                                                            | 26.23                                                          | 27.09                                                 | <b>2</b> 6·45                                           | 26.22                              | . 25 ° 05                                        | 25.28                                         | 25.80                                                         | $C = 64^{\circ} 49' 26'' \cdot 23$                                                                        |  |  |
|                                                                                 |                                                                                                                    |                                                               |                                                                                   |                                                                | At X                                                  | XX (N                                                   | ok)                                |                                                  |                                               | •                                                             |                                                                                                           |  |  |
| t.<br>Decemb                                                                    | March 18<br>ber 1874                                                                                               | 874; obs<br>; obse <b>rv</b>                                  | served by<br>ed by C                                                              | y Lieut.<br>aptain 1                                           | J. Hill<br>U. W. 1                                    | l, R.E.,<br>Roger's,                                    | with Ba<br>R.E., u                 | prrow's ?<br>with Bar                            | 2 <b>4-inch<br/>row's 2</b> 4                 | Theodol<br>L-inch Ti                                          | ite No.2.<br>heodolite No.2.                                                                              |  |  |
| Angle     Circle readings, telescope being set on XXXIII     M = Mean of Groups |                                                                                                                    |                                                               |                                                                                   |                                                                |                                                       |                                                         |                                    |                                                  |                                               |                                                               |                                                                                                           |  |  |
| Angle<br>between                                                                | 241°34′                                                                                                            | 61°34′                                                        | 820° 46′                                                                          | 140° 46′                                                       | 39° 58'                                               | 219° 58′                                                | 119°11′                            | 299° 11′                                         | 198° <b>22′</b>                               | 18° 22′                                                       | w = Relative Weight<br>C = Concluded Angle                                                                |  |  |
| XXXIII &<br>XXXII                                                               | "<br>h 15°72<br>h 15°14<br>h 14°06                                                                                 | "                                                             | "<br><b>h</b> 15 · 52<br><b>h</b> 13 · 02<br><b>h</b> 16 · 60<br><b>l</b> 13 · 52 | " 16.28 16.38 13.30 14.92 14.04 15.64                          | "<br>h 16 ° 08<br>h 15 ° 12<br>h 13 ° 70<br>h 15 ° 96 | "<br><b>h</b> 16°20<br><b>h</b> 16°16<br><b>h</b> 14°60 | "<br>h 15°66<br>h 16°10<br>h 14°68 | ".<br>h 15°06<br>h 14°86<br>h 14°72              | "<br><b>h</b> 15°44<br>h 15°24<br>h 14°60     | "<br>k 14°04<br>k 15°26<br>k 15°64                            | $M = 15'' \cdot 08$ $w = 31 \cdot 59$ $\frac{1}{w} = 0 \cdot 03$ $C = 55^{\circ} 50' 15'' \cdot 08$       |  |  |
|                                                                                 | 14.97                                                                                                              | 14.81                                                         | 14.67                                                                             | 15.09                                                          | 15.31                                                 | 15.62                                                   | 15.48                              | 14.88                                            | 15.09                                         | 14.98                                                         |                                                                                                           |  |  |
| •<br>XXXII &<br>XXXI                                                            | <b>Å</b> 11 · 42<br><b>Å</b> 8 · 36<br><b>Å</b> 12 · 28<br><b>Å</b> 8 · 82<br><b>Å</b> 13 · 14<br><b>Å</b> 12 · 46 | k 11 · 58<br>k 12 · 08<br>k 10 · 52<br>k 12 · 52<br>k 10 · 74 | h 13.86<br>h 13.04<br>h 12.30<br>h 10.76                                          | l 11.40<br>l 13.70<br>l 15.28<br>l 13.20<br>l 11.40<br>l 11.30 | l 10°16<br>h 12°06<br>h 11°70                         | h 11.80<br>h 10.18<br>h 9.82                            | h 13.72<br>h 12.62<br>h 13.06      | h 12 · 18<br>h 12 · 82<br>h 11 · 48<br>h 15 · 26 | h 14.52<br>h 13.22<br>h 13.82                 | h 12 · 34<br>h 12 · 86<br>h 11 · 24<br>h 11 · 28<br>h 12 · 04 | $M = 12'' \cdot 15$ $w = 7 \cdot 02$ $\frac{1}{w} = 0 \cdot 14$                                           |  |  |
|                                                                                 | 11.08                                                                                                              | 11.49                                                         | 12.49                                                                             | 12.71                                                          | 11.31                                                 | 10.60                                                   | 13.13                              | 12.94                                            | 13.82                                         | 11.92                                                         | $C = 62^{\circ} 36^{\circ} 12^{''} \cdot 14$                                                              |  |  |
|                                                                                 |                                                                                                                    |                                                               | Circ                                                                              | le reading                                                     | s, telesco                                            | pe being s                                              | set on XX                          | XXI                                              |                                               |                                                               |                                                                                                           |  |  |
|                                                                                 | 0° 2′                                                                                                              | 180° 2′                                                       | <b>79° 11′</b>                                                                    | 259° 11′                                                       | 158° 24′                                              | 838° 24'                                                | <b>2</b> 37° 37′                   | 57° 36′                                          | <b>8</b> 16° 50'                              | 136° 50′                                                      | M                                                                                                         |  |  |
| XXXI &<br>XXVII                                                                 | "<br>l 48.68<br>l 48.72<br>l 48.80                                                                                 | "<br>2 47 • 78<br>2 48 • 68<br>2 48 • 10                      | "<br>2 46 · 76<br>2 47 · 94<br>2 47 · 76<br>2 47 · 68                             | "<br><b>h</b> 45 ° 40<br><b>h</b> 46 ° 44<br><b>h</b> 46 ° 80  | "<br>h 47 · 56<br>h 46 · 80<br>h 47 · 88              | "<br>h 48 · 72<br>h 49 · 36<br>l 48 · 32                | "<br>l 46.66<br>l 46.54<br>h 47.12 | "<br>h 47°58<br>h 46°24<br>h 45°48<br>h 47°12    | "<br>h 46 ° 22<br>h 47 ° 20<br>h 47 ° 70      | "<br>h 47°04<br>h 47°64<br>h 47°10                            | $w = 47^{\circ} \cdot 40$ $w = 11 \cdot 84$ $\frac{1}{w} = 0 \cdot 08$ $C = 68^{\circ} 24' 47'' \cdot 46$ |  |  |
|                                                                                 | 48.73                                                                                                              | 48.19                                                         | 47.54                                                                             | 46 . 21                                                        | 47.41                                                 | 48.80                                                   | 46.77                              | 46.60                                            | 47.04                                         | 47 • 26                                                       |                                                                                                           |  |  |
| · †<br>XXVII &<br>XXVIII                                                        | l 37.66<br>l 37.12<br>l 37.64                                                                                      | 2 37 54<br>2 37 14<br>2 36 94                                 | l 39°30<br>l 38°72<br>l 38°14                                                     | h 38 · 40<br>h 39 · 44<br>h 39 · 12                            | h 38.60<br>h 37.52<br>h 37.62                         | h 38°14<br>h 38°06<br>l 39°86                           | l 38.88<br>l 38.36<br>h 37.56      | h 38.68<br>h 38.44<br>h 38.48                    | h 38 · 82<br>h 39 · 08<br>h 38 · 18           | h 37.68<br>h 36.42<br>h 37.40                                 | $M = 38'' \cdot 17$<br>$w = 18 \cdot 50$<br>$\frac{1}{2} = 0.25$                                          |  |  |
|                                                                                 | 37 • 47                                                                                                            | 37.21                                                         | 38.72                                                                             | 38.99                                                          | 37.91                                                 | 38.69                                                   | 38.27                              | 38.23                                            | 38.69                                         | 37.17                                                         | $w = 53^{\circ} - 53^{\circ}$<br>$C = 53^{\circ} - 2^{\circ} 38^{''} \cdot 17^{\circ}$                    |  |  |

At XXXI (Mongolia)

+March 1874; observed by Lieut. J. Hill, R. E., with Barrow's 24-inch Theodolite No. 2. \*December 1874; observed by Captain M. W. Rogers, R. E., with Barrow's 24-inch Theodolite No. 2.

| Angle                |                                                                |                                                                                        | M - Mean of Groups                                       |                                                                                                                     |                                                          |                                                    |                                                                            |                                                                         |                                                                      |                                                                                                  |                                                                                                             |
|----------------------|----------------------------------------------------------------|----------------------------------------------------------------------------------------|----------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------|----------------------------------------------------|----------------------------------------------------------------------------|-------------------------------------------------------------------------|----------------------------------------------------------------------|--------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------|
| between              | 0° 2′                                                          | 180° 2′                                                                                | 79° 14′                                                  | 259° 14′                                                                                                            | 158° 24′                                                 | <b>3</b> 38° <b>23</b> ′                           | 237° 36′                                                                   | 57° 35′                                                                 | <b>3</b> 16° <b>4</b> 9′                                             | 1 <b>36° 4</b> 9′                                                                                | <ul> <li>w = Relative Weight</li> <li>C = Concluded Angle</li> </ul>                                        |
| *<br>XXIX &<br>XXVII | k 43°32<br>k 43°70<br>k 41°80                                  | # 42.78<br># 43.08<br># 42.82                                                          | <i>k</i> 44 · 54<br><i>k</i> 43 · 60<br><i>k</i> 42 · 88 | k 43.02<br>k 42.32<br>k 43.73                                                                                       | <i>k</i> 42 · 78<br><i>k</i> 43 · 36<br><i>l</i> 43 · 84 | <i>k</i> 42°14<br><i>k</i> 42°96<br><i>k</i> 43°34 | <i>k</i> 43 ° 98<br><i>k</i> 42 ° 88<br><i>k</i> 42 ° 38                   | <i>n</i><br><i>h</i> 42.62<br><i>h</i> 43.66<br><i>h</i> 43.18<br>43.15 | # 42.22<br># 41.06<br># 42.90                                        | 2 44.08<br>2 42.38<br>2 42.20<br>2 44.52<br>42.20                                                | $M = 43'' \cdot 02$ $w = 30 \cdot 72$ $\frac{1}{w} = 0 \cdot 03$ $C = 38^{\circ} 31' 43'' \cdot 02$         |
| XXVII &<br>XXX       | 49.08<br>49.84<br>49.84<br>49.90<br>49.61                      | 1 49.38<br>h 49.38<br>h 48.58<br>h 48.62<br>48.86                                      | 43 07<br>\$ 50.42<br>\$ 49.88<br>\$ 50.04<br>50.11       | 43 02<br>h 47 26<br>h 47 82<br>hl48 52<br>47 87                                                                     | 43 33<br>2 47 84<br>2 46 46<br>2 46 46<br>46 92          | . h 47 · 86<br>h 48 · 72<br>h 48 · 68<br>48 · 42   | \$ 47.46<br>\$ 47.66<br>\$ 47.50<br>47.54                                  | +3 +3<br>h 49 • 46<br>h 49 • 04<br>h 48 • 80<br>49 • 10                 | 12 00<br>h 48.72<br>h 49.76<br>h 49.88<br>49.45                      | 43 30<br>1 47.44<br>1 47.06<br>1 46.94<br>47.15                                                  | $M = 48'' \cdot 50$<br>$w = 7 \cdot 90$<br>$\frac{1}{w} = 0 \cdot 13$<br>$C = 64^{\circ} 5' 48'' \cdot 50$  |
|                      | 0° 0′                                                          | 180°0′                                                                                 | Cir<br>79° 13'                                           | rcle readin<br>259°13'                                                                                              | gs, telesco<br>158°25'                                   | ope being<br>888°25'                               | set on XX<br>237° 37′                                                      | X<br>57° 86′                                                            | 316° 49′                                                             | 136° 48'                                                                                         |                                                                                                             |
| *<br>XXX &<br>XXXII  | \$ 57°76<br>\$ 55°24<br>\$ 55°90                               | <i>k</i> 53 92<br><i>h</i> 55 98<br><i>k</i> 57 14<br><i>h</i> 56 02<br><i>h</i> 56 12 | k 54°68<br>l 54°82<br>l 55°02                            | *<br>2 54 <sup>-</sup> 84<br>2 55 <sup>-</sup> 18<br>2 55 <sup>-</sup> 86                                           | "<br>2 56 ° 34<br>2 55 ° 96<br>2 56 ° 24                 | 2 55 98<br>2 58 96<br>2 55 42<br>2 56 42           | *<br>2 56 ° 64<br>3 55 ° 24<br>3 56 ° 56                                   | *<br>* 54 · 92<br>* 56 · 38<br>* 55 · 88                                | <i>k</i> 54 72<br><i>l</i> 53 30<br><i>l</i> 54 10<br><i>l</i> 54 84 | <b>k</b> 53 · 38<br><b>l</b> 55 · 70<br><b>l</b> 55 · 40<br><b>l</b> 57 · 72<br><b>l</b> 56 · 46 | $M = 55^{"} \cdot 70$ $w = 12 \cdot 65$ $\frac{1}{w} = 0 \cdot 08$ $C = 50^{\circ} 15^{'} \cdot 50^{\circ}$ |
|                      | 56.30                                                          | 55.84                                                                                  | 54.84                                                    | 55.39                                                                                                               | 56.18                                                    | 56.70                                              | 56.12                                                                      | 55°73                                                                   | 54.24                                                                | 55.23                                                                                            | 0 = 30 17 35 70                                                                                             |
| *<br>XXXII &<br>XXXV | k 10.76<br>k 13.98<br>k 12.12<br>k 15.28<br>k 12.50<br>k 12.72 | k 16.28<br>k 11.42<br>k 13.16<br>h 11.32                                               | k 10°18<br>l 12°76<br>l 14°38<br>l 14°22                 | 2 9 <sup>.</sup> 88<br>2 11 <sup>.</sup> 68<br>2 11 <sup>.</sup> 02<br>2 14 <sup>.</sup> 72<br>2 12 <sup>.</sup> 30 | l 12.86<br>l 13.30<br>l 11.68                            | l 13.98<br>l 14.08<br>l 14.42                      | l 11 · 54<br>l 14 · 82<br>l 12 · 52<br>l 13 · 00<br>l 15 · 76<br>l 14 · 54 | l 13.68<br>l 12.40<br>l 12.60                                           | k 13.78<br>k 13.84<br>k 13.68                                        | <u>h 13.84</u><br>l 14.18<br>l 14.50                                                             | $M = 13'' \cdot 21$ $w = 10 \cdot 14$ $\frac{1}{w} = 0 \cdot 10$                                            |
|                      | 12.89                                                          | 13.02                                                                                  | 12.88                                                    | 11.92                                                                                                               | 12.01                                                    | 14.16                                              | 13.70                                                                      | 12.89                                                                   | 13.22                                                                | 14.12                                                                                            | $C = 54^{\circ} 41^{\circ} 13^{''} \cdot 17$                                                                |

At XXXII (Pabusar)

December 1874; observed by Captain M. W. Rogers, R. E., with Barrow's 24-inch Theodolite No. 2.

| Angle          |                                    | Circle readings, telescope being set on XXXV |                                                                      |                                    |                                          |                              |                                          |                                                                           |                                               |                                           |                                                                  |  |  |
|----------------|------------------------------------|----------------------------------------------|----------------------------------------------------------------------|------------------------------------|------------------------------------------|------------------------------|------------------------------------------|---------------------------------------------------------------------------|-----------------------------------------------|-------------------------------------------|------------------------------------------------------------------|--|--|
| between        | <b>0°</b> 0′                       | 180° 0′                                      | 79° 18′                                                              | <b>259° 13'</b>                    | 158° 24′                                 | <b>3</b> 38° <b>24</b> ′     | <b>2</b> 37° 37′                         | 57° <b>86</b> ′                                                           | 816° 48'                                      | 186° 48′                                  | C = Concluded Angle                                              |  |  |
| XXXV &<br>XXXI | "<br>h 16·70<br>h 16·92<br>h 17·98 | "<br>h 17°04<br>h 16°08<br>h 16°60           | <i>k</i> 17°36<br><i>k</i> 15°80<br><i>k</i> 16°16<br><i>k</i> 16°90 | "<br>h 15°78<br>h 15°82<br>h 17°02 | "<br>h 16 ° 08<br>h 17 ° 00<br>l 15 ° 38 | "<br>17.38<br>16.76<br>17.90 | "<br>2 16 · 84<br>2 17 · 54<br>2 15 · 72 | "<br>l 17 <sup>•</sup> 22<br>l 17 <sup>•</sup> 72<br>l 17 <sup>•</sup> 34 | "<br>h 18 98<br>h 18 94<br>h 16 84<br>h 16 78 | "<br><b>h</b> 16°54<br>h 16°48<br>h 16°80 | $M = 16'' \cdot 87$ $w = 22 \cdot 52$ $\frac{1}{w} = 0 \cdot 04$ |  |  |
|                | 17.30                              | 16.22                                        | 16.26                                                                | 16.51                              | 16.12                                    | 17.35                        | 16.20                                    | 17.43                                                                     | 17.88                                         | 16.01                                     | $\tilde{C} = 69^{\circ} 27' 16'' \cdot 87$                       |  |  |

## PRINCIPAL TRIANGULATION. OBSERVED ANGLES.

At XXXII (Pabusar)—(Continued).

|          |                                  |                        |                    |                    |                    |                         |                |                    | · · · · · ·                      |                    | 1                                                              |
|----------|----------------------------------|------------------------|--------------------|--------------------|--------------------|-------------------------|----------------|--------------------|----------------------------------|--------------------|----------------------------------------------------------------|
| Angle    |                                  |                        | Circ               | cle reading        | gs, telesco        | ope being               | set on XX      | XXV                |                                  |                    | M – Mean of Groups<br>w = Relative Weight                      |
| between  | 0° 0′                            | 180° 0′                | • 79° 13′          | 259° 13′           | 158° 24′           | <b>3</b> 38° <b>24'</b> | 237° 87′       | 57° 36′            | <b>3</b> 16° <b>48</b> ′         | 1 <b>36° 4</b> 8′  | C = Concluded Angle                                            |
|          | "                                |                        | "                  | H                  | "                  | "                       | "              | "                  | "                                | . "                |                                                                |
|          | h 56.64                          | <b>h</b> 54.30         | h 53.60            | h 55 54            | h 55.20            | 2 54.46                 | 2 54.32        | 1 54.60            | h 52.92                          | h 55°36            | $M = 54'' \cdot 94$                                            |
| XXXI &   | h 54.80                          | h 55°08                | h 53°52<br>h 54°32 | h 54.32            | h 54°54<br>h 56°80 | 1 55.18                 | 1 54 00        | 1 50°44<br>1 51°02 | <i>h</i> 55°32<br><i>h</i> 55°66 | h 55°02<br>h 53°78 | an - 14 168                                                    |
| XXX      | h 52.88                          | h 56.14                | ·· J+ J-           | h 54.38            | h 57.30            | - 51 - 11               | 0000           | - 51 9-            | h 57 . 98                        | ·· 33 /·           | $w = 14^{-00}$                                                 |
|          | \$ 54.10                         |                        |                    | h 55°44            | h 56.13            |                         |                |                    | h 55°44                          |                    | $\frac{1}{w} = 0.07$                                           |
|          | 54°74                            | 55°44                  | 53.81              | 54.88              | 50.02              | 54.69                   | 54.08          | 55.32              | 55.46                            | 54.92              | $C = 67^{\circ} 5' 54'' \cdot 97$                              |
|          | kar .08                          | h                      | k 20.00            | h 20.88            | h 20.12            | 1 22.68                 | 1 22:50        | 1 22:08            | h 21.16                          | h 21.50            |                                                                |
| XXX A    | h 20.34                          | h 20.94                | h 19.98            | h 22.02            | h 22.04            | l 21.92                 | 1 22.98        | 1 20.50            | h 19.40                          | h 21 °08           | $M = 21'' \cdot 54$                                            |
| XXXIII   | h 22.90                          | h 20.86                | h 19.82            | h 21°30            | h 22°14            | 8 21.84                 | l 21.92        | 1 23 28            | h 22.78                          | h 20.72            | m = 12.24                                                      |
|          | h 23 72                          | <b>n</b> 20 70         |                    | h 22 40            |                    |                         |                | 6 22 20            | $h_{21}^{\circ}_{24}$            |                    |                                                                |
|          |                                  |                        |                    |                    |                    |                         |                | ···· • ····        |                                  |                    | $\frac{1}{w} = 0.07$                                           |
|          | 21.99                            | 21.40                  | 19.93              | 21.83              | 21.43              | 22.12                   | 22.42          | 22.03              | 20*97                            | 21.10              | $C = 61^{\circ} 59^{\circ} 21^{''} \cdot 55$                   |
|          | ħ 44 · 44                        | <b>h</b> 44 • 90       | h +7.06            | h 48.90            | h 46.30            | 1 44 . 96               | i<br>44°18     | 1 45.90            | h 44 ° 08                        | h 44 · 76          | M - 45":00                                                     |
| XXXIII & | h 46.50                          | h 44 32                | h 46.86            | h 45 10            | h 45 . 30          | 1 43 96                 | 7 44.88        | 1 44 92            | h 45 92                          | h 44 ° 26          | $m = 45^{-00}$                                                 |
| XXXIV    | h 43 40                          | <b>n</b> 45 10         | h45.46             | h 40 40<br>h 45 48 | h 44 04            | 645 02                  | 1 45 02        | 1 44 74            | h 43.66                          | <i>n</i> +3 00     | w = 13.34                                                      |
|          | h 43.62                          |                        | .5 .               | h 44 ° 00          | •••••              |                         |                |                    | 10                               |                    | $\frac{1}{-} = 0.07$                                           |
|          |                                  |                        |                    |                    |                    |                         |                |                    |                                  |                    | $w = 0.0^{\circ} 06' 4r'' 001$                                 |
|          | 44`34                            | 44.80                  | 46.46              | 45`99              | 45.02              | 44.85                   | 44.96          | 44.69              | 44.29                            | 44 • 29            | 0 = 94 20 45 01                                                |
|          | h 40°08                          | h 40.82                | <b>h</b> 39.56     | h 39.02            | h 39°98            | 1 39.84                 | <b>h</b> 41.16 | 141.28             | h 40°90                          | h41.00             | $M = 40^{\prime\prime}$                                        |
| XXXIV &  | h 40.00                          | h41.56                 | h 42.00            | h 40°14            | h 40°26            | 1 40.86                 | h 40'38        | 1 41.80            | h 39.76                          | h 40°28            | 112 - 40 44                                                    |
| XXXV     | 741 IA                           | <i>1</i> 41 0 <i>4</i> | h41°22             | <i>∎</i> 40 52     | 1 30 32            | 640 40                  | <i>n</i> 39 20 | 140.44             | <i>1</i> 40 40                   | h 38.70            | w = 19.74                                                      |
|          |                                  |                        | h 39 · 44          |                    |                    |                         |                |                    |                                  | <b>h</b> 39.22     | $\frac{1}{-} = 0.05$                                           |
|          | 40.40                            | 41.40                  | 40.76              | 39.89              | 39.29              | 40.32                   | 40.22          | 40.01              | 40.32                            | 40'49              | $\overset{w}{C} = 67^{\circ} \circ 40^{\prime\prime} \cdot 46$ |
|          |                                  |                        |                    |                    |                    |                         |                |                    |                                  |                    | 1                                                              |
|          |                                  |                        |                    | At                 |                    | III (Bil                | (ampur         | 1                  |                                  |                    | •                                                              |
| Decembe  | r 1874;                          | observe                | d by Ca            | ptain M            | . W. R             | ogers, I                | R.E., wit      | h Barr             | 010'8 24                         | -inch The          | eodolite No. 2.                                                |
| Angle    |                                  |                        | Circ               | le reading         | s, telesco         | pe being s              | et on XX       | XIV                |                                  | •                  | M = Mean of Groups                                             |
| between  | <b>0°</b> 0′                     | 180° 0′                | 79° 13′            | <b>259° 13′</b>    | 158° 25′           | 338° 25′                | 237° 87′       | 57° 36′            | <b>316° 48</b> ′                 | 136° 48′           | w = Kelative Weight<br>C = Concluded Angle                     |
|          | "                                |                        |                    |                    |                    |                         |                |                    |                                  |                    | 1                                                              |
|          | h 35.22                          | <b>h</b> 35.76         | h 34.10            | h 36.10            | h 36·38            | <b>h</b> 37°06          | h 34 · 34      | 1 38.02            | 1.36.80                          | 1 35.36            | $M = 36'' \cdot 14$                                            |
| XXXIV &  | <b>A</b> 39°14<br><b>A</b> 22°02 | h 37.86                | h 36.02            | h 33.82            | h 36.18            | h 35°36                 | 136.26         | 1 36.68            | 1 36.14                          | 136.04             |                                                                |
| XXXII    | h35.12                           | h 36.64                | ~ 33 YU            | h 35.40            | ng0 /2             | #30 I4                  | 135.86         | 1 35°54            | . 30 70                          | • 35 /0            | w = 14.44                                                      |
|          | -                                |                        |                    |                    |                    |                         | -              | 1 35.80            |                                  |                    | $\frac{1}{20} = 0.07$                                          |
|          |                                  |                        |                    |                    |                    |                         |                |                    |                                  |                    | $\tilde{C} = 40^{\circ} 46' 36'' \cdot 16$                     |
|          | 35.85                            | 36.84                  | 35.38              | 35.41              | 36.43              | 36.19                   | 35.83          | 37.14              | 36.22                            | 35.73              |                                                                |
|          |                                  |                        |                    |                    |                    |                         |                |                    |                                  |                    |                                                                |

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| At XXXIII (Bikampur)—(Continued). |                                    |                               |                                                                    |                                                       |                                               |                                          |                                         |                           |                                                          |                                    |                                                                  |  |
|-----------------------------------|------------------------------------|-------------------------------|--------------------------------------------------------------------|-------------------------------------------------------|-----------------------------------------------|------------------------------------------|-----------------------------------------|---------------------------|----------------------------------------------------------|------------------------------------|------------------------------------------------------------------|--|
| Angle<br>between                  | 0° 0,                              | 180° 0′                       | Circ.<br>79° 13′                                                   | le reading<br>259° 13′                                | s, telesco<br>158°25'                         | pe being s<br>338°25'                    | et on XX<br>237° 37′                    | XIV<br>57°36'             | <b>316° 48′</b>                                          | 136° 48′                           | M = Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle |  |
| XXXII &<br>XXX                    | *<br>\$21.70<br>\$22.22<br>\$20.58 | # 22°90<br>h 22°68<br>h 23°72 | "<br>h 22 · 42<br>h 24 · 30<br>h 21 · 86<br>h 25 · 00<br>h 23 · 20 | "<br>h 21 ° 54<br>h 24 ° 62<br>h 23 ° 64<br>h 24 ° 00 | "<br>h 20'72<br>h 20'96<br>h 23'56<br>h 21'82 | "<br>h 23 * 84<br>h 24 * 86<br>h 25 * 04 | "<br>h 23 °68<br>h 24 ° 24<br>h 24 ° 12 | 24.56<br>223.14<br>224.58 | "<br>l 21.68<br>l 22.38<br>l 23.98<br>l 24.82<br>l 23.64 | "<br>  22°20<br>  23°56<br>  22°06 | $M = 23'' \cdot 18$ $w = 8 \cdot 26$ $\frac{1}{w} = 0 \cdot 12$  |  |
|                                   | 21.20                              | 23.10                         | 23.30                                                              | 23.45                                                 | 21.77                                         | 24.58                                    | 24'01                                   | 24.09                     | 23.30                                                    | 22.01                              | $C = 62^{\circ} 10' 23'' \cdot 18$                               |  |

## At XXXIV (Phulasar)

December 1874 and January 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle             |                                                     |                                             | Circl                                                                                   | le reading                                                           | s, telesco                                                     | pe being s                                             | et on XX                                    | XVII                                             |                                             |                                                     | M = Mean of Groups                                                                                                 |
|-------------------|-----------------------------------------------------|---------------------------------------------|-----------------------------------------------------------------------------------------|----------------------------------------------------------------------|----------------------------------------------------------------|--------------------------------------------------------|---------------------------------------------|--------------------------------------------------|---------------------------------------------|-----------------------------------------------------|--------------------------------------------------------------------------------------------------------------------|
| between           | 121°0′                                              | <b>3</b> 01° 0′                             | 200° 11′                                                                                | 20°11′                                                               | <b>279° 23′</b>                                                | 99° 23′                                                | <b>358° 34′</b>                             | 178° 34′                                         | 77° 47′                                     | 257° 47'                                            | to = Relative Weight<br>C = Concluded Angle                                                                        |
| XXXVII &<br>XXXVI | "<br>1 58 • 74<br>1 58 • 02<br>1 58 • 98<br>58 • 58 | "<br>1 58·78<br>1 58·70<br>1 59·18<br>58·89 | "<br>h 57 · 72<br>h 59 · 44<br>h 59 · 02<br>h 58 · 28<br>58 · 62                        | "<br>h 58 · 10<br>h 56 · 56<br>h 57 · 54<br>57 · 40                  | "<br>h 58.04<br>h 58.30<br>h 60.34<br>h 59.98<br>59.16         | "<br>l 58·10<br>l 58·12<br>l 59·40<br>d 57·60<br>58·31 | "<br>h 59`70<br>h 59`10<br>h 58`32<br>59`04 | "<br>h 59 °98<br>h 59 °12<br>h 58 °72<br>59 °27  | "<br>2 58.64<br>2 58.06<br>2 58.40<br>58.37 | "<br>2 59 · 24<br>2 59 · 12<br>2 58 · 36<br>58 · 91 | $M = 58'' \cdot 65$ $w = 24 \cdot 34$ $\frac{1}{w} = 0 \cdot 04$ $C = 68^{\circ} 16' 58'' \cdot 65$                |
| XXXVI &<br>XXXV   | 2 48.66<br>2 48.64<br>2 49.34                       | 2 49 °00<br>2 49 °24<br>2 48 °68            | h 49 · 42<br>h 50 · 42<br>h 47 · 28<br>h 45 · 50<br>h 50 · 64<br>h 46 · 68<br>h 47 · 10 | h 47 °06<br>h 47 °34<br>h 51 °24<br>h 49 °56<br>h 50 °10<br>h 50 °22 | h 51°16<br>h 51°62<br>h 47°04<br>l 49°44<br>l 49°02<br>l 49°72 | l 47 · 80<br>l 47 · 80<br>l 48 · 52<br>d 47 · 10       | h 49`82<br>h 48`70<br>h 49`04               | h 48 · 98<br>h 46 · 82<br>h 47 · 26<br>h 47 · 08 | l 49.66<br>l 49.68<br>l 48.32               | 2 48 · 18<br>2 49 · 62<br>2 49 · 42                 | $M = 48'' \cdot 77$<br>$w = 11 \cdot 68$<br>$\frac{1}{w} = 0 \cdot 09$<br>$C = 57^{\circ} 57' 48'' \cdot 76$       |
|                   | 48.88                                               | <b>48</b> °97                               | 48.15                                                                                   | 49.25                                                                | 49.67                                                          | 47.81                                                  | 49.19                                       | 47.53                                            | 49.22                                       | 49.07                                               |                                                                                                                    |
| XXXV &<br>XXXII   | k 49 ° 06<br>k 48 ° 90<br>k 47 ° 40                 | h 50°52<br>h 49°30<br>h 47°78<br>h 49°70    | 2 49 · 12<br>2 49 · 24<br>2 49 · 30                                                     | 2 47 · 66<br>2 47 · 58<br>2 48 · 90                                  | h 50.08<br>h 47.30<br>h 49.44<br>h 47.22<br>l 48.28            | l 49.60<br>l 47.08<br>l 48.26<br>l 46.06<br>l 47.12    | h 48 · 10<br>h 48 · 92<br>h 47 · 72         | h 48 · 24<br>h 48 · 18<br>h 48 · 06              | l 48·28<br>l 48·58<br>l 48·40               | l 49.60<br>l 49.48<br>l 48.44                       | $M = 48'' \cdot 51$ $w = 19 \cdot 90$ $\frac{1}{w} = 0 \cdot 05$ $G = 65^{\circ} 55' \cdot 8'' \cdot 5''$          |
|                   | 48.45                                               | 49'33                                       | 49.22                                                                                   | 48.05                                                                | 48.46                                                          | 47 62                                                  | 48.25                                       | 48.10                                            | 48.42                                       | 49'17                                               | c = 07 59 40 50                                                                                                    |
| XXXII &<br>XXXIII | Å 38 · 54<br>Å 37 · 18<br>Å 39 · 26                 | h 37 · 36<br>h 37 · 10<br>h 38 · 92         | 2 38·84<br>2 39·12<br>2 37·82                                                           | 2 38·88<br>2 37·70<br>2 37·28                                        | h 36.98<br>h 37.68<br>h 39.89<br>h 41.80<br>l 40.80<br>l 40.36 | l 37 · 26<br>l 36 · 40<br>l 59 · 22<br>l 39 · c8       | h 38 36<br>h 39 44<br>h 39 62               | h 38·32<br>h 37·72<br>h 39·04                    | 2 39 · 16<br>2 38 · 98<br>2 38 · 50         | 2 39 · 22<br>2 38 · 96<br>2 38 · 40                 | $M = 38'' \cdot 55$ $w = 16 \cdot 11$ $\frac{1}{w} = 0 \cdot 06$ $G = 43^{\circ} 46' \cdot 6^{\circ} = 10^{\circ}$ |
|                   | 38.33                                               | 37.79                                       | 38.29                                                                                   | 37°95                                                                | 39.60                                                          | 37°99                                                  | 39.14                                       | 38.30                                            | 38.88                                       | 38.80                                               | $c = 44^{-} 40^{-} 38^{-} 58$                                                                                      |

#### At XXXV (Girondi)

January 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| ·                  |                                                                                 |                                                   |                                    |                                               |                                               |                                                               |                                                       |                                                   |                                          |                                          |                                                                                                              |
|--------------------|---------------------------------------------------------------------------------|---------------------------------------------------|------------------------------------|-----------------------------------------------|-----------------------------------------------|---------------------------------------------------------------|-------------------------------------------------------|---------------------------------------------------|------------------------------------------|------------------------------------------|--------------------------------------------------------------------------------------------------------------|
| Angle              |                                                                                 |                                                   | Circ                               | ele reading                                   | zs, telesco                                   | pe being a                                                    | set on XI                                             | XXI                                               |                                          |                                          | M = Mean of Groups<br>w = Relative Weight                                                                    |
| 0et <b>ween</b>    | 859° 59′                                                                        | 179° 59′                                          | 79° 13′                            | 259° 13′                                      | 158° 24′                                      | 338° 24′                                                      | 237° <b>37′</b>                                       | 57° 87′                                           | 316° 48'                                 | 136° 48′                                 | C = Concluded Angle                                                                                          |
| XXXI &<br>XXXII    | n<br>h 28 ° 02<br>h 27 ° 10<br>h 31 ° 20<br>h 29 ° 20<br>h 31 ° 12<br>h 30 ° 40 | # 30°30<br>l 30°32<br>l 29°72                     | "<br>l 30.62<br>l 29.74<br>l 29.90 | *<br>l 29°26<br>l 28°94<br>l 31°46<br>l 29°92 | "<br>  29°02<br>  31°34<br>  29°38<br>  30°16 | "<br>k 29°12<br>k 28°12<br>k 27°70                            | "<br>h 31 ° 26<br>h 33 ° 24<br>h 30 ° 70<br>h 30 ° 10 | "<br>2 31.02<br>2 28.36<br>2 29.94<br>2 30.12     | "<br>2 31 · 14<br>2 29 · 86<br>2 30 · 08 | l 28·72<br>l 28·64<br>l 30·22            | $M = 29'' \cdot 86$<br>$w = 11 \cdot 42$<br>$\frac{1}{w} = 0 \cdot 09$<br>$C = 55^{\circ} 51' 29'' \cdot 87$ |
|                    | 29.21                                                                           | 30.11                                             | 30.00                              | 29.90                                         | 29.97                                         | 28.31                                                         | 31.33                                                 | 29.86                                             | 30.30                                    | 29.19                                    |                                                                                                              |
| XXXII &<br>XXXIV   | k 32°04<br>k 30°98<br>k 31°78                                                   | h 31.62<br>h 34.12<br>l 30.96<br>l 31.64          | l 32.02<br>l 31.46<br>l 30.66      | 2 30°76<br>2 31°54<br>2 31°86                 | l 31.80<br>l 31.70<br>l 32.74                 | h 30°24<br>h 32°52<br>h 28°50<br>h 31°86<br>h 28°48           | h 30`88<br>h 31`46<br>h 31`94                         | l 28.90<br>l 31.88<br>l 31.78<br>l 30.60          | l 32°80<br>l 32°04<br>l 32°12            | l 31°48<br>l 31°26<br>l 32°44<br>l 32°04 | $M = 31'' \cdot 52$ $w = 15 \cdot 62$ $\frac{1}{w} = 0 \cdot 06$                                             |
|                    | 31.00                                                                           | 32.09                                             | 31.38                              | 31:39                                         | 32.08                                         | 30.32                                                         | 31.43                                                 | 30.79                                             | 32.32                                    | 31.81                                    | $C = 44^{\circ} 59' 31'' \cdot 50$                                                                           |
| XXXIV &<br>XXXVI   | h 25 ° 32<br>h 21 ° 34<br>h 23 ° 56<br>h 24 ° 96                                | h 22°36<br>l 24°66<br>l 22°56<br>l 22°60          | l 22.52<br>l 23.68<br>l 23.62      | l 24 · 22<br>l 23 · 36<br>l 22 · 34           | l 23·18<br>l 22·44<br>l 22·86                 | h 22 · 96<br>h 23 · 20<br>h 25 · 30<br>h 25 · 38<br>h 23 · 94 | h 22°16<br>h 23°32<br>h 22°26                         | ! 21 · 36<br>! 20 · 28<br>! 22 · 92<br>! 22 · 78  | l 20°60<br>l 21°32<br>l 23°36<br>l 21°64 | l 22°54<br>l 20°96<br>l 22°72<br>l 21°58 | $M = 22'' \cdot 86$ $w = 10 \cdot 14$ $\frac{1}{w} = 0 \cdot 10$                                             |
|                    | 23.80                                                                           | 23.04                                             | 23°27                              | 23.31                                         | 22.83                                         | 24.30                                                         | 22.58                                                 | 21.84                                             | 21.73                                    | 21.02                                    | $C = 70^{\circ} 37' 22'' \cdot 86$                                                                           |
| XXXVI &<br>XXXVIII | h 27 °66<br>h 27 °98<br>h 29 °26<br>h 27 °20<br>28 °03                          | h 30°52<br>h 30°30<br>l 28°10<br>l 28°94<br>29°46 | 28.54<br>27.66<br>29.16<br>28.45   | 29.42<br>28.14<br>29.16<br>28.91              | l 27°10<br>l 28°52<br>l 29°00<br>28°21        | h 26°42<br>h 28°78<br>h 29°10<br>h 28°74<br>28°26             | h 28.78<br>h 29.22<br>h 26.66<br>h 27.82<br>28.12     | l 28.95<br>l 31.42<br>l 28.88<br>l 28.68<br>29.49 | 28.96                                    | 28.46<br>29.24<br>30.56<br>29.34         | $M = 28'' \cdot 73$ $w = 17 \cdot 75$ $\frac{1}{w} = 0 \cdot 06$ $C = 73^{\circ} 44' \cdot 28'' \cdot 74$    |
|                    |                                                                                 |                                                   |                                    |                                               |                                               |                                                               |                                                       |                                                   |                                          |                                          |                                                                                                              |

## At XXXVI (Mankasar)

January 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle           |       |                                    | Circ                                                          | ele reading                              | gs, telesco                                | pe being                                 | set on XX                                                | XXV                                           |                                    |                                     | M = Mean of Groups                                                |
|-----------------|-------|------------------------------------|---------------------------------------------------------------|------------------------------------------|--------------------------------------------|------------------------------------------|----------------------------------------------------------|-----------------------------------------------|------------------------------------|-------------------------------------|-------------------------------------------------------------------|
| between         | 0° 1′ | 180° 1′                            | 79° 12′                                                       | <b>2</b> 59° 12′                         | 158° 25'                                   | <b>3</b> 38° 25′                         | <b>237°</b> 36′                                          | 57° 36′                                       | <b>316° 48'</b>                    | 1 <b>3</b> 6° <b>4</b> 8′           | c = Concluded Angle                                               |
| XXXV &<br>XXXIV | "     | *<br>  48.00<br>  47.22<br>  48.82 | "<br><b>h</b> 48 · 64<br><b>h</b> 47 · 66<br><b>h</b> 49 · 20 | n<br>h 48 • 42<br>h 49 • 06<br>h 48 • 44 | # 47 <sup>*</sup> 92<br>l 48*70<br>l 49*90 | l 48.60<br>h 46.98<br>h 49.60<br>h 47.86 | n<br>h 46·30<br>h 47·52<br>h 48·24<br>l 49·44<br>l 48·94 | "<br>  46°94<br>  48°54<br>  48°96<br>  48°52 | "<br>  49°02<br>  50°24<br>  48°00 | 7 48 • 24<br>7 48 • 88<br>7 48 • 68 | $M = 48'' \cdot 49$ $w = 32 \cdot 78$ $\frac{1}{w} = 0 \cdot c_3$ |
|                 | 48.63 | 48.01                              | 48.50                                                         | 48.64                                    | 48.84                                      | 48.26                                    | 48.09                                                    | 48.24                                         | 49° <b>09</b>                      | 48.60                               | $C = 51^{\circ} 24' 48''' \cdot 47$                               |

| $\mathbf{At}$ | XXXVI | (Mankasar)                     | )( | (Continued | ). |
|---------------|-------|--------------------------------|----|------------|----|
|               |       | / and one we we we we we we we |    | 00.000.000 |    |

| Angle             |                                                                                    |                                                                             | Cir                                         | cle readin                                                           | gs, telesco                                                                | ope being                                                           | set on X                                 | XXV                               |                                                                          |                                                       | M = Mean of Groups                                                                                         |
|-------------------|------------------------------------------------------------------------------------|-----------------------------------------------------------------------------|---------------------------------------------|----------------------------------------------------------------------|----------------------------------------------------------------------------|---------------------------------------------------------------------|------------------------------------------|-----------------------------------|--------------------------------------------------------------------------|-------------------------------------------------------|------------------------------------------------------------------------------------------------------------|
| between           | 0° 1′                                                                              | 180° 1′                                                                     | 79° 12′                                     | <b>2</b> 59° 12 <b>′</b>                                             | 158° 25′                                                                   | 838° 25′                                                            | 2 <b>37°</b> 36'                         | <b>57° 36′</b>                    | <b>316° 48</b> ′                                                         | 136° 48′                                              | w = Relative Weight<br>C = Concluded Angle                                                                 |
| XXXIV &<br>XXXVII | "<br>h 22 ° 80<br>h 21 ° 68<br>h 24 ° 02<br>l 20 ° 68<br>l 20 ° 64                 | "<br>  21 • 48<br>  20 • 96<br>  20 • 14                                    | n<br>h 22°04<br>h 22°90<br>h 21°82          | n<br>h 20.68<br>h 20.46<br>h 20.70<br>d 21.50                        | "<br>h 24 °00<br>l 22 °22<br>l 20 °34<br>l 19 °88<br>l 21 °10              | "<br>l 19.56<br>h 21.80<br>h 23.72<br>h 23.10<br>h 24.70<br>h 23.14 | "<br>h 22 ° 72<br>h 22 ° 26<br>h 20 ° 86 | 222.74<br>224.16<br>223.10        | <pre>% 2 23 * 88 2 19 * 52 2 21 * 54 h 23 * 76 h 23 * 76 h 23 * 50</pre> | "<br>2 21 · 88<br>2 24 · 14<br>2 21 · 82<br>2 23 · 46 | $M = 22'' \cdot 09$ $w = 9 \cdot 46$ $\frac{1}{w} = 0 \cdot 11$ $C = 45^{\circ} 48' 22'' \cdot 10$         |
|                   | <b>2</b> 1.96                                                                      | 20.86                                                                       | 22.35                                       | 20.84                                                                | 21.21                                                                      | 22.67                                                               | 21.92                                    | 23.33                             | 22.67                                                                    | 22.82                                                 |                                                                                                            |
| XXXVII &<br>XXXIX | h 25 · 22<br>h 22 · 26<br>h 25 · 32<br>h 24 · 82<br>h 24 · 60                      | <b>h</b> 21 ° 74<br>h 23 ° 04<br>h 24 ° 58<br>h 24 ° 48<br><b>h</b> 26 ° 54 | <b>h</b> 23.86<br>h 24.10<br><b>h</b> 24.62 | h 25 °08<br>h 23 °50<br>h 26 °60<br>h 25 °48<br>h 23 °96<br>d 25 °81 | h 21 ° 74<br>l 22 ° 36<br>l 22 ° 06<br>h 23 ° 36<br>h 24 ° 38<br>h 24 ° 68 | l 23.80<br>l 25.94<br>h 27.02<br>h 26.44<br>h 25.16<br>h 23.96      | h 25 · 46<br>h 25 · 56<br>h 25 · 14      | l 23°14<br>l 24°38<br>l 22°98     | l 25°66<br>l 25°28<br>l 24°68                                            | l 23.20<br>l 23°48<br>l 23°12                         | $M = 24'' \cdot 36$ $w = 9 \cdot 59$ $\frac{1}{w} = 0 \cdot 10$ $G = 66^{\circ} 14' \cdot 27$              |
|                   | 24.44                                                                              | 24.08                                                                       | 24.19                                       | 25.07                                                                | 23.10                                                                      | 25.39                                                               | 25.39                                    | 23.20                             | 25.21                                                                    | 23.27                                                 | 0 = 70 14 24 3/                                                                                            |
| XXXIX &<br>XL     | k 58°34<br>k 59°30<br>k 58°78                                                      | h 55°82<br>h 56°40<br>h 57°30                                               | h 55°78<br>h 57°86<br>h 57°78<br>h 57°10    | h 56 80<br>h 56 26<br>h 59 32<br>h 59 48<br>h 57 8                   | k 58.68<br>2 57.86<br>2 59.52                                              | l 58·46<br>l 58·66<br>l 58·98                                       | h 57°44<br>h 58°02<br>h 57°96<br>h 56°08 | h 58°04<br>h 57°86<br>h 57°06     | h 57°92<br>h 57°24<br>h 57°88                                            | h 55°78<br>h 56°62<br>h 57°14                         | $M = 57'' \cdot 68$ $w = 11 \cdot 20$ $\frac{1}{m} = 0 \cdot 09$                                           |
|                   | 58.81                                                                              | 56.21                                                                       | 57.13                                       | 57°79                                                                | 58.69                                                                      | 58.70                                                               | 57:38                                    | 57.65                             | 57.68                                                                    | 56.21                                                 | $\int_{0}^{\infty} C = 89^{\circ} 43' 57'' \cdot 68$                                                       |
| XL &<br>XXXVIII   | k 15 ° 76<br>k 18 ° 02<br>k 18 ° 32<br>k 19 ° 60<br>l 15 ° 38                      | l 18.06<br>l 17.26<br>l 18.76                                               | h 21 · 40<br>h 18 · 30<br>h 19 · 22         | h 17°16<br>h 18°36<br>h 17°62                                        | 18.38<br>18.36<br>17.58                                                    | l 16.76<br>l 17.94<br>l 15.40<br>l 18.44<br>l 16.30                 | h 17°30<br>h 16°88<br>h 16°24            | h 16.76<br>h 16.16<br>h 16.48     | λ 17 · 22<br>λ 15 · 86<br>λ 18 · 68<br>λ 16 · 72                         | k 16.44<br>k 16.60<br>k 18.02                         | $M = 17^* \cdot 53$ $w = 8 \cdot 98$ $\frac{1}{w} = 0 \cdot 11$                                            |
|                   | 17.42                                                                              | 18.03                                                                       | 19.64                                       | 17.71                                                                | 18.11                                                                      | 16.92                                                               | 16.81                                    | 16.47                             | 17.13                                                                    | 17.02                                                 | $C = 47^{\circ} 20' 17'' \cdot 52$                                                                         |
| XXXVIII &<br>XXXV | k 13 · 18<br>k 9 · 42<br>k 9 · 74<br>k 8 · 88<br>k 7 · 36<br>l 10 · 32<br>l 9 · 38 | 2 8.16<br>2 12.92<br>3 10.10<br>2 9.98<br>2 9.22<br>2 8.64                  | h 11.08<br>h 10.56<br>h 8.86<br>h 9.60      | k 10 °00<br>k 9 °70<br>k 8 °72                                       | 7 8·86<br>7 9·84<br>7 9·44                                                 | l 10°06<br>l 9°26<br>l 9°72                                         | k 10°70<br>k 10°26<br>k 9°92<br>k 9°32   | 111.06<br>18.98<br>19.64<br>19.70 | 2 8.52<br>2 9.78<br>2 9.10                                               | l 10°54<br>l 6°98<br>l 8°46<br>l 10°22                | $M = 9'' \cdot 62$<br>$w = 23 \cdot 08$<br>$\frac{1}{w} = 0 \cdot 04$<br>$C = 49^{\circ} 28' 9'' \cdot 65$ |
|                   | 9.75                                                                               | 9.84                                                                        | 10.03                                       | 9°47                                                                 | 9.38                                                                       | 9.68                                                                | 10.02                                    | 9.84                              | 9.13                                                                     | 9.02                                                  |                                                                                                            |

.

## At XXXVII (Uperthal)

January 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle            |                                                                            |                                                                                         | Ci                                               | ircle read                          | ings, teles                              | cope being                                      | ; set on X                                                         | LI                                                                                           |                                          |                                                     | M - Mean of Groups                                                                                           |
|------------------|----------------------------------------------------------------------------|-----------------------------------------------------------------------------------------|--------------------------------------------------|-------------------------------------|------------------------------------------|-------------------------------------------------|--------------------------------------------------------------------|----------------------------------------------------------------------------------------------|------------------------------------------|-----------------------------------------------------|--------------------------------------------------------------------------------------------------------------|
| between          | 170° <b>48</b> ′                                                           | <b>850° 48′</b>                                                                         | <b>250° 0′</b>                                   | 70° 0′                              | 829° 12′                                 | 149°12′                                         | 48° 24′                                                            | 228° 24′                                                                                     | 127° 86′                                 | 207° 36′                                            | w = Relative Weight<br>C = Concluded Angle                                                                   |
| XLI &<br>XXXIX   | "<br>\$ 55`52<br>\$ 54`78<br>\$ 54`12                                      | "<br>h 54·36<br>h 54·28<br>h 54·02                                                      | "<br>h 53°08<br>h 52°94<br>h 55°40<br>h 53°98    | "<br>h 55`34<br>h 53`72<br>h 55`40  | "<br>h 56·56<br>h 55·90<br>h 54·72       | "<br>h 56·96<br>l 54·60<br>l 54·50<br>h 55·02   | "<br>2 53 ° 74<br>2 56 ° 58<br>h 54 ° 36<br>h 52 ° 84<br>h 53 ° 26 | "<br>h 51 · 72<br>h 53 · 60<br>h 55 · 66<br>h 54 · 26<br>h 56 · 80<br>h 53 · 12<br>h 54 · 04 | "<br>h 52`52<br>h 53`82<br>h 54`46       | "<br>h 55°28<br>h 54°96<br>h 55°50                  | $M = 54'' \cdot 59$<br>$w = 12 \cdot 84$<br>$\frac{1}{w} = 0 \cdot 08$<br>$C = 62^{\circ} 27' 54'' \cdot 57$ |
|                  | 54.81                                                                      | 54.22                                                                                   | 53.85                                            | 54.82                               | 55.73                                    | 55°27                                           | 54.16                                                              | 54.17                                                                                        | 53.60                                    | 55.25                                               |                                                                                                              |
| XXXIX &<br>XXXVI | k 55 · 58<br>k 53 · 56<br>k 55 · 32<br>k 55 · 98                           | h 56°02<br>h 55°44<br>h 54°78<br>h 56°82<br>h 56°10                                     | h 56 ° 24<br>h 55 ° 36<br>h 55 ° 36<br>h 57 ° 42 | h 55°86<br>h 56°14<br>h 55°64       | h 54 48<br>h 53 56<br>h 56 00<br>h 54 26 | <b>h</b> 52°32<br>l 54°10<br>l 53°86<br>l 54°96 | 2 56 56<br>2 56 18<br>2 53 86<br>2 57 80<br>2 57 80<br>2 57 30     | h 56°02<br>h 54°68<br>h 53°42<br>h 54°18                                                     | h 56°86<br>h 55°08<br>h 55°12            | k 56 ° 12<br>k 55 ° 74<br>∿k 55 ° 30                | $M = 55'' \cdot 34$ $w = 12 \cdot 10$ $\frac{1}{w} = 0 \cdot c8$                                             |
|                  | 55.11                                                                      | 55.83                                                                                   | 56.10                                            | 55.88                               | 54°57                                    | 53.81                                           | 56.14                                                              | 54.28                                                                                        | 55.69                                    | 55°72                                               | $\tilde{C} = 60^{\circ} 49' 55'' \cdot 34$                                                                   |
| XXXVI &<br>XXXIV | h 38 · 84<br>h 39 · 68<br>h 37 · 50<br>h 38 · 42<br>h 36 · 34<br>h 38 · 88 | k 39 · 26<br>k 39 · 70<br>k 36 · 88<br>k 41 · 78<br>k 41 · 26<br>k 38 · 58<br>k 40 · 38 | k 41 °02<br>k 42 °50<br>k 39 °42<br>k 38 °74     | h 37 · 90<br>h 39 · 78<br>h 38 · 16 | h 39°00<br>h 38°66<br>h 39°62            | k 40°14<br>k 40°26<br>l 39°08                   | l 37 96<br>l 37 86<br>l 38 86<br>l 37 18<br>h 39 50                | h 40°58<br>h 41°58<br>h 41°00                                                                | k 38·32<br>k 40·36<br>k 40·34<br>k 39·02 | h 39 80<br>h 38 94<br>h 38 28<br>h 39 60<br>h 38 88 | $M = 39'' \cdot 39$<br>$w = 9 \cdot 23$<br>$\frac{1}{w} = 0 \cdot 11$<br>$C = 65^{\circ} 54' 20'' \cdot 27$  |
|                  | 38.28                                                                      | 39.69                                                                                   | 40°42                                            | 38.61                               | 39.09                                    | 39.83                                           | 38.27                                                              | 41.02                                                                                        | 39.21                                    | 39.10                                               | 0 - 05 54 59 37                                                                                              |

At XXXVIII (Bithnok)

January 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle                                                                                                          |                                                          |                                          | Circ                                                     | cle readings, telescope being set on XXXV |                                                          |                                               |                                 |                                    |                                    |                                          | M = Mean of Groups                                               |
|----------------------------------------------------------------------------------------------------------------|----------------------------------------------------------|------------------------------------------|----------------------------------------------------------|-------------------------------------------|----------------------------------------------------------|-----------------------------------------------|---------------------------------|------------------------------------|------------------------------------|------------------------------------------|------------------------------------------------------------------|
| between                                                                                                        | 0° 0′                                                    | 108° 0′                                  | 79° 12′                                                  | <b>2</b> 59° 12′                          | 158° 30′                                                 | 838° 80′                                      | 237° 87′                        | 57° 87′                            | <b>3</b> 16° 48′                   | 186° 48′                                 | C - Concluded Angle                                              |
| XXXV &<br>XXXVI                                                                                                | "<br>h 22°52<br>h 22°72<br>h 24°34<br>h 24°10<br>h 22°32 | "<br>h 21 • 50<br>h 22 • 72<br>h 22 • 42 | "<br>h 19°16<br>h 21°00<br>h 21°84<br>h 20°96<br>h 22°36 | "<br>h 21 ° 78<br>h 21 ° 74<br>h 20 ° 00  | "<br>l 23.56<br>l 22.10<br>l 20.26<br>l 23.50<br>l 23.56 | "<br>l 23°86<br>l 22°96<br>l 21°82<br>l 22°40 | " h 21 · 70 h 21 · 78 h 21 · 18 | "<br>h 22°94<br>h 21°88<br>h 20°68 | "<br>h 23°16<br>h 22°80<br>h 22°76 | "<br>h 22 ° 90<br>h 21 ° 38<br>h 22 ° 60 | $M = 22'' \cdot 22$ $w = 10 \cdot 44$ $\frac{1}{w} = 0 \cdot 10$ |
| 99 - 199 - 199 - 199 - 199 - 199 - 199 - 199 - 199 - 199 - 199 - 199 - 199 - 199 - 199 - 199 - 199 - 199 - 199 | 23.80                                                    | 22.31                                    | 31.06                                                    | 21.12                                     | 22.60                                                    | 22.76                                         | 21.22                           | 21.83                              | <b>22.</b> 91                      | 22.29                                    | $C = 56^{\circ} 47' 22'' \cdot 23$                               |

,

|                  |                                                                            |                                                                                                              | A                                                                  | t XXX                                    | VIII (I                                                 | Bithnok                                        | )—(Con                                                                    | tinued).                                         |                                                       |                                                       |                                                                                                     |
|------------------|----------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------|------------------------------------------|---------------------------------------------------------|------------------------------------------------|---------------------------------------------------------------------------|--------------------------------------------------|-------------------------------------------------------|-------------------------------------------------------|-----------------------------------------------------------------------------------------------------|
| A                | 1                                                                          |                                                                                                              | Circl                                                              | e reading                                | s, telesco                                              | pe being                                       | set on X                                                                  | xxv                                              |                                                       |                                                       | M = Mean of Groups                                                                                  |
| Angle<br>between | 0° 0′                                                                      | 180° 0′                                                                                                      | 79° 12′                                                            | 259° 12′                                 | 158° 30'                                                | 838° 30'                                       | 237° 37′                                                                  | 57° 37′                                          | 316° 48′                                              | 136° 48′                                              | w = Relative Weight<br>C = Concluded Angle                                                          |
| XXXVI &<br>XL    | "<br>h 33 ° 68<br>h 33 ° 86<br>h 31 ° 24<br>h 32 ° 68                      | "<br>h 34 · 14<br>h 32 · 84<br>h 32 · 62                                                                     | "<br>h 35 · 50<br>h 32 · 78<br>h 34 · 34<br>h 31 · 92<br>h 32 · 94 | "<br>h 33 · 38<br>h 32 · 64<br>h 33 · 56 | "<br>l 31 · 82<br>l 31 · 08<br>l 33 · 34<br>l 30 · 54   | "<br>2 31 · 52<br>2 32 · 48<br>2 31 · 16       | "<br>h 33 · 58<br>h 33 · 00<br>h 31 · 78                                  | "<br>h 32 · 74<br>h 32 · 78<br>h 34 · 58         | "<br>h 35 * 44<br>h 32 * 86<br>h 32 * 74<br>h 31 * 08 | "<br>h 30 ° 64<br>h 32 ° 68<br>h 31 ° 76<br>h 32 ° 68 | $M = 32'' \cdot 73$ $w = 13 \cdot 10$ $\frac{1}{w} = 0 \cdot 08$                                    |
|                  | 32.87                                                                      | 33.30                                                                                                        | 33.20                                                              | 33.10                                    | 31.60                                                   | 31.23                                          | 32.29                                                                     | 33°37                                            | <u>33</u> .03                                         | 31.94                                                 | $C = 62^{\circ} 5' 32'' \cdot 73$                                                                   |
|                  |                                                                            |                                                                                                              |                                                                    |                                          | At XX                                                   | XIX (I                                         | Modia)                                                                    |                                                  |                                                       |                                                       |                                                                                                     |
| Januar           | y 1875;                                                                    | observe                                                                                                      | d by Ca                                                            | ptain M                                  | . W. R                                                  | ogers, I                                       | R.E., wit                                                                 | th Barro                                         | no's 24-1                                             | inch The                                              | odolite No. 2.                                                                                      |
| A                |                                                                            |                                                                                                              | Ci                                                                 | rcle readim                              | ngs, teles                                              | cope being                                     | g set on X                                                                | LI                                               |                                                       |                                                       | M = Mean of Groups                                                                                  |
| Angle<br>between | 0° 1′                                                                      | 180° 0′                                                                                                      | 79° 18′                                                            | <b>2</b> 59° 12′                         | 158° 24′                                                | 838° 24'                                       | 237° 37′                                                                  | 57 <b>°</b> 36′                                  | 816° 48′                                              | 136° 48′                                              | w = Relative Weight<br>C = Concluded Angle                                                          |
| XLI &<br>XLIII   | "<br>h 4.88<br>h 5.34<br>h 3.64                                            | "<br>h 3·96<br>h 3·30<br>l 3·58                                                                              | 1 4 42<br>1 2 48<br>1 3 76<br>1 4 30                               | h 4.68<br>h 2.86<br>h 4.36<br>h 4.20     | <pre>k 5 * 22 k 3 * 04 h 4 * 06 l 1 * 90 l 2 * 38</pre> | 1 5 74<br>1 4 76<br>1 2 06<br>1 3 04<br>1 3 02 | "<br>l 2.64<br>l 2.66<br>l 5.10<br>l 2.46                                 | h 5°48<br>h 3°58<br>h 2°50<br>h 4°00             | n<br>h 2·78<br>h 3·70<br>h 3·82                       | "<br>l 2·30<br>l 2·44<br>l 3·12                       | $M = 3'' \cdot 62$ $w = 19 \cdot 34$ $\frac{1}{w} = 0 \cdot 05$                                     |
|                  | 4.63                                                                       | 3.01                                                                                                         | 3.74                                                               | 4.03                                     | 3.32                                                    | 3.72                                           | 3.51                                                                      | 3.80                                             | 3.43                                                  | 2.62                                                  | $C = 83^{\circ} 20' 3'' \cdot 62$                                                                   |
| XLIII &<br>XLIV  | k 55 * 14<br>k 57 * 12<br>k 58 * 78<br>k 59 * 70<br>k 57 * 88<br>k 57 * 50 | h58 · 10<br>h58 · 12<br>h59 · 18                                                                             | l 56°42<br>l 56°90<br>l 56°22<br>l 57°20                           | h 57°14<br>h 59 12<br>h 57°00            | h 57°00<br>h 57°42<br>l 56°90<br>l 57°36                | 2 56 98<br>2 57 18<br>2 59 84<br>2 58 18       | l 57 58<br>l 58 26<br>l 55 20<br>l 57 98<br>h 59 00                       | h 57 58<br>h 59 38<br>h 59 08<br>h 58 32         | h 57 °66<br>h 58 °00<br>h 58 °30                      | 2 57·78<br>2 56·44<br>2 57·86                         | $M = 57'' \cdot 74$ $w = 17 \cdot 80$ $\frac{1}{w} = 0 \cdot 06$                                    |
|                  | 57.69                                                                      | 58.47                                                                                                        | 56.69                                                              | 57.75                                    | 57.17                                                   | 58.04                                          | 57.60                                                                     | 58.29                                            | 57 99                                                 | 57:36                                                 | $C = 50^{\circ} 7' 57'' \cdot 73$                                                                   |
| XLIV &<br>XLII   | k 24 · 22<br>k 24 · 52<br>k 23 · 42                                        | k 24 · 28<br>k 25 · 86<br>k 24 · 84                                                                          | l 25°96<br>l 23°68<br>l 24°38<br>l 26°44                           | k 24 ° 08<br>k 24 ° 08<br>k 24 ° 02      | k 25°98<br>k 26°02<br>l 28°10<br>l 26°80                | l 24.76<br>l 24.08<br>l 24.12<br>l 26.14       | l 28.02<br>k 26.56<br>k 23.40<br>k 24.98<br>k 27.36<br>k 24.60<br>d 23.57 | k 23 · 80<br>k 24 · 78<br>k 24 · 26<br>k 24 · 82 | k 27°40<br>k 25°28<br>k 24°48<br>k 26°26              | 24.54<br>26.70<br>24.26<br>26.60                      | $M = 25'' \cdot 10$ $w = 10 \cdot 07$ $\frac{1}{w} = 0 \cdot 10$ $C = 20^{\circ} 17' 27'' \cdot 10$ |
| •                | 24.05                                                                      | · 24·99                                                                                                      | 25.12                                                              | 24.00                                    | 26.72                                                   | 24.78                                          | 25.20                                                                     | 24.41                                            | 25.86                                                 | 25.52                                                 | ~ - 39 1/ 25 13                                                                                     |
| XLII &<br>XL     | k 11 · 20<br>k 11 · 60<br>k 11 · 30                                        | <b>h</b> 12 °90<br><b>h</b> 9 °88<br><b>l</b> 9 °18<br><b>l</b> 13 °26<br><b>l</b> 13 °10<br><b>l</b> 12 °42 | l 12.02<br>l 12.88<br>l 12.84                                      | k 13.52<br>k 14.42<br>k 13.34<br>k 13.10 | h 12.28<br>h 12.78<br>l 10.28<br>l 12.06<br>d 11.81     | l 13°12<br>l 15°40<br>l 12°50<br>l 13°22       | l 13.76<br>h 13.28<br>h 16.72<br>d 12.34                                  | h 10.28<br>h 13.12<br>h 12.28                    | h 11 · 82<br>h 11 · 22<br>h 13 · 64<br>h 12 · 36      | l 11.50<br>l 12.94<br>l 11.58                         | $M = 12'' \cdot 49$ $w = 8 \cdot 65$ $\frac{1}{w} = 0 \cdot 12$                                     |
|                  | 11.32                                                                      | 11.20                                                                                                        | 12.28                                                              | 13.00                                    | 11.84                                                   | 13.20                                          | 14.02                                                                     | 11.80                                            | 12.30                                                 | 12.01                                                 | $C = 49^{\circ}$ 1' 12" · 50                                                                        |

|                    |                                                                         |                                                                          |                                                     | At XX                                                             | XIX (                                                         | Modia)-                                     | -(Conti                                                                   | nued).                                                      |                                                     |                                                                  |                                                                                                              |
|--------------------|-------------------------------------------------------------------------|--------------------------------------------------------------------------|-----------------------------------------------------|-------------------------------------------------------------------|---------------------------------------------------------------|---------------------------------------------|---------------------------------------------------------------------------|-------------------------------------------------------------|-----------------------------------------------------|------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------|
| Angle<br>between   | 0°1′                                                                    | 180° 0′                                                                  | Ci<br>79° 18′                                       | rcle readii<br>259° 12'                                           | ngs, teles<br>158°24'                                         | 20pe being<br>838° 24'                      | ; set on X<br>237° 37′                                                    | LI<br>57°36'                                                | <b>316<sup>•</sup> 48'</b>                          | 136° 48′                                                         | M = Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle                                             |
| XL &<br>XXXVI      | k 63 ° 02<br>k 63 ° 64<br>k 59 ° 94<br>k 62 ° 60<br>k 61 ° 80           | # 60 * 82<br># 62 * 74<br>l 62 * 40<br>l 60 * 16<br>l 60 * 46<br>61 * 32 | "<br>l 61·52<br>l 62·12<br>l 61·08                  | "<br>h 59`70<br>h 59`70<br>h 03`18<br>h 59`26<br>h 60`30<br>60`43 | "<br>h 62 · 78<br>h 61 · 16<br>l 62 · 18<br>d 62 · 00         | "<br>1 60°72<br>1 59°34<br>1 60°90<br>60°32 | "<br>\$ 59:98<br>\$ 58:58<br>\$ 57:08<br>\$ 58:12<br>58:44                | n<br>h 60°28<br>h 61°86<br>h 60°12<br>60°75                 | "<br>h 60 · 94<br>h 61 · 08<br>h 59 · 88<br>60 · 63 | "<br>l 61 · 30<br>l 62 · 08<br>l 61 · 22<br>l 61 · 98<br>61 · 65 | $M = 60'' \cdot 93$<br>$w = 6 \cdot 94$<br>$\frac{1}{w} = 0 \cdot 14$<br>$C = 36^{\circ} 37'  0'' \cdot 93$  |
| XXXVI &<br>XXXVII  | k 37.76<br>k 38.84<br>k 44.96<br>k 41.28<br>k 42.22<br>k 42.66<br>41.29 | h 43 °00<br>h 41 °28<br>l 40 °38<br>l 40 °30<br>41 °24                   | 2 40.08<br>2 42.00<br>2 42.08<br>41.39              | h 43 · 20<br>h 43 · 78<br>h 40 · 44<br>h 41 · 94<br>42 · 34       | h 39 26<br>h 42 42<br>l 41 50<br>l 40 14<br>d 40 79<br>40 82  | 2 40.84<br>2 40.50<br>2 40.18<br>40.51      | l 44.86<br>l 43.70<br>l 44.74<br>h 44.64<br>h 42.28<br>44.04              | h +2 · 90<br>h 40 · 96<br>h 43 · 70<br>h +3 · 42<br>42 · 75 | h 41 · 26<br>h 41 · 80<br>h 42 · 48<br>41 · 85      | l 44.80<br>l 42.46<br>l 41.92<br>l 42.76<br>l 43.10<br>43.01     | $M = 41'' \cdot 92$<br>$w = 6 \cdot 13$<br>$u = 0 \cdot 16$<br>$C = 42^{\circ} 55' 41'' \cdot 94$            |
| XXXVII &<br>XLI    | k 40.50<br>k 38.10<br>k 37.32<br>k 36.58<br>k 38.42                     | h 36 • 56<br>h 37 • 76<br>l 37 • 22                                      | l 40°56<br>l 37°32<br>l 36°18<br>l 39°24<br>l 39°08 | h 36.78<br>h 35.28<br>h 35.12<br>h 36.70                          | h 38 · 34<br>h 35 · 56<br>l 38 · 58<br>l 40 · 42<br>l 38 · 28 | 1 38·34<br>1 38·06<br>1 39·06               | l 36·34<br>l 36·22<br>l 35·42<br>l 41·56<br>h 36·30<br>h 37·64<br>h 38·80 | h 36°52<br>h 37°48<br>h 37°68<br>h 38°82                    | h 38 · 12<br>h 38 · 78<br>h 36 · 94                 | 2 38 04<br>2 37 00<br>2 39 48<br>2 36 24<br>2 39 48              | $M = 37'' \cdot 81$<br>$w = 12 \cdot 16$<br>$\frac{1}{w} = 0 \cdot 08$<br>$C = 58^{\circ} 40' 37'' \cdot 82$ |
| Januar             | 38 <sup>-18</sup><br>y 1875;                                            | observed                                                                 | 38 48                                               | 30°47                                                             | 38°24<br>At X.<br>W. Ro                                       | 38'49<br>L (Rone<br>ogers, R                | 37°47<br>esar)<br>.E., with                                               | 37'03                                                       | 37'95<br>w's 24-i                                   | nch Theo                                                         | dolite No. 2.                                                                                                |
| Angle<br>between   | <b>0°</b> 1′                                                            | 180° 1'                                                                  | Circle<br>79° 12′                                   | readings<br>259°12′                                               | , telescop<br>158° 25′                                        | e being se<br>838° 25'                      | t on XXX<br>237° 37″                                                      | KVIII<br>57° 37'                                            | <b>3</b> 16° 49′                                    | 136° 49'                                                         | M = Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle                                             |
| XXXVIII &<br>XXXVI | "<br>h 11 ° 98<br>h 11 ° 36<br>h 9 ° 84<br>h 11 ° 48<br>h 9 ° 78        | "<br>h 9.72<br>h 8.48<br>h 8.96                                          | "<br>2 9.58<br>2 8.64<br>2 7.92<br>2 9.86           | "<br>1 9.28<br>1 9.06<br>1 8.92                                   | "<br>k 9.60<br>h 9.14<br>k 9.08                               | "<br>k 10°52<br>k 10°66<br>k 9°76           | "<br>k 8.64<br>l 8.50<br>l 10.48                                          | "<br>10°24<br>10°50<br>19°08                                | "<br>2 9.64<br>2 12.56<br>2 11.26<br>2 10.30        | "<br>10.30<br>10.00<br>10.10                                     | $M = 9'' \cdot 78$ $w = 13 \cdot 62$ $\frac{1}{w} = 0 \cdot 07$                                              |

9.31

3.49

9'94

3.42

10.04

2.96

10.80

2.80

XXXVI & XXXIX

9.05

3.23

9.00

4.01

9.00

3'37

9.32

3.67

h 4·22 h 3·18 l 3·08 l 2·68 h 3·84 h 2·02 h 3·14 h 3·18 h 3·14 h 3·10 h 0·86 h 4·22 l 5·80 h 4·32 h 2·94 h 3·68 h 4·08 h 3·44 h 3·60 h 4·34 h 3·60 h 3·38 l 1·88 h 2·94 h 4·24 h 3·70 h 3·26 h 3·72 h 2·14 h 2·54 h 2·30 l 4·98 h 3·54 h 2·74 h 4·54 h 3·66 h 3·80

10.31

3.13

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= 0.07  $\tilde{C} = 70^{\circ} 34' 9'' \cdot 80$ 

 $M = 3'' \cdot 38$ 

w = 31.99

0.03

 $\tilde{C} = 53^{\circ}39' 3''' \cdot 39$ 

I =

w

10.14

3.33

|                   |                                                     |                                               |                                          | At X                                                          | L (Ron                                              | esar)—(                                                      | Continu                                                                         | ed).                                                           |                                                                            |                                               |                                                                                                    |
|-------------------|-----------------------------------------------------|-----------------------------------------------|------------------------------------------|---------------------------------------------------------------|-----------------------------------------------------|--------------------------------------------------------------|---------------------------------------------------------------------------------|----------------------------------------------------------------|----------------------------------------------------------------------------|-----------------------------------------------|----------------------------------------------------------------------------------------------------|
| Angle             |                                                     |                                               | Circle                                   | readings,                                                     | , telescope                                         | being set                                                    | on XXX                                                                          |                                                                |                                                                            |                                               | M - Mean of Groups                                                                                 |
| between           | 0°1′                                                | 180° 1′                                       | 79° 12′                                  | <b>2</b> 59° 12′                                              | 158° 25′                                            | 888° 25'                                                     | <b>2</b> 37° 37′                                                                | 67° 87′                                                        | <b>8</b> 16° <b>4</b> 9′                                                   | 186° 49′                                      | C = Concluded Angle                                                                                |
| XXXIX &<br>XLII   | k 39 ° 60<br>k 37 ° 90<br>k 38 ° 24<br>k 39 ° 54    | h 39°80<br>h 38°92<br>h 39°20                 | k 38 • 26<br>k 39 • 74<br>k 38 • 64      | h 39 · 82<br>h 41 · 46<br>h 38 · 34<br>h 40 · 84<br>h 39 · 48 | h 43°10<br>h 41°40<br>h 40°34<br>h 41°08<br>h 40°12 | h 41 °66<br>h 38 ° 30<br>h 38 ° 98<br>h 39 ° 04<br>h 39 ° 90 | h 39 · 98<br>h 39 · 88<br>h 39 · 30                                             | n<br>h 38 · 90<br>h 39 · 54<br>h 39 · 70                       | n<br>h 39°02<br>h 39°28<br>h 39°24                                         | *                                             | $M = 39'' \cdot 55$ $w = 15 \cdot 27$ $\frac{1}{w} = 0 \cdot 07$                                   |
|                   | 38.82                                               | 39.31                                         | 38.88                                    | 39.99                                                         | 41'21                                               | 39.58                                                        | 39.72                                                                           | 39.38                                                          | <b>3</b> 9•18                                                              | 39.42                                         | $C = 51^{\circ} 44' 39'' \cdot 58$                                                                 |
| Januar            | y 1875;                                             | observed                                      | l by Ca <sub>1</sub>                     | otain M.                                                      | At X.                                               | LI (Sac                                                      | hu)<br>. <i>E., wit</i>                                                         | h Barre                                                        | no's 24-1                                                                  | inch The                                      | odolite No. 2.                                                                                     |
| Angle<br>between  | 256° 39′                                            | 76° 89′                                       | Circ<br><b>335° 52'</b>                  | le reading:<br>155°52'                                        | zs, telesco<br>55°4'                                | pe being :<br>285°4'                                         | 184°15'                                                                         | JIII<br>814° 15′                                               | 218° 28′                                                                   | 88° 27'                                       | M - Mean of Groups<br>$\omega$ = Relative Weight<br>C = Concluded Angle                            |
| XLIII &<br>XXXIX  | "<br>h 21 · 58<br>h 22 · 86<br>h 20 · 66            | "<br>h 23.82<br>h 21.26<br>h 22.88<br>h 21.22 | *<br>h 21 · 20<br>h 22 · 72<br>h 22 · 58 | "<br>  25°38<br>  22°40<br>  24°68<br>  23°12                 | "<br>19.20<br>19.02<br>19.44<br>21.20<br>21.00      | "<br>l 23°54<br>l 22°26<br>l 24°26<br>k 23°90                | "<br>2 21 · 98<br>2 20 · 38<br>2 20 · 26<br>2 23 · 52<br>2 21 · 92<br>2 21 · 72 | *<br>  22°14<br>  20°90<br>  20°68                             | "<br>1 19 56<br>1 21 74<br>1 22 74<br>1 21 64<br>1 20 68                   | "<br>2 22.80<br>2 21.50<br>2 23.24<br>2 24.92 | $M = 22'' \cdot 08$ $w = 6 \cdot 13$ $\frac{1}{w} = 0 \cdot 16$ $C = 44^{\circ} 20' 22'' \cdot 07$ |
|                   | 21.70                                               | 22.30                                         | 22.17                                    | 23.89                                                         | 20.03                                               | 23.49                                                        | 21.63                                                                           | 21.34                                                          | 21.27                                                                      | 23.12                                         | · · · · · · · · · · · · · · · · · · ·                                                              |
| XXXIX &<br>XXXVII | h 29°74<br>h 27°46<br>h 26°88<br>h 30°02<br>h 29°04 | h 26°48<br>h 27°62<br>h 28°22                 | h 30°14<br>h 29°02<br>h 28°56            | h 28 · 22<br>l 27 · 76<br>l 27 · 02                           | l 31 · 20<br>l 28 · 32<br>l 31 · 28<br>l 29 · 68    | l 28.76<br>l 29.16<br>l 29.14                                | l 28.96<br>l 30.10<br>l 29.44                                                   | l 32°10<br>l 30°78<br>l 32°56<br>h 29°98<br>h 29°92<br>h 28°10 | l 31 · 78<br>l 29 · 56<br>h 27 · 64<br>h 29 · 54<br>h 27 · 96<br>h 31 · 70 | h 28 · 96<br>h 29 · 86<br>h 29 · 34           | $M = 29^{w} \cdot 13$ $w = 7 \cdot 53$ $\frac{1}{w} = 0 \cdot 13$                                  |
|                   | 28.63                                               | 27.44                                         | 29.24                                    | 27.67                                                         | 30.13                                               | 29.02                                                        | 29.50                                                                           | <b>3°*5</b> 7                                                  | 29.70                                                                      | 29.39                                         | $\int C = 58^{\circ} 51' 29'' \cdot 17$                                                            |
| January and       | d Februa                                            | ry 1875 ;                                     | ; observe                                | ed by Ca                                                      | At XI<br>ptain M                                    | II (Joc                                                      | lasar)<br>gers, R.                                                              | E., with                                                       | Barroi                                                                     | o's 24-in(                                    | h Theodolite No. 2.                                                                                |
| Angle<br>between  | <b>0°</b> 0′                                        | 180°0′                                        | C<br>79°13′                              | ircle read<br>259°13'                                         | ings, teles<br>158°25'                              | cope being<br>' 888°24                                       | 3 set on X<br>' 287° 87'                                                        | L<br>' 57*87'                                                  | 816° 48'                                                                   | ' 186° 48′                                    | M – Mean of Groups<br>- Relative Weight<br>C – Concluded Angle                                     |
|                   | <b>k</b> 8.52                                       | 8·42                                          | •<br>h 8·22<br>h 8·6                     | *<br>h 12°18                                                  | # 12.00                                             | <i>k</i> 10.78                                               | k 9.02                                                                          | *<br>h 9*82                                                    | n<br>h 9.84                                                                | k 7.94                                        | $M = 9" \cdot 53$                                                                                  |

| Angle         |                                                        |                                 |                                                           | M - Mean of Groups                            |                                                       |                                             |                                       |                                          |                                                                      |                                                   |                                                                                                         |
|---------------|--------------------------------------------------------|---------------------------------|-----------------------------------------------------------|-----------------------------------------------|-------------------------------------------------------|---------------------------------------------|---------------------------------------|------------------------------------------|----------------------------------------------------------------------|---------------------------------------------------|---------------------------------------------------------------------------------------------------------|
| between       | 0° 0′                                                  | 180°0′                          | 79° 18′                                                   | <b>2</b> 59° 13′                              | 158° 25'                                              | <b>888° 24</b> ′                            | <b>28</b> 7° 87′                      | 57° 87′                                  | 816° 48′                                                             | 186° 48′                                          | C = Concluded Angle                                                                                     |
| XL &<br>XXXIX | *<br>k 8.52<br>k 12.38<br>h 10.74<br>h 10.58<br>k 8.98 | "<br>l 8·42<br>l 9·22<br>l 8·64 | h 8·22<br>h 8·16<br>h 9·76<br>l 6·84<br>l 11·24<br>l 6·00 | k 12 · 18<br>k 9 · 62<br>k 9 · 56<br>k 9 · 46 | *<br>* 12.00<br>* 9.10<br>* 10.70<br>* 8.72<br>* 8.94 | *<br>h 10.78<br>h 9.00<br>h 8.32<br>h 10.00 | k 9°02<br>k 10°52<br>k 9°82<br>k 7°40 | к<br>9.82<br>л 10.44<br>л 8.12<br>л 9.28 | *<br>h 9 <sup>.84</sup><br>h 10 <sup>.52</sup><br>h 9 <sup>.66</sup> | k 7'94<br>l 7'56<br>l 11'36<br>l 10'22<br>l 11'28 | $M = 9'' \cdot 53$ $w = 13 \cdot 15$ $\frac{1}{w} = 0 \cdot 08$ $C = 70^{\circ} 14' \cdot 0'' \cdot 52$ |
| ·····         | 10.34                                                  | 8.76                            | 8.37                                                      | 10.31                                         | 9.89                                                  | 9.52                                        | 9.19                                  | 9.42                                     | 10.01                                                                | 9.67                                              | - 0 - 79 14 9 52                                                                                        |

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#### PRINCIPAL TRIANGULATION. OBSERVED ANGLES.

|                                                                                                                      |                                                                                                    |                                                                                                                      |                                                                    | At XI                                               | II (Jod                                             | lasar) —                                 | (Contin                                          | ued).                                               |                                    |                                                     |                                                                                                                                                       |  |  |  |
|----------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------|-----------------------------------------------------|-----------------------------------------------------|------------------------------------------|--------------------------------------------------|-----------------------------------------------------|------------------------------------|-----------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------|--|--|--|
| Angle<br>between                                                                                                     | 0° 0′                                                                                              | 180° 0′                                                                                                              | C<br>79° 13′                                                       | ircle read<br>259° 13′                              | ings, teles<br>158° 25'                             | scope bein<br>338°24'                    | g set on 2<br>237° 37'                           | KL<br>57° 87'                                       | 816° 48'                           | 186° 48′                                            | $M = Mean of Groups \cdot \\ w = Relative Weight \\ C = Concluded Angle$                                                                              |  |  |  |
| XXXIX &<br>XLIV                                                                                                      | <i>h</i> 7.84<br><i>h</i> 3.34<br><i>h</i> 4.36<br><i>h</i> 5.22<br><i>h</i> 6.76<br><i>h</i> 3.28 | "<br>1 7 <sup>•</sup> 24<br>1 6 <sup>•</sup> 40<br>1 7 <sup>•</sup> 96<br>1 4 <sup>•</sup> 08<br>1 5 <sup>•</sup> 20 | "<br>1 6·46<br>1 5·40<br>1 7·22                                    | "<br>h 3°48<br>h 7°40<br>"h 4°78<br>h 5°08          | "<br>h 6.68<br>h 5.32<br>h 3.58<br>h 4.54<br>h 2.90 | h 5.00<br>h 6.02<br>h 4.72               | "<br>h 4`14<br>h 3`96<br>h 5`10<br>h 5`22        | "<br>h 2.60<br>h 1.94<br>h 2.86<br>h 3.80<br>h 4.76 | "<br>h 4.36<br>h 3.92<br>h 4.16    | n<br>k 4°84<br>k 4°42<br>k 3°56                     | $M = 4^{w} \cdot 89$ $w = 8 \cdot 06$ $\frac{1}{w} = 0 \cdot 12$ $C = 88^{\circ} 44' 4^{*} \cdot 89$                                                  |  |  |  |
|                                                                                                                      | 5.13                                                                                               | 6.18                                                                                                                 | 6.30                                                               | 5.19                                                | 4.60                                                | 5.52                                     | 4.01                                             | 3.10                                                | 4.12                               | 4.32                                                |                                                                                                                                                       |  |  |  |
| At XLIII (Mugrala)<br>February 1875; observed by Captain M. W. Rogers, B.E., with Barrow's 24-inch Theodolite No. 2. |                                                                                                    |                                                                                                                      |                                                                    |                                                     |                                                     |                                          |                                                  |                                                     |                                    |                                                     |                                                                                                                                                       |  |  |  |
| Angle<br>between                                                                                                     | <b>2</b> 02 <sup>•</sup> 1′                                                                        | 22° 1′                                                                                                               | Ci1<br>281° 13'                                                    | cle readin<br>101°13'                               | ugs, telesc<br>0° 25'                               | ope being<br>1 <b>80° 25'</b>            | set on R.<br>79°37′                              | . M.<br>259° 37'                                    | 158° 49'                           | <b>336° 4</b> 8′                                    | $ \begin{array}{ll} \underline{M} = & \text{Mean of Groups} \\ \underline{w} = & \text{Relative Weight} \\ C = & \text{Concluded Angle} \end{array} $ |  |  |  |
| R. M. &<br>XLVI                                                                                                      | "<br>1 41 · 50<br>1 42 · 04<br>1 40 · 58                                                           | "<br>  42 · 30<br>  42 · 06<br>  43 · 04                                                                             | "<br>l 41°24<br>l 42°36<br>l 41°66                                 | "<br>k 42 * 24<br>k 41 * 94<br>k 42 * 54            | "<br>l 42.62<br>l 44.92<br>l 42.32<br>k 42.46       | "<br>h 42 · 54<br>h 42 · 56<br>h 41 · 86 | "<br>\$ 41.42<br>\$ 42.24<br>\$ 41.58            | "                                                   | "<br>  40.66<br>  41.94<br>  41.38 | "<br>k 41 · 62<br>k 41 · 72<br>k 40 · 20            | $M = 42^{"} \cdot 03$ $w = 18 \cdot 00$ $\frac{1}{w} = 0 \cdot 06$ $C = 22^{"} \cdot 16^{"} \cdot 16^{"}$                                             |  |  |  |
|                                                                                                                      | 41.37                                                                                              | 43 `47                                                                                                               | 41.72                                                              | 42.34                                               | 43 ° 08                                             | 42.32                                    | + <sup>1</sup> .22                               | 42.85                                               | 41 . 29                            | 41.18                                               | $C = 55^{\circ} 11 42^{\circ} 04$                                                                                                                     |  |  |  |
| XLVI &<br>XLV                                                                                                        | h 58.50<br>h 58.88<br>h 58.80                                                                      | h 57°98<br>h 58°06<br>h 57°82                                                                                        | l 58-88<br>l 57-70<br>l 58-08                                      | h 56°24<br>h 55°94<br>h 59°32<br>h 58°02<br>h 56°84 | \$ 56.58<br>\$ 58.62<br>\$ 57.28<br>\$ 57.36        | k 58 94<br>k 58 04<br>k 57 22            | h 58 · 10<br>l 58 · 18<br>l 58 · 42              | h 57 °98<br>h 57 °08<br>h 58 ° 10<br>h 56 °62       | h 58°64<br>h 58°18<br>h 58°22      | h 58 · 98<br>h 58 · 42<br>h 58 · 00                 | $M = 58'' \cdot 02$ $w = 27 \cdot 42$ $\frac{1}{m} = 0 \cdot 04$                                                                                      |  |  |  |
|                                                                                                                      | 58.23                                                                                              | 57`95                                                                                                                | 58.22                                                              | 57.27                                               | 57:46                                               | 58.07                                    | 58.23                                            | 57*45                                               | 58.35                              | 58.47                                               | $C = 46^{\circ} 42' 57'' \cdot 99$                                                                                                                    |  |  |  |
| XLV &<br>XLIV                                                                                                        | 2 2 18<br>2 3 80<br>2 1 10<br>2 3 18                                                               | 2 4.62<br>2 3.28<br>2 1.30                                                                                           | l 5.92<br>l 6.88<br>l 6.38<br>h 2.88<br>h 1.08<br>h 3.80<br>h 3.06 | k 3.40<br>k 2.26<br>k 5.66<br>k 4.12<br>k 4.06      | l 5 28<br>l 2 36<br>l 4 82<br>h 3 52                | k 4.00<br>k 2.32<br>k 2.32<br>k 2.96     | k 3.04<br>l 4.06<br>l 3.10                       | h 4·52<br>h 4·54<br>l 4·10                          | 2 3·48<br>2 3·94<br>2 4·44         | 2 5.40<br>2 3.88<br>2 4.98                          | $M = 3'' \cdot 70$<br>$w = 10 \cdot 66$<br>$\frac{1}{w} = 0 \cdot 09$<br>$C = 56'' \cdot 5'' \cdot 3''' \cdot 70$                                     |  |  |  |
|                                                                                                                      | 2.27                                                                                               | 3.02                                                                                                                 | 4.39                                                               | 3.90                                                | 3.99                                                | 2.62                                     | 3.40                                             | 4.39                                                | 3.92                               | 4.75                                                |                                                                                                                                                       |  |  |  |
| XLIV &<br>XXXIX                                                                                                      | l 37.60<br>l 34.86<br>l 35.26<br>l 35.94                                                           | l 33 98<br>l 33 56<br>l 33 90<br>l 32 80<br>h 33 88                                                                  | h 34°02<br>l 33°82<br>h 35°38                                      | h 34°24<br>h 34°00<br>h 35°98                       | h 33 98<br>h 33 70<br>h 33 40                       | h 34°38<br>h 35°94<br>h 34°84<br>h 35°20 | h 35 · 12<br>h 35 · 56<br>h 33 · 40<br>h 34 · 66 | h 32 · 96<br>h 34 · 64<br>h 34 · 96<br>h 34 · 32    | l 35°10<br>l 34°68<br>l 33°76      | l 32.76<br>l 35.54<br>l 34.42<br>l 32.48<br>l 34.78 | M = 34'' + 49<br>$w = 15 \cdot 58$<br>$\frac{1}{w} = 0 \cdot 06$                                                                                      |  |  |  |
|                                                                                                                      | 35.92                                                                                              | 33.02                                                                                                                | 34.41                                                              | 34.24                                               | 33:69                                               | 35.09                                    | 34.08                                            | 34.22                                               | 34.21                              | 34.00                                               | $C = 77^{\circ} 27' 34^{\circ} 49$                                                                                                                    |  |  |  |

Nore.-R. M. denotes Referring Mark.

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|                                                                                    |                                                                                                                            |                                                                                        |                                                   | At XL                                                          | III (M                                              | ugrala)-                                              | –(Conti                                             | nued).                                                        |                                               |                                          |                                                                                                                    |  |  |
|------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------|---------------------------------------------------|----------------------------------------------------------------|-----------------------------------------------------|-------------------------------------------------------|-----------------------------------------------------|---------------------------------------------------------------|-----------------------------------------------|------------------------------------------|--------------------------------------------------------------------------------------------------------------------|--|--|
| Angle<br>between                                                                   | -<br>202° 1′                                                                                                               | <b>22° 1</b> ′                                                                         | Cire<br>281°13'                                   | cle readin<br>101°13'                                          | gs, telesco<br>0°25'                                | ope being<br>180°25'                                  | set on F<br>79° 37′                                 | 259° 87'                                                      | 158° 49′                                      | \$38° 48′                                | M = Mean of Groups $w = Relative Weight$ $C = Concluded Angle$                                                     |  |  |
| XXXIX &<br>XLI                                                                     | "<br>  34.54<br>  34.20<br>  37.20<br>  36.94<br>  36.62                                                                   | "<br>2 34 96<br>2 39 66<br>2 38 04<br>2 38 04<br>2 36 76<br>2 37 60<br>2 35 88         | "<br>1 35 °64<br>1 38 °36<br>1 37 °50<br>1 36 °76 | "<br>k 36 * 14<br>k 35 * 90<br>k 36 * 50                       | "<br>h 36 · 46<br>h 37 · 04<br>h 35 · 86            | "                                                     | "<br><b>h</b> 35°04<br>h 36°48<br>h 35°94           | "<br><b>h</b> 37 · 12<br><b>h</b> 36 · 16<br><b>h</b> 37 · 88 | "<br>2 36 °00<br>2 37 °94<br>2 36 ° 12        | "<br>1 36·72<br>1 36·74<br>1 36·60       | $M = 36'' \cdot 62$<br>$w = 18 \cdot 78$<br>$\frac{1}{w} = 0 \cdot 05$<br>$C = 52^{\circ} 10' 36'' \cdot 63$       |  |  |
|                                                                                    | 35.90                                                                                                                      | 37.12                                                                                  | 37°07                                             | 36.18                                                          | 36.45                                               | 37.24                                                 | 35.82                                               | 37.05                                                         | 36.69                                         | 36.69                                    |                                                                                                                    |  |  |
|                                                                                    |                                                                                                                            |                                                                                        |                                                   |                                                                | At XL                                               | IV (Kh                                                | irsar)                                              |                                                               |                                               |                                          |                                                                                                                    |  |  |
| February 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theod |                                                                                                                            |                                                                                        |                                                   |                                                                |                                                     |                                                       |                                                     |                                                               |                                               |                                          |                                                                                                                    |  |  |
| Angle<br>between                                                                   | 255° 88′                                                                                                                   | 75 <b>°</b> 88′                                                                        | Cir<br>834° 50'                                   | cle readin<br>154° 50'                                         | gs, telesc<br>54° 1′                                | ope being<br>234° 1'                                  | set on X<br>133°14'                                 | LII<br>313° 14'                                               | <b>2</b> 12° 26′                              | 82° 26′                                  | M = Mean of Groups<br>$\infty = Relative Weight$<br>C = Concluded Angle                                            |  |  |
| XLII &<br>XXXIX                                                                    | "                                                                                                                          | "<br><b>h</b> 31 * 14<br><b>h</b> 30 * 58<br><b>h</b> 31 * 88                          | "<br>k 30°42<br>k 32°12<br>k 29°08                | "<br>\$ 32°96<br>\$ 33°24<br>\$ 31°90                          | "<br>h 32 * 22<br>h 30 * 34<br>h 30 * 26            | "<br>h 31 ° 38<br>h 29 ° 54<br>h 31 ° 68<br>h 29 ° 98 | "<br>h 30°78<br>k 30°70<br>k 30°02                  | "                                                             | "<br>l 32.62<br>l 29.96<br>l 31.88<br>l 29.86 | "<br>2 31 · 58<br>2 31 · 56<br>2 31 · 62 | $M = 31'' \cdot 16$<br>$w = 16 \cdot 52$<br>$\frac{1}{w} = 0 \cdot 06$<br>$C = 51^{\circ} 58' \cdot 21'' \cdot 15$ |  |  |
|                                                                                    | 31.07                                                                                                                      | 31.30                                                                                  | 30°54                                             | 32.70                                                          | 30.94                                               | 30.62                                                 | 30.20                                               | 31.35                                                         | 31.08                                         | 31.29                                    | 0 - 51 50 51 75                                                                                                    |  |  |
| XXXIX &<br>XLIII                                                                   | h 28°94<br>h 29°42<br>h 29°48<br>d 29°79                                                                                   | k 29°50<br>k 28°72<br>k 28°44                                                          | h 31 · 12<br>h 29 · 88<br>l 29 · 40               | l 28.04<br>l 29.76<br>l 30.18<br>l 28.92                       | h 27.66<br>h 31.04<br>h 29.30<br>h 29.94<br>h 29.90 | h 29°18<br>h 28°30<br>h 28°18                         | h 27°40<br>h 30°60<br>h 29°00<br>h 29°28<br>h 28°62 | k 32°52<br>k 30°34<br>k 29°38<br>k 30°80<br>k 31°66           | l 28.98<br>l 29.08<br>l 29.28                 | l 30°10<br>l 30°64<br>l 29°82            | $M = 29^{"} \cdot 50$ $w = 14 \cdot 41$ $\frac{1}{m} = 0 \cdot 07$                                                 |  |  |
|                                                                                    | <b>2</b> 9°41                                                                                                              | 28.89                                                                                  | 30.13                                             | 29.23                                                          | <b>2</b> 9°57                                       | 28.55                                                 | <b>28</b> •98                                       | <b>30°9</b> 4                                                 | 29.11                                         | 30.19                                    | $C = 52^{\circ} 24' 29'' \cdot 51$                                                                                 |  |  |
| XLIII &<br>XLV                                                                     | k 57°74<br>k 58°94<br>k 58°36<br>k 60°56                                                                                   | <b>Å</b> 60°18<br><b>Å</b> 57°12<br><b>Å</b> 58°34<br><b>Å</b> 58°56<br><b>Å</b> 57°96 | k 55°44<br>k 57°62<br>l 58°18<br>l 57°52          | l 60°52<br>l 57°10<br>l 59°48<br>l 58°74<br>l 58°30            | h 56°94<br>h 58°12<br>h 59°20<br>h 58°46            | k 59°28<br>k 58°26<br>k 59°44                         | k 58°54<br>k 58°74<br>k 59°04                       | h 57°74<br>h 58°50<br>h 59°46                                 | l 59°66<br>l 59°02<br>l 58°40                 | 2 59°78<br>2 59°96<br>2 59°42            | $M = 58'' \cdot 66$ $w = 15 \cdot 57$ $\frac{1}{w} = 0 \cdot 06$                                                   |  |  |
|                                                                                    | 58.90                                                                                                                      | 58.43                                                                                  | 57.19                                             | 58.83                                                          | 58.18                                               | 58.99                                                 | 58.77                                               | 58.57                                                         | 59.03                                         | 59.72                                    | $C = 61^{\circ} 46' 58'' \cdot 64$                                                                                 |  |  |
| XLV &<br>XLVII                                                                     | <b>1</b> 49°52<br><b>1</b> 52°58<br><b>1</b> 50°26<br><b>1</b> 47°12<br><b>1</b> 49°88<br><b>1</b> 47°80<br><b>1</b> 47°88 | <b>k</b> 49°30<br>k 51°26<br><b>k</b> 50°68                                            | h 50° 48<br>h 50° 46<br>l 48° 88                  | l 47°48<br>l 51°02<br>l 46°84<br>h 50°20<br>h 49°34<br>h 51°42 | h 50°86<br>h 48°44<br>h 49°46<br>h 48°70            | h 50°66<br>h 49°84<br>h 50°72                         | k 50°94<br>h 50°60<br>k 49°94                       | h 48°98<br>h 49°36<br>h 49°52                                 | 2 48*08<br>2 48*68<br>2 49*78                 | l 48°06<br>l 48°50<br>l 48°62            | $\dot{M} = 49'' \cdot 58$<br>$w = 11 \cdot 47$<br>$\frac{1}{w} = 0 \cdot 09$<br>$G = 42^{\circ} 28' 40'' \cdot 56$ |  |  |
|                                                                                    | 49.29                                                                                                                      | 50.41                                                                                  | 49'94                                             | 49.38                                                          | 49`37                                               | 50.41                                                 | 50°49                                               | 49.29                                                         | 48.85                                         | 48.39                                    | 0 — 44 30 49 50                                                                                                    |  |  |

Nore.---R. M. denotes Referring Mark.

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At XLV (Bhada)

February and March 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle<br>between |                                                             |                                    | Çire                                     | ele reading                              | s, telesco                                                    | pe being a                               | set on XL                           | VII                                                                        |                                                       |                                          | M = Mean of Groups<br>w = Relative Weight                                                                              |
|------------------|-------------------------------------------------------------|------------------------------------|------------------------------------------|------------------------------------------|---------------------------------------------------------------|------------------------------------------|-------------------------------------|----------------------------------------------------------------------------|-------------------------------------------------------|------------------------------------------|------------------------------------------------------------------------------------------------------------------------|
|                  | 0° 0′                                                       | 180° 0′                            | 79° 12′                                  | 259°12′                                  | 158° 24′                                                      | 838° 24′                                 | 237° 37′                            | 57° 37′                                                                    | 816° 49′                                              | 136° 49′                                 | C = Concluded Angle                                                                                                    |
| XLVII &<br>XLIV  | n<br>h 51°40<br>h 52°50<br>h 53°86<br>h 54°78<br>h 53°24    | "<br>h 52°06<br>h 53°54<br>h 52°42 | "<br>l 52.88<br>l 52.34<br>l 52.12       | "<br>1 53 • 26<br>1 54 • 08<br>1 52 • 98 | "<br>h 53°48<br>h 50°84<br>h 50°98<br>h 51°08                 | "<br>h 52°36<br>h 52°00<br>h 53°74       | "<br>h 52°08<br>h 52°64<br>h 52°90  | "<br>1 54 · 72<br>h 53 · 96<br>h 52 · 64<br>h 52 · 02                      | "<br>h 53 · 42<br>h 51 · 42<br>h 51 · 66<br>h 52 · 84 | h 55°20<br>h 55°24<br>h 53°24<br>h 53°08 | $M = 52'' \cdot 84$ $w = 13 \cdot 74$ $\frac{1}{w} = 0 \cdot 67$ $C = 58^{\circ} 6' \cdot 50'' \cdot 85$               |
|                  | 53.10                                                       | 52.67                              | 52.42                                    | 53.44                                    | 51.60                                                         | 52.70                                    | 52°54                               | 53 33                                                                      | 52.34                                                 | 54.19                                    | C = 78  0  52  85                                                                                                      |
| XLIV &<br>XLIII  | k 58·50<br>k 59·66<br>k 59·00                               | h 58 86<br>h 58 92<br>h 58 64      | l 58°74<br>l 59°48<br>l 57°82            | l 57·92<br>l 58·28<br>l 59·54            | h 58 · 38<br>h 61 · 00<br>h 58 · 98<br>h 58 · 96<br>h 58 · 92 | h 58°92<br>h 59°48<br>h 58°90            | h 59°62<br>h 60°02<br>h 59°14       | h 57°92<br>h 59°26<br>h 58°82                                              | h 59°42<br>h 60°38<br>h 59°56                         | h 59°64<br>h 59°98<br>h 59°50            | $M = 59^{*} \cdot 12$ $w = 32 \cdot 92$ $\frac{1}{w} = 0 \cdot 03$                                                     |
|                  | 59.02                                                       | 58.81                              | 58.68                                    | 58.28                                    | 59.25                                                         | 59°10                                    | 59.29                               | 58.67                                                                      | 59°79                                                 | 59.71                                    | $\tilde{C} = 62^{\circ} 7' 59^{*} \cdot 12$                                                                            |
| XLIII &<br>XLVI  | h 5°08<br>h 6°60<br>h 5°08                                  | h 5°44<br>h 5°54<br>h 5°12         | 2 5°12<br>2 5°60<br>2 5°54               | 2 5·46<br>2 5·34<br>2 4·72               | h 4.78<br>h 5.20<br>h 5.40                                    | h 5°94<br>h 5°46<br>h 5°28               | h 5°28<br>h 5°56<br>h 5°42          | h 4°24<br>h 5°94<br>h 4°80                                                 | h 5.52<br>h 6.28<br>h 5.02                            | h 5.66<br>h 4.54<br>h 5.50               | $M = 5'' \cdot 35$ $w = 100 \cdot 25$ $\frac{1}{2} = 0 \cdot 01$                                                       |
|                  | 5*59                                                        | 5.37                               | 5.42                                     | 5.12                                     | 5.13                                                          | 5.20                                     | 5.43                                | 4 99                                                                       | 2.91                                                  | 5.33                                     | $C = 57^{\circ} 7' 5'' 35$                                                                                             |
| XLVI &<br>XLVIII | ћ 59°20<br>ћ 57°48<br>ћ 57°84                               | h 58.60<br>h 57.80<br>h 57.98      | l 57.80<br>l 56.78<br>l 59.00<br>l 56.90 | 2 57 90<br>2 57 70<br>2 57 50            | h 57 · 52<br>h 56 · 94<br>h 58 · 28                           | h 56 · 82<br>h 57 · 78<br>h 57 · 34      | h 57 · 48<br>h 55 · 98<br>h 57 · 84 | h 57°60<br>h 57°18<br>h 57°20                                              | h 56 82<br>h 56 06<br>h 57 40                         | h 57 ° 20<br>h 55 ° 62<br>h 57 ° 88      | $M = 57'' \cdot 46$<br>$w = 28 \cdot 15$<br>$\frac{1}{2} = 0 \cdot 04$                                                 |
|                  | 58.17                                                       | 58.13                              | 57.62                                    | 57.70                                    | 57.58                                                         | 57.31                                    | 57.10                               | 57.33                                                                      | 56.26                                                 | 56.90                                    | $C = 43^{\circ} 59' 57'' \cdot 46$                                                                                     |
| XLVIII &<br>XLIX | k 12.65<br>k 8.54<br>k 10.02<br>k 9.48<br>7 9.90<br>l 10.02 | h 10°74<br>h 10°66<br>h 11°10      | l 10°22<br>l 10°94<br>l 9°58             | l 10°38<br>l 9°32<br>l 9°28              | h 11.40<br>h 11.54<br>h 11.16                                 | k 8.80<br>k 10.92<br>k 10.82             | k 10.40<br>k 8.94<br>k 10.10        | h 9.80<br>h 11.38<br>h 9.66                                                | h 10°38<br>h 10°96<br>h 10°02                         | k 9°20<br>k 9°60<br>k 10°44              | $M = 10'' \cdot 27$ $w = 22 \cdot 58$ $\frac{1}{w} = 0 \cdot 04$                                                       |
|                  | 10,10                                                       | 10.83                              | 10.52                                    | <b>9.</b> 66                             | 11.37                                                         | 10.12                                    | 9.81                                | 10.38                                                                      | 10.42                                                 | 9.75                                     | $U = 00^{-}54 \ 10^{-}20$                                                                                              |
| XLIX &<br>XLVII  | k 49°76<br>k 53°80<br>k 53°78<br>k 51°64<br>l 51°94         | k 54°30<br>k 53°86<br>k 53°58      | l 53·52<br>l 52·42<br>l 54·04            | 2 53 86<br>2 53 00<br>2 53 12<br>2 51 64 | h 53°42<br>h 50°68<br>h 53°56<br>h 51°16                      | h 53°48<br>h 52°56<br>h 55°24<br>h 53°54 | h 54 ° 46<br>h 54 ° 56<br>h 53 ° 08 | h 55 · 56<br>h 52 · 36<br>h 55 · 94<br>h 56 · 74<br>h 55 · 52<br>h 52 · 16 | h 55°52<br>h 54°30<br>h 55°16                         | h 54°30<br>h 52°92<br>h 54°72            | $M = 53'' \cdot 59$ $w = 7 \cdot 93$ $\frac{1}{w} = 0 \cdot 13$ $C = 78^{\circ} c c c c c c c c c c c c c c c c c c c$ |
|                  | 52.18                                                       | 53.91                              | 53.33                                    | 52.91                                    | 52.30                                                         | 53.71                                    | 54.03                               | 54.21                                                                      | 54°99                                                 | 53.98                                    | $C = 57^{\circ} 43^{\circ} 53^{\circ} 58^{\circ}$                                                                      |

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# At XLVI (Habib)

February 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle<br>between | 0° 1′                                                                           | 180° 0′                                  | Circ.<br>79° 18′                   | le reading<br>259°13′                               | s, telescop<br>158°25'                   | e being so<br>838° 25'             | et on XL<br>237° 36'                     | VIII<br>57°36'                     | 816° 49′                           | 136° 48′                           | M = Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle                                         |
|------------------|---------------------------------------------------------------------------------|------------------------------------------|------------------------------------|-----------------------------------------------------|------------------------------------------|------------------------------------|------------------------------------------|------------------------------------|------------------------------------|------------------------------------|----------------------------------------------------------------------------------------------------------|
| XLVIII &<br>XLV  | "<br>h 31 · 34<br>h 26 · 62<br>h 30 · 90<br>h 30 · 42<br>h 29 · 08<br>h 31 · 10 | "<br>h 27 ° 74<br>h 28 ° 68<br>h 27 ° 64 | "<br>h 27.64<br>h 26.78<br>h 27.82 | "<br>h 27`64<br>h 28`72<br>h 26`96                  | "<br>l 28·72<br>l 28·58<br>l 28·88       | "<br>1 28.42<br>1 26.52<br>1 27.60 | "<br>l 28·32<br>l 29·96<br>l 29·34       | "<br>  29`10<br>  30`74<br>  29`92 | "<br>l 26·28<br>l 27·34<br>l 27·08 | "<br>h 29°42<br>h 28°78<br>h 27°94 | $M = 28'' \cdot 41$ $w = 7 \cdot 38$ $\frac{1}{w} = 0 \cdot 14$ $C = 61^{\circ} 41' \cdot 28'' \cdot 43$ |
| <b>f</b>         | 29.91                                                                           | 28.02                                    | 27.41                              | 27.77                                               | 28.73                                    | 27.21                              | 29.31                                    | 29.92                              | 26.90                              | 28.71                              |                                                                                                          |
| XLV &<br>XLIII   | k 56°98<br>k 56°62<br>k 56°44                                                   | h 56.84<br>h 57.14<br>h 57.50            | h 56°30<br>h 58°28<br>h 56°68      | h 57°94<br>h 55°72<br>h 56°80<br>h 57°28<br>h 56°48 | l 55°94<br>l 58°06<br>l 56°72<br>l 59°52 | 2 56·88<br>2 56·18<br>2 57·12      | l 58.04<br>l 55.90<br>l 56.74<br>l 56.74 | l 57 96<br>l 57 38<br>l 58 02      | 2 58 88.<br>2 57 98<br>2 59 14     | h 58°90<br>h 58°44<br>h 58°42      | $M = 57'' \cdot 40$ $w = 14 \cdot 21$ $\frac{1}{w} = 0 \cdot 07$                                         |
|                  | 56.68                                                                           | 57.16                                    | 57.09                              | 56.84                                               | 57.26                                    | 56.73                              | 56.86                                    | 57.79                              | 58.67                              | 58.29                              | $\tilde{C} = 76^{\circ} 9' 57'' \cdot 39$                                                                |

#### At XLVII (Karamala)

March 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle         |                                               |                                    |                                    | M - Mean of Groups                 |                                       |                                    |                                                                     |                                    |                                     |                                     |                                                                                                              |
|---------------|-----------------------------------------------|------------------------------------|------------------------------------|------------------------------------|---------------------------------------|------------------------------------|---------------------------------------------------------------------|------------------------------------|-------------------------------------|-------------------------------------|--------------------------------------------------------------------------------------------------------------|
| between       | <b>22</b> 6° 18′                              | <b>46° 18'</b>                     | 805° 31′                           | 125° 31′                           | 24° 42′                               | <b>2</b> 04° 42′                   | 103°54′                                                             | 283° 54′                           | 183° 6′                             | 3° 6′                               | C = Concluded Angle                                                                                          |
| XLIV &<br>XLV | "<br>k 20`84<br>k 19`44<br>k 18`70<br>k 19`36 | "<br>h 20°02<br>h 18°06<br>h 18°78 | "<br>k 18·90<br>k 18·64<br>k 19·24 | "<br>h 18·64<br>h 17·94<br>h 18·22 | "<br>h 17 •98<br>h 18 •46<br>h 18 •96 | "<br>h 17°78<br>h 17°52<br>h 18°06 | "<br>l 18.74<br>h 18.96<br>h 19.20<br>h 18.46<br>l 17.48<br>l 16.70 | "<br>h 19°60<br>h 19°22<br>h 19°26 | "<br>h 18*80<br>h 20*16<br>h 18*52  | "<br>k 18°74<br>k 19°58<br>k 20°28  | $M = 18'' \cdot 83$<br>$w = 20 \cdot 40$<br>$\frac{1}{w} = 0 \cdot 05$<br>$C = 50^{\circ} 14' 18'' \cdot 83$ |
|               | 19.29                                         | 18.02                              | 18.93                              | 18.22                              | 18.47                                 | 17.79                              | 18.32                                                               | 19.36                              | 19.10                               | 19.23                               | 0 - 39 - 7 - 0 3                                                                                             |
| XLV &<br>XLIX | k 36·32<br>k 37·96<br>k 38·76<br>k 36·12      | h 35°20<br>h 35°36<br>h 36°26      | k 36°50<br>k 37°20<br>k 36°16      | h 35 °74<br>h 37 ° 20<br>h 36 °74  | k'35°72<br>k 36°24<br>k 36°50         | h 35 86<br>l 35 22<br>l 36 72      | l 36.86<br>l 34.00<br>h 33.98<br>h 35.00<br>h 35.88                 | h 35 98<br>h 35 62<br>h 35 82      | h 36 • 40<br>h 35 • 82<br>h 35 • 44 | h 36 · 68<br>h 35 · 58<br>h 36 · 32 | $M = 36'' \cdot 12$ $w = 19 \cdot 33$ $\frac{1}{w} = 0 \cdot 05$                                             |
|               | 37.29                                         | 32.01                              | 36.63                              | 36.20                              | 36.12                                 | 35 93                              | 35.14                                                               | 35.81                              | 35.89                               | 36.19                               | $\tilde{C} = 74^{\circ} 27' 36'' \cdot 12$                                                                   |

| At XLVIII (Phogala)<br>February 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2. |                                                       |                                                                                                                                             |                                               |                                                                                                                                                             |                                                                                   |                                                                                |                                                   |                                        |                                                                    |                                                |                                                                                                             |  |  |
|-----------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------|--------------------------------------------------------------------------------|---------------------------------------------------|----------------------------------------|--------------------------------------------------------------------|------------------------------------------------|-------------------------------------------------------------------------------------------------------------|--|--|
| Angle<br>between                                                                                                      | y 1873;<br>0°1'                                       | 180°1'                                                                                                                                      | Ci<br>79° 18'                                 | rcle readi<br>259° 13'                                                                                                                                      | ngs, teles<br>158° 25'                                                            | cope bein<br>338° 25'                                                          | g set on<br>237° 37'                              | и Батто<br><br>LI<br>57° 37′           | 816°49'                                                            | 136° 48'                                       | M = Mean of Groups $w = Relative Weight$ $C = Concluded Angle$                                              |  |  |
| LI & L                                                                                                                | "<br>h 39 · 20<br>h 37 · 68<br>h 36 · 70<br>h 38 · 26 | "<br>h 35 * 20<br>h 34 * 88<br>h 34 * 44<br>l 35 * 60                                                                                       | "<br>1 34 °00<br>1 34 °98<br>1 35 °30         | "<br>1 35.50<br>1 36.66<br>1 35.44                                                                                                                          | "<br><b>k</b> 33 ° 36<br><b>h</b> 34 ° 16<br><b>h</b> 35 ° 50<br><b>k</b> 35 ° 14 | "<br>h 37°54<br>h 35°44<br>h 34°18<br>h 32°02<br>h 35°28<br>h 35°28<br>h 34°44 | "<br>h 36 ° 78<br>h 35 ° 94<br>h 35 ° 50          | "<br>h 36`18<br>h 36`90<br>h 36`32     | "<br>h 34 · 12<br>l 36 · 34<br>l 33 · 32<br>l 35 · 42<br>l 34 · 36 | "<br>2 36 · 02<br>2 36 · 44<br>2 35 · 88       | $M = 35'' \cdot 63$<br>$w = 7 \cdot 14$<br>$\frac{1}{w} = 0 \cdot 14$<br>$C = 72^{\circ} 28' 35'' \cdot 62$ |  |  |
| L & XLIX                                                                                                              | 37 ° 96                                               | 35°03<br>h 51°18<br>h 48°66<br>h 48°40<br>l 49°12<br>l 50°06                                                                                | 34.76<br>249.84<br>249.34<br>247.52<br>249.34 | 35 <sup>.87</sup><br><sup>1</sup> 47 <sup>.</sup> 42<br><sup>1</sup> 44 <sup>.</sup> 92<br><sup>1</sup> 47 <sup>.60</sup><br><sup>1</sup> 46 <sup>.80</sup> | 34°54<br>h 47°64<br>h 46°98<br>h 45°54<br>h 47°28                                 | 34 * 82<br>h 47 * 12<br>h 48 * 16<br>h 45 * 88<br>h 48 * 00                    | 36.07<br>h 48.06<br>h 48.16<br>h 45.98<br>h 46.96 | 36.47<br>h 47.58<br>h 45.70<br>h 47.00 | 34 ° 71<br>h 47 ° 24<br>l 47 ° 26<br>l 47 ° 38<br>l 46 ° 26        | 36 · 11<br>2 46 · 16<br>2 47 · 32<br>2 46 · 32 | $M = 47'' \cdot 58$ $w = 7 \cdot 17$ $u = -0 \cdot 14$                                                      |  |  |
|                                                                                                                       | 48.84                                                 | 49.48                                                                                                                                       | 49.01                                         | 46.68                                                                                                                                                       | 46.86                                                                             | 47°29                                                                          | 47 . 29                                           | 46.76                                  | 47.04                                                              | 46.60                                          | $\frac{1}{w} = 53^{\circ} 14^{\circ}$ $C = 53^{\circ} 12' 47'' \cdot 59$                                    |  |  |
| XLIX & XLV                                                                                                            | h 7.12<br>h 9.40<br>h 8.14<br>h 6.80                  | h       5.08         h       6.34         h       8.66         l       9.18         l       5.76         l       10.70         l       5.44 | 2 8.08<br>2 7.46<br>2 9.04                    | l 8.94<br>l 9.18<br>l 8.54                                                                                                                                  | h 7.68<br>h 8.48<br>h 6.94<br>h 7.88                                              | k 9°26<br>k 7°66<br>k 7°82                                                     | k 9°10<br>k 8°24<br>k 8°04<br>l 9°88              | h 7°22<br>h 7°34<br>h 7°28             | k 8.96<br>l 7.46<br>l 9.48<br>l 8.36                               | 2 9°14<br>2 8°08<br>2 9°32                     | $M = 8'' \cdot 18$ $w = 14 \cdot 66$ $\frac{1}{w} = 0 \cdot 07$ $C = 58^{\circ} 88' \cdot 8'' \cdot 58$     |  |  |
|                                                                                                                       | 7.87                                                  | 7.31                                                                                                                                        | 8.19                                          | 8.89                                                                                                                                                        | 7.74                                                                              | 8.25                                                                           | 8.82                                              | 7 . 28                                 | 8.26                                                               | 8.85                                           | C = 75 30 0 15                                                                                              |  |  |
| XLV & XLVI                                                                                                            | h 34 · 14<br>h 31 · 74<br>h 33 · 84<br>h 34 · 48      | <b>k</b> 36 · 28<br><i>k</i> 36 · 64<br><i>k</i> 34 · 12<br><i>l</i> 33 · 02<br><i>l</i> 35 · 32                                            | l 33°34<br>l 35°00<br>l 34°26                 | 2 36 98<br>2 35 54<br>2 38 38<br>2 35 72                                                                                                                    | h 34°82<br>h 34°40<br>h 36°62<br>h 34°22                                          | h 32 ° 96<br>h 34 ° 40<br>h 35 ° 42<br>h 35 ° 26                               | h 34 °66<br>l 34 °42<br>l 35 °70                  | h 34 · 58<br>h 35 · 40<br>h 35 · 12    | h 36 · 16<br>l 33 · 76<br>l 34 · 84<br>l 35 · 66                   | 2 35 86<br>2 35 50<br>2 35 48                  | $M = 34'' \cdot 97$ $w = 10 \cdot 76$ $\frac{1}{m} = 0 \cdot 09$                                            |  |  |
|                                                                                                                       | 33.22                                                 | 35.08                                                                                                                                       | 34°20                                         | 36.66                                                                                                                                                       | 32.01                                                                             | 34.21                                                                          | 34.93                                             | 35.03                                  | 35.11                                                              | 32.01                                          | $\tilde{C} = 74^{\circ} 18' 34'' \cdot 97$                                                                  |  |  |

At XLIX (Bhulan)

March 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle                                                      |                                    | Circle readings, telescope being set on XLVII            |                                                |                                    |                               |                                    |                                    |                                    |                                          |                                          |                                                                  |  |  |  |  |
|------------------------------------------------------------|------------------------------------|----------------------------------------------------------|------------------------------------------------|------------------------------------|-------------------------------|------------------------------------|------------------------------------|------------------------------------|------------------------------------------|------------------------------------------|------------------------------------------------------------------|--|--|--|--|
| Angle<br>between 0°<br>XLVII & h 32°<br>XLV h 32°<br>h 32° | 0° 1′                              | 180° 1′                                                  | <b>79°</b> 12′                                 | <b>25</b> 9° 13′                   | 158° 25′                      | 83,8° 24'                          | <b>237° 3</b> 6′                   | 57° 86′                            | <b>8</b> 16° 49′                         | 186° 48′                                 | C = Concluded Angle                                              |  |  |  |  |
| XLVII &<br>XLV                                             | "<br>h 32°74<br>h 32°34<br>k 32°94 | "<br>h 29°20<br>h 30°06<br>h 29°96<br>h 31°28<br>h 30°92 | ".<br>h 29°36<br>l 31°22<br>l 30°74<br>l 28°86 | "<br>l 32`34<br>l 32`28<br>l 32`06 | 2 30°50<br>2 31°74<br>2 30°42 | "<br>  32.68<br>  31.20<br>  32.02 | "<br>h 32°54<br>h 32°22<br>h 30°92 | "<br>h 30°78<br>h 30°36<br>h 30°34 | l 29°92<br>h 32°24<br>h 30°92<br>h 31°18 | "<br>h 31 · 34<br>h 31 · 96<br>h 31 · 48 | $M = 31'' \cdot 31$ $w = 10 \cdot 95$ $\frac{1}{w} = 0 \cdot 09$ |  |  |  |  |
|                                                            | 32.67                              | 30.28                                                    | 30.02                                          | 32.23                              | 30.89                         | 31.97                              | 31.89                              | <b>3</b> 0°49                      | 31.06                                    | <b>3</b> 1°59                            | $C = 47^{\circ} 48' 31''' 30$                                    |  |  |  |  |

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|                  |                                                       |                                                               |                                          | At XL                                               | IX (Bh                             | ulan)—                                | (Contin                                  | ued).                                    |                                             |                                          |                                                                  |
|------------------|-------------------------------------------------------|---------------------------------------------------------------|------------------------------------------|-----------------------------------------------------|------------------------------------|---------------------------------------|------------------------------------------|------------------------------------------|---------------------------------------------|------------------------------------------|------------------------------------------------------------------|
| Angle<br>between | 0° 1′                                                 | 180° 1′                                                       | Circ<br>79° 12′                          | ele reading<br>259° 13'                             | s, telesco<br>158° 25'             | pe being s<br>338° 24'                | et on XL<br>237° 36′                     | VII<br>57° 36'                           | 316° 49′                                    | 136° 48′                                 | M = Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle |
| XLV &<br>XLVIII  | "<br>h 43 ° 00<br>h 42 ° 84<br>h 42 ° 98<br>d 43 ° 22 | "<br><b>h</b> 44 · 22<br><b>h</b> 44 · 42<br><b>h</b> 45 · 88 | "<br>2 43 • 46<br>2 44 • 16<br>2 42 • 50 | "<br>l 43`54<br>l 42`94<br>l 43`76                  | "<br>  44`20<br>  43`78<br>  43`84 | "<br>l 42 °90<br>l 43 °04<br>l 43 °78 | "<br>h 42 ° 36<br>h 42 ° 74<br>h 42 ° 52 | k 44 · 16<br>k 43 · 10<br>k 42 · 88      | "<br>\$ 43 * 84<br>\$ 43 * 48<br>\$ 43 * 94 | "<br>h 42 · 86<br>k 43 · 90<br>h 43 · 42 | $M = 43'' \cdot 49$ $w = 23 \cdot 35$ $\frac{1}{w} = 0 \cdot 04$ |
|                  | 43 ° 01                                               | 44.84                                                         | 43 37                                    | 43'41                                               | 43 94                              | 43 . 24                               | 42.24                                    | 43 * 38                                  | <del>4</del> 3°75                           | 43 . 39                                  | $C = 43^{\circ} 27' 43''' 49$                                    |
| XLVIII & L       | k 26°26<br>k 25°82<br>k 25°32<br>k 23°86<br>d 25°60   | h 23 · 56<br>h 24 · 90<br>h 24 · 14                           | l 25.80<br>l 23.90<br>l 24.30            | l 23.16<br>l 23.88<br>l 24.34<br>l 25.42<br>l 24.42 | l 24°48<br>l 23°92<br>l 25°34      | l 24°16<br>l 25°02<br>l 25°30         | h 25 · 82<br>h 26 · 30<br>h 26 · 54      | h 25°52<br>h 27°80<br>l 26°04<br>l 25°58 | l 25°66<br>l 23°62<br>h 25°52<br>h 27°18    | h 26°06<br>h 25°68<br>h 25°72            | $M = 25'' \cdot 17$ $w = 13 \cdot 14$ $\frac{1}{w} = 0 \cdot 08$ |
|                  | 25.37                                                 | 24.30                                                         | 24.67                                    | 24.24                                               | 24.58                              | 24.83                                 | 26.33                                    | 26.34                                    | 25.49                                       | 25.82                                    | $C = 54^{\circ} 14' 25'' \cdot 17$                               |
| L & LII          | h 58.66<br>h 58.94<br>h 60.60                         | h 61 °00<br>h 57 °72<br>h 59 °02<br>h 58 °84<br>h 59 °06      | l 58·42<br>l 56·68<br>l 58·46            | 2 58.70<br>2 57.72<br>2 55.76<br>2 57.04            | h 58.62<br>h 58.36<br>h 59.18      | h 58°28<br>h 57°80<br>h 58°24         | h 58°24<br>h 58°96<br>h 58°74            | h 58°02<br>h 57°98<br>l 59°18            | l 56.26<br>l 56.70<br>h 57.98<br>h 58.72    | h 58 · 76<br>h 56 · 90<br>h 58 · 50      | $M = 58'' \cdot 30$ $w = 14 \cdot 73$ $\frac{1}{w} = 0 \cdot 07$ |
|                  | 59°40                                                 | 59.13                                                         | 57.85                                    | 57.31                                               | 58.72                              | 58.11                                 | 58.02                                    | 58.39                                    | 57.41                                       | 58.02                                    | $\tilde{C} = 52^{\circ} 24' 58'' \cdot 30$                       |

At L (Soma)

March 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle<br>between | ው ው                                                                                              | 180° 0′                                  | Ci:<br>79° 13′                           | rcle readin<br>259°12'             | ngs, teles<br>158°24'              | cope being<br>338°23'                    | g set on ]<br>237°36'               | LII<br>57° 36'                     | 816° 48′                           | 136° 48′                           | M = Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle                                    |
|------------------|--------------------------------------------------------------------------------------------------|------------------------------------------|------------------------------------------|------------------------------------|------------------------------------|------------------------------------------|-------------------------------------|------------------------------------|------------------------------------|------------------------------------|-----------------------------------------------------------------------------------------------------|
| LII & XLIX       | <i>k</i> 53 · 18<br><i>k</i> 53 · 60<br><i>k</i> 53 · 56<br><i>l</i> 55 · 64<br><i>k</i> 52 · 72 | "<br>h 51°64<br>h 52°98<br>h 51°74       | *<br>h 53 · 26<br>h 54 · 58<br>l 52 · 68 | "<br>1 53 36<br>1 53 20<br>1 51 70 | "<br>  53.62<br>  53.38<br>  54.28 | "<br>h 51 ° 74<br>h 51 ° 60<br>h 52 ° 68 | "<br>h 53°42<br>l 52°46<br>l 52°72  | "<br>l 52°04<br>l 52°42<br>l 52°90 | "<br>l 52°00<br>l 51°60<br>h 52°80 | "<br>h 52°58<br>h 52°40<br>h 52°70 | $M = 52^* \cdot 79$ $w = 17 \cdot 37$ $\frac{1}{w} = 0 \cdot 06$ $C = 43^{\circ} 28' 52'' \cdot 80$ |
|                  | 53.74                                                                                            | 52.13                                    | 53.21                                    | 52.25                              | 53.20                              | 52.01                                    | 52.87                               | 52.42                              | 52.13                              | 52.26                              | 0 — 4 <u>5</u> 20 <u>5</u> 00                                                                       |
| XLIX &<br>XLVIII | k 48 • 46<br>k 49 • 22<br>l 49 • 08<br>k 46 • 70<br>k 48 • 52                                    | h 48°94<br>h 50°16<br>h 48'70<br>h 47'68 | h 49°52<br>l 48°88<br>l 47°26<br>l 49°42 | l 48°36<br>l 47°92<br>l 47°90      | l 49°76<br>l 49°90<br>l 50°26      | ћ 47 °96<br>ћ 49 °88<br>ћ 48 °78         | k 48 · 72<br>l 49 · 26<br>l 50 · 54 | l 48.84<br>l 49.18<br>l 48.50      | l 49°56<br>l 50°18<br>h 48°68      | h 48°64<br>h 49°74<br>h 48°50      | $M = 48'' \cdot 97$ $w = 21 \cdot 60$ $\frac{1}{w} = 0 \cdot 05$                                    |
|                  | 48.40                                                                                            | 48.87                                    | 48.77                                    | 48.06                              | <del>4</del> 9 <sup>.</sup> 97     | 48.87                                    | 49.21                               | 48.84                              | 49`47                              | 48.96                              | $\tilde{C} = 72^{\circ} 32' 48'' \cdot 96$                                                          |

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|                | At L (Soma)—(Continued).                                                                                                                 |                                          |                                                                     |                                                     |                                                                    |                                                   |                                                      |                                               |                                             |                                                                                 |                                                                                                              |  |  |  |
|----------------|------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------|---------------------------------------------------------------------|-----------------------------------------------------|--------------------------------------------------------------------|---------------------------------------------------|------------------------------------------------------|-----------------------------------------------|---------------------------------------------|---------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------|--|--|--|
| Angle          |                                                                                                                                          |                                          | C                                                                   | ircle readi                                         | ngs, teles                                                         | cope bein                                         | g set on I                                           | л                                             |                                             |                                                                                 | M - Mean of Groups                                                                                           |  |  |  |
| between        | 0° 0′                                                                                                                                    | 180° 0′                                  | 79° 13′                                                             | <b>259° 12′</b> `                                   | 158° 24′                                                           | 838° 23'                                          | 237° 36′                                             | <b>57° 86′</b>                                | <b>316° 48</b> ′                            | 136° 48′                                                                        | w = Relative Weight<br>C = Concluded Angle                                                                   |  |  |  |
| XLVIII &<br>LI | n<br>h 55°98<br>l 57°06<br>h 57°38<br>h 55°94<br>d 54°03                                                                                 | *                                        | "<br>1 55 96<br>1 59 24<br>1 56 30<br>1 58 40<br>1 54 24<br>2 57 78 | "<br>1 55 °90<br>1 56 °86<br>1 55 °82               | "<br>l 55 · 18<br>l 54 · 90<br>l 54 · 18<br>h 57 · 38<br>h 55 · 08 | "<br>\$ 56°02<br>\$ 58°18<br>\$ 55°60<br>\$ 56°34 | "<br>k 53 *88<br>l 56 * 30<br>l 55 * 40<br>l 54 * 66 | *<br>1 53 74<br>1 55 52<br>1 53 96<br>* 55 44 | "<br>1 54 • 86<br>1 55 • 34<br>1 56 • 50    | "<br>h 54 · 14<br>h 58 · 36<br>h 55 · 26<br>h 55 · 64<br>h 58 · 20<br>h 56 · 42 | $M = 56'' \cdot 00$ $w = 9 \cdot 74$ $\frac{1}{w} = 0 \cdot 10$ $C = 53^{\circ} 42' \cdot 56'' \cdot 01$     |  |  |  |
|                | 56.08                                                                                                                                    | 57:26                                    | 56 <b>.99</b>                                                       | 56.19                                               | 55-34                                                              | 56.23                                             | 55.00                                                | 54.67                                         | 55-57                                       | 56.34                                                                           | 0 = 33 44 30 01                                                                                              |  |  |  |
| LI & LIII      | h 19°84<br>l 18°66<br>l 18°66<br>h 18°92<br>d 16°88                                                                                      | k 17.62<br>k 16.94<br>k 19.26<br>k 17.92 | 2 18.56<br>2 15.06<br>2 15.94<br>2 18.44<br>2 16.58                 | l 18·28<br>l 18·22<br>l 18·24                       | l 16°90<br>l 17°26<br>l 16°82<br>l 16°60                           | k 17°60<br>k 17°20<br>k 17°30                     | k 18.66<br>l 17.32<br>l 18.42<br>l 18.38             | l 16.82<br>l 19.02<br>l 18.08<br>l 16.70      | l 17°54<br>k 18°90<br>k 16°38<br>k 17°76    | k 18.00<br>k 15.64<br>k 17.68<br>k 16.24                                        | $M = 17'' \cdot 63$ $w = 17 \cdot 58$ $\frac{1}{m} = 0 \cdot 06$                                             |  |  |  |
|                | 18.29                                                                                                                                    | 37.94                                    | 16.73                                                               | 18.22                                               | 16.80                                                              | 17.37                                             | 18.30                                                | 17.65                                         | 17.65                                       | 16.89                                                                           | $\tilde{C} = 42^{\circ} 10' 17'' \cdot 63$                                                                   |  |  |  |
| LIII & LIV     | <b>h</b> 10 · 18<br><i>l</i> 15 · 20<br><i>l</i> 16 · 06<br><b>h</b> 13 · 44<br><i>h</i> 13 · 20<br><i>h</i> 12 · 76<br><b>h</b> 12 · 76 | k 14.86<br>k 14.16<br>k 12.16<br>k 12.36 | l 11 98<br>l 14 98<br>l 12 62<br>l 15 70<br>l 14 40                 | l 15.56<br>l 15.54<br>l 15.04<br>h 13.38<br>h 12.78 | l 14.84<br>l 15.36<br>l 15.42<br>h 13.78<br>h 12.98                | k 14.64<br>l 13.74<br>l 12.46<br>l 11.98          | k 10°92<br>l 13°88<br>l 13°70<br>l 14°28<br>k 12°52  | l 13·32<br>l 14·48<br>l 14·10                 | 2 15°32<br>\$ 13°74<br>\$ 12°72<br>\$ 13°74 | k 13.12<br>k 14.56<br>k 12.62                                                   | $M = 13'' \cdot 72$<br>$w = 16 \cdot 90$<br>$\frac{1}{w} = 0 \cdot 06$<br>$C = 63^{\circ} 22' 13'' \cdot 72$ |  |  |  |
|                | 13.37                                                                                                                                    | 13.39                                    | 13.94                                                               | 14.40                                               | 14.48                                                              | 13.30                                             | 13.00                                                | 13.97                                         | 13.88                                       | 13.43                                                                           | · · · · · · · · · · · · · · · · · · ·                                                                        |  |  |  |
| LIV & LII      | k 50°52<br>k 50°92<br>l 48°94<br>k 51°60                                                                                                 | k 51,30<br>k 51,12<br>k 51,60            | k 50°84<br>k 52°26<br>k 51°88                                       | l 50°26<br>l 51°02<br>l 52°04                       | l 52°08<br>l 49°56<br>l 50°20<br>l 50°68                           | k 51.62<br>l 51.10<br>l 52.84                     | k 52°28<br>h 51°54<br>l 51°60                        | l 51°52<br>l 50°34<br>l 51°84                 | l 49°76<br>l 50°12<br>h 50°66               | h 53 · 58<br>h 50 · 28<br>h 51 · 64<br>h 51 · 54<br>h 52 · 24                   | $M = 51^{w} \cdot 22$ $w = 18 \cdot 13$ $\frac{1}{w} = 0 \cdot 06$                                           |  |  |  |
|                | 50.20                                                                                                                                    | 51.34                                    | 51.66                                                               | 51.11                                               | 50.63                                                              | 51.85                                             | 51.81                                                | 51.53                                         | 50.18                                       | 51.80                                                                           | $\tilde{C} = 84^{\circ} 42' 51'' \cdot 22$                                                                   |  |  |  |

At LI (Telu)

March 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle    |                                 | Circle readings, telescope being set on LIII                        |                                               |                                    |                        |                                 |                                 |                                 |                                    |                                 |                                                                                                  |  |
|----------|---------------------------------|---------------------------------------------------------------------|-----------------------------------------------|------------------------------------|------------------------|---------------------------------|---------------------------------|---------------------------------|------------------------------------|---------------------------------|--------------------------------------------------------------------------------------------------|--|
| between  | 0° 1′                           | <b>180° 1′</b>                                                      | 79° 18′                                       | <b>25</b> 9° 1 <b>8′</b>           | 158° 24′               | 888° 24′                        | <b>287° 86'</b>                 | 57° 86′ .                       | 816° 48′.                          | 136° 48′                        | C = Concluded Angle                                                                              |  |
| LIII & L | "<br>k 4.78<br>k 4.42<br>k 3.50 | "<br>\$ 2.20<br>\$ 5.76<br>\$ 6.40<br>\$ 3.90<br>\$ 3.12<br>\$ 4.78 | "<br>\$ 2.36<br>\$ 2.98<br>\$ 3.36<br>\$ 3.40 | "<br>\$ 3.26<br>\$ 4.28<br>\$ 3.44 | " k 4°08 k 4°54 k 4°62 | "<br>k 4.26<br>k 4.48<br>k 4.42 | "<br>k 4.22<br>k 3.76<br>k 4.08 | "<br>k 4.02<br>k 3.84<br>k 3.94 | "<br>\$ 3*46<br>\$ 3*28<br>\$ 4*86 | "<br>1 4.60<br>1 5.72<br>1 4.80 | $M = 4'' \cdot 09$ $w = 22 \cdot 50$ $\frac{1}{w} = 0 \cdot 04$ $C = 61^{\circ} 1' 4'' \cdot 08$ |  |
|          | 4.33                            | 4.30                                                                | 3.03                                          | 3.00                               | <b>4</b> °4I           | 4.39                            | 4.03                            | 3.93                            | 3.87                               | 5.04                            |                                                                                                  |  |

At LI (Telu)—(Continued).

|                  |                                    |                                                                                                                           | •                                  |                                    |                                    | iu) (0                             |                                    | •)•                                |                                    |                                    |                                                                  |  |
|------------------|------------------------------------|---------------------------------------------------------------------------------------------------------------------------|------------------------------------|------------------------------------|------------------------------------|------------------------------------|------------------------------------|------------------------------------|------------------------------------|------------------------------------|------------------------------------------------------------------|--|
| Angle<br>between | <b>0° 1′</b> `                     | Circle readings, telescope being set on LIII<br>0°1′ 180°1′ 79°13′ 259°13′ 158°24′ 838°24′ 237°36′ 57°36′ 816°48′ 136°48′ |                                    |                                    |                                    |                                    |                                    |                                    |                                    |                                    |                                                                  |  |
| L & XLVIII       | "<br>h 29°38<br>h 29°02<br>h 28°82 | "<br>h 28°84<br>h 29°12<br>h 28°04                                                                                        | "<br>h 29°30<br>h 29°06<br>h 29°08 | "<br>h 29°30<br>h 28°84<br>h 28°60 | "<br>h 29°24<br>h 29°72<br>h 29°50 | "<br>h 29°22<br>h 30°72<br>h 29°94 | "<br>h 29°38<br>h 29°16<br>k 29°36 | "<br>h 28°40<br>h 29°84<br>h 28°88 | "<br>h 30°14<br>h 29°70<br>h 29°82 | "<br>2 30°26<br>2 28°88<br>2 29°86 | $M = 29'' \cdot 32$ $w = 43 \cdot 50$ $\frac{1}{w} = 0 \cdot 02$ |  |
| н.<br>1          | 29.07                              | 28.67                                                                                                                     | 29.15                              | 28.91                              | 29.49                              | 29.96                              | 29.30                              | 29.04                              | 29.89                              | 29.67                              | $C = 53^{\circ} 48' 29'' \cdot 32$                               |  |

#### At LII (Aukli)

March 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle<br>between | 0°1′                                     | 180° 1′                         | Cir.<br>79° 12′                          | cle readin<br>259° 12'                              | gs, telesco<br>158° 24'          | ope being<br>838° 24'                     | set on X<br>237°36'              | LIX<br>57° 36'                   | 816° 49′                         | 136° 48′                                             | M = Mean of Groups<br>w = Relative Weight<br>C = Concluded Angle |
|------------------|------------------------------------------|---------------------------------|------------------------------------------|-----------------------------------------------------|----------------------------------|-------------------------------------------|----------------------------------|----------------------------------|----------------------------------|------------------------------------------------------|------------------------------------------------------------------|
| XLIX & L         | "                                        | "<br>k 8°96<br>k 7°98<br>k 9°16 | "<br>k 9°26<br>k 10°94<br>k 9°12         | "<br>  10°40<br>  9°30<br>  8°84                    | "<br>1 9.08<br>1 10.42<br>1 9.50 | "<br>2 8·78<br>2 9·14<br>2 9·14<br>2 9·14 | "<br>h 9.96<br>h 9.48<br>h 10.22 | "<br>k 9°80<br>k 10°06<br>k 9°64 | "<br>k 10°08<br>k 9°84<br>k 9°36 | "<br>h 8°36<br>h 10°20<br>h 6°72<br>h 8°66<br>h 9°02 | $M = 9'' \cdot 4I$ $w = 25 \cdot 8I$ $\frac{I}{w} = 0 \cdot 04$  |
|                  | 9*37                                     | 8.70                            | 9`77                                     | 9.21                                                | 9.67                             | 9.03                                      | 9.89                             | 9.83                             | 9.76                             | 8.29                                                 | $C = 84^{\circ} \circ 9^{\circ} \cdot 39$                        |
| L & LIV          | k 18.36<br>k 15.98<br>k 16.66<br>k 15.50 | h 16°38<br>h 17°46<br>h 16°84   | h 14°34<br>h 15°06<br>h 14°94<br>h 15°98 | l 15.06<br>l 16.30<br>l 18.34<br>l 15.80<br>l 15.88 | l 16°18<br>l 16°22<br>l 15°92    | l 17.00<br>l 17.16<br>l 16.02             | k 16.64<br>k 16.58<br>k 16.10    | h 16°48<br>h 17°46<br>h 15°88    | k 17.18<br>k 15.76<br>k 16.88    | k 17 °08<br>k 17 ° 32<br>k 15 ° 72                   | $M = 16'' \cdot 40$ $w = 23 \cdot 17$ $\frac{1}{w} = 0 \cdot 04$ |
|                  | 16.63                                    | 16.89                           | 15.08                                    | 16.38                                               | 16.11                            | 16.73                                     | 16.34                            | 16.91                            | 16.91                            | 16.21                                                | $C = 47^{\circ}  18'  16'' \cdot 38$                             |

#### At LIII (Mansa)

December 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle    |          | Circle readings, telescope being set on LVI   |                                                           |                                          |                                    |                                    |                                     |                                     |                                     |                                    |                                                                  |  |  |  |  |
|----------|----------|-----------------------------------------------|-----------------------------------------------------------|------------------------------------------|------------------------------------|------------------------------------|-------------------------------------|-------------------------------------|-------------------------------------|------------------------------------|------------------------------------------------------------------|--|--|--|--|
| between  | 246° 56′ | 66° 56′                                       | 826° 7′                                                   | 146°7'                                   | <b>45° 19′</b>                     | 225° 19′                           | 124° 31′                            | 304° 31′                            | 203° 43′                            | <b>23° 43′</b>                     | $\omega$ = Relative weight $C$ = Concluded Angle                 |  |  |  |  |
| LVI & LV | "        | "<br>h 24°52<br>h 27°10<br>h 24°16<br>h 26°32 | ."<br>h 27°38<br>h 28°46<br>h 27°06<br>h 25°92<br>h 25°20 | "<br>h 27 • 46<br>h 25 • 90<br>h 26 • 36 | "<br>h 25.68<br>h 25.96<br>h 26.10 | "<br>h 26°72<br>h 25°78<br>h 26°66 | ."<br>h 25°98<br>h 25°50<br>h 26°30 | h 26 * 32<br>h 25 * 82<br>h 25 * 78 | h 24 · 32<br>h 26 · 28<br>h 25 · 02 | "<br>h 25°76<br>h 26°22<br>h 25°88 | $M = 26'' \cdot 00$ $w = 22 \cdot 20$ $\frac{I}{w} = 0 \cdot 05$ |  |  |  |  |
|          | 25.78    | 25.23                                         | 26.80                                                     | 26.27                                    | 25.91                              | <b>2</b> 6·39                      | 25.93                               | 25°97                               | 25.31                               | 25.95                              | $C = 00^{\circ} 42^{\circ} 20^{\prime\prime} \cdot 01$           |  |  |  |  |

| At LIII (Mansa)—(Continued). |                               |                               |                                                                                                  |                               |                                         |                                                          |                                          |                                          |                                    |                               |                                                                  |  |  |
|------------------------------|-------------------------------|-------------------------------|--------------------------------------------------------------------------------------------------|-------------------------------|-----------------------------------------|----------------------------------------------------------|------------------------------------------|------------------------------------------|------------------------------------|-------------------------------|------------------------------------------------------------------|--|--|
| Angle                        |                               |                               | Ci                                                                                               | rcle readi                    | ngs, telesc                             | ope being                                                | set on L                                 | VI                                       |                                    |                               | M = Mean of Groups                                               |  |  |
| between                      | 246° 56′                      | 66° 56′                       | <b>8</b> 26° 7′                                                                                  | 146°7′                        | <b>45°19'</b>                           | <b>225°</b> 19 <b>′</b>                                  | 124°31′                                  | <b>304° 31′</b>                          | 203° 43′                           | 23° 43′                       | w = Relative Weight<br>C = Concluded Angle                       |  |  |
| LV & LIV                     | k 57°08<br>k 55°28<br>k 55°88 | h 57°50<br>h 56°90<br>h 55°68 | <i>k</i> 54 · 12<br><i>k</i> 56 · 26<br><i>k</i> 55 · 82<br><i>k</i> 56 · 60<br><i>k</i> 55 · 74 | k 57 28<br>k 57 96<br>k 56 40 | n<br>h 57 °08<br>h 55 ° 34<br>h 56 ° 06 | <i>h</i> 57 · 12<br><i>h</i> 55 · 86<br><i>h</i> 57 · 18 | n<br>h 56 · 40<br>h 55 · 90<br>h 54 · 74 | n<br>h 56 · 88<br>h 55 · 60<br>h 57 · 40 | "<br>h 55°78<br>h 57°64<br>h 56°28 | k 56°76<br>k 56°52<br>k 57°62 | $M = 56'' \cdot 44$ $w = 22 \cdot 61$ $\frac{1}{w} = 0 \cdot 04$ |  |  |
|                              | 56.08                         | 56.69                         | 55.41                                                                                            | 57.31                         | 56.16                                   | 56.72                                                    | 55.68                                    | 56.63                                    | 56.22                              | 56.92                         | $C = 52^{\circ} 22' 56'' \cdot 43$                               |  |  |

March 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle   |                                                                                       |                                     | Ci                                                    | rcle readi                         | ngs, teleso                         | cope being                                    | g set on L                                                    | IV                                 |                                               |                                          | M = Mean of Groups                                                                                  |
|---------|---------------------------------------------------------------------------------------|-------------------------------------|-------------------------------------------------------|------------------------------------|-------------------------------------|-----------------------------------------------|---------------------------------------------------------------|------------------------------------|-----------------------------------------------|------------------------------------------|-----------------------------------------------------------------------------------------------------|
| between | <b>0°0</b> * -                                                                        | 180°0′                              | <b>79° 13′</b>                                        | 259° 12′                           | 158° 25'                            | <b>3</b> 38° <b>25′</b>                       | 237° 37′                                                      | 57° 87′                            | <b>316° 49′</b>                               | 136 <b>° 4</b> 8′                        | C = Concluded Angle                                                                                 |
| LIV & L | *<br>\$ 56 * 24<br>\$ 52 * 68<br>\$ 52 * 60<br>\$ 53 * 66<br>\$ 55 * 82<br>\$ 54 * 76 | "<br>h 55°38<br>h 55°02<br>l 56°10  | "<br>2 54 ° 94<br>2 56 ° 04<br>2 53 ° 38<br>2 54 ° 32 | "<br>2 53`54<br>2 53`12<br>2 53`80 | "<br>2 55°04<br>2 54°70<br>2 54°90  | "<br>2 53.68<br>2 56.54<br>2 53.02<br>2 54.80 | "<br>2 54 °60<br>2 53 ° 18<br>2 55 ° 66<br>2 55 ° 36          | 7<br>2 53°12<br>2 52°48<br>2 53°84 | "<br>2 53°66<br>2 56°12<br>2 55°44<br>2 55°12 | "<br>2 53 · 36<br>2 55 · 10<br>2 54 · 96 | $M = 54'' \cdot 51$ $w = 13 \cdot 81$ $\frac{1}{w} = 0 \cdot 07$ $C = 44^{\circ} 16' 54'' \cdot 52$ |
|         | 54.63                                                                                 | 55.20                               | 54.67                                                 | 53.49                              | 54.88                               | 54.21                                         | 54.70                                                         | 53.12                              | 55.09                                         | 54.47                                    | 0 - ++ -0 J+ J-                                                                                     |
| L & LI  | h 39°60<br>h 40°98<br>h 38°60                                                         | k 38 ° 06<br>k 38 ° 78<br>l 39 ° 32 | l 40°18<br>l 38°24<br>l 38°74                         | l 37°80<br>l 39°42<br>l 38°80      | 2 38 · 14<br>2 37 · 48<br>2 38 · 98 | l 40°82<br>l 40°12<br>l 38°68<br>l 40°08      | l 41 · 36<br>l 40 · 82<br>l 38 · 32<br>l 39 · 72<br>l 38 · 30 | l 40°72<br>l 39°32<br>l 39°54      | l 40°26<br>l 40°10<br>l 39°74                 | l 38°24<br>l 38°96<br>l 38°60            | $M = 39'' \cdot 25$ $w = 15 \cdot 55$ $\frac{1}{w} = 0 \cdot 06$                                    |
|         | 39*73                                                                                 | 38.72                               | 39.02                                                 | 38.67                              | 38.20                               | 39.93                                         | 39.70                                                         | 39.86                              | 40.03                                         | 38.60                                    | $\bar{C} = 76^{\circ} 48' 39'' \cdot 26$                                                            |

At LIV (Marot)

March 1875; observed by Captain M. W. Bogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle   |                                    | Circle readings, telescope being set on LII              |                                               |                                          |                                    |                                    |                                                          |                                                                                                                                                          |                                          |                                                 |                                                                  |  |  |  |
|---------|------------------------------------|----------------------------------------------------------|-----------------------------------------------|------------------------------------------|------------------------------------|------------------------------------|----------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------|-------------------------------------------------|------------------------------------------------------------------|--|--|--|
| between | 812° 2′                            | <b>132° 1′</b>                                           | 81° 14′                                       | 211° 14′                                 | 110 <b>° 26'</b>                   | 290° 26′                           | 189° 38′                                                 | <b>9° 3</b> 8′                                                                                                                                           | <b>268°</b> 50′                          | <b>88° 50′</b> .                                | c = Concluded Angle                                              |  |  |  |
| LII & L | n<br>h 50°70<br>h 52°54<br>h 52°42 | "<br>h 53°08<br>h 53°50<br>h 55°40<br>h 51°78<br>h 52°08 | "<br>h 52 · 82<br>h 52 · 20<br>h 52 · 92<br>l | "<br>h 51 ° 20<br>h 52 ° 64<br>h 52 ° 10 | "<br>h 52°62<br>l 52°28<br>l 51°82 | "<br>2 53°30<br>2 52°82<br>2 52°90 | "<br>1 50'66<br>1 54'14<br>1 51'90<br>1 51'20<br>1 51'90 | <i>k</i><br><i>k</i><br><i>5</i><br><i>i</i><br><i>6</i><br><i>5</i><br><i>5</i><br><i>5</i><br><i>5</i><br><i>5</i><br><i>5</i><br><i>5</i><br><i>5</i> | "<br>h 52 · 86<br>h 51 · 96<br>h 51 · 96 | \$<br>\$<br>53.66<br>\$<br>54.40<br>\$<br>53.08 | $M = 52'' \cdot 55$ $w = 14 \cdot 38$ $\frac{1}{w} = 0 \cdot 07$ |  |  |  |
| -       | 51.89                              | 53.17                                                    | 52.65                                         | .51*98                                   | 52.34                              | 53.01                              | 51.96                                                    | 52.29                                                                                                                                                    | 52.26                                    | 53°71 <sup>°</sup>                              | $C = 47^{\circ} 58' 52'' \cdot 55$                               |  |  |  |

At LIV (Marot)—(Continued).

| Angle    |                                                               |                                       | Ci                                    | rcle readi                                                    | ngs, teles                            | cope bein                          | g set on I                               | ,II                                                                     |                                    |         | M - Mean of Groups                                                 |
|----------|---------------------------------------------------------------|---------------------------------------|---------------------------------------|---------------------------------------------------------------|---------------------------------------|------------------------------------|------------------------------------------|-------------------------------------------------------------------------|------------------------------------|---------|--------------------------------------------------------------------|
| between  | 812° 2′                                                       | 182° 1′                               | 81° 14′                               | 211° <b>14'</b>                                               | 110° 26′                              | 290° 26′                           | 189° 38′                                 | 9° 38′                                                                  | <b>268° 50′</b>                    | 88° 50′ | w = Relative Weight $C = Concluded Angle$                          |
| L & LIII | "<br>\$ 55.08<br>\$ 54.08<br>\$ 52.84<br>\$ 51.92<br>\$ 51.98 | "<br>\$ 52°14<br>\$ 52°12<br>\$ 52°36 | "<br>\$ 52°36<br>\$ 52°52<br>\$ 52°26 | "<br><b>h</b> 51 ° 50<br><b>h</b> 51 ° 86<br><b>h</b> 51 ° 48 | "<br>\$ 52°78<br>\$ 52°68<br>\$ 52°18 | "<br>  52°28<br>  52°68<br>  51°34 | "<br>2 52 ° 66<br>2 52 ° 76<br>2 53 ° 30 | "<br>\$ 54 ° 16<br>\$ 51 ° 80<br>\$ 54 ° 02<br>\$ 52 ° 58<br>\$ 52 ° 42 | "<br>h 52°26<br>h 52°98<br>h 52°54 | "       | $M = 52^{w} \cdot 43$ $w = 23 \cdot 43$ $\frac{1}{w} = 0 \cdot 04$ |
|          | 53.18                                                         | 52.31                                 | 52.38                                 | 51.91                                                         | 52.22                                 | 5 <b>2.</b> 10                     | 52.91                                    | 53.00                                                                   | 52.29                              | 51.82   | $C = 72^{\circ} 20^{\circ} 52^{\circ} 44$                          |

December 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle     | ··········                                                    |                                                         | Cir                                                                  | cle readir                                    | igs, telesc                              | ope being                                                            | set on L.                                             | III                                                 |                                                   |                                          | M = Mean of Groups                                               |
|-----------|---------------------------------------------------------------|---------------------------------------------------------|----------------------------------------------------------------------|-----------------------------------------------|------------------------------------------|----------------------------------------------------------------------|-------------------------------------------------------|-----------------------------------------------------|---------------------------------------------------|------------------------------------------|------------------------------------------------------------------|
| between   | 267° 8′                                                       | 87° 8′                                                  | 846° 16′                                                             | 166° 16′                                      | 65° 27′                                  | 245° 27'                                                             | 1 <b>44° 39</b> ′                                     | 824° 39'                                            | 223° 52′                                          | 48° 52′                                  | w = Relative Weight<br>C = Concluded Angle                       |
| LIII & LV | "<br>\$ 59°50<br>\$ 58°82<br>\$ 58°44                         | "<br><b>h</b> 60°10<br><b>h</b> 59°44<br><b>h</b> 58°84 | "<br>\$ 57.58<br>\$ 58.10<br>\$ 57.80                                | "<br>h 60°32<br>h 57°80<br>h 58°66<br>h 58°38 | "<br>2 58 · 92<br>2 60 · 84<br>2 59 · 94 | "<br>2 60°28<br>2 58°46<br>2 60°34                                   | "<br>1 60 · 80<br>1 60 · 08<br>1 60 · 54<br>1 58 · 86 | "<br>2 61 · 30<br>2 60 · 20<br>2 60 · 74            | "<br>\$ 59.66<br>\$ 57.26<br>\$ 58.84<br>\$ 58.70 | "<br>h 58 · 88<br>h 57 · 38<br>h 58 · 80 | $M = 59'' \cdot 24$ $w = 10 \cdot 55$ $\frac{1}{w} = 0 \cdot 09$ |
|           | 58.92                                                         | 59.46                                                   | 57.83                                                                | 58.79                                         | 59.90                                    | 59.69                                                                | 60.02                                                 | 60.75                                               | 58.62                                             | 58.35                                    | $C = 47^{\circ} 41' 59'' \cdot 24$                               |
| LV & LVII | k 17 · 28<br>k 18 · 02<br>k 18 · 06<br>k 20 · 70<br>k 19 · 50 | <b>k</b> 20°42<br><b>k</b> 20°08<br><b>k</b> 20°72      | <b>k</b> 22°44<br><b>k</b> 21°14<br><b>k</b> 20°14<br><b>k</b> 19°68 | k 20°04<br>k 20°44<br>k 21°22                 | l 20°66<br>l 19°72<br>l 21°08            | l 19 <sup>.</sup> 80<br>l 19 <sup>.</sup> 52<br>l 20 <sup>.</sup> 06 | l 18.98<br>l 18.70<br>l 18.82                         | l 20°00<br>l 18°16<br>l 21°76<br>h 21°14<br>h 20°16 | k 20°26<br>k 19°74<br>k 20°74                     | k 21 · 18<br>k 19 · 92<br>k 21 · 44      | $M = 20'' \cdot 10$ $w = 12 \cdot 60$ $\frac{I}{w} = 0 \cdot 08$ |
|           | 18.71                                                         | 20.41                                                   | 20.85                                                                | <b>2</b> 0°57                                 | <b>20°4</b> 9                            | 19.29                                                                | 18.83                                                 | 20°24                                               | 20.32                                             | 20.85                                    | $C = 45^{\circ} 15' 20'' \cdot 09$                               |

#### At LV (Hasan)

December 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle      |                               | Circle readings, telescope being set on LIX |                                                                                                          |                                    |                                               |                                    |                                                 |                                    |                                    |                               |                                                                  |  |  |  |  |
|------------|-------------------------------|---------------------------------------------|----------------------------------------------------------------------------------------------------------|------------------------------------|-----------------------------------------------|------------------------------------|-------------------------------------------------|------------------------------------|------------------------------------|-------------------------------|------------------------------------------------------------------|--|--|--|--|
| between    | 0 <sup>e</sup> 1'             | 180° 1′                                     | <b>79°</b> 12′                                                                                           | <b>259°</b> 12′                    | 158° 23′                                      | <b>338° 24'</b>                    | 237° 87′                                        | 57° 87′                            | <b>816° 48'</b>                    | 186° 48′                      | c = Concluded Angle                                              |  |  |  |  |
| LIX & LVII | k 17°10<br>k 16°04<br>k 17°00 | "<br>h 15°54<br>h 17°16<br>h 15°42          | <b>7</b><br><b>1</b><br><b>1</b><br><b>1</b><br><b>1</b><br><b>1</b><br><b>1</b><br><b>1</b><br><b>1</b> | *<br>k 15°20<br>k 15°54<br>k 14°94 | "<br>h 15°46<br>h 17°94<br>h 15°20<br>h 16°02 | "<br>h 15°12<br>h 15°60<br>h 14°94 | 14.82         16.36         15.90         15.86 | "<br>2 15°98<br>2 15°94<br>2 14°74 | "<br>k 15°92<br>k 15°24<br>k 15°24 | k 15.66<br>k 15.10<br>k 14.74 | $M = 15'' \cdot 65$ $w = 25 \cdot 18$ $\frac{1}{w} = 0 \cdot 04$ |  |  |  |  |
|            | 16.21                         | 16.04                                       | 15.18                                                                                                    | 15.33                              | 16.19                                         | 15.33                              | 15.73                                           | 15.22                              | 15.47                              | 15.12                         | $C = 56^{\circ} 49' 15'' \cdot 65$                               |  |  |  |  |

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|---------------------------------------|----------------------------------------------------------------|--------------------------------------------------|---------------------------------------------------------------------------|---------------------------------------------------|------------------------------------------|----------------------------------------------|------------------------------------------|----------------------------------------------------------|--------------------------------------|-------------------------------------|--------------------------------------------------------------------------------------------------------------|
| Angle                                 |                                                                |                                                  | Cir                                                                       | rcle readin                                       | ngs, telesc                              | ope being                                    | set on L                                 | IX                                                       |                                      |                                     | M = Mean of Groups                                                                                           |
| between                               | 0°1′                                                           | 180° 1′                                          | 79° 12′                                                                   | <b>25</b> 9° 12′                                  | 158° 23'                                 | <b>33</b> 8° 24′                             | 237° 37′                                 | 57° 37′                                                  | 816° 48′                             | <b>136° 48'</b>                     | w = Relative Weight<br>C = Concluded Angle                                                                   |
| LVII & LIV                            | "<br>h 27°10<br>h 26°80<br>k 25°02<br>h 26°90                  | "<br>k 24°74<br>k 25°54<br>l 25°08               | "<br>  26°72<br>  25°14<br>  26°78                                        | "<br>h 23 °96<br>h 26 °00<br>h 26 °68<br>h 26 °08 | 7<br>h 25 * 82<br>h 25 * 24<br>h 25 * 38 | "<br>\$ 25 • 46<br>\$ 26 • 28<br>\$ 24 • 86  | "<br>h 25 · 70<br>h 25 · 52<br>h 25 · 76 | "<br>l 25°54<br>h 26°72<br>h 24°66<br>h 26°16<br>h 26°06 | "<br>k 26·94<br>k 25·24<br>k 26·34   | 7<br>h 25°62<br>h 26°10<br>h 24°28  | $M = 25'' \cdot 75$ $w = 30 \cdot 81$ $\frac{1}{w} = 0 \cdot c3$                                             |
|                                       | 26.40                                                          | 25.12                                            | 26.51                                                                     | 25.68                                             | 25.48                                    | 25*53                                        | 25.66                                    | 25.83                                                    | 26.12                                | 25.33                               | $C = 60^{\circ} 2' 25'' \cdot 76$                                                                            |
| LIV & LIII                            | k 6.76<br>h 6.06<br>k 7.38<br>k 5.72                           | k 8.14<br>h 5.10<br>l 6.06<br>l 7.08<br>l 4.80   | l 3.76<br>l 5.38<br>l 5.26                                                | h 8.68<br>h 6.12<br>h 6.10<br>h 6.98              | h 5°40<br>h 5°58<br>h 4°66               | h 4°18<br>h 6°14<br>h 4°32                   | h 6°26<br>h 5°84<br>h 5°94               | l 6.00<br>h 4.84<br>h 5.76                               | h 5°02<br>h 5°26<br>h 7°26<br>h 4°60 | ћ 5°20<br>ћ 4°88<br>ћ 5°50          | $M = 5'' \cdot 68$ $w = 14 \cdot 05$ $\frac{1}{m} = 0 \cdot 07$                                              |
|                                       | 6.48                                                           | 6.34                                             | 4.80                                                                      | 6.92                                              | 5.51                                     | 4.88                                         | 6.01                                     | 5.23                                                     | 5*54                                 | 5.19                                | $C = 79^{\circ} 55' 5^{*} 7^{\circ}$                                                                         |
| LIII & LVI                            | h 8.26<br>h 11.00<br>h 8.82<br>h 9.18                          | k 10, 15<br>k 10, 15<br>f 11, 54                 | l 10'96<br>l 8'56<br>l 11'46<br>l 11'04                                   | k 8.80<br>h 10.02<br>h 10.58                      | h 11°00<br>h 10°26<br>h 9°92<br>h 11°88  | k 10°14<br>k 10°12<br>k 9°62                 | k 10°42<br>k 9°60<br>k 10°54             | l 9°92<br>h 8°90<br>h 9°24                               | k 10.72<br>k 9.72<br>k 9.40          | h 9.92<br>h 10.38<br>h 9.98         | $M = 10'' \cdot 07$<br>$w = 23 \cdot 99$<br>$\frac{1}{2} = 0 \cdot 04$                                       |
|                                       | 9.32                                                           | 10.26                                            | 10.20                                                                     | 9.80                                              | 10.22                                    | 9.96                                         | 10.10                                    | 9.35                                                     | 9.92                                 | 10.00                               | $C = 37^{\circ} 21' 10'' \cdot 07$                                                                           |
| LVI & LVIII                           | h 29 96<br>h 23 58<br>h 27 92<br>h 26 34<br>h 27 18<br>h 27 34 | h 26.68<br>h 26.02<br>l 26.36                    | l 23.34<br>l 27.62<br>l 25.60<br>l 24.14<br>l 28.44<br>l 24.98<br>l 26.32 | h 26.68<br>h 28.00<br>h 27.28                     | h 26.54<br>h 26.26<br>h 27.43            | h 24 °92<br>h 25 °88<br>h 27 °36<br>h 26 °86 | h 26°48<br>h 26°58<br>h 26°90            | l 29.78<br>h 25.96<br>h 25.88<br>h 25.24<br>h 26.24      | h 25°36<br>h 26°56<br>h 25°28        | h 26 · 04<br>h 26 · 94<br>h 26 · 28 | $M = 26'' \cdot 49$<br>$w = 14 \cdot 97$<br>$\frac{1}{w} = 0 \cdot 07$<br>$C = 60^{\circ} 4' 26'' \cdot 48$  |
|                                       | 27*05                                                          | 26.32                                            | 25.78                                                                     | 27.32                                             | 26.76                                    | 26.30                                        | 26.65                                    | 26.62                                                    | 25.73                                | 26.42                               |                                                                                                              |
| LVIII & LIX                           | h 30 · 86<br>h 35 · 64<br>h 33 · 82<br>h 34 · 78<br>h 35 · 04  | h 34 ° 20<br>h 35 ° 92<br>l 36 ° 38<br>l 36 ° 34 | l 39.76<br>l 38.20<br>l 35.68<br>l 38.06<br>l 34.76<br>l 37.76<br>l 36.76 | h 36°00<br>h 34°90<br>h 34°88                     | h 36°04<br>h 36°70<br>h 35°12            | h 34 · 42<br>h 36 · 20<br>h 36 · 36          | h 34`94<br>h 35`28<br>h 35`84            | l 34·48<br>h 35·84<br>h 36·34                            | h 35 • 48<br>h 35 • 74<br>h 37 • 08  | h 35 * 88<br>h 35 * 44<br>h 36 * 20 | $M = 35'' \cdot 67$<br>$w = 10 \cdot 04$<br>$\frac{1}{w} = 0 \cdot 10$<br>$C = 65^{\circ} 47' 35'' \cdot 68$ |
|                                       | 34.03                                                          | 35.21                                            | 37 . 28                                                                   | 35.30                                             | 35 95                                    | 35.00                                        | 35.35                                    | 35.22                                                    | 36.10                                | 35.84                               | с — су т/ уу ««                                                                                              |

· At LV (Hasan)-(Continued).

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## At LVI (Sultán)

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December 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle      |                                                               | Circle readings, telescope being set on LVIII |                                          |                                          |                                                       |                                    |                                                               |                                                  |                                          |                                          |                                                                  |  |  |  |
|------------|---------------------------------------------------------------|-----------------------------------------------|------------------------------------------|------------------------------------------|-------------------------------------------------------|------------------------------------|---------------------------------------------------------------|--------------------------------------------------|------------------------------------------|------------------------------------------|------------------------------------------------------------------|--|--|--|
| between    | 0° 0′                                                         | 180° 0′                                       | 79° 18′                                  | <b>25</b> 9° 13′                         | 158° 24′                                              | 838° 24′                           | <b>2</b> 87° <b>3</b> 7′                                      | 57° 37'                                          | <b>8</b> 16° 49′                         | 186° 48′                                 | C = Concluded Angle                                              |  |  |  |
| LVIII & LV | "<br>h 24 ° 90<br>h 24 ° 22<br>h 25 ° 10                      | "<br>h 23 · 32<br>h 22 · 76<br>h 23 · 36      | "<br>h 23 ° 30<br>h 23 ° 02<br>h 24 ° 96 | "<br>k 24 • 44<br>k 22 • 94<br>k 23 . 90 | "<br>l 22 · 18<br>l 21 · 20<br>l 22 · 30<br>l 23 · 58 | "<br>  23°10<br>  21°44<br>  23°20 | "<br>h 24 °64<br>h 22 °64<br>h 22 °96                         | "<br>h 22°56<br>h 24°18<br>h 22°34               | "<br>h :4 · 22<br>h :4 · 50<br>h :4 · 30 | "<br>h 23 ° 32<br>h 23 ° 16<br>h 23 ° 68 | $M = 23'' \cdot 45$ $w = 14 \cdot 39$ $\frac{1}{w} = 0 \cdot 07$ |  |  |  |
|            | 24*74                                                         | 23.15                                         | 23.76                                    | 23.76                                    | 22.32                                                 | 22.58                              | 23.41                                                         | 23.03                                            | 24.34                                    | 23.39                                    | $C = 62^{\circ} 9' 23'' \cdot 44$                                |  |  |  |
| LV & LIII  | k 28 ° 04<br>k 26 ° 18<br>k 26 ° 14<br>k 24 ° 44<br>k 26 ° 48 | h 23 84<br>h 23 80<br>h 25 52                 | h 23 °66<br>h 24 ° 32<br>h 23 °72        | h 24 · 36<br>h 24 · 56<br>h 24 · 46      | l 26.70<br>l 24.28<br>l 24.74<br>l 24.20              | l 23.64<br>l 24.76<br>l 23.56      | h 23 · 40<br>h 22 · 08<br>h 22 · 12<br>h 21 · 66<br>h 22 · 62 | h 23 · 10<br>h 24 · 38<br>h 21 · 92<br>h 24 · 30 | h 23°24<br>h 22°60<br>h 23°94            | h 24 ° 20<br>h 23 ° 72<br>h 24 ° 00      | $M = 24'' \cdot 10$ $w = 7 \cdot 93$ $\frac{1}{w} = 0 \cdot 13$  |  |  |  |
|            | 26.30                                                         | 24.39                                         | 23.90                                    | 24.40                                    | 24.98                                                 | 23.99                              | 22.38                                                         | 23.43                                            | 23, 20                                   | 23.97                                    | $\tilde{C} = 81^{\circ} 56' 24'' \cdot 10$                       |  |  |  |

## At LVII (Bijli)

December 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

|                  | 1                                                                                            |                                                  |                                    |                                    |                                                       |                                                  |                                                 |                                    |                                                                           |                                                     | 1                                                                                                            |
|------------------|----------------------------------------------------------------------------------------------|--------------------------------------------------|------------------------------------|------------------------------------|-------------------------------------------------------|--------------------------------------------------|-------------------------------------------------|------------------------------------|---------------------------------------------------------------------------|-----------------------------------------------------|--------------------------------------------------------------------------------------------------------------|
| Angle<br>between | . 0°1′                                                                                       | 180° 1′                                          | C<br>79° 12′                       | ircle read<br>259° 12′             | ings, teles<br>158°24'                                | cope being<br>838° 24'                           | g set on L<br>237°87'                           | IV<br>57° 36'                      | <b>816° 49'</b>                                                           | 136° 48′                                            | M - Mean of Groups<br>- Relative Weight<br>C - Concluded Angle                                               |
| LIV & LV         | "<br>k 16 · 40<br>k 15 · 96<br>k 17 · 28<br>k 16 · 22<br>l 15 · 44<br>l 14 · 30<br>l 14 · 54 | "                                                | "<br>l 13.00<br>k 13.76<br>k 13.66 | "<br>h 13°26<br>h 13°06<br>h 13°74 | "<br>h 14 · 10<br>h 14 · 08<br>h 13 · 76<br>h 14 · 58 | "<br>h 13 · 56<br>h 13 · 62<br>h 15 · 08         | "<br>k 14 · 12<br>k 15 · 18<br>k 13 · 84        | "<br>h 14.26<br>h 13.88<br>h 14.46 | "<br>h 13 <sup>-</sup> 84<br>l >4 <sup>-</sup> 34<br>l 14 <sup>-</sup> 00 | "<br>  13 · 82<br>  15 · 34<br>  13 · 60            | $M = 14'' \cdot 24$<br>$w = 17 \cdot 78$<br>$\frac{1}{w} = 0 \cdot 06$<br>$C = 74^{\circ} 42' 14'' \cdot 27$ |
|                  | 15.23                                                                                        | 14.69                                            | 13.47                              | 13.32                              | 14.13                                                 | 14.09                                            | 14.38                                           | 14.30                              | 14.00                                                                     | 14.32                                               |                                                                                                              |
| LV & LIX         | h 57°64<br>h 55°30<br>h 57°32<br>h 54°16<br>h 54°18<br>l 56°02                               | h 54 · 50<br>h 54 · 72<br>h 56 · 76<br>h 55 · 44 | 2 53 42<br>h 55 34<br>h 53 52      | \$ 56°60<br>\$ 56°38<br>\$ 56°36   | k 54 · 54<br>k 53 · 86<br>k 55 · 22                   | h 56 ° 04<br>h 53 ° 06<br>h 55 ° 32<br>h 54 ° 52 | h 53 °00<br>h 55 ° 30<br>h 55 ° 54<br>h 55 ° 84 | h 55°30<br>h 54°42<br>h 54°52      | k 56°96<br>l 54°68<br>l 54°70<br>l 55°00                                  | l 56.60<br>l 53.82<br>l 56.34<br>l 53.44<br>l 53.88 | $M = 55'' \cdot 08$ $w = 13 \cdot 39$ $\frac{1}{w} = 0 \cdot 07$                                             |
|                  | 55.22                                                                                        | 55.30                                            | 54.09                              | 50.42                              | 54.24                                                 | 54.13                                            | 54.92                                           | 54.75                              | 55:34                                                                     | 54.82                                               | $C = 53^{\circ} 56' 55'' \cdot 09$                                                                           |

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#### PRINCIPAL TRIANGULATION. OBSERVED ANGLES.

|                  |                                                                                |                                    | Cir                                | · At L'                          | VII (Bi                      | ijli)((                            | Continue                                 | ed).                               |                                    |                                    | M - Meen of Ground                                                                                 |
|------------------|--------------------------------------------------------------------------------|------------------------------------|------------------------------------|----------------------------------|------------------------------|------------------------------------|------------------------------------------|------------------------------------|------------------------------------|------------------------------------|----------------------------------------------------------------------------------------------------|
| Angle<br>between | 0° 1′                                                                          | 180° 1′                            | 79° 12′                            | 259° 12'                         | 158° 24′                     | 838° 24'                           | 237° 37'                                 | 57° 86'                            | 816° 49′                           | 136° 48′                           | w - Relative Weight<br>C - Concluded Angle                                                         |
| LIX & XXI        | "<br>h 15.16<br>h 14.26<br>h 13.62<br>h 13.08<br>l 16.94<br>l 16.84<br>l 16.44 | "<br>h 17°24<br>h 17°24<br>k 16°26 | "<br>h 16·72<br>h 16·40<br>h 15·38 | и<br>10°52<br>д 16°52<br>д 16°08 | и<br>15°40<br>16°62<br>17°02 | л<br>л 16.93<br>л 19.00<br>л 19.08 | "<br>h 17 · 72<br>h 16 · 44<br>h 17 · 12 | ,<br>h 17,48<br>h 16,24<br>h 16,18 | "<br>  16·32<br>  15·82<br>  15·78 | "<br>l 16°20<br>l 15°58<br>l 15°46 | $M = 16'' \cdot 36$ $w = 17 \cdot 65$ $\frac{1}{w} = 0 \cdot 06$ $C = 63^{\circ} 2' 16'' \cdot 33$ |
|                  | 15.19                                                                          | 16.91                              | 16.12                              | 16 <b>.</b> 63 ·                 | 17.01                        | 16.30                              | 17.09                                    | 16.63                              | 15.92                              | 15.22                              |                                                                                                    |

# At LVIII (Panchkot)

December 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle<br>between | 0° 1′                                               | 180° 1′                                     | Circle readings, telescope being set on XIX<br>180° 1' 79° 12' 259° 12' 158° 25' 838° 25' 237° 36' 57° 87' 816° 49' 186° 49' |                                          |                                                                      |                                             |                                                |                                             |                                               |                                             |                                                                                                                    |  |  |
|------------------|-----------------------------------------------------|---------------------------------------------|------------------------------------------------------------------------------------------------------------------------------|------------------------------------------|----------------------------------------------------------------------|---------------------------------------------|------------------------------------------------|---------------------------------------------|-----------------------------------------------|---------------------------------------------|--------------------------------------------------------------------------------------------------------------------|--|--|
| XIX & LIX        | "<br>h 15 ° 78<br>h 15 ° 32<br>k 15 ° 12<br>15 ° 41 | "<br>h 15.84<br>h 15.00<br>h 15.38<br>J5.41 | "<br>h 16 · 14<br>h 14 · 76<br>h 14 · 14<br>15 · 01                                                                          | "<br>h 15.42<br>h 16.12<br>h 15.32       | <i>k</i> 16.76<br><i>h</i> 14.64<br><i>k</i> 15.92<br><i>k</i> 15.04 | "<br>h 15°12<br>h 15°80<br>h 14°56<br>15°16 | "<br>h 14 °44<br>h 14 74<br>h 14 °72<br>14 °63 | "<br>h 15°12<br>h 14°88<br>h 14°72<br>14°91 | "<br>h 15.60<br>h 16.72<br>h 14.28<br>h 17.26 | "<br>h 14.82<br>h 15.38<br>h 15.18<br>15.13 | $M = 15'' \cdot 28$<br>$w = 35 \cdot 30$<br>$\frac{1}{w} = 0 \cdot 03$<br>$C = 61^{\circ} 36' \cdot 15'' \cdot 29$ |  |  |
| LIX & LV         | k 42 ° 10<br>k 41 ° 20<br>k 42 ° 20                 | k 40 · 80<br>k 42 · 42<br>k 41 · 24         | h41°04<br>h41°46<br>h42°34                                                                                                   | k 40°52<br>k 40°42<br>k 38°26<br>k 41°32 | h 41 · 20<br>h 40 · 06<br>h 40 · 78                                  | k41°44<br>k41°54<br>k41°56                  | k 42 ° 04<br>k 40 ° 76<br>k 41 ° 46            | k 41 °00<br>k 41 °26<br>k 41 °42            | k 42 ° 04<br>k 41 ° 40<br>k 40 ° 98           | k 40°96<br>k 40°94<br>k 42°04               | $M = 41'' \cdot 27$ $w = 27 \cdot 24$ $\frac{1}{w} = 0 \cdot 04$ $C = 44^{\circ} 5' 41'' \cdot 25$                 |  |  |
|                  | 41.83                                               | 41.49                                       | 41.01                                                                                                                        | 40.13                                    | 40.68                                                                | 41.20                                       | 41.43                                          | 41.33                                       | 41°47                                         | 41.31                                       |                                                                                                                    |  |  |
| LV & LVI         | y 8.90<br>y 8.90<br>y 10,10                         | k 10°34<br>k 9°30<br>k 10°70                | k 9.62<br>k 9.74<br>k 9.84                                                                                                   | h 10°04<br>h 11°06<br>h 12°30<br>h 9°58  | h 10°36<br>h 11°18<br>h 10°50                                        | k 10°86<br>k 11°34<br>k 10°68               | h 10°18<br>h 10°34<br>h 10°58                  | h 9.70<br>h 10.78<br>h 10.16                | h 11.06<br>h 3.04<br>h 10.68                  | k 9.10<br>k 10.58<br>k 11.08                | $M = 10'' \cdot 31$ $w = 33 \cdot 68$ $\frac{1}{2} = 0 \cdot 03$                                                   |  |  |
|                  | 9.28                                                | 10.11                                       | 9*73                                                                                                                         | 10.75                                    | 10.43                                                                | 10.92                                       | 10.32                                          | 10.31                                       | 10.20                                         | 10.12                                       | $C = 57^{\circ} 46' 10'' \cdot 32$                                                                                 |  |  |

NOTE.-Stations XIX and XXI appertain to the Sutlej Series.

## At LIX (Randu)

December 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle       |                                                     | M = Mean of Groups                       |                                                                |                                                     |                                                               |                                                               |                                          |                                                   |                                                                   |                                          |                                                                                                                    |
|-------------|-----------------------------------------------------|------------------------------------------|----------------------------------------------------------------|-----------------------------------------------------|---------------------------------------------------------------|---------------------------------------------------------------|------------------------------------------|---------------------------------------------------|-------------------------------------------------------------------|------------------------------------------|--------------------------------------------------------------------------------------------------------------------|
| between     | <b>0</b> ° 0′                                       | 180° 0'                                  | <b>79°13′</b>                                                  | 259° 13′                                            | 158° 24′                                                      | <b>3</b> 38° 24'                                              | <b>2</b> 37° 36'                         | 57° 36'                                           | 816° 49′                                                          | 136° 49′                                 | C = Concluded Angle                                                                                                |
| LVII & LV   | "<br>k 48.68<br>k 49.26<br>l 48.06                  | "<br>l 49`54<br>l 48`30<br>l 49`30       | "<br>2 48 • 52<br>2 49 • 46<br>2 47 • 90                       | "<br>2 48 • 66<br>2 47 • 88<br>2 49 • 56            | "<br>k 49`56<br>k 50`96<br>k 49`14                            | "<br>k 48 • 42<br>k 47 • 82<br>k 49 • 00                      | "<br>k 49°26<br>k 50°08<br>k 49°84       | "<br>\$ 50°28<br>\$ 48°00<br>\$ 49°48<br>\$ 49°76 | "<br>2 48 88<br>2 48 90<br>2 47 98                                | "<br>2 48 ° 08<br>2 48 ° 16<br>2 47 ° 52 | $M = 48'' \cdot 90$<br>$w = 20 \cdot 13$<br>$\frac{1}{w} = 0 \cdot 05$<br>$C = 60^{\circ} 12' \cdot 48'' \cdot 00$ |
|             | 48.67                                               | 49°05                                    | 48.63                                                          | 48.70                                               | 49.89                                                         | 48.41                                                         | 49.73                                    | 49.38                                             | 48.59                                                             | 47 92                                    | 0 - 09 13 40 90                                                                                                    |
| LV & LVIII  | k 44 · 78<br>k 43 · 34<br>k 44 · 72<br>44 · 28      | 2 42.62<br>2 43.38<br>2 43.46<br>43.15   | 2 43.98<br>2 41.90<br>2 43.72<br>2 41.34<br>42.74              | 2 43 94<br>2 44 42<br>2 42 80<br>43 72              | h 42 · 30<br>h 43 · 34<br>h 43 · 92<br>43 · 19                | h 43°76<br>h 42°46<br>h 42°66<br>42°96                        | h 42 · 52<br>h 42 · 32<br>h 43 · 46      | h 43.80<br>h 42.86<br>h 42.70<br>43.12            | 2 43 <sup>.82</sup><br>2 44 <sup>.16</sup><br>2 43 <sup>.20</sup> | 2 43 90<br>2 44 36<br>2 43 36<br>43 87   | $M = 43'' \cdot 35$ $w = 24 \cdot 05$ $\frac{1}{w} = 0 \cdot 04$ $C = 70^{\circ} 4' 43'' \cdot 34$                 |
|             |                                                     |                                          |                                                                |                                                     |                                                               |                                                               |                                          |                                                   |                                                                   |                                          |                                                                                                                    |
| LVIII & XIX | h 17.82<br>h 16.50<br>l 16.14<br>h 16.02<br>d 18.14 | l 13.62<br>l 15.62<br>l 14.50<br>h 15.62 | l 14.38<br>l 15.74<br>l 14.30<br>h 14.14                       | l 14.68<br>l 17.74<br>l 17.62<br>l 17.76<br>l 17.00 | h 14 · 18<br>h 17 · 40<br>h 14 · 22<br>h 14 · 52<br>h 13 · 62 | h 15.06<br>h 19.00<br>h 14.76<br>h 17.38<br>h 16.30           | h 15.86<br>h 15.68<br>h 17.72<br>h 16.26 | h 15°20<br>h 15°98<br>h 16°04                     | l 15°34<br>l 15°48<br>l 16°52                                     | l 15°58<br>l 16°26<br>l 15°86            | $M = 15'' \cdot 85$ $w = 10 \cdot 06$ $\frac{1}{w} = 0 \cdot 10$                                                   |
|             | 16.95                                               | 14.84                                    | 14.64                                                          | 16.96                                               | 14.29                                                         | 16.20                                                         | 16.38                                    | 15.24                                             | 15.78                                                             | 15.90                                    | $C = 65^{\circ} 57' 15'' \cdot 86$                                                                                 |
| XIX & XXI   | h 42.62<br>h 44.20<br>l 42.00<br>l 43.74<br>d 44.66 | 2 45°96<br>2 45°06<br>2 45°90            | l 44 °08<br>l 44 °92<br>l 44 °32<br>k 43 °18                   | l 43.82<br>l 44.70<br>l 42.80<br>l 45.46            | h 47°24<br>h 44°72<br>h 44°98<br>h 45°30                      | h 43 · 82<br>h 45 · 90<br>h 44 · 46<br>h 46 · 20              | h 44°64<br>h 44°76<br>h 44°22            | h 42°72<br>h 44°80<br>h 44°44<br>h 44°60          | l 44°10<br>l 44°34<br>l 43°60                                     | l 43°94<br>l 43°60<br>l 44°66            | $M = 44'' \cdot 48$ $w = 14 \cdot 37$ $\frac{1}{w} = 0 \cdot 07$                                                   |
|             | 43.44                                               | 45.64                                    | 44.13                                                          | 44.19                                               | 45.26                                                         | 45.10                                                         | 44°54                                    | 44.14                                             | 44.01                                                             | 44°07                                    | $\tilde{C} = 73^{\circ} 52' 44'' \cdot 47$                                                                         |
| XXI & LVII  | k 25.88<br>k 26.96<br>l 25.50                       | l 27.30<br>l 28.38<br>l 28.76<br>h 27.70 | l 29 48<br>l 29 74<br>l 31 14<br>h 27 36<br>h 27 92<br>h 26 00 | l 27°40<br>l 25°02<br>l 27°22<br>l 27°16            | k 24 ° 96<br>k 27 ° 00<br>k 26 ° 88<br>k 25 ° 28              | h 28 · 22<br>h 25 · 08<br>h 26 · 44<br>h 26 · 36<br>h 28 · 36 | h 26 ° 00<br>h 27 ° 00<br>h 26 ° 76      | k 26 · 50<br>k 26 · 70<br>k 28 · 64<br>k 27 · 56  | l 25·32<br>l 26·40<br>l 26·08                                     | 2 27 · 32<br>2 26 · 64<br>2 26 · 74      | $M = 26'' \cdot 91$ $w = 9 \cdot 70$ $\frac{1}{w} = 0 \cdot 10$                                                    |
|             | 26.11                                               | 28.04                                    | 28.01                                                          | 26.70                                               | 26.03                                                         | 26.89                                                         | 26.29                                    | 27.35                                             | 25.93                                                             | <b>2</b> 6.90                            | $U = 80^{\circ} 51^{\circ} 26^{\circ} 94$                                                                          |

NOTE.-Stations\_XIX and XXI appertain to the Sutlej Series.

#### At XIX (Kaimsir)

January 1876; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle       |                                                                    | Circle readings, telescope being set on XXI |                                    |                                    |                                                     |                                 |                                               |                                          |                                                       |                                                          |                                                                  |  |  |  |
|-------------|--------------------------------------------------------------------|---------------------------------------------|------------------------------------|------------------------------------|-----------------------------------------------------|---------------------------------|-----------------------------------------------|------------------------------------------|-------------------------------------------------------|----------------------------------------------------------|------------------------------------------------------------------|--|--|--|
| between     | 251° 41′                                                           | 71° 40′                                     | <b>83</b> 0° <b>58′</b>            | 150° 52′                           | 50° 4′.                                             | 230° 4′                         | 129° 16′                                      | <b>3</b> 09° 16′                         | 208° 29′                                              | <b>28° 29'</b>                                           | w = Relative Weight<br>C = Concluded Angle                       |  |  |  |
| XXI & LIX   | "<br>k 23 · 18<br>k 26 · 84<br>l 25 · 36<br>l 23 · 84<br>l 23 · 12 | "<br>l 25°28<br>l 23°66<br>l 25°70          | "<br>l 22°42<br>l 23°06<br>l 24°24 | "<br>l 23·44<br>l 23·82<br>k 25·26 | "<br>h 25°24<br>h 25°20<br>k 24°66                  | "<br>k25°14<br>k24°34<br>l24°10 | "<br>l 23°42<br>l 25°52<br>l 24°08<br>l 24°84 | "<br>  23 • 44<br>  25 • 38<br>  25 • 18 | "<br>h 25 ° 28<br>h 24 ° 32<br>h 23 ° 66<br>h 24 ° 18 | "<br>h 25°90<br>h 25°74<br>h 26°92<br>h 25°64<br>h 23°32 | $M = 24'' \cdot 53$ $w = 16 \cdot 74$ $\frac{1}{w} = 0 \cdot 06$ |  |  |  |
|             | 24.47                                                              | 24.88                                       | 23.24                              | 24.17                              | 25.03                                               | 24.53                           | 24.47                                         | 24.67                                    | 24.30                                                 | 25.20                                                    | $C = 55^{\circ} 53^{\circ} 24^{\circ} .55$                       |  |  |  |
| LIX & LVIII | k 28°44<br>k 29°28<br>k 29°18                                      | h 29°14<br>h 31°24<br>h 27°82<br>h 28°38    | h 28°44<br>h 28°16<br>h 29°76      | h 27°94<br>h 28°10<br>h 28°08      | h 26.88<br>h 29.76<br>h 29.92<br>l 29.76<br>l 28.36 | h 28°74<br>h 30°36<br>l 29°42   | l 30°22<br>l 30°30<br>l 29°24                 | l 29°08<br>l 29°60<br>l 29°60            | k 28°18<br>k 28°34<br>k 28°74                         | k 30°22<br>k 28°52<br>k 29°80                            | $M = 29'' \cdot 07$ $w = 20 \cdot 18$ $\frac{1}{w} = 0 \cdot 05$ |  |  |  |
|             | 28.97                                                              | 29.15                                       | 28.79                              | 28.04                              | 28.94                                               | 29.51                           | 29.92                                         | 29.43                                    | 28.42                                                 | 29.51                                                    | $C = 52^{\circ} 26' 29'' \cdot 07$                               |  |  |  |

At XXI (Kanda) ·

December 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle      |                                               |                                                                      |                               | M = Mean of Groups            |                                               |                                          |                                    |                               |                                                          |                                    |                                                                  |
|------------|-----------------------------------------------|----------------------------------------------------------------------|-------------------------------|-------------------------------|-----------------------------------------------|------------------------------------------|------------------------------------|-------------------------------|----------------------------------------------------------|------------------------------------|------------------------------------------------------------------|
| between    | 273° 40′                                      | 98° 40′                                                              | <b>85</b> 3° 52'              | 172° 52′                      | 72° 5′                                        | <b>25</b> 2° 5′                          | 151° 16'                           | 331° 16′                      | 230° 28′                                                 | 50° 28′                            | c - Kelative Weight<br>C - Concluded Angle                       |
| LVII & LIX | "<br>k 15°74<br>k 16°66<br>k 18°08<br>k 16°20 | "<br>k 16 98<br>k 18 10<br>k 18 02                                   | "                             | "<br>17.58<br>17.42<br>18.08  | "<br>h 16°28<br>h 18°20<br>k 16°96<br>l 15°52 | "<br>h 17 ° 46<br>h 17 ° 26<br>h 16 ° 02 | "<br>k 18.66<br>h 17.92<br>k 17.90 | "                             | "<br>k 17 °08<br>k 16 °74<br>k 18 °06                    | n<br>h 16°64<br>h 15°92<br>h 18°16 | $M = 17'' \cdot 25$ $w = 23 \cdot 39$ $\frac{1}{w} = 0 \cdot 04$ |
|            | 16.62                                         | 17.70                                                                | 17.71                         | 17.69                         | 16.4                                          | 16.01                                    | 18.10                              | 16.44                         | 17.29                                                    | 16.91                              | $C = 36^{\circ} 6' 17'' \cdot 23$                                |
| LIX & XIX  | l 49°36<br>l 50°00<br>l 49°20                 | l 49 <sup>.</sup> 88<br>l 49 <sup>.</sup> 10<br>l 50 <sup>.</sup> 14 | l 49°08<br>l 49°10<br>l 50°00 | l 50°54<br>l 50°52<br>l 49°74 | h 50°56<br>h 50°88<br>h 49°14                 | h 48°54<br>h 48°24<br>h 49°68            | l 50°42<br>l 50°12<br>l 50°80      | l 50°90<br>l 49°89<br>l 49°68 | h 51 °70<br>h 48 °58<br>h 48 °74<br>l 48 °56<br>l 47 °78 | h 50°00<br>h 49°20<br>h 49°94      | $M = 49'' \cdot 73$ $w = 22 \cdot 09$ $\frac{1}{w} = 0 \cdot 05$ |
|            | 49.52                                         | 49.71                                                                | 49:39                         | 50.37                         | 50.19                                         | 48.82                                    | 50.45                              | 50.13                         | 49`07                                                    | 49.21                              | $C = 50^{\circ} 13' 49'' 72$                                     |

NOTE.-Stations XIX and XXI appertain to the Sutlej Series.

J. B. M. HENNESSEY, In charge of Computing Office.

**August** 1878.



# At LIX (Randu)

December 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle<br>between | 0°0′                                                | 180° 0'                                          | Cir<br>79°13′                                                  | cle readin<br>259° 13′                              | gs, telesc<br>158° 24'                                        | ope being<br>338° 24'                                         | set on L<br>237° 36'                     | VII<br>57°36'                                                                 | <b>816° 4</b> 9′                   | 136° 49'                                 | M - Mean of Groups<br>w - Relative Weight<br>C - Concluded Angle  |
|------------------|-----------------------------------------------------|--------------------------------------------------|----------------------------------------------------------------|-----------------------------------------------------|---------------------------------------------------------------|---------------------------------------------------------------|------------------------------------------|-------------------------------------------------------------------------------|------------------------------------|------------------------------------------|-------------------------------------------------------------------|
| LVII & LV        | "<br>k 48 · 68<br>k 49 · 26<br>l 48 · 06            | "<br>l 49`54<br>l 48`30<br>l 49`30               | "<br>2 48·52<br>2 49·46<br>2 47·90                             | "<br>2 48.66<br>2 47.88<br>2 49.56                  | "<br>h 49°56<br>h 50°96<br>h 49°14                            | "<br>h 48 • 42<br>h 47 • 82<br>h 49 • 00                      | "<br>h 49°26<br>h 50°08<br>h 49°84       | "<br><b>h</b> 50° 28<br><b>h</b> 48° 00<br><b>h</b> 49° 48<br><b>h</b> 49° 76 | "<br>2 48 88<br>2 48 90<br>2 47 98 | "<br>l 48.08<br>l 48.16<br>l 47.52       | $M = 48'' \cdot 90$ $w = 20 \cdot 13$ $\frac{1}{w} = 0 \cdot 05$  |
|                  | 48.67                                               | 49.02                                            | 48.63                                                          | 48.70                                               | 49.89                                                         | 48.41                                                         | 49`73                                    | 49.38                                                                         | 48.29                              | 47°9 <b>2</b>                            | $C = 69^{\circ} 13' 48'' \cdot 90$                                |
| LV & LVIII       | h 44°78<br>h 43°34<br>h 44°72                       | l 42.62<br>l 43.38<br>l 43.46                    | 2 43 98<br>2 41 90<br>2 43 72<br>2 41 34                       | l 43°94<br>l 44°42<br>l 42°80                       | h 42°30<br>h 43°34<br>h 43°92                                 | h 43 · 76<br>h 42 · 46<br>h 42 · 66                           | h 42 · 52<br>h 42 · 32<br>h 43 · 46      | h 43 · 80<br>h 42 · 86<br>h 42 · 70                                           | l 43.82<br>l 44.16<br>l 43.20      | l 43·90<br>l 44·36<br>l 43·36<br>l 43·36 | $M = 43'' \cdot 35$ $w = 24 \cdot 05$ $\frac{1}{20} = 0 \cdot 04$ |
|                  | 44 • 28                                             | 43.12                                            | 42.74                                                          | 43.72                                               | 43.19                                                         | <b>42</b> •96                                                 | <b>42</b> .77                            | 43.12                                                                         | 43.73                              | 43.87                                    | $C = 70^{\circ} 4' 43'' \cdot 34$                                 |
| LVIII & XIX      | h 17.82<br>h 16.50<br>l 16.14<br>h 16.02<br>d 18.14 | l 13.62<br>l 15.62<br>l 14.50<br>h 15.62         | l 14°38<br>l 15°74<br>l 14°30<br>h 14°14                       | l 14.68<br>l 17.74<br>l 17.62<br>l 17.76<br>l 17.00 | h 14 · 18<br>h 17 · 40<br>h 14 · 22<br>h 14 · 52<br>h 13 · 62 | h 15.06<br>h 19.00<br>h 14.76<br>h 17.38<br>h 16.30           | h 15.86<br>h 15.68<br>h 17.72<br>h 16.26 | h 15 ° 20<br>h 15 ° 98<br>h 16 ° 04                                           | l 15.34<br>l 15.48<br>l 16.52      | l 15.58<br>l 16.26<br>l 15.86            | $M = 15'' \cdot 85$ $w = 10 \cdot 06$ $\frac{1}{w} = 0 \cdot 10$  |
|                  | 16.93                                               | 14.84                                            | 14.64                                                          | 16.96                                               | 14.29                                                         | 16.20                                                         | 16.38                                    | 15.24                                                                         | 15.78                              | 15.90                                    | $\tilde{C} = 65^{\circ} 57' 15'' \cdot 86$                        |
| XIX & XXI        | h 42.62<br>h 44.20<br>l 42.00<br>l 43.74<br>d 44.66 | l 45°96<br>l 45°06<br>l 45°90                    | l 44.08<br>l 44.92<br>l 44.32<br>k 43.18                       | l 43.82<br>l 44.70<br>l 42.80<br>l 45.46            | h 47°24<br>h 44°72<br>h 44°98<br>h 45°30                      | h 43 82<br>h 45 90<br>h 44 46<br>h 46 20                      | h 44°64<br>h 44°76<br>h 44°22            | h 42.72<br>h 44.80<br>h 44.44<br>h 44.60                                      | l 44°10<br>l 44°34<br>l 43°60      | l 43°94<br>l 43°60<br>l 44°66            | $M = 44'' \cdot 48$ $w = 14 \cdot 37$ $\frac{1}{m} = 0 \cdot 07$  |
|                  | 43.44                                               | 45.64                                            | 44.13                                                          | 44.19                                               | 45.26                                                         | 45'10                                                         | 44.24                                    | 44.14                                                                         | 44.01                              | 44.07                                    | $\tilde{C} = 73^{\circ} 52' 44'' \cdot 47$                        |
| XXI & LVII       | k 25 · 88<br>k 26 · 96<br>l 25 · 50                 | l 27 · 30<br>l 28 · 38<br>l 28 · 76<br>h 27 · 70 | l 29 48<br>l 29 74<br>l 31 14<br>h 27 36<br>h 27 92<br>h 26 00 | l 27 · 40<br>l 25 · 02<br>l 27 · 22<br>l 27 · 16    | k 24 ° 96<br>k 27 ° 00<br>k 26 ° 88<br>k 25 ° 28              | h 28 · 22<br>h 25 · 08<br>h 26 · 44<br>h 26 · 36<br>h 28 · 36 | h 26 °00<br>h 27 °00<br>h 26 °76         | <b>Å 26</b> · 50<br><b>Å 26</b> · 70<br><b>Å 28</b> · 64<br><b>Å 27 · 56</b>  | l 25°32<br>l 26°40<br>l 26°08      | l 27·32<br>l 26·64<br>l 26·74            | $M = 26'' \cdot 91$ $w = 9 \cdot 70$ $\frac{1}{w} = 0 \cdot 10$   |
|                  | 26.11                                               | 28.04                                            | 28.01                                                          | 26.70                                               | 26.03                                                         | 26.89                                                         | <b>2</b> 6.59                            | 27.35                                                                         | 25.93                              | <b>2</b> 6.90                            | $U = 80^{\circ} 51^{\circ} 26^{\circ} 94$                         |

Norg.-Stations\_XIX and XXI appertain to the Sutlej Series.
### At XIX (Kaimsir)

January 1876; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle       |                                                                                                       |                                          |                                    | M - Mean of Groups                 |                                                     |                                          |                                                       |                                          |                                                       |                                                                    |                                                                                                     |
|-------------|-------------------------------------------------------------------------------------------------------|------------------------------------------|------------------------------------|------------------------------------|-----------------------------------------------------|------------------------------------------|-------------------------------------------------------|------------------------------------------|-------------------------------------------------------|--------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------|
| between     | <b>251° 41′</b>                                                                                       | 71° <b>40′</b>                           | <b>83</b> 0° <b>58′</b>            | 150° 52'                           | 50° 4′                                              | <b>230° 4′</b>                           | 129°16′                                               | 309° 16′                                 | 208° 29′                                              | 28° 29′                                                            | w - Relative Weight<br>C - Concluded Angle                                                          |
| XXI & LIX   | "<br><b>h</b> 23 · 18<br><b>h</b> 26 · 84<br><i>l</i> 25 · 36<br><i>l</i> 23 · 84<br><i>l</i> 23 · 12 | "<br>  25°28<br>  23°66<br>  25°70       | "<br>  22°42<br>  23°06<br>  24°24 | "<br>  23°44<br>  23°82<br>  25°26 | "<br>h 25°24<br>h 25°20<br>k 24°66                  | "<br>k 25 ° 14<br>k 24 ° 34<br>l 24 ° 10 | "<br>  23 • 42<br>  25 • 52<br>  24 • 08<br>  24 • 84 | "<br>2 23 ° 44<br>2 25 ° 38<br>2 25 ° 18 | "<br>h 25 ° 28<br>h 24 ° 32<br>h 23 ° 66<br>h 24 ° 18 | "<br>h 25 ° 90<br>h 25 ° 74<br>h 26 ° 92<br>h 25 ° 64<br>h 23 ° 32 | $M = 24'' \cdot 53$ $w = 16 \cdot 74$ $\frac{1}{w} = 0 \cdot 06$ $C = 55^{\circ} 52' 24'' \cdot 55$ |
|             | 24.47                                                                                                 | 24.88                                    | 23.24                              | 24.17                              | 25.03                                               | 24.53                                    | 24.47                                                 | 24.67                                    | 24.30                                                 | 25.20                                                              | 0 = 55 53 24 55                                                                                     |
| LIX & LVIII | k 28°44<br>k 29°28<br>k 29°18                                                                         | h 29°14<br>h 31°24<br>h 27°82<br>h 28°38 | h 28°44<br>h 28°16<br>h 29°76      | h 27°94<br>h 28°10<br>h 28°08      | h 26.88<br>h 29.76<br>h 29.92<br>l 29.76<br>l 28.36 | k 28°74<br>k 30°36<br>l 29°42            | l 30°22<br>l 30°30<br>l 25°24                         | l 29°08<br>l 29°60<br>l 29°60            | k 28°18<br>k 28°34<br>k 28°74                         | k 30°22<br>k 28°52<br>k 29°80                                      | $M = 29'' \cdot 07$ $w = 20 \cdot 18$ $\frac{1}{w} = 0 \cdot 05$                                    |
|             | 28.97                                                                                                 | 29.15                                    | 28.79                              | 28.04                              | 28.94                                               | 29.51                                    | 29`92                                                 | 29.43                                    | 28.42                                                 | 29.51                                                              | $C = 52^{\circ} 26' 29'' \cdot 07$                                                                  |

## At XXI (Kanda) ·

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December 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

| Angle      |                                               |                                       | Cir                                        | rcle readir                        | ngs, telesc                                   | ope being                                | set on L                           | VII                                                   |                                                          |                                    | M - Mean of Groups                                               |  |
|------------|-----------------------------------------------|---------------------------------------|--------------------------------------------|------------------------------------|-----------------------------------------------|------------------------------------------|------------------------------------|-------------------------------------------------------|----------------------------------------------------------|------------------------------------|------------------------------------------------------------------|--|
| between    | 273° 40′                                      | 98° 40′                               | <b>852°</b> 52′                            | 172° 52′                           | 72° 5′                                        | 252° 5′                                  | 151° 16'                           | 331°16′                                               | <b>230° 28′</b>                                          | 50° 28′                            | $\omega$ = Relative Weight<br>C = Concluded Angle                |  |
| LVII & LIX | "<br>k 15.74<br>k 16.66<br>k 18.08<br>k 16.20 | "<br>\$ 16.98<br>\$ 18.10<br>\$ 18.02 | "<br>h 17°94<br>h 16°82<br>h 18°3 <b>8</b> | "<br>7 17`58<br>7 17`42<br>7 18`08 | "<br>h 16·28<br>h 18·20<br>h 16·96<br>l 15·52 | "<br>h 17 • 46<br>h 17 • 26<br>h 16 • 02 | "<br>k 18.66<br>k 17.92<br>k 17.90 | "<br>h 16 · 84<br>h 15 · 82<br>h 17 · 18<br>h 17 · 24 | "<br>k 17 ° 08<br>k 16 ° 74<br>k 18 ° 06                 | "<br>h 16°64<br>h 15°92<br>h 18°16 | $M = 17'' \cdot 25$ $w = 23 \cdot 39$ $\frac{1}{w} = 0 \cdot 04$ |  |
|            | 10.62                                         | 17.20                                 | 17.71                                      | 17.69                              | 16.44                                         | 16.01                                    | 18.10                              | 16.22                                                 | 17.29                                                    | 16.01                              | $C = 36^{\circ} 6' 17'' \cdot 23$                                |  |
| LIX & XIX  | l 49°36<br>l 50°00<br>l 49°20                 | l 49.88<br>l 49.10<br>l 50.14         | l 49°08<br>l 49°10<br>l 50°00              | l 50°54<br>l 50°52<br>l 49°74      | h 50°56<br>h 50°88<br>h 49°14                 | h 48°54<br>h 48°24<br>h 49°68            | l 50°42<br>l 50°12<br>l 50°80      | l 50°90<br>l 49°89<br>l 49°68                         | h 51 °70<br>h 48 °58<br>h 48 °74<br>l 48 °56<br>l 47 °78 | k 50°00<br>k 49°20<br>k 49°94      | $M = 49'' \cdot 73$ $w = 22 \cdot 09$ $\frac{1}{w} = 0 \cdot 05$ |  |
|            | 49*52                                         | 4 <u>9</u> .71                        | 49:39                                      | 50.27                              | 50.10                                         | 48.82                                    | 50.42                              | 50.13                                                 | 49`07                                                    | 49°71                              | $C = 50^{\circ} 13' 49'' \cdot 72$                               |  |

Nors.-Stations XIX and XXI appertain to the Sutlej Series.

**August** 1878.

J. B. M. HENNESSEY, In charge of Computing Office.

**61** 



Sums of Squares of Apparent Errors of Single Observations, and of Apparent Errors of Single Zeros.

| Station of<br>Observation. | Observed Angle. | Number of<br>Observa-<br>tions. | Sum of Squares of<br>Errors of single<br>Observations. | Number of<br>Zeros. | Sum of Squares of<br>Errors of single<br>Zeros. | Remarks.               |
|----------------------------|-----------------|---------------------------------|--------------------------------------------------------|---------------------|-------------------------------------------------|------------------------|
| XLI                        | XLIV & I        | 34                              | 15.37                                                  | 10                  | 4`47                                            | ]                      |
| 33                         | I&II            | 32                              | 18.78                                                  | 10                  | <b>2</b> ·76                                    |                        |
| XLIV                       | I & II          | 36                              | 25.52                                                  | IO                  | 4-18                                            |                        |
| ,,                         | II & XLI        | 37                              | 26.53                                                  | 10                  | 3.33                                            |                        |
| I                          | IV & III        | 36                              | 45.23                                                  | ю                   | 5·4 <b>2</b>                                    |                        |
| ,,                         | III & II        | 32                              | 8.33                                                   | 10                  | 6.22                                            |                        |
| 27                         | II & XLI        | 39                              | 40°69                                                  | 10                  | 3.69                                            |                        |
| 37                         | XLI & XLIV      | 41                              | 41.82                                                  | 10                  | 5.71                                            |                        |
| 11                         | XLI & XLIV      | 37                              | 33.10                                                  | 10                  | 1.94                                            |                        |
| <b>2</b> 7                 | XLIV & I        | 38                              | 22.12                                                  | 10                  | 3.24                                            |                        |
| 27                         | I & III         | 38                              | <b>2</b> 9'54                                          | 10                  | <b>4</b> °49                                    | Barrow's 24 inch Mr. G |
| "                          | III & V         | 36                              | 18.27                                                  | 10                  | 4.52                                            | Darrow 8 24-men No. 2. |
| III                        | VI & VII        | 36                              | 28.10                                                  | 10                  | 2.76                                            |                        |
| <b>3</b> 7                 | VII & V         | 38                              | 17.40                                                  | 10                  | 3.28                                            |                        |
| 37                         | V & 11          | 34                              | 16.22                                                  | 10                  | 6.00                                            |                        |
| <b>2</b> 7                 | II & I          | 31                              | 8.11                                                   | 10                  | 2.39                                            |                        |
| · <b>))</b>                | I & IV          | 34                              | <b>2</b> 4'66                                          | 10                  | 1.85                                            |                        |
| **                         | IV & VI         | 37                              | 36.60                                                  | 10                  | 2.20                                            |                        |
| IV                         | VI & III        | 33                              | 23.77                                                  | 10                  | 6.29                                            |                        |
| "                          | III & I         | 33                              | 14.20                                                  | 10                  | 5.28                                            |                        |
| v                          | II & III        | 33                              | 20.81                                                  | 10                  | 1.39                                            |                        |
| 22                         | III & VII       | 35                              | 15.24                                                  | 10                  | 5'74                                            | J                      |

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Norz.-Stations XLI and XLIV appertain to the Karachi Longitudinal Series.

## SUMS OF SQUARES OF APPARENT ERRORS.

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| Station of<br>Observation. | Observed Angle. | Number of<br>Observa-<br>tions. | Sum of Squares of<br>Errors of single<br>Observations. | Number of<br>Zeros.<br>Sum of Squares of<br>Errors of single<br>Zeros. |              | Remarks.                |
|----------------------------|-----------------|---------------------------------|--------------------------------------------------------|------------------------------------------------------------------------|--------------|-------------------------|
| VI                         | IX & VIII       | 32                              | 9.26                                                   | 10                                                                     | 3.32         |                         |
| 12                         | VIII & VII      | 32                              | 20.24                                                  | io                                                                     | 3.67         |                         |
| 33                         | VII & III       | 34                              | 16.03                                                  | 10                                                                     | 1.42         |                         |
| >>                         | III & IV        | 35                              | 19.90                                                  | 10                                                                     | 2.72         |                         |
| VII                        | V & 111         | 36                              | 24.74                                                  | 10                                                                     | 1.72         |                         |
| <b>9</b> 7                 | III & VI        | 35                              | 16.97                                                  | 10                                                                     | 1.10         |                         |
| ,,                         | VI & VIII       | <b>3</b> 6 ·                    | 22.10                                                  | 10                                                                     | 5.23         |                         |
| ,,                         | VIII & X        | 36                              | , 20.92                                                | 10                                                                     | <b>4</b> ·88 |                         |
| VIII                       | VII & VI        | 35                              | 17.37                                                  | 10 .                                                                   | 3.20         |                         |
| <b>3</b> 7                 | VI & IX         | 34                              | 15.71                                                  | 10                                                                     | 4'74         |                         |
| ,,                         | IX & XI         | 36                              | 27.72                                                  | 10                                                                     | 5'24         |                         |
| <b>2</b> 7                 | XI & XII        | 35                              | 23.87                                                  | 10                                                                     | 4.44         |                         |
| >>                         | XII & X         | 33                              | 20.92                                                  | 10                                                                     | 1.94         |                         |
| <b>3</b> 9                 | X & VII         | 36                              | 34'95                                                  | 10                                                                     | 1.42         |                         |
| IX v                       | XI & VIII       | 32                              | 16.70                                                  | 10                                                                     | 1.40         |                         |
| 23                         | VIII & VI       | 38                              | 37.09                                                  | 10                                                                     | 1.46         |                         |
| . <b>X</b>                 | VII & VIII      | 30                              | 10.01                                                  | 10                                                                     | 1'44         |                         |
| "                          | VIII & XII      | 35                              | 23.07                                                  | 10                                                                     | I.53         |                         |
| XI                         | XIV & XIII      | 31                              | 14.65                                                  | 10                                                                     | 5.77         |                         |
| "                          | XIII & XII      | 31                              | 12.31                                                  | 10                                                                     | 1.15         |                         |
| "                          | XII & VIII      | 37                              | 25.69                                                  | 10                                                                     | <b>2</b> .88 | Barrow's 24-inch No. 2. |
| "                          | VIII & IX       | 35                              | 12.58                                                  | 10                                                                     | 2.33         |                         |
| XII                        | X & VIII        | 33                              | 21.53                                                  | 10                                                                     | 2.39         |                         |
| "                          | VIII & XI       | 30                              | 11.20                                                  | 10                                                                     | 2.37         |                         |
| "                          | XI & XIII       | 36                              | 27.99                                                  | 10                                                                     | 3.37         |                         |
| "                          | XIII & XV       | 34                              | 20.66                                                  | 10                                                                     | 8.63         |                         |
| XIII                       | XII & XI        | 31                              | 12.39                                                  | 10                                                                     | 3.49         | · ·                     |
| >>                         | XI & XIV        | 33                              | 16.28                                                  | 10                                                                     | 2.06         |                         |
| >>                         | XIV & XVI       | 34                              | 20.47                                                  | 10                                                                     | 3.02         |                         |
| "                          | XVI & XVII      | 31                              | 11.88                                                  | 10                                                                     | 3.33         |                         |
| "                          | XVII & XV       | 31                              | 15.17                                                  | 10                                                                     | 2.03         |                         |
| "                          | XV & XII        | 32                              | 15.53                                                  | 10                                                                     | 4.08         |                         |
| XIV                        | XVI & XIII      | 35                              | 24.47                                                  | 10                                                                     | 5.16         |                         |
| "                          | XIII & XI       | 31                              | 11.64                                                  | 10                                                                     | 3.42         |                         |
| xv                         | XII & XIII      | 34                              | 21.77                                                  | 10                                                                     | 3.93         |                         |
| "                          | XIII & XVII     | 34                              | 19.09                                                  | 10                                                                     | <b>3</b> .60 |                         |
| XVI                        | XIX & XVIII     | 30                              | 8.70                                                   | 10                                                                     | 4.77         |                         |
| <b>3</b> 3                 | XVIII & XVII    | 32                              | 11.31                                                  | 10                                                                     | 4.09         |                         |
| "                          | XVII & XIII     | 32                              | 7.57                                                   | 10                                                                     | 2.12         |                         |
| "                          | XIII & XIV      | 31                              | 13.07                                                  | 10                                                                     | 1.12         |                         |
| XVII                       | XV & XIII       | 32                              | 10.00                                                  | 10                                                                     | 2.48         |                         |

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| Station of<br>Observation.              | Observed Angle. | Number of<br>Observa-<br>tions. | Sum of Squares of<br>Errors of single<br>Observations. | f Number of Sum of Squares of Errors of single Zeros. |       | Remarks.                |
|-----------------------------------------|-----------------|---------------------------------|--------------------------------------------------------|-------------------------------------------------------|-------|-------------------------|
| XVII                                    | XIII&XVI        | 33                              | 14-35                                                  | 10                                                    | 1.62  |                         |
| "                                       | XVI & XVIII     | 31                              | 12.37                                                  | 10                                                    | 4-53  | !                       |
| "                                       | XVIII & XX      | 32                              | 16.60                                                  | 10                                                    | 3-83  |                         |
| XVIII                                   | XXI & XXII      | 32                              | 17.37                                                  | 10                                                    | 0.92  |                         |
| "                                       | XXII & XX       | 30                              | 8.19                                                   | 10                                                    | 1.13  | 1                       |
| <b>n</b> .                              | XX & XVII       | 30                              | 7'32                                                   | 10                                                    | 2.32  |                         |
| "                                       | XVII & XVI      | 31                              | 7'34                                                   | ю                                                     | 1.50  | '                       |
| "                                       | XVI & XIX       | 31                              | 9.92                                                   | 10                                                    | 1.01  | /                       |
| "                                       | XIX & XXI       | 31                              | 8.47                                                   | 10                                                    | 7.79  |                         |
| XIX .                                   | XXI & XVIII     | 30                              | 9.21                                                   | 10                                                    | 1.40  | ''                      |
| "                                       | XVIII & XVI     | 30                              | 3.61                                                   | 10                                                    | 3.87  |                         |
| XX                                      | XVII & XVIII    | 32                              | 17.98                                                  | 10                                                    | 4.73  | 11 ,                    |
| , , I                                   | XVIII & XXII    | 30                              | 7.01                                                   | 10                                                    | 5.20  |                         |
| XXI                                     | XXIII & XXIV    | 30                              | 7.13                                                   | 10                                                    | 3.29  |                         |
| ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | XXIV & XXII     | 33                              | 12.25                                                  | 10                                                    | 3.11  |                         |
| "                                       | XXII & XVIII    | · 32                            | 8.78                                                   | 10                                                    | 0.20  |                         |
| , ,,                                    | XVIII & XIX     | 34                              | 11.20                                                  | 10                                                    | 4.22  |                         |
| XXII                                    | XX & XVIII      | 32                              | 15.06                                                  | 10                                                    | 1.45  |                         |
| "                                       | XVIII & XXI     | 30                              | 5.51                                                   | 10                                                    | 5*24  |                         |
| <b>"</b>                                | XXI & XXIII     | 31                              | 9.84                                                   | 10                                                    | 5.89  |                         |
| , , ,                                   | XXIII & XXIV    | 30                              | 10.26                                                  | 10                                                    | 4-14  | Barrow's 24-inch No. 2. |
| XXIII                                   | XXV & XXVI      | 34                              | 21.40                                                  | 10                                                    | 1.72  |                         |
| <b>"</b>                                | XXVI & XXIV     | 33                              | 19.48                                                  | 10                                                    | 7.43  |                         |
| , , , I                                 | XXIV & XXII     | 33                              | 12.20                                                  | 10                                                    | 5:30  |                         |
| ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | XXII & XXI      | 32                              | 13-86                                                  | 10                                                    | 2.67  |                         |
| XXIV                                    | XXII & XXI      | 32                              | 10.42                                                  | 10                                                    | 0.69  |                         |
| "                                       | XXI & XXIII     | 33                              | 12.05                                                  | 10                                                    | 2*55  |                         |
| "                                       | XXIII & XXV     | 32                              | 709                                                    | 10                                                    | 6.25  |                         |
| · "                                     | XXV & XXVI      | 33                              | 21-17                                                  | 10                                                    | 3.27  |                         |
| XXV                                     | XXVIII & XXVII  | 31                              | 14.18                                                  | 10                                                    | 5-81  |                         |
| "                                       | XXVII & XXVI    | 30                              | 7.72                                                   | 10                                                    | 4.37  |                         |
| ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | XXVI & XXIV     | 33                              | 18.60                                                  | 10                                                    | 1.42  |                         |
| ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | XXIV & XXIII    | 32                              | 14.03                                                  | 10                                                    | 1-81  |                         |
| XXVI                                    | XXIV & XXIII    | 30                              | 10-26                                                  | 10                                                    | 6.03  |                         |
|                                         | XXIII & XXV     | 30                              | 9-28                                                   | 10                                                    | 4-25  |                         |
| "                                       | XXV & XXVII     | 36                              | 25.85                                                  | 10                                                    | 3.94  |                         |
| "                                       | XXVII & R. M.   | 33                              | 13.70                                                  | 10                                                    | 2-13  |                         |
| "                                       | R.M. & XXIX     | 32                              | 18.90                                                  | 10                                                    | 2*96  |                         |
| XXVII                                   | XXIX & XXVI     | 33                              | 16.28                                                  | 10                                                    | 2.03  |                         |
| , ,,                                    | XXVI & XXV      | 30.                             | 10.11                                                  | 10                                                    | 1.98  |                         |
| "                                       | XXV & XXVIII    | 34                              | 20.13                                                  | 10                                                    | 2.73  |                         |
| , <sup>,</sup> ,                        | 1               | , . ,                           |                                                        | 1 '                                                   | · · · | j                       |

Nore.-R. M. denotes Referring Mark.

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## SUMS OF SQUARES OF APPARENT ERRORS.

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| Station of<br>Observation.              | Observed Angle. | Number of<br>Observa-<br>tions. | Sum of Squares of<br>Errors of single<br>Observations. | Number of<br>Zeros. | Sum of Squares of<br>Errors of single .<br>Zeros. | REMARKS.              |
|-----------------------------------------|-----------------|---------------------------------|--------------------------------------------------------|---------------------|---------------------------------------------------|-----------------------|
| XXVII                                   | XXVIII & XXX    | 33                              | 12.61                                                  | 10                  | 1.48                                              | )                     |
| 11                                      | XXX & XXXI      | 32                              | 10.63                                                  | 10                  | 1.82                                              |                       |
| "                                       | XXXI & XXIX     | 34                              | 16.62                                                  | 10                  | 2.80                                              |                       |
| XXVIII                                  | XXX & XXVII     | 36                              | 27.71                                                  | 10                  | 1.52                                              |                       |
| "                                       | XXVII & XXV     | 32                              | 15.83                                                  | 10                  | 1.12                                              |                       |
| XXIX                                    | XXVI & XXVII    | 33                              | 15.20                                                  | 10                  | 2.47                                              |                       |
| "                                       | XXVII & XXXI    | . 33                            | 13.40                                                  | . 10 .              | 4.41                                              |                       |
| XXX                                     | XXXIII & XXXII  | <b>3</b> 5                      | 26.44                                                  | 10                  | o <sup>.</sup> 80                                 |                       |
| R                                       | XXXII & XXXI    | 43                              | 57.35                                                  | 10                  | 9.63                                              |                       |
| *                                       | XXXI & XXVII    | 32                              | 7.63                                                   | 10                  | 6.92                                              |                       |
| , ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | XXVII & XXVIII  | 30                              | 6.61                                                   | 10                  | 4.13                                              |                       |
| XXXI                                    | XXIX & XXVII    | 31                              | 13.22                                                  | 10                  | 1.01                                              |                       |
| "                                       | XXVII & XXX     | 30                              | 4.68                                                   | 10                  | 10.86                                             |                       |
| 29                                      | XXX & XXXII     | 36                              | 30.89                                                  | 10                  | 4*85 .                                            |                       |
| n                                       | XXXII & XXXV    | 40                              | 68°0 <u>9</u>                                          | 10                  | 4.24                                              |                       |
| XXXII                                   | XXXV & XXXI     | 32                              | 12.32                                                  | 10                  | 2.92                                              |                       |
| n                                       | XXXI & XXX      | 39                              | 33.14                                                  | 10                  | 4.01                                              |                       |
| n                                       | XXX & XXXIII    | 38                              | 28.63                                                  | 10                  | 4.86                                              |                       |
| "                                       | XXXIII & XXXIV  | 38                              | 35.61                                                  | 10                  | 4.38                                              |                       |
| "                                       | XXXIV & XXXV    | 35                              | 28.38                                                  | 10                  | 2.30                                              | Barrow's 24 inch No 2 |
| XXXIII                                  | XXXIV & XXXII   | 36                              | . 41 * 22                                              | 10                  | 3.31                                              | Darrows 23-men No. 2. |
| "                                       | XXXII & XXX     | 36                              | 29.16                                                  | 10                  | 8.73                                              |                       |
| XXXIV                                   | XXXVII & XXXVI  | 33                              | 11.83                                                  | 10                  | 2.68                                              |                       |
| 79                                      | XXXVI & XXXV    | 43                              | 59.00                                                  | 10                  | 4.40                                              |                       |
| <i>n</i>                                | XXXV & XXXII    | 35                              | 22.17                                                  | 10                  | 2.81                                              |                       |
| >>                                      | XXXII & XXXIII  | 34                              | 32.12                                                  | 10                  | 3.00                                              | (                     |
| XXXV                                    | XXXI & XXXII    | 37                              | 34.80                                                  | 10                  | 5.42                                              |                       |
| 27                                      | XXXII & XXXIV   | 35                              | 30.13                                                  | 10                  | 3.38                                              |                       |
| n                                       | XXXIV & XXXVI   | 37                              | 34.49                                                  | 10                  | 6.47                                              |                       |
| ,,                                      | XXXVI & XXXVIII | 37                              | 29.21                                                  | IO                  | 3.07                                              |                       |
| XXXVI                                   | XXXV & XXXIV    | 36                              | 23.74                                                  | 10                  | 1.03                                              |                       |
| 'n                                      | XXXIV & XXXVII  | 42                              | 60°47                                                  | , <b>10</b>         | 6.23                                              |                       |
| "                                       | XXXVII & XXXIX  | 43                              | 44.24                                                  | 10                  | 6.98                                              |                       |
| , ,,                                    | XXXIX & XL      | 34                              | 19.09                                                  | 10                  | 6•48 ·                                            |                       |
| »                                       | XL & XXXVIII    | 35                              | 32.68                                                  | 10                  | 7.46                                              |                       |
| "                                       | XXXVIII & XXXV  | 41                              | 49.92                                                  | 10                  | 1.11                                              |                       |
| XXXVII                                  | XLI & XXXIX     | 38                              | 39.72                                                  | 10                  | 4.33                                              |                       |
| "                                       | XXXIX & XXXVI   | 39                              | 29.70                                                  | 10                  | 5.57                                              |                       |
| "                                       | XXXVI & XXXIV   | 43                              | 43.91                                                  | 10                  | 7:37                                              |                       |
| XXXVIII                                 | XXXV & XXXVI    | 37                              | 30.22                                                  | 10                  | 6.46                                              | .                     |
| "                                       | XXXVI & XL      | 36                              | 36.00                                                  | , 10                | 4.26                                              | J                     |

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| Station of<br>Observation. | Observed Angle. | Number of<br>Observa-<br>tions. | Sum of Squares of<br>Errors of single<br>Observations. | Number of<br>Zeros. | Sum of Squares of<br>Errors of single .<br>Zeros. | REMARKS.                                 |
|----------------------------|-----------------|---------------------------------|--------------------------------------------------------|---------------------|---------------------------------------------------|------------------------------------------|
| XXXIX                      | XLI & XLIII     | 38                              | 32.41                                                  | 10                  | 2.56                                              | <b>)</b>                                 |
| "                          | XLIII & XLIV    | 39                              | 33.35                                                  | 10                  | 2.98                                              |                                          |
| <b>39</b>                  | XLIV & XLII     | 40                              | 43.42                                                  | 10                  | 6.31 .                                            |                                          |
| 25                         | XLII & XL       | 39                              | 45.35                                                  | 10                  | 7.52                                              |                                          |
| "                          | XL & XXXVI      | 39                              | 34.69                                                  | 10                  | 10.84                                             |                                          |
| **                         | XXXVI & XXXVII  | 42                              | 69.49                                                  | IO                  | 10.89                                             |                                          |
| >>                         | XXXVII & XLI    | 44                              | 75.76                                                  | 10                  | 3.66                                              |                                          |
| XL                         | XXXVIII & XXXVI | 34                              | 16.36                                                  | 10                  | 5.33                                              |                                          |
| 39                         | XXXVI & XXXIX   | 37                              | <b>2</b> 4·99                                          | 10                  | 1.11                                              | 1.                                       |
| <b>23</b>                  | XXXIX & XLII    | 37                              | 23.73                                                  | 10                  | 4.31                                              |                                          |
| XLI                        | XLIII & XXXIX   | 41                              | 40.85                                                  | 10                  | 12.32                                             |                                          |
| 33                         | XXXIX & XXXVII  | 39                              | 47'33                                                  | 10                  | 8.84                                              |                                          |
| XLII                       | XL & XXXIX      | 43                              | 66·6 <b>8</b>                                          | 10                  | 3.41                                              |                                          |
| 22                         | XXXIX & XLIV    | 41                              | 53.32                                                  | 10                  | 8.08                                              | PT                                       |
| XLIII                      | R.M. & XLVI     | 31                              | 11.14                                                  | 10                  | 3.92                                              |                                          |
| н                          | XLVI & XLV      | 34                              | 14.44                                                  | 10                  | <b>2</b> °08                                      |                                          |
| 33                         | XLV & XLIV      | 39                              | 55.16                                                  | 10                  | <b>4</b> ·98                                      | (t                                       |
| n                          | XLIV & XXXIX    | 38                              | 23.44                                                  | 10                  | 4.33                                              | ~                                        |
| "                          | XXXIX & XLI     | 37                              | 33.77                                                  | 10                  | <b>3'43</b>                                       | 12                                       |
| XLIV                       | XLII & XXXIX    | 35                              | 21.53                                                  | 10                  | 3.24                                              | •                                        |
| n                          | XXXIX & XLIII   | 38                              | 23.23                                                  | 10                  | 4.73                                              | Barrow's 24-inch No. 2.                  |
| 22                         | XLIII & XLV     | 37                              | 26.34                                                  | 10                  | 3.92                                              |                                          |
| "                          | XLV & XLVII     | - 38                            | 48.69                                                  | 10                  | 4.23                                              |                                          |
| XL▼                        | XLVII & XLIV    | 36                              | 27.11                                                  | 10                  | 4.60                                              | · · ·                                    |
| <b>27</b>                  | XLIV & XLIII    | 32                              | 9.79                                                   | 10                  | 1.82                                              |                                          |
| 22                         | XLIII & XLVI    | . 30                            | 5.57                                                   | 10                  | 0.30                                              |                                          |
| "                          | XLVI & XLVIII   | 31                              | 12.24                                                  | 10                  | 2.02                                              | · · · ·                                  |
| "                          | XLVIII & XLIX   | 34                              | 18.42                                                  | . 10                | <b>3</b> .44                                      | ι.                                       |
| 32                         | XLIX & XLVII    | 38                              | 49.00                                                  | . 10                | 8.11                                              | с. — — — — — — — — — — — — — — — — — — — |
| XLVI                       | XLVIII & XLV    | 33                              | 25.33                                                  | 10                  | 10.01                                             |                                          |
| "                          | XLV & XLIII     | 34                              | 16.72                                                  | · 10                | 4'94                                              |                                          |
| XLVII                      | XLIV & XLV      | 34                              | 12.92                                                  | 10                  | 3.32                                              | 1*                                       |
| "                          | XLV & XLIX      | 33                              | 16.01                                                  | 10                  | 3*22 .                                            | e                                        |
| XLVIII                     | LI & L          | 38                              | 31.92                                                  | 10                  | IO'44                                             |                                          |
| "                          | L & XLIX        | 39                              | 30.18                                                  | . 10                | 10.62                                             | c.                                       |
|                            | XLIX & XLV      | 38                              | 42.35                                                  | 10                  | 3.36                                              |                                          |
| "                          | XLV & XLVI      | 37                              | 32.30                                                  | 10                  | 6.13                                              |                                          |
| XLIX                       | XLVII & XLV     | 34                              | 13:40                                                  | 10                  | 7'12                                              | e                                        |
| >9                         | XLV & XLVIII    | 31                              | <b>5</b> .69                                           | 10                  | 3.33                                              |                                          |
| »» ·                       | XLVIII & L      | 36                              | 20.88                                                  | 10                  | 5'32                                              |                                          |
| >>                         | L & LII         | 34                              | 22.00                                                  | 10                  | 4.28                                              | <b>)</b>                                 |

Norg.-R. M. denotes Referring Mark.

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### SUMS OF SQUARES OF APPARENT ERRORS.

| Station of<br>Observation.            | Observed Angle. | Number of<br>Observa-<br>tions. | Sum of Squares of<br>Errors of single<br>Observations. | Number of<br>Zeros. | Sum of Squares of<br>Errors of single<br>Zeros. | Remarks.                |
|---------------------------------------|-----------------|---------------------------------|--------------------------------------------------------|---------------------|-------------------------------------------------|-------------------------|
| L                                     | LII & XLIX      | 32                              | 12.46                                                  | 10                  | 4'04                                            | 1                       |
| **                                    | XLIX & XLVIII   | 34                              | 16.26                                                  | 10                  | . 2.77                                          |                         |
| . "                                   | XLVIII & LI     | 44                              | 59.50                                                  | 10                  | 6.39                                            |                         |
| r<br>33                               | LI & LIII       | 40                              | 29.00                                                  | 10                  | 3.39                                            |                         |
| , ,,                                  | LIII & LIV      | 45                              | 66.10                                                  | 10                  | 2.29                                            |                         |
| · · · ·                               | LIV & LII       | 34                              | 19'35                                                  | 10                  | 3.32                                            |                         |
| LI                                    | LIII & L        | 34                              | 17.42                                                  | <sup>.</sup> 10     | <b>3</b> .26                                    |                         |
| <b>39</b>                             | L & XLVIII      | 30                              | 4.23                                                   | 10                  | 1.64                                            |                         |
| LII                                   | XLIX & L        | 33                              | 16°08                                                  | 10                  | 3.06                                            |                         |
| >>                                    | · L & LIV       | 34                              | 17.59                                                  | 10                  | <b>3</b> .41                                    |                         |
| LIII                                  | LVI & LV        | 35                              | 26.39                                                  | 10                  | <b>3.</b> 01                                    |                         |
| "                                     | LV & LIV        | • 32                            | 16.22                                                  | 10                  | <b>2</b> .39                                    |                         |
| "                                     | LIV & L         | 37                              | 30.31                                                  | . 10                | 4.43                                            |                         |
|                                       | L & LI          | 33                              | 19.97                                                  | 10                  | 4.02                                            | -                       |
| LIV                                   | LII & L         | 35                              | 39.14                                                  | 10                  | 3.34                                            |                         |
| >>                                    | L & LIII        | 36                              | 20.39                                                  | 10                  | 2.32                                            |                         |
| · · · · · · · · · · · · · · · · · · · | LIII & LV       | 33                              | 16.32                                                  | 10                  | 7.13                                            |                         |
| · · ·                                 | LV & LVII       | 35                              | 23.42                                                  | 10                  | 5.37                                            |                         |
| LV                                    | LIX & LVII      | 33                              | 13.03                                                  | 10                  | 2.39                                            |                         |
| <b>33</b>                             | LVII & LIV      | 34                              | 15.93                                                  | 10                  | 1.01                                            |                         |
| ,<br>33                               | LIV & LIII      | 35                              | · 23·50 · ·                                            | 10                  | 4 63                                            | Barrow's 24-inch No. 2. |
| <b>33</b>                             | LIII & LVI      | 33                              | 16.27                                                  | 10                  | 2.33                                            |                         |
| 33                                    | LVI & LVIII     | 40                              | 61.93                                                  | 10                  | 2.27                                            |                         |
| 33                                    | LVIII & LIX     | 37                              | 42.86                                                  | 10                  | 5.85                                            |                         |
| LVI                                   | LVIII & LV      | 31                              | 13.30                                                  | 10                  | 4.96                                            |                         |
| , ,,                                  | LV & LIII       | 36                              | 20.63                                                  | 10                  | 9.84                                            | • • • •                 |
| LVII .                                |                 | 36                              | 15.23                                                  | 10                  | 3.88                                            |                         |
| 37                                    | LV & LIX        | 39                              | 40'97                                                  | 10                  | 4'11                                            |                         |
| , "                                   | LIX & XXI       | 34                              | 20.23                                                  | 10                  | 3.32                                            |                         |
| LVIII                                 | XIX & LIX       | 32                              | 12.03                                                  | 10                  | 1.40                                            |                         |
| n                                     | LIX & LV        | 31                              | 10.92                                                  | 10                  | 2.52                                            |                         |
| _ "                                   | LV & LVI        | 31                              | 9.88                                                   | 10                  | 1.22                                            |                         |
| LIX                                   | LVII & LV       | 31                              | 10'74                                                  | 10                  | 3.38                                            |                         |
| "                                     | LV & LVIII      | 31                              | 13.05                                                  | 10                  | <b>3</b> .39                                    |                         |
| "                                     | LVIII & XIX     | 41                              | 40'44                                                  | 10                  | 6.68                                            |                         |
| "                                     | XIX & XXI       | 37                              | 22.55                                                  | 10                  | 4.69                                            |                         |
| n                                     | XXI & LVII      | 39                              | 38.86                                                  | 10                  | 6.87                                            |                         |
| XIX                                   | XXI & LIX       | 36                              | 30.09                                                  | 10                  | 3.12                                            |                         |
| n                                     | LIX & LVIII     | 33                              | 19.42                                                  | 10                  | <b>2</b> .83                                    |                         |
| XXI                                   | LVII & LIX      | 33                              | 15.67                                                  | 10                  | 2.20                                            | 1                       |
| "                                     | LIX & XIX       | 32                              | 15.49                                                  | 10                  | <b>3</b> .61                                    | ן                       |

. Norz.-Stations XIX and XXI appertain to the Sutlej Series.

67.



From the preceding data of the sums of the squares of the apparent errors, in the measurement of each angle, we may ascertain the e.m.s. (error of mean square) of observation of a single measure of an angle, and the e.m.s. of graduation and observation of the mean of the measures on a single zero, for each group of angles measured with the same instrument, by the same observer, and under similar circumstances.

The instrument employed was Barrow's 24-inch Theodolite No. 2, having 5 microscopes to read the azimuthal circle; observations were taken on 5 pairs of zeros (*face right* and *face left*) giving circle readings at 7° 12' apart.

The c.m.s. of observation of a single measure of an angle.

 $\sqrt{\frac{\text{Sum of squares of apparent errors of observations.}}{\text{No. of observations}-\text{No. of angles} \times \text{No. of changes of zero.}}}$ 

The e.m.s. of graduation and observation of the mean of the measures on a single zero.  $= \sqrt{\frac{\text{Sum of squares of apparent errors of zero.}}{\text{No. of angles } \times (\text{No. of changes of zero-1})}$ 

|        |                                                                    | <b>D8</b> .        | n ge                                               |                                     | Numb    | er of            |               |                                                                         |                                                                        |
|--------|--------------------------------------------------------------------|--------------------|----------------------------------------------------|-------------------------------------|---------|------------------|---------------|-------------------------------------------------------------------------|------------------------------------------------------------------------|
| Group. | Instrument and<br>Observer.                                        | Position of statio | Intervals betwee<br>microscope readi<br>of circle. | Measures on each<br>zero (average). | Angles. | Single measures. | Single zeros. | s. m. s. of observation of<br>a single measure.                         | e.m.s. of graduation and<br>observation of a single zero.              |
| I      | Barrow's 24-inch Theodolite<br>No. 2; Capt. M. W. Rogers,<br>B. E. | Hills,             | •                                                  | 8•59                                | 152     | 5455             | 1520          | $\left\{\frac{4186.07}{5455-1620}\right\}^{\frac{1}{2}} = \pm 1.081$    | $\left\{\frac{638\cdot59}{1520-152}\right\}^{\frac{1}{2}} = \pm 0.683$ |
| ņ      | Barrow's 24-inch Theodolite )<br>No. 2; Lieut. J. Hill, B. E. )    | _ <b>)</b> )       | 7 12                                               | <b>8</b> ∙20                        | 71      | 8278             | 710           | $\left\{\frac{957\cdot 18}{2272-710}\right\}^{\frac{1}{2}} = \pm 0.783$ | $\left\{\frac{244\cdot 86}{710-71}\right\}^{\frac{1}{2}} = \pm 0.618$  |
| ш      | Barrow's 24-inch Theodolite<br>No. 2; Capt. M. W. Rogers,<br>R. E. | Plains,            | 7 12                                               | 8-85                                | 4       | 184              | 40            | $\left\{\frac{80.67}{184-40}\right\}^{\frac{1}{2}} = \pm 0.926$         | $\left\{\frac{11.09}{40-4}\right\}^{\frac{1}{2}} = \pm 0.555$          |

August 1878.

J. B. N. HENNESSEY,

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# PRINCIPAL TRIANGULATION. REDUCTION OF FIGURES.

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|     | Obse             | rved    | Angles    |                |                                         | Equations to be satisfied |                   |                  |                  |                       |  |  |  |
|-----|------------------|---------|-----------|----------------|-----------------------------------------|---------------------------|-------------------|------------------|------------------|-----------------------|--|--|--|
|     |                  |         |           | al .           | x <sub>1</sub>                          | + x <sub>2</sub>          | + x <sub>3</sub>  | + x <sub>4</sub> | $= e_1 = + c$    | <b>5.198, λ</b> 1     |  |  |  |
| No. |                  | Valu    | 6         | iproc<br>eight | x <sub>3</sub>                          | + x4                      | + x <sub>5</sub>  | + x <sub>6</sub> | $= e_{g} = + c$  | ο·493, λ <sub>3</sub> |  |  |  |
|     |                  |         |           | Rec<br>W       | X <sub>5</sub>                          | + x <sub>6</sub>          | + x <sub>7</sub>  | + x <sub>8</sub> | $= e_3 = + o$    | ο·517, λ <sub>3</sub> |  |  |  |
|     |                  |         |           |                |                                         | $-9 \mathbf{x}_1$         | +4 x <sub>2</sub> | $-22 x_{3}$      |                  |                       |  |  |  |
| I   | 。<br>68          | ,<br>33 | "<br>0.17 | •05            |                                         | + 12 x <sub>6</sub>       | +6 x <sub>7</sub> | $+29 x_8$        | $= e_4 = - A$    | 4·2, λ <sub>4</sub>   |  |  |  |
| 2   | 42               | 1       | 19.78     | •05            |                                         |                           | <u></u>           |                  | <u> </u>         |                       |  |  |  |
| 3   | 38               | 58      | 35.75     | •06            |                                         |                           | Equations         | between the fac  | ctors            |                       |  |  |  |
| 4   | 30               | 27      | 8.60      | •06            |                                         |                           |                   |                  |                  |                       |  |  |  |
| 5   | 37               | 19      | 9.21      | •07            |                                         |                           |                   | Co-eff           | icients of       |                       |  |  |  |
| 6   | 72               | 15      | 11.27     | •00            | No. of<br>e                             | Value of<br>e             |                   |                  |                  |                       |  |  |  |
| 7   | 32               | 57      | 39.54     | •07            |                                         |                           | λ                 | λ                | λ <sub>8</sub> · | $\lambda_{4}$         |  |  |  |
| 8   | 36               | 28      | 3.43      | •06            |                                         |                           | +0.33             | +0.13            | ······           |                       |  |  |  |
|     |                  |         |           | •              | 1                                       | - 0 190                   |                   | <b>TO 14</b>     |                  | - 1 5/                |  |  |  |
|     |                  |         |           |                | 2                                       | + 0.493                   |                   | +0.38            | +0.12            | - 0.34                |  |  |  |
|     | •                |         |           |                | 3                                       | + 0.212                   |                   | *                | +0.39            | + 3.24                |  |  |  |
|     |                  |         |           |                | 4                                       | - 4.3                     | ·                 |                  | •                | +99.83                |  |  |  |
| ٦   | Values           | of t    | he Factor | rs             | Angular errors in seconds               |                           |                   |                  |                  |                       |  |  |  |
|     | λ <sub>1</sub> : | = ·     | + 0.087   | 2              | $x_1 = + \cdot 087$ $x_5 = + \cdot 240$ |                           |                   |                  |                  |                       |  |  |  |
|     | λ <sub>2</sub> : | = ·     | - 0.913   | 2              | $x_3 =035$ $x_6 = +.110$                |                           |                   |                  |                  |                       |  |  |  |
|     | λ <sub>3</sub> : | = ·     | + 4.338   | I              | $x_3 = + \cdot 193$ $x_7 = + \cdot 226$ |                           |                   |                  |                  |                       |  |  |  |
| •   | λ_ :             | = ·     | - 0.183   | 7              | $x_4 = - \cdot 050$ $x_8 = - \cdot 059$ |                           |                   |                  |                  |                       |  |  |  |
|     |                  |         |           |                |                                         | $[wx^2] = 2.58$           |                   |                  |                  |                       |  |  |  |

Figure No. 1.

\* In the tables of the equations between the factors the co-efficients of the terms below the disgonal are omitted for convenience, the co-efficient of the *ptk* term in the *ptk* line being always the same as the co-efficient of the *qtk* term in the *ptk* line.

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| Figure | No. | 2. |
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|     | Obse               | rved           | Angles         |                                       | · Equations to be satisfied |                                   |                    |                   |                            |                                  |                |                          |                  | Fa | ctor           |
|-----|--------------------|----------------|----------------|---------------------------------------|-----------------------------|-----------------------------------|--------------------|-------------------|----------------------------|----------------------------------|----------------|--------------------------|------------------|----|----------------|
|     |                    |                |                |                                       | -                           | x1                                | +:                 | K <sub>S</sub>    |                            | + x <sub>8</sub>                 | =              | $e_1 = -$                | - 0.427,         | 7  | λ              |
|     |                    |                | •              | cal                                   |                             | X4                                | +:                 | K <sub>5</sub>    |                            | + x <sub>6</sub>                 | =              | e <sub>2</sub> = -       | ⊦ o·647,         | 7  | λ              |
| No. |                    | Val            | ue             | iipro<br>/eigl                        |                             | x <sub>7</sub>                    | +:                 | K <sub>8</sub>    |                            | + x <sub>9</sub>                 | =              | e <sub>3</sub> = -       | - 0.357,         | 2  | λ <sub>8</sub> |
|     | •                  |                |                | Red                                   |                             | <b>x</b> <sub>10</sub>            | +:                 | <b>x</b> 11       | -                          | + x <sub>13</sub>                | =              | e <sub>4</sub> = -       | - 0158,          | 7  | λ4             |
|     |                    |                |                |                                       |                             | <b>x</b> <sub>13</sub>            | +:                 | x <sub>14</sub>   |                            | + x <sub>15</sub>                | =              | e <sub>5</sub> = -       | - 0.731,         | 2  | λ <sub>5</sub> |
|     | 0                  | ,<br>          | "              |                                       | а.<br>1                     | <b>x</b> 16                       | +                  | к <sub>17</sub>   | -                          | + x <sub>18</sub>                | =              | e <sub>6</sub> = -       | - 0.538,         | 7  | λ <sub>6</sub> |
|     | 5÷                 | 30             | 34 04          | •04                                   | x <sub>1</sub>              | +x4 +                             | +x <sub>7</sub> +: | K <sub>10</sub> - | + x <sub>13</sub> ·        | + x <sub>16</sub>                | =              | e <sub>7</sub> = -       | ⊦ o <b>∙33</b> , | 2  | λ <sub>7</sub> |
|     | 67                 | 5              | 15-20          | •07                                   |                             | 10 x <sub>8</sub>                 | -11                | x <sub>2</sub>    | +1                         | 9 x <sub>6</sub> )               |                |                          |                  |    |                |
| 3   | 05<br>50           | 10             | 15 11          | •08                                   | · ·                         | — 3 x <sub>5</sub>                | + 3                | x9                | -1                         | 4 x <sub>8</sub>                 |                | e                        | - 0.7            |    | <b>`</b>       |
| .4  | 50<br>81           | 30             | 4/ 94          | •06                                   |                             | + 9 x <sub>12</sub>               | -16                | x <sub>11</sub>   | + 20                       | $x_{15}$                         | _              | c <sub>8</sub> — -       | - 9 /3           | 4  | ~8             |
| 5   | 48                 | 14<br>6        | 48.20          | •00                                   | ļ ·                         | 10 x <sub>14</sub>                | + 16 :             | K <sub>18</sub>   | - 2                        | 1 <sup>•</sup> x <sub>17</sub> ) |                |                          |                  |    |                |
|     | 40<br>43           | ں<br>۲         | 40 30          | ~3<br>•0f                             |                             |                                   |                    | Fanati            | one hot-                   | on the f                         | antom          |                          |                  |    |                |
| 8   | 43<br>55           | ე<br>ი         | דד דד<br>25יקג | •08                                   |                             | . <u></u>                         |                    | uquall            | OTIS DCIM(                 |                                  |                |                          |                  |    |                |
| 0   | 33<br>81           | 51             | ~3 /3<br>52·67 | •04                                   | 1                           |                                   |                    |                   |                            | Co-ef                            | ficients (     | of                       |                  |    |                |
| 10  | 50                 | 58             | 28.01          | •05                                   | No. of                      | Value of                          | ļ                  |                   |                            |                                  |                |                          |                  |    |                |
|     | 52                 | J <sup>0</sup> | J0 01          | .03                                   |                             |                                   | λ <sub>1</sub>     | λ <sub>8</sub> ΄  | λ <sub>8</sub>             | λ4                               | λ <sub>5</sub> | λ <sub>6</sub>           | λ <sub>7</sub>   |    | λ <sub>8</sub> |
| 12  | 5-<br>67           | 47             | 13.42          | •03                                   | Т                           | - 0.427                           | +0.13              |                   |                            |                                  |                |                          | +0.04            | _  | 0.18           |
| 12  | 71                 | -7/<br>15      | -J +J<br>47.74 | •o6                                   | 2                           | + 0.647                           |                    | +0.1              | 7                          |                                  |                |                          | +0.08            | +  | 0.39           |
| 14  | 62                 | -J<br>28       | 57.54          | •05                                   | 3                           | - 0.322                           |                    |                   | +0.12                      | 1                                |                |                          | +0.02            | _  | 1.00           |
| 15  | 46                 | Š              | 18.34          | •10                                   | 4                           | - 0.128                           |                    |                   |                            | +0.11                            |                |                          | +0.02            | _  | 0.31           |
| 16  | 82                 | 22             | 28·98          | •04                                   | 5                           | - 0.731                           |                    |                   | *                          |                                  | +0.31          | C C                      | +0.02            | ÷  | 1.20           |
| 17  | 44                 | 56             | 44.18          | • • • • • • • • • • • • • • • • • • • | 6                           | - 0.538                           |                    |                   |                            |                                  |                | +0.31                    | +0.04            | +  | 0.13           |
| 18  | .52                | 40             | 51.29          | •10                                   | 7                           | + 0.33                            |                    |                   |                            |                                  |                |                          | +0.32            |    |                |
|     |                    | ·              |                |                                       | 8                           | - 9.7                             |                    |                   |                            |                                  |                |                          |                  | +1 | 55·67.         |
|     | Values             | of t           | he Factor      | 8                                     |                             | <u></u>                           |                    | Ang               | ular erroi                 | s in sec                         | onds           |                          |                  |    |                |
|     | λ <sub>1</sub> =   | = -            | - 2.9130       | )                                     |                             | <b>x</b> <sub>1</sub> =           | •000               | ·                 | x <sub>7</sub> = -         | 010                              |                | X19 =                    | 060              |    |                |
|     | λ <sub>3</sub> =   | = .            | + 2.5698       |                                       |                             | x, = -                            | - • 183            |                   | <b>x</b> <sub>8</sub> = ·  | - • 199                          |                | x <sub>14</sub> =        | — ·167           |    |                |
|     | λ <sub>3</sub> =   | = . •          | - 3.2902       | ;                                     |                             | x, = -                            | - :244             |                   | <b>x</b> <sub>9</sub> = ·  | - •139                           |                | $x_{15} =$               | - · 504          |    |                |
|     | λ <sub>4</sub> =   | = •            | - 2.8657       | 1                                     |                             | <b>x</b> <sub>4</sub> = -         | + •438             |                   | $x_{10} = -$               | + .002                           |                | <b>x</b> <sub>16</sub> = | 007              |    |                |
|     | λ <sub>δ</sub> =   | <b>z</b> •     | - 3.9031       | :                                     |                             | $\mathbf{x}_{s} = \mathbf{x}_{s}$ | + •164             |                   | $\mathbf{x}_{n} = \cdot$   | 059                              |                | <b>x</b> <sub>17</sub> = | 132              |    |                |
|     | λ <sub>6</sub> , = | = •            | - 3.0799       | )                                     |                             | <b>x</b> <sub>6</sub> = -         | + •045             |                   | <b>x</b> <sub>19</sub> = · | - • 101                          |                | x <sub>18</sub> =        | 399              |    |                |
|     | λ <sub>7</sub> =   | =              | + 2.9048       | <b>;</b>                              |                             |                                   |                    |                   |                            |                                  |                |                          |                  |    |                |
|     | λ <sub>8</sub> =   | = •            | - 0.0271       | I                                     |                             |                                   |                    |                   | [wx <sup>8</sup> ] =       | : 10.26                          |                |                          |                  |    |                |

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| Figure | No. | 3. |
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|     | Observed Angles          |               |                       |                               | Equ                                | atior    | ns to be sa             | tisfied           |                  |                |                                       | Fa     | ctor           |
|-----|--------------------------|---------------|-----------------------|-------------------------------|------------------------------------|----------|-------------------------|-------------------|------------------|----------------|---------------------------------------|--------|----------------|
|     |                          |               |                       | x <sub>1</sub>                | + x <sub>3</sub>                   |          | + x,                    | 8                 | $= e_1$          | = +            | - o·og6,                              |        | λ              |
|     |                          | cal t         |                       | x4                            | + x <sub>5</sub>                   |          | + x,                    | 6                 | $= e_{g}$        |                | - 0.121,                              | :      | λջ             |
| No. | Value                    | iproo<br>eigh |                       | <b>x</b> <sub>7</sub>         | + <b>x</b> <sub>8</sub>            |          | + x <sub>g</sub>        | )                 | = e,             | = -            | - 0.449,                              |        | λ3 .           |
|     |                          | Reci          |                       | <b>x</b> <sub>10</sub>        | + <b>x</b> <sub>11</sub>           |          | + <b>x</b> <sub>1</sub> | 12                | = e4             | = +            | ⊦ o.o34,                              |        | λ4             |
|     |                          |               | 1                     | <b>x</b> <sub>13</sub>        | + x <sub>14</sub>                  | ,        | + <b>x</b> <sub>1</sub> | 15                | = e <sub>s</sub> | = +            | - 0.326,                              |        | λ              |
|     | o / //                   | _             |                       | <b>x</b> <sub>16</sub>        | + x <sub>17</sub>                  |          | + <b>x</b> <sub>1</sub> | 18                | = e <sub>6</sub> | = -            | - 0.088,                              | :      | λ              |
|     | 73 29 40.52              | •06           | <b>x</b> <sub>1</sub> | + x <sub>4</sub> -            | + x <sub>7</sub> + x <sub>10</sub> | -        | $+x_{13} + x_1$         | .6                | = e <sub>7</sub> | = -            | - 0.43,                               | 2      | λ <sub>7</sub> |
| 2   | 48 42 31.60              | •06           |                       | 14 X <sub>8</sub>             | -19 x <sub>2</sub>                 |          | + 19 <b>x</b>           | 5)                |                  |                |                                       |        | ÷              |
| 3   | 57 47 5°°94              | •08           |                       | — 4 x <sub>5</sub>            | + 3 x,                             |          | — 12 X <sub>s</sub>     | . (               |                  |                |                                       |        |                |
| 4   | 54 5 20.92               | •05           | · ·                   | + бх <sub>12</sub>            | -15 x <sub>11</sub>                |          | + 13 x                  | 15                | $= e_8$          |                | - 0°0,                                |        | ∧ <sub>8</sub> |
| 5   | 78 52 36.91              | •07           |                       | - 13 x <sub>14</sub>          | + 19 x <sub>18</sub>               |          | -13 x                   | <sub>17</sub> )   |                  |                |                                       |        | •              |
| 6   | 47 2 5.03                | •03           |                       |                               |                                    |          |                         |                   |                  |                |                                       |        |                |
| 7   | 40 23 3.39               | •04           |                       |                               | Ec                                 | luati    | ions betwee             | en the            | factors          |                |                                       |        |                |
| 8   | 58 28 49.46              | •03           |                       |                               |                                    |          |                         | Core              | flicients of     |                | · · · · · · · · · · · · · · · · · · · |        |                |
| 9   | 81 8 9.46                | ·05           | No. of                | Value of                      |                                    | <b>`</b> |                         | 00-01             |                  |                |                                       |        |                |
| 10  | 54 17 19.28              | •07           | е.                    | е                             | λ <sub>1</sub>                     | λ        | λ <sub>3</sub>          | λ4                | $\lambda_5$      | λ <sub>6</sub> | λ <sub>7</sub>                        |        | λ <sub>8</sub> |
| 11  | 53 27 4 <sup>8</sup> ·55 | •04           | I                     | + 0.000                       | +0.30                              |          |                         |                   |                  |                | +0.06                                 | ·<br>— | 0.03           |
| 12  | 72 14 54.72              | •05           | 2                     | - 0.131                       | +0                                 | .12      |                         |                   |                  |                | +0.02                                 | +      | 0·29           |
| 13  | o5 7 39·43               | •08           | 3                     | - 0.440                       |                                    | U        | +0.13                   |                   |                  |                | +0.04                                 | -      | 0.31           |
| 14  | 57 6 10.78               | •04           | 4                     | + 0.034                       |                                    |          |                         | <u>ار، ۱۹، ۱۹</u> | <b>`</b>         |                | +0.02                                 | -      | 0.30           |
| 15  | 57 40 12.47              | •04           | 5                     | + 0.326                       |                                    |          | ×                       | -                 | +0.10            |                | +0.08                                 |        | 0.00           |
| 10  | 72 30 50.03              | •07           | 6                     | - o·o88                       |                                    |          | ×                       |                   | •+•              | 0.16           | +0.02                                 | +      | 0.43           |
| 17  | 59 31 54.48              | •04           | 7                     | - 0.43                        |                                    |          |                         |                   |                  |                | +0.37                                 |        | 4              |
| 18  | 47 51 12.20              | •05           | 8                     | - 0.6                         |                                    |          |                         |                   |                  | <u>`</u>       | •••                                   | + 1    | 03.19          |
| •   |                          |               |                       |                               | 1                                  | _        |                         |                   |                  | <u> </u>       | <u> </u>                              |        |                |
| 1   | Values of the Factors    | 5             |                       |                               |                                    | Ang      | ular errors             | in sec            | onds             | ``             |                                       |        |                |
|     | $\lambda_1 = + 1.0346$   |               |                       | $\mathbf{x}_1 = \mathbf{x}_1$ | - •049                             |          | $\mathbf{x}_7 = -$      | • 200             | x <sub>1</sub>   | s =            | ÷ •089                                |        |                |
|     | $\lambda_{g} = -0.1704$  |               |                       | $x_2 = \cdot$                 | + •073                             |          | x <sub>8</sub> = -      | ·091              | x <sub>1</sub>   | . =            | + 124                                 |        |                |
|     | $\lambda_3 = -3.1415$    |               |                       | x <sub>8</sub> = -            | + .072                             |          | x <sub>9</sub> = -      | · 158             | . <b>x</b> 1     | s =            | + 113                                 |        |                |
|     | $\lambda_{4} = + 1.0044$ |               |                       | x <sub>4</sub> = -            | - •101                             |          | $x_{10} = -$            | •059              | x <sub>1</sub>   | • =            | - · 110                               |        |                |
|     | $\lambda_5 = . + 2.9635$ |               |                       | x <sub>5</sub> = -            | - •009                             |          | $x_{11} = +$            | •046              | x <sub>1</sub>   | , =            | + .017                                |        |                |
|     | $\lambda_6 = + 0.2866$   |               | .0                    | $x_6 = -$                     | 011                                |          | $\lambda_{12} = +$      | •047              | <b>x</b> 1       |                | + .003                                |        |                |
|     | $\lambda_7 = -1.8520$    |               |                       |                               |                                    |          |                         |                   |                  | •              |                                       | ) vy   |                |
|     | $\lambda_8 = -0.0098$    |               | · .                   |                               |                                    |          | [wx <sup>2</sup> ] =    | 3.31              |                  |                |                                       |        |                |

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|      | Obcomed                                 | Angles           |               | Equations to be satisfied |                                                     |                                           |                |                            |               |           |                          |                   | Fa     | ctor           |
|------|-----------------------------------------|------------------|---------------|---------------------------|-----------------------------------------------------|-------------------------------------------|----------------|----------------------------|---------------|-----------|--------------------------|-------------------|--------|----------------|
|      | Ubserved                                | Angles           |               |                           | Χ.                                                  | + 1                                       |                | +r                         |               | _         | e, = ∔                   | 0.202-            | _ av   | <br>h          |
|      | :                                       |                  |               |                           | 1<br>X.                                             |                                           | 7              | <br>+ 1                    | 0             | =         | e, = +                   | · 0'010.          | 2      | -1<br>\        |
| Na   | Value                                   |                  | oroci<br>ight |                           | ~4<br>X-                                            | م،<br>+ +                                 | <b>.</b>       | + <del>-</del>             | U<br>A        | _         | -, — T                   | 0.011             | י<br>נ | -*             |
| 110. | · • • • • • • • • • • • • • • • • • • • | •                | tecit<br>Wei  |                           | . •••7<br>Tre                                       | 4 I                                       | 8              | + <del>-</del>             | <b>v</b>      |           | e. = -                   | • <b>0</b> •015   | ,      | -8             |
|      |                                         |                  | <b>H</b>      |                           | -10<br>T                                            | د ۲ <sup>.</sup><br>۲۰                    |                | -⊤▲<br>-⊥-                 |               | _         | -4 — т<br>е. — —         | • 0.101           | י<br>נ | -4             |
|      | o •                                     | "                |               |                           | -12<br>12                                           | · + *                                     | 14             | م ر<br>+ +                 | .19           |           | -,                       | · 0`· 246         | ,      | -5             |
| Ĩ    | 71 <sup>°</sup> 30                      | 20.04            | •05           | т.                        | −16<br>+ T. ⊥                                       |                                           | ·17<br>(m. +▼  |                            |               | -         | -•.= -                   | • 0•40.           | י<br>נ | יד<br>ר        |
| 2    | 58 35                                   | 4·3 <u>0</u>     | •03           |                           | 18 x. '                                             | -7 -12                                    | -10 1.3        | ×⊤ 81                      | . 10          |           | -1                       | ~ <del>4</del> ~) | ,      | 7              |
| 3    | <b>4</b> 9 5 <sup>4</sup>               | 37.79            | •06           |                           | - IA Y.                                             | بر بر<br>سیان                             | <b>3</b><br>(a | - 24 -                     |               |           |                          |                   |        |                |
| 4    | 55 <b>44</b>                            | 32.32            | •06           |                           |                                                     |                                           | -9<br>T        | — 24 x<br>⊥ 8 <del>v</del> |               | Ŧ         | e <sub>8</sub> = -       | - 7.1,            | 2      | λ <sub>8</sub> |
| 5    | 55 52                                   | 6•98             | • 1 2         |                           |                                                     |                                           | -11            | F •                        | <sup>15</sup> |           |                          |                   |        |                |
| 6    | 68 23                                   | 22.31            | •06           |                           |                                                     |                                           | -18            | 3 x                        | -17           | •         |                          |                   | _      |                |
| 7    | 71 51                                   | 28.83            | •04           |                           |                                                     | 1                                         | Equation       | s betwee                   | n the fa      | actors    |                          |                   |        |                |
| 8    | 41 2                                    | 28.70            | •06           |                           | }                                                   |                                           |                |                            |               | i         |                          |                   |        |                |
| 9    | 67 6                                    | 3.29             | •04           | No of                     | Value of                                            |                                           |                |                            | Co-eff        | icients ( | of                       |                   |        |                |
| 10   | 62 58                                   | 19.29            | •05           | e                         | e e                                                 | λ.                                        | λ.             | λ-                         | λ.            | λ.        | λ.                       | λ-                |        | <u>λ</u>       |
| 11   | 66 39                                   | 51.28            | •03           |                           |                                                     |                                           |                |                            | ~~4           |           | ~~6                      | '''               |        |                |
| 12   | 50 21                                   | 50.02            | •03           | I                         | + 0.393                                             | +0.14                                     |                | i.                         | •             | ·         |                          | +0:05             | +      | 0.00           |
| 13   | <b>49 3</b>                             | 52.65            | •05           | 2                         | + 0.019                                             |                                           | +0.34          |                            | 1             |           |                          | +0.06             | -      | <b>I</b> •14   |
| 14   | - 6 <u>3</u> 50                         | 17.42            | •03           | 3                         | - 0.041                                             | А. С. |                | +0.14                      |               |           |                          | +0.04             | -      | 1.08           |
| 15   | 67 5                                    | 50.74            | •08           | 4                         | + 0.012                                             |                                           |                |                            | +0.11         |           |                          | +0.02             | +      | 0.24           |
| 16   | 48 51                                   | 26.47            | . •04         | 5                         | - 0.101                                             |                                           |                | *                          | •             | +0.10     | 5                        | +0.02             | +      | 0.31           |
| 17   | 77 40                                   | 50°21            | •05           | 6                         | - 0.346                                             |                                           |                |                            |               | •         | +0.12                    | +0.04             | +      | 1.03           |
| 18   | 53 27                                   | 44.05            | •08           | 7                         | - 0.40                                              |                                           |                |                            | •             |           |                          | +0.39             |        | •              |
|      |                                         |                  |               | 8                         | - 7·I                                               |                                           |                |                            |               |           |                          |                   | + 1    | 32.27          |
|      | Values of t                             | the Factor       | 8             |                           |                                                     |                                           | Angula         | ar errors                  | in seco       | onds      |                          |                   |        |                |
|      | $\lambda_1 = \cdot$                     | + 3.1093         |               |                           | $\mathbf{x}_{\mathbf{i}} = \mathbf{x}_{\mathbf{i}}$ | + •055                                    | I              | in = -                     | •088          |           | -x <sub>13</sub> =       | 095               |        |                |
|      | λ <sub>2</sub> = ·                      | + 0.2855         |               | 1                         | <b>x</b> <sub>9</sub> = ·                           | + •118                                    | X              | k <sub>8</sub> = +         | •078          |           | $x_{14} =$               | + .034            |        |                |
|      | λ <sub>8</sub> = ·                      | - c·199 <b>3</b> |               |                           | <b>x</b> <sub>8</sub> = -                           | + •119                                    | 3              | <b>(</b> <sub>9</sub> = -  | •031          |           | <b>x</b> <sub>15</sub> = | 030               |        |                |
|      | λ <sub>4</sub> =                        | + 1.1845         |               |                           | x, = ·                                              | - •103                                    | 3              | <sup>4</sup> 10 = -        | •041          |           | <b>x</b> <sub>16</sub> = | - ·128            |        |                |
|      | $\lambda_{5} = -$                       | + 0.1160         |               |                           | $\mathbf{x}_{5} = \mathbf{x}_{5}$                   | + •139                                    | x              | $x_{11} = +$               | •052          |           | <b>x</b> <sub>17</sub> = | 044               |        |                |
|      | λ <sub>6</sub> = ·                      | - 1.1860         | i.            |                           | $\mathbf{x}_6 = \mathbf{x}_6$                       | 012                                       | 2              | x <sub>18</sub> = +        | •004          |           | ' x <sub>18</sub> =      | - •174            |        |                |
|      | $\lambda_7 = -$                         | - 2.0075         | i             |                           |                                                     |                                           |                |                            |               |           |                          |                   |        |                |
|      | λ <sub>8</sub> =                        | - 0.0622         | ,             |                           |                                                     |                                           | -              | [wx <sup>9</sup> ] =       | 2.58          |           |                          |                   |        |                |

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Figure No. 4.



|     | Obs            | erve           | l Angles  |              |                | Equations to be satisfied |                    |                   |                             |                  |                |                     |                | F  | actor          |
|-----|----------------|----------------|-----------|--------------|----------------|---------------------------|--------------------|-------------------|-----------------------------|------------------|----------------|---------------------|----------------|----|----------------|
| ·   |                |                |           |              | -              | x <sub>1</sub>            | + 3                | C <sub>2</sub>    | +:                          | с <sub>8</sub>   | =              | $e_1 = +$           | 0.042,         |    | λ              |
|     |                |                |           | cal .        |                | X4                        | + 2                | с <sub>5</sub>    | +:                          | ¢8               | =              | e <sub>s</sub> = +  | 0.004,         |    | λ              |
| No. |                | Valu           | le        | ipro<br>eigh | 1              | <b>x</b> 7                | + 2                | к <sub>8</sub>    | +>                          | Kg _             | =              | e <sub>3</sub> = +  | <u>0.095</u> , |    | λ              |
|     |                |                |           | Rec          |                | <b>x</b> <sub>10</sub>    | + 3                | ¢11               | +>                          | C <sub>12</sub>  | =              | e <sub>4</sub> = +  | 0.031,         |    | λ              |
|     |                | <u>-</u>       |           |              |                | <b>x</b> <sub>13</sub>    | +3                 | <sup>c</sup> 14   | +:                          | K <sub>15</sub>  | =              | e <sub>s</sub> = +  | 0.144,         |    | λ              |
| _   | 0<br>6 6       | ,              | "         |              |                | X <sub>16</sub>           | + x                | 17                | +2                          | с <sub>18</sub>  | =              | e <sub>6</sub> = -  | 0.017,         |    | λ <sub>6</sub> |
| I   | 00             | 30             | 31.41     | •02          | x <sub>1</sub> | +x, +                     | x <sub>7</sub> + 2 | ĸ <sub>10</sub> − | + <b>x<sub>13</sub> +</b> : | x <sub>16</sub>  | =              | $e_7 = -$           | 0.40,          |    | λ7             |
| 2   | 01             | 47             | 49.77     | •00          |                | 17 x <sub>8</sub>         | 11 3               | 2                 | + 12 3                      | <sup>(</sup> 8)  |                |                     |                |    |                |
| 3   | 51             | 41             | 39.74     | •06          |                | - 1 3 x <sub>5</sub>      | + 14 1             | <sup>2</sup> 9    | - 10 :                      | K <sub>8</sub>   |                | _                   | 0              |    |                |
| 4   | 61             | 22             | 37.03     | •03          |                | + 6 x <sub>12</sub>       | - 14 2             | <sup>(</sup> 11   | + 10 :                      | K <sub>15</sub>  | =              | e <sub>8</sub> = -  | 9.9,           |    | <b>^</b> 8     |
| 5   | 58             | 51             | 57.43     | •06          |                | – 16 x <sub>14</sub>      | + 14 3             | c <sub>18</sub>   | -11:                        | <sub>K17</sub> ) |                |                     |                |    |                |
| 6   | 59             | 45             | 26.48     | •07          |                |                           |                    |                   |                             |                  |                |                     |                |    |                |
| 7   | 57             | 22             | 36.77     | •02          |                |                           |                    | Equati            | ons betw                    | een the          | factors        |                     |                |    |                |
| 8   | 65             | 3 <del>4</del> | 7.65      | •07          |                |                           | 1                  |                   |                             |                  |                |                     |                |    |                |
| 9   | 57             | 3              | 16.64     | .03          | No. of         | Value of                  |                    |                   |                             | Со-е             | fficients      | of                  |                |    |                |
| 10  | <b>4</b> 9     | 1              | 44 • 98   | •03          | e              | е                         | λ                  | λ                 | λ,                          | λ,               | λ <sub>5</sub> | λ <sub>6</sub>      | λ <sub>7</sub> |    | λ <sub>8</sub> |
| 11  | 56             | 13             | 30.01     | •06          |                |                           |                    |                   |                             |                  |                |                     | ·              |    |                |
| 12  | 74             | 44             | 45.85     | •02          |                | + 0 042                   | +0.14              |                   |                             |                  |                |                     | +0.03          | +  | 0.30           |
| 13  | 62             | 51             | 44.46     | •10          | 2              | + 0.004                   | +                  | .0.10             |                             |                  |                |                     | +0.03          | +  | 0.00           |
| 14  | 54             | 5              | 31.92     | •06          | 3              | + 0.092                   |                    |                   | +0.13                       |                  |                |                     | +0.03          | -  | 0.38           |
| 15  | 63             | 2,             | 44.21     | •03          | 4              | + 0.031                   |                    |                   |                             | +0.11            |                |                     | +0.03          |    | 0.73           |
| 16  | 62             | 50             | 44.95     | •03          | 5              | + 0.144                   |                    |                   |                             |                  | +0.19          |                     | +0.10          | -  | 0.96           |
| 17  | 61             | 13             | 13.78     | •05          | 6              | - 0.012                   |                    |                   | *                           |                  |                | +0'14               | +0.03          | +  | 0.39           |
| 18  | 55             | 56             | 1.97      | •06          | 7              | - 0.40                    |                    |                   |                             |                  |                |                     | +0.33          |    |                |
|     |                |                |           |              | 8              | - 9.8                     |                    | _                 |                             |                  |                |                     |                | +1 | 06.32          |
| 1   | Value          | s of           | the Facto | ) <b>rs</b>  |                | Angular errors in seconds |                    |                   |                             |                  |                |                     |                |    |                |
|     | λ              | =              | + 0.940   | ъб           |                | $x_1 = -$                 | - •043             |                   | $\mathbf{x}_{\eta} = -$     | •039             | :              | $x_{13} = -$        | •098           |    |                |
|     | λ              | =              | + 0.634   | t1           |                | $x_2 = -$                 | + •107             |                   | $x_8 = +$                   | • 133            | :              | $x_{14} = +$        | • 201          |    |                |
|     | λ <sub>8</sub> | =              | + 1.122   | 7I           |                | <b>x</b> <sub>3</sub> = - | 022                |                   | $x_9 = +$                   | .001             | :              | $x_{15} = +$        | •041           |    | ĺ              |
|     | λ4             | =              | + 0.620   | x            |                | x <sub>4</sub> = -        | 074                |                   | $x_{10} = -$                | •074             | :              | $x_{16} = -$        | •072           |    |                |
|     | $\lambda_5$    | =              | + 2.118   | 81           |                | x. = -                    | + ·008             |                   | x., = +                     | .102             |                | x <sub>17</sub> = + | •078           |    |                |

 $x_6 = - \cdot 020$ 

 $x_{12} = + .003$ 

 $[wx^{9}] = 2.46$ 

### Figure No. 5.

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+ 0.7016

- 3.0941

 $\lambda_8 = -0.0772$ 

 $\lambda_{R}$ 

 $\lambda_7$ 

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 $x_{18} = - \cdot 023$ 

|        | Obs                                                              | erve                | l Angles                                |                              |                  |                                                                                                                                                                                                                             | Equations                                                              | to be satisfied                                                 |                                           | Factor                                                                  |  |  |  |
|--------|------------------------------------------------------------------|---------------------|-----------------------------------------|------------------------------|------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------|-----------------------------------------------------------------|-------------------------------------------|-------------------------------------------------------------------------|--|--|--|
| No.    |                                                                  | Va                  | lue                                     | Reciprocal<br>Weight         |                  | x <sub>1</sub> + x<br>x <sub>3</sub> + x<br>x <sub>6</sub> + x                                                                                                                                                              | $x_{8} + x_{8}$<br>$x_{4} + x_{5}$<br>$x_{6} + x_{7}$                  | + x <sub>4</sub><br>+ x <sub>6</sub><br>+ x <sub>8</sub>        | $= e_1 = -$<br>$= e_3 = +$<br>$= e_3 = +$ | 0.009, J <sub>1</sub><br>0.328, J <sup>2</sup><br>0.311, J <sup>8</sup> |  |  |  |
| I      | °<br>59                                                          | 13                  | <i>"</i><br>25 <sup>.</sup> 64          | •02                          |                  | - 13 3<br>+ 18 3                                                                                                                                                                                                            | x <sub>1</sub> + 8 x <sub>9</sub><br>x <sub>6</sub> - 4 x <sub>7</sub> | $\left.\begin{array}{c}-20 x_{3}\\+17 x_{8}\end{array}\right\}$ | $= e_4 = -$                               | 9°3, λ,                                                                 |  |  |  |
| 2<br>3 | 33<br>37                                                         | 40<br>25            | 35`94<br>49`28                          | •06<br>•08                   |                  | <u>.</u> .                                                                                                                                                                                                                  | Equation                                                               | s between the f                                                 | actors                                    |                                                                         |  |  |  |
| 4<br>5 | 49<br>49                                                         | <b>4</b> 0<br>15    | 9 <sup>.</sup> 77<br>47 <sup>.</sup> 97 | •03<br>•05                   | No. of           | Value of                                                                                                                                                                                                                    |                                                                        | Co-ei                                                           | fficients of                              |                                                                         |  |  |  |
| 6<br>7 | <b>4</b> 3<br><b>3</b> 5                                         | 38<br>22            | 14.00<br>3.67                           | •04<br>•07                   | e                | e                                                                                                                                                                                                                           | λ <sub>1</sub>                                                         | λ                                                               | λ                                         | λι                                                                      |  |  |  |
| 8      | 51                                                               | 43                  | 55.33                                   | •04                          | I<br>2<br>3<br>4 | - 0.009<br>+ 0.328<br>+ 0.311<br>- 9.3                                                                                                                                                                                      | +0.10                                                                  | +0.11<br>+0.20                                                  | +0.09<br>+0.30                            | - 1.38<br>- 0.88<br>+ 1.12<br>+64.86                                    |  |  |  |
|        | Value                                                            | s of t              | the Fact                                | ors                          |                  | <u>.</u>                                                                                                                                                                                                                    | Angula                                                                 | ar errors in seco                                               | nds                                       |                                                                         |  |  |  |
| 2      | $\lambda_1 =$<br>$\lambda_2 =$<br>$\lambda_3 =$<br>$\lambda_4 =$ | = -<br>= -{<br>= -{ | - 2.20<br>- 1.00<br>- 2.31<br>- 0.21    | 40<br>81<br>3 <b>8</b><br>66 |                  | $x_{1} = + \cdot 012 \qquad x_{5} = + \cdot 166$ $x_{9} = - \cdot 236 \qquad x_{6} = - \cdot 023$ $x_{3} = + \cdot 251 \qquad x_{7} = + \cdot 223$ $x_{4} = - \cdot 036 \qquad x_{8} = - \cdot 055$ $[wx^{9}] = 3 \cdot 11$ |                                                                        |                                                                 |                                           |                                                                         |  |  |  |

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Figure No. 6.

| Observed Angles                                                                                      | Equations to be satisfied H                                                                                                                                                                         | factor                                             |
|------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------|
| No. Value                                                                                            | $ \begin{array}{cccccccccccccccccccccccccccccccccccc$                                                                                                                                               | λ <sub>1</sub><br>λ <sub>2</sub><br>λ <sub>3</sub> |
| I 30 10 42·39 ·08                                                                                    | $ \left. \begin{array}{ccc} -36  x_1 & -8  x_2 & -18  x_3 \\ +  26  x_6 & +  x_7 & +19  x_8 \end{array} \right\} = e_4 = -  34 \cdot 8, $                                                           | λ <u>.</u>                                         |
| 2 47 2 9.09 .06<br>3 64 22 53.99 .08                                                                 | Equations between the factors                                                                                                                                                                       | .:<br>•                                            |
| 4 38 24 15·32 ·10<br>5 36 46 56·86 ·04<br>6 40 25 54·72 ·03                                          | No. of Value of<br>e e                                                                                                                                                                              |                                                    |
| 7 54 21 25·11 ·04<br>8 48 25 44·05 ·06                                                               | $\lambda_1 \qquad \lambda_2 \qquad \lambda_3 \qquad \lambda_4 \qquad \lambda_2$                                                                                                                     | <b>'4</b>                                          |
|                                                                                                      | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                                                                                               | •66<br>•96<br>•42                                  |
| Values of the Factors                                                                                | Angular errors in seconds                                                                                                                                                                           | :                                                  |
| $\lambda_1 = - 9.8654$<br>$\lambda_2 = + 5.7692$<br>$\lambda_3 = + 2.4556$<br>$\lambda_4 = - 0.4741$ | $x_{1} = + \cdot 576 \qquad x_{5} = + \cdot 329$ $x_{2} = - \cdot 364 \qquad x_{5} = - \cdot 123$ $x_{3} = + \cdot 355 \qquad x_{7} = + \cdot 079$ $x_{4} = - \cdot 410 \qquad x_{8} = - \cdot 393$ |                                                    |
|                                                                                                      | $[wx^3] = 15.56$                                                                                                                                                                                    |                                                    |

Figure No. 7.

|          | Obs              | erve     | d Angles       |               | Equations to be satisfied |                        |                    |                   |                       |                        |                        |                  | F        | actor |                  |
|----------|------------------|----------|----------------|---------------|---------------------------|------------------------|--------------------|-------------------|-----------------------|------------------------|------------------------|------------------|----------|-------|------------------|
|          |                  |          |                |               |                           | x <sub>1</sub>         | + 3                | <b>S</b>          | +                     | x <sub>8</sub>         | $= e_{j}$              | ı = +            | - 0.210, |       | λ                |
|          |                  |          |                | cal           |                           | X.                     | + x                | 5                 | +                     | x <sub>6</sub>         | = e                    | s' = -           | - 0175,  |       | λ <sub>3</sub> . |
| No.      |                  | Val      | ue             | iipro<br>eigh |                           | x <sub>7</sub>         | + x                | 8                 | +                     | x <sub>9</sub>         | = e,                   | , = -            | - 0.149, |       | λ <sub>8</sub> . |
|          |                  |          |                | W             |                           | <b>x</b> <sub>10</sub> | + x                | -<br>411          | +                     | x <sub>19</sub>        | = e                    | 4 = +            | - 0.556, |       | λ,               |
|          |                  |          |                |               |                           | <b>x</b> <sub>13</sub> | + 3                | <sup>4</sup> 14   | +                     | x <sub>15</sub>        | = e                    | <sub>6</sub> = - | - 0.013, |       | λ                |
| _        | 0                | ,        | "              |               |                           | <b>x</b> <sub>16</sub> | + x                | <sup>4</sup> 17   | +                     | x <sub>18</sub>        | = e                    | 6 = -            | - 0.208, |       | λ <sub>6</sub>   |
|          | 52               | 25<br>70 | 40.45          | -03           | x1                        | + x <sub>4</sub> + x   | ε <sub>7</sub> + 2 | c <sub>10</sub> + | • x <sub>18</sub> +   | <b>x</b> <sub>16</sub> | = e                    | n = −            | - 0.02,  |       | λη               |
|          | 05<br>61         | 53       | 52.01          | -00           |                           | 12 X <sub>8</sub>      | — 10 <b>x</b>      | 2                 | +10                   | X <sub>6</sub> )       |                        |                  |          |       |                  |
| 3        | 60               | 40<br>28 | 20-44          | -07           |                           | — 16 х <sub>5</sub>    | + 27 x             | 9                 | -10                   | x <sub>8</sub> (       |                        | •                | ~~~~     |       | 、                |
| 4        | 03               | 20       | 54.03          | -04           |                           | + 9 x <sub>12</sub>    | — 10 x             | -<br>11           | + 6                   | x <sub>15</sub>        | =                      | e <sub>8</sub> = | -57-3,   |       | ∧ <sub>8</sub> . |
| 5        | 52               | 30       | 19.51          | -09           |                           | 16 x <sub>14</sub>     | + 1 3 x            | 18                | -16                   | x <sub>17</sub> )      |                        |                  |          |       |                  |
| -        | 03               | 54<br>28 | 40.40          | 104           |                           |                        |                    |                   | • .                   |                        |                        |                  |          | i     |                  |
| 2<br>0   | 70<br>64         | 30       | 51.00          | 105           |                           |                        | Ľ                  | quation           | as betwee             | en the fa              | ctors                  |                  |          |       |                  |
| 0        | 04<br>08         | 49       | 20-23          | -00           |                           |                        |                    |                   |                       | Co-ef                  | ficients o             | of.              |          |       |                  |
| 9        | 30               | 31       | 43.02          | 103           | No. of                    | Value of               |                    |                   |                       |                        |                        |                  |          |       |                  |
| 10       | 47<br>64         | 29<br>-  | 25.00          | •03           | e                         | e                      | λ <sub>1</sub>     | $\lambda_{2}$     | λ                     | λ4                     | $\lambda_{5}$          | λ <sub>6</sub>   | λ7       |       | λ <sub>8</sub>   |
| 11       | 04<br>           | 5        | 40.20          | -13           | I                         | + 0.310                | +0.16              |                   |                       |                        |                        |                  | +0.03    | +     | 0.24             |
| 14       | 50               | *4<br>TO | 47 40          | .00           | 2                         | - 0.175                |                    | +0.12             |                       |                        |                        |                  | +0.04    | -     | 1.04             |
| 13       | 53               | 19<br>0  | 40 09<br>08.17 | 03<br>• 05    | 3                         | - 0.140                |                    | •                 | +0.14                 |                        |                        |                  | +0.02    | +     | 0.21             |
|          | 53<br>70         | 4        | 30 17          | 05            | 4                         | + 0.556                |                    |                   | •                     | +0.34                  |                        |                  | +0.03    |       | 0.58             |
| 15       | 73<br>66         | 37       | 42 00          | 04<br>• or    | 5                         | - 0.013                |                    |                   | ×                     | •                      | +0.12                  |                  | +0.03    | _     | 0.26             |
| 10<br>T# | 50               | 31<br>25 | 40 99          | •03           | 6                         | - 0.208                |                    |                   |                       |                        |                        | +0.16            | i + 0.02 | +     | 0·56             |
| -/<br>78 | 33<br>50         | 33<br>47 | 43 40          | •08           | 7                         | + 0.02                 |                    |                   |                       |                        |                        |                  | +0.23    |       | Ŭ                |
| 10       | 59               | 47       | 10 15          | 00            | 8                         | -57.3                  |                    |                   |                       |                        |                        |                  |          | +1    | 25.01            |
|          |                  |          |                |               |                           | •                      |                    |                   |                       |                        |                        |                  |          |       |                  |
| V        | alues            | of t     | he Facto       | r8            |                           |                        |                    | Angul             | ar errors             | in secon               | nds                    |                  |          |       |                  |
|          | λ <sub>1</sub> = | +        | 1 • 8938       | -             |                           | $x_1 = +$              | •084               | X                 | ν <sub>η</sub> = +    | •014                   | x <sub>11</sub>        | " =  —           | •053     |       |                  |
|          | $\lambda_{g} =$  |          | 4.3117         |               |                           | $x_{g} = +$            | •415               | x                 | <sub>8</sub> = +      | • 263                  | <b>x</b> 14            | . = +            | • 267    |       |                  |
|          | λ <sub>8</sub> = | -        | 0.6375         | 1             |                           | $x_8 = -$              | • 289              | X                 | i, =                  | •425                   | X1                     | s = -            | • 227    |       |                  |
|          | λ, =             | +        | 0.9908         |               |                           | $x_4 = -$              | •136               | X                 | $x_{10} = +$          | •057                   | <b>x</b> <sub>10</sub> | s = +            | •054     |       |                  |
|          | $\lambda_5 =$    | -        | 2.6764         |               |                           | $x_{5} = +$            | •334               | x                 | n = +                 | •781                   | x <sub>12</sub>        | , = +            | • 246    |       |                  |
|          | λ <sub>6</sub> = | +        | 0.1204         |               |                           | $x_6 = -$              | •373 ·             | x                 | - = -                 | • 282                  | <b>x</b> <sub>10</sub> | , = -            | • 508    |       |                  |
|          | λ <sub>7</sub> = | +        | 0.9113         |               | •                         |                        |                    |                   | ,                     |                        |                        |                  |          |       |                  |
|          | λ <sub>8</sub> = | -        | 0.2012         | •             |                           |                        |                    | C                 | wx <sup>2</sup> ] = ( | 30.22                  |                        |                  |          | • .   |                  |

Figure No. 8.

| Figure | No. | 9. |
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|         | Obs            | erve | d Angles        |              |        |                     | Equa                    | tions to be                      | satisfied                     |                    |                | Factor         |
|---------|----------------|------|-----------------|--------------|--------|---------------------|-------------------------|----------------------------------|-------------------------------|--------------------|----------------|----------------|
|         |                |      |                 |              | l x    |                     | -<br>+ x.               |                                  | + x.                          | = e, =             | + 2.115.       | λ,             |
| No      |                | Vo   | luo             | ight         | x      | 1                   | + x.                    |                                  | + x.                          | $= e_{a} =$        | - 0.804.       | کر<br>ا        |
| 110.    |                | ۷a   | IUG             | Recip<br>Wei | T T    | •                   | + <b>x</b> <sub>0</sub> |                                  | + 30                          | = e. =             | - 0.134        | ۰.<br>م        |
|         | •              |      |                 |              | x      | 7                   | + x.,                   |                                  | + 7.10                        | = e, =             | - 0.770.       | λ.             |
|         | o              | ,    | "               |              | x      | 10                  | + x <sub>1</sub>        |                                  | + X16                         | = e, =             | - 0.730.       | λ.             |
| I       | 67             | 5    | 54.97           | •07          | x      |                     | + X7                    | + 310                            | + X1.                         | = e, =             | - 1.14,        | λ              |
| 2       | 62             | 36   | 12.14           | • 14         | 17 x   | . — IOX.            | + 14 X.                 | -15 Xr                           | + 8x,)                        | U                  |                | - 0            |
| 3       | 50             | 17   | 55.70           | •08          | -21 X  | $+24 X_{10}$        | -21 X,,                 | + 15 X15                         | -11 x <sub>14</sub>           | = e <sub>7</sub> = | + 20 · 5,      | λη             |
| 4       | 69             | 27   | 16.87           | •04          |        | 8 1 12              |                         | - 0 10                           |                               |                    |                |                |
| 5       | 54             | 41   | 13.17           | •10          |        |                     | Equ                     | ations bet                       | ween the fact                 | tors               |                |                |
| 6       | 55             | 51   | 29.87           | •09          |        | <u> </u>            |                         |                                  | Coreffi                       | cients of          |                |                |
| 7       | 67             | 0    | 40.46           | •05          | No. of | Value of            |                         |                                  |                               |                    |                |                |
| 8       | 44             | 59   | 31.20           | •06          | e      | e                   | λ                       | λ                                | λ <sub>3</sub> λ <sub>4</sub> | , λ <sub>5</sub>   | <b>λ</b> 6     | λ <sub>7</sub> |
| 9       | 67             | 59   | 48.20           | •05          | ·      | <u></u>             |                         |                                  | ·····                         |                    |                |                |
| 10      | <b>94</b>      | 26   | 45.01           | •07          | 1      | + 2.115             | +0.39                   |                                  |                               |                    | +0.02 .        | - 0.04         |
| 11      | 44             | 46   | 38.28           | •06          | 2      | <u>- 0.894</u>      |                         | +0.33                            |                               |                    | +0.04 ·        | - 0.34         |
| 12      | 40             | 46   | 36.16           | •07          | 3      | - 0.134             |                         |                                  | +0.10                         |                    | +0.02 .        | - o·86         |
| 13      | 61             | 59   | 21 • 55         | •07          | 4      | - 0.779             |                         |                                  | +0                            | 20                 | +0.02          | + 0.43         |
| 14 .    | 62             | 10   | 23 · 18         | •12          | 5      | - 0.730             |                         |                                  | *                             | +0.33              | +0.02 -        | o·87           |
| 15      | 55             | 50   | 15.08           | •03          | 6      | - 1.14              |                         |                                  |                               |                    | +0.30          |                |
| 1       |                |      |                 | ·            | 7      | + 20 . 5            |                         |                                  |                               |                    |                | + 194 • 97     |
|         | Value          | s of | the Facto       | rs           |        |                     | A                       | ngular err                       | ors in second                 | s                  |                |                |
| · · · · | λ              | =    | + 8.433         | 7            |        |                     |                         |                                  |                               | _                  | 9              |                |
|         | λ              | =    | — 2·963         | 6            |        | $x_1 = +$           | * 204                   | x <sub>6</sub> =                 | - 131                         | x <sub>11</sub> =  | - '205         |                |
|         | $\lambda_8$    | =    | + 1.198         | 3            |        | x <sub>2</sub> = +: | 1 230                   | x <sub>7</sub> =                 | - 1/3                         | ×19 =              | τ·007          |                |
| -       | λ4             | =    | - 2.488         | 7            |        | x <sub>3</sub> = +  | 041<br>• 001            | ∧ <sub>8</sub> ==                |                               | ▲ <sub>18</sub> =  | - 445          |                |
|         | $\lambda_{5}$  | =    | - 1.408         | 8            |        | x <sub>4</sub> = -  | 305                     |                                  |                               | ▲ <sub>14</sub> == | — зн<br>т •ооб |                |
|         | λ <sub>6</sub> | =    | <b>- 4</b> .663 | 8            |        | ▲; = →              | 400                     | ×10 ==                           | - 201                         | A15 ==             | T 000          |                |
|         | λ <sub>7</sub> | =    | + 0.102         | 6            |        |                     |                         | <b>[wx</b> <sup>2</sup> <b>]</b> | = 30.82                       | ·                  |                |                |
|         |                |      |                 |              | 1      |                     |                         |                                  |                               |                    |                |                |

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Figure No. 10.

|      |                        |            |                        |                          |                      | Ob      | serve                  | d Angles          |                      |     |                   |           |                      |
|------|------------------------|------------|------------------------|--------------------------|----------------------|---------|------------------------|-------------------|----------------------|-----|-------------------|-----------|----------------------|
| No.  |                        | Val        | ue                     | Reciprocal<br>Weight     | No.                  |         | Val                    | lue               | Reciprocal<br>Weight | No. |                   | Value     | Reciprocal<br>Weight |
|      | o                      | ,          | "                      |                          |                      | o       | ,                      | "                 |                      |     | o                 | , ,,      |                      |
| I    | 51                     | 24         | 48.47                  | •03                      | 12                   | 36      | 37                     | 0.93              | •14                  | 23  | 44                | 29 22.07  | ·16                  |
| 2    | 57                     | 57         | 48.76                  | .09                      | 13                   | 76      | 14                     | 24.37             | .10                  | 24  | 52                | 10 36.63  | ·c5                  |
| 3    | 70                     | 37         | 22.86                  | .10                      | 14                   | 42      | 55                     | 41.94             | • 16                 | 25  | 50                | 7 57.73   | •06                  |
| 4    | <b>49</b>              | 28         | 9.65                   | •04                      | 15                   | бо      | 49                     | 55°34             | ·08                  | 26  | 77                | 27 34.49  | •06                  |
| 5    | 73                     | 44         | 28.74                  | •06                      | 16                   | 45      | 48                     | 22.10             | .11                  | 27  | 52                | 24 29.51  | •07                  |
| 6    | 56                     | <b>4</b> 7 | 22 · 23                | •10                      | 17                   | 65      | 54                     | 39.37             | •11                  | 28  | 39                | 17 25.13  | .10                  |
| 7    | 47                     | 20         | 17.52                  | •11                      | 18                   | 68      | 16                     | 58.65             | •04                  | 29  | 51                | 58 31.12  | •06                  |
| 8    | 62                     | 5          | 32.73                  | •08                      | 19                   | 58      | 40                     | 37 · 82           | •08                  | 30  | 88                | 44 4.89   | •12                  |
| 9    | 70                     | 34         | 9.80                   | •07                      | 20                   | 62      | 27                     | 54.22             | •08                  | 31  | <b>4</b> 9        | 1 12.20   | •12                  |
| 10   | 89                     | 43         | 57.68                  | •09                      | 21                   | 58      | 51                     | 29.17             | .13                  | 32  | <b>79</b>         | 14 9.52   | •08                  |
| 11   | 53                     | 39         | 3.39                   | •03                      | 22                   | 83      | 20                     | 3.62              | ·05                  | 33  | 51                | 44 39.58  | •07                  |
|      | •                      |            |                        |                          | Equati               | ions to | be s                   | atisfied          |                      |     |                   |           | Factor               |
|      | x <sub>1</sub>         | +          | x <sub>2</sub>         | + x <sub>3</sub>         | •••                  | ••      | •                      |                   |                      | =   | e <sub>1</sub> =  | - 0.764,  | λ <sub>1</sub>       |
|      | x4                     | +          | x <sub>5</sub>         | + x <sub>6</sub>         | •••                  | ••      | •                      |                   | •••                  | =   | e <sub>2</sub> =  | — 0·236,  | λ <sub>2</sub>       |
|      | x,                     | +          | x <sub>8</sub>         | + x <sub>9</sub>         | •••                  | ••      | •                      | •••               | •••                  | =   | e <sub>s</sub> =  | - 0.841,  | λ <sub>3</sub>       |
|      | <b>x</b> <sub>10</sub> | +          | <b>x</b> <sub>11</sub> | + x <sub>13</sub>        | •••                  | ••      | •                      | •••               | •••                  | =   | e, =              | + 0.468,  | λ4                   |
|      | <b>X</b> 18            | +          | x <sub>14</sub>        | + x <sub>15</sub>        | •••                  |         | •                      |                   |                      | =   | e <sub>5</sub> =  | + 0.082,  | $\lambda_5$          |
|      | <b>X</b> 16            | +          | <b>x</b> <sub>17</sub> | + x <sub>18</sub>        | •••                  | ••      | •                      | •••               |                      | =   | e <sub>6</sub> =  | - 0.767,  | λ <sub>6</sub>       |
|      | <b>X</b> 19            | +          | x <sub>90</sub>        | + x <sub>21</sub>        | •••                  | • ••    | •                      | •••               | •••                  | =   | e <sub>7</sub> =  | — 0.70б,  | λ <sub>7</sub>       |
|      | X <sub>23</sub>        | +          | x <sub>23</sub>        | + x <sub>24</sub>        | •••                  |         | •                      | •••               | •••                  | =   | e <sub>8</sub> =  | - 0.101,  | λ <sub>8</sub>       |
|      | X <sub>25</sub>        | +          | X <sub>26</sub>        | + x <sub>27</sub>        | •••                  | ••      | •                      | •••               | •••                  | =   | e <sub>9</sub> =  | - 0.315,  | λ <sub>9</sub>       |
|      | x <sub>28</sub>        | +          | x <sub>29</sub>        | + <b>x</b> <sub>30</sub> | •••                  | ••      | •                      | •••               | •••                  | =   | e <sub>10</sub> = | - 0.468,  | λ <sub>10</sub>      |
|      | <b>x</b> <sub>81</sub> | +          | x <sub>32</sub>        | + x <sub>88</sub>        | •••                  | ••      | •                      | •••               | •••                  | =   | e <sub>11</sub> = | - 0.325,  | λ <sub>11</sub>      |
|      | x <sub>1</sub>         | +          | x4                     | + x <sub>7</sub>         | + x <sub>10</sub>    | +,      | r <sub>18</sub>        | + x <sub>16</sub> | ••••                 | =   | e <sub>19</sub> = | - 0.21,   | λ <sub>12</sub>      |
|      | X <sub>12</sub>        | +          | <br>x <sub>14</sub>    | + x <sub>19</sub>        | + x <sub>23</sub>    | + 3     | <sup>6</sup> 25        | + x <sub>28</sub> | + x <sub>81</sub>    | =   | e <sub>13</sub> = | - 0.33,   | λ <sub>13</sub>      |
| 7    | X <sub>3</sub>         | -13<br>-16 | X <sub>2</sub><br>X    | $+ 14 x_6$               | $-7 x_5$             | + 72    | <b>K</b> g<br>K10      | $-11 x_8$         | }                    | =   | $e_{14} =$        | -15.7,    | λ <sub>14</sub>      |
| T 49 | -19<br>X.c             | -10        | <b>~</b> 11<br>▼       | + 16 x                   | ~3 ~14               | +       | -18                    | _ 17 -            | /<br>                |     |                   |           |                      |
| -    | *18<br>X <sub>30</sub> | + 4        | ^15<br>X <sub>26</sub> | - 16 x <sub>27</sub>     | + 22 X <sub>23</sub> | -173    | -32<br>5 <sub>94</sub> | $+11 x_{20}$      | $-13 x_{21}$         | =   | e <sub>15</sub> = | + 14 • 5, | $\lambda_{15}$       |

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| Figure | No. | 10( | (Continu | ed). |
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|        |     |     |          |      |

|            |                                                                                                                                                                                        |                                                                                                |                                                                                  |               | 1                                       | Equati                                                                                                                                                          | ons be         | tween t                                                                                         | he fac                  | tors                                                                                                                                                   |                 |                                                                           |                 |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |                                                                                      |      |                 |
|------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------|---------------|-----------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------|-------------------------------------------------------------------------------------------------|-------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------|---------------------------------------------------------------------------|-----------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------|------|-----------------|
| No. of     | Value of                                                                                                                                                                               |                                                                                                |                                                                                  |               |                                         |                                                                                                                                                                 |                | C                                                                                               | o-effici                | ents of                                                                                                                                                |                 |                                                                           |                 |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |                                                                                      |      |                 |
| e          | .e                                                                                                                                                                                     | λ                                                                                              | λ                                                                                | $\lambda_{s}$ | λ,                                      | λ                                                                                                                                                               | λ <sub>6</sub> | λη                                                                                              | λ <sub>8</sub>          | λ <sub>9</sub>                                                                                                                                         | λ <sub>10</sub> | λ <sub>11</sub>                                                           | λ <sub>19</sub> | λ <sub>13</sub>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | $\lambda_{14}$                                                                       |      | λ <sub>15</sub> |
| I          | - 0.764                                                                                                                                                                                | + 0.33                                                                                         |                                                                                  |               |                                         |                                                                                                                                                                 |                |                                                                                                 |                         |                                                                                                                                                        |                 |                                                                           | +0.03           | -                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | - 0 <sup>.</sup> 4                                                                   | 7    |                 |
| 2          | - 0.236                                                                                                                                                                                |                                                                                                | + 0.30                                                                           |               |                                         |                                                                                                                                                                 |                |                                                                                                 |                         |                                                                                                                                                        |                 |                                                                           | + 0.04          | •                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | + 0.9                                                                                | 8    |                 |
| 3          | - 0.841                                                                                                                                                                                |                                                                                                |                                                                                  | +0.30         | 5                                       |                                                                                                                                                                 |                |                                                                                                 |                         |                                                                                                                                                        |                 |                                                                           | +0.11           | -                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | - 0.3                                                                                | 9    |                 |
| <b>4</b> ' | + 0.468                                                                                                                                                                                |                                                                                                |                                                                                  |               | +0.36                                   | i                                                                                                                                                               |                |                                                                                                 |                         |                                                                                                                                                        |                 |                                                                           | +0.09           | +0.14                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 | + 3.2                                                                                | 8 +  | 0.48            |
| 5          | + 0.083                                                                                                                                                                                |                                                                                                |                                                                                  |               |                                         | +0.3                                                                                                                                                            | 4              |                                                                                                 |                         |                                                                                                                                                        |                 |                                                                           | + 0.10          | +0.16 ·                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | - 2.7                                                                                | 2 -  | 0.46            |
| 6          | - 0.767                                                                                                                                                                                |                                                                                                |                                                                                  |               |                                         |                                                                                                                                                                 | +0.3           | 6                                                                                               |                         |                                                                                                                                                        |                 |                                                                           | +0.11           |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | — 0 <sup>.</sup> 7                                                                   | '4   |                 |
| 7          | - 0.706                                                                                                                                                                                |                                                                                                |                                                                                  |               |                                         |                                                                                                                                                                 |                | +0.5                                                                                            | 9                       |                                                                                                                                                        |                 |                                                                           |                 | + 0.08                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                                                                                      |      | <b>0.8</b> 3    |
| 8          | - 0.101                                                                                                                                                                                |                                                                                                |                                                                                  |               |                                         |                                                                                                                                                                 | •              |                                                                                                 | +0.3                    | 26                                                                                                                                                     |                 |                                                                           |                 | +0.02                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |                                                                                      | +    | <b>2</b> .62    |
| 9          | - 0.312                                                                                                                                                                                |                                                                                                |                                                                                  |               |                                         |                                                                                                                                                                 |                |                                                                                                 |                         | +0.                                                                                                                                                    | 19              |                                                                           |                 | +0.00                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |                                                                                      | -    | 0.8             |
| 10         | - 0.468                                                                                                                                                                                |                                                                                                |                                                                                  |               |                                         | *                                                                                                                                                               |                |                                                                                                 |                         |                                                                                                                                                        | +0.             | 28                                                                        |                 | +0.10                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |                                                                                      | +    | 0.90            |
| 11         | - 0.325                                                                                                                                                                                |                                                                                                |                                                                                  |               |                                         |                                                                                                                                                                 |                |                                                                                                 |                         |                                                                                                                                                        |                 | +0.3                                                                      | 27              | + 0.13                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                                                                                      |      | 0.8             |
| 12         | - 0.31                                                                                                                                                                                 |                                                                                                |                                                                                  |               |                                         |                                                                                                                                                                 |                |                                                                                                 |                         |                                                                                                                                                        |                 |                                                                           | +0.48           | 3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                                                                                      | +    | 0.2             |
| 13         | - 0.33                                                                                                                                                                                 |                                                                                                |                                                                                  |               |                                         |                                                                                                                                                                 |                |                                                                                                 |                         |                                                                                                                                                        |                 |                                                                           |                 | +0.71                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 | + . 0.                                                                               | 38   |                 |
| 14         | -15.7                                                                                                                                                                                  |                                                                                                |                                                                                  |               | -                                       |                                                                                                                                                                 |                |                                                                                                 |                         |                                                                                                                                                        |                 |                                                                           |                 |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | + 291.5                                                                              | 58 — | 19.2            |
| 15         | +14.2                                                                                                                                                                                  |                                                                                                |                                                                                  |               |                                         |                                                                                                                                                                 |                |                                                                                                 |                         |                                                                                                                                                        |                 |                                                                           |                 |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |                                                                                      | +    | 203.0           |
| 1          | Values of th                                                                                                                                                                           | e Facto                                                                                        | rs                                                                               |               | •                                       |                                                                                                                                                                 | • ·            |                                                                                                 | Ang                     | ular er                                                                                                                                                | rors in         | secon                                                                     | ds              |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |                                                                                      |      |                 |
|            | $\lambda_1 = -$ $\lambda_3 = -$ $\lambda_3 = -$ $\lambda_4 = +$ $\lambda_6 = -$ $\lambda_7 = -$ $\lambda_6 = -$ $\lambda_7 = -$ $\lambda_10 = -$ $\lambda_{11} = -$ $\lambda_{11} = -$ | 3.897<br>0.901<br>3.976<br>2.653<br>1.105<br>3.842<br>2.362<br>0.934<br>1.512<br>1.91<br>1.151 | 2 2<br>4 4<br>5 3<br>3 0<br>5 5<br>5 5<br>7 1<br>4 1<br>1 2<br>5 5<br>7 2<br>5 4 |               | · · ·<br>· ·<br>· · ·<br>· · ·<br>· · · | Σ <sub>1</sub><br>Σ <sub>8</sub><br>Σ <sub>3</sub><br>Σ <sub>4</sub><br>Σ <sub>6</sub><br>Σ <sub>7</sub><br>Σ <sub>8</sub><br>Σ <sub>9</sub><br>Σ <sub>10</sub> |                | · 076<br>· 220<br>· 468<br>· 018<br>· 007<br>· 247<br>· 288<br>· 219<br>· 334<br>· 361<br>· 156 | · · ·<br>· · ·<br>· · · | $X_{19} =$<br>$X_{13} =$<br>$X_{14} =$<br>$X_{15} =$<br>$X_{16} =$<br>$X_{17} =$<br>$X_{18} =$<br>$X_{19} =$<br>$X_{20} =$<br>$X_{21} =$<br>$X_{23} =$ |                 | 049<br>049<br>275<br>242<br>274<br>299<br>194<br>170<br>146<br>390<br>034 |                 | $     \begin{array}{rcl}         & x_{33} & = & + \\         & x_{34} & = & - \\         & x_{35} & = & - \\         & x_{36} & = & - \\         & x_{37} & = & - \\         & x_{39} & = & - \\         & x_{30} & = & - \\         & x_{30} & = & - \\         & x_{31} & = & - \\         & x_{32} & = & - \\         & x_{33} & = & - \\        $ | •021<br>•088<br>•076<br>•079<br>•160<br>•167<br>•065<br>•236<br>•109<br>•077<br>•139 |      |                 |
|            | $\lambda_{13} = +$<br>$\lambda_{13} = +$<br>$\lambda_{16} = -$<br>$\lambda_{15} = +$                                                                                                   | 0.24<br>0.11<br>0.04                                                                           | 5 <del>4</del><br>70<br>22<br>85                                                 |               | • • •                                   |                                                                                                                                                                 |                |                                                                                                 |                         | [wx <sup>\$</sup> _                                                                                                                                    | ] = 10          | 5.26                                                                      |                 |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |                                                                                      |      |                 |

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| Figure    | No. | 11. |
|-----------|-----|-----|
| 2 99 40 0 |     |     |

|     | Observed Angles              |              |                | <u></u>                 | E                          | quations            | s to be sat                                        | tisfied                 |             |                          |                | Fac | tor            |
|-----|------------------------------|--------------|----------------|-------------------------|----------------------------|---------------------|----------------------------------------------------|-------------------------|-------------|--------------------------|----------------|-----|----------------|
|     |                              |              |                | x <sub>1</sub>          | + 2                        | د <u>م</u> .        | + x                                                | 8                       | =           | $e_1 = -$                | 0.218,         | λ   | 1              |
|     |                              | cal<br>t     |                | x4                      | + 2                        | ۲.                  | + x                                                | 6                       | =           | e <sub>3</sub> = -       | 0.140,         | λ   | 2              |
| No. | Value                        | ipro<br>eigh |                | <b>x</b> <sub>7</sub> - | +:                         | K.8                 | + x                                                | <b>4</b> 9              | =           | e <sub>s</sub> = -       | 0.222,         | λ   | 8              |
|     | ``                           | Rec<br>W     |                | <b>x</b> <sub>10</sub>  | +:                         | <b>K</b> 11         | + x                                                | <sup>6</sup> 1 <b>2</b> | =           | e <sub>4</sub> = +       | 0.734,         | λ   | 4              |
|     |                              |              |                | <b>x</b> <sub>18</sub>  | +:                         | x <sub>14</sub>     | + x                                                | <sup>2</sup> 15         | =           | $e_{5} = +$              | 0·140,         | λ   | 5              |
|     |                              |              |                | <b>x</b> <sub>16</sub>  | +:                         | к <sub>17</sub>     | + x                                                | <sup>2</sup> 18         | =           | e <sub>6</sub> = -       | 0.539,         | λ   | 6              |
|     | 02 7 <u>5</u> 9 12           | •03          | x <sub>1</sub> | +x, +                   | • <b>x</b> <sub>7</sub> +: | κ <sub>10</sub> +   | x <sub>18</sub> + x                                | 16                      | =           | e <sub>7</sub> = -       | · 1·38,        | λ   | 7              |
| 2   | 50 5 3.70                    | •09          |                | 12 x <sub>8</sub>       | -15                        | K <sub>S</sub>      | +12 X                                              | 6)                      |             |                          |                |     |                |
| 3   | 01 40 50.04                  | -00          | .              | -23 x5                  | +19:                       | K.9                 | — 6 x                                              | 8                       | _           | o I                      |                | ``  |                |
| 4   | 78 0 52.85                   | •07          |                | + 5 x <sub>19</sub>     | - 23                       | x <sub>11</sub>     | +11 x                                              | ×15                     | -           | e <sub>8</sub> = +       | 47*9,          |     | 8              |
| 5   | 42 38 49.50                  | •09          |                | — бх <sub>14</sub> .    | + 19                       | x <sub>18</sub>     | — 5 x                                              | ( <sub>17</sub> )       |             |                          |                |     |                |
| 0   | 59 14 18.83                  | •05          |                |                         |                            |                     |                                                    |                         |             |                          |                |     |                |
| . 7 | 57 43 53.58                  | •13          |                |                         |                            | Equatio             | ns betwee                                          | n the fa                | ctors       |                          |                |     |                |
| 0   | 74 27 30.12                  | •05          |                |                         |                            |                     |                                                    | Coeffi                  | niente      | of                       |                |     |                |
| 9   | 47 48 31.30                  | •09          | No. of         | Value of                |                            |                     |                                                    | C0-em                   |             | <u> </u>                 |                |     |                |
| 10  | 00 54 10.20                  | •04          | e              | e                       | λ                          | λ                   | λ <sub>s</sub>                                     | λ4                      | $\lambda_5$ | $\lambda_6$              | λ <sub>7</sub> |     | λ <sub>8</sub> |
|     | 43 27 43.49                  | •04          | T              | - 0,218                 | +0.18                      | · <u>····</u> ····· |                                                    |                         |             |                          | +0.03          |     | 0.63           |
| 12  | 75 38 8.15                   | •07          | 2              | - 0.140                 |                            | +0.31               |                                                    |                         |             |                          | +0.02          | _   | 1.42           |
| 13  | <b>43</b> 59 57 40           | •04          | 2              | - 0.322                 |                            |                     | +0.22                                              |                         |             |                          | +0.13          | +   | 1.41           |
| 14  | 74 18 34.97                  | •09          | 3              | + 0.721                 |                            |                     | 10 -)                                              | +0.12                   |             |                          | +0.04          | _   | 0.57           |
| 15  | 01 41 28.43                  | •14          |                | + 0.140                 |                            |                     |                                                    |                         | +0.3        | 7                        | +0.04          | +   | 1.00           |
| 10  | 57 7 5.35                    | •01          | 6              | - 0.20                  | ]                          |                     | *                                                  |                         |             | /<br>+0.13               | +0.01          | •   | 0.41           |
| 17  | 70 9 57.39                   | •07          | 7              | - 1.38                  |                            |                     |                                                    |                         |             |                          | +0.33          | •   | ~ 7-           |
| 18  | 40 42 57 99                  | •04          | 8              | + 47.0                  |                            |                     |                                                    |                         |             |                          | 10 34          | ±1' | 77.07          |
|     |                              |              |                | T 4/ 9                  |                            |                     |                                                    |                         |             |                          | •              |     |                |
|     | Values of the Factor         | <b>rs</b>    |                |                         |                            | Angu                | lar errors                                         | in secor                | 1 <b>d8</b> | •                        |                |     |                |
|     | $\lambda_1 = + 1.0128$       | 8            |                | $x_1 = -$               | - • 157                    |                     | $x_{7} = -$                                        | •758                    |             | x <sub>13</sub> =        | - • 242        |     |                |
|     | $\lambda_3 = + 3.7811$       | Ľ            |                | x, = -                  | - • 365                    |                     | $x_8 = -$                                          | •080                    |             | <b>x</b> <sub>14</sub> = | — ·165         |     |                |
|     | $\lambda_3 = + 0.4230$       | Ċ            |                | $x_3 = +$               | • • 304                    |                     | x <sub>9</sub> = +                                 | •616                    |             | <b>x</b> <sub>15</sub> = | + • 547        |     |                |
|     | $\lambda_4 = + 7.843$        | 5            |                | $x_4 = -$               | - • 173                    |                     | $x_{10} = +$                                       | •064                    |             | <b>x</b> <sub>16</sub> = | - 114          |     |                |
|     | $\lambda_{5} = + 0.1932$     | 4            |                | $x_s = -$               | - • 359                    |                     | $x_{11} = +$                                       | •003                    |             | <b>x</b> <sub>17</sub> = | 477            |     |                |
| 1   | $\lambda_6 = -5.1249$        | 9            |                | $x_6 = +$               | • 392                      |                     | $x_{12} = +$                                       | •667                    |             | <b>x</b> <sub>18</sub> = | + .052         |     |                |
|     | $\lambda_7 = - 6 \cdot 2498$ | 8            |                |                         |                            |                     |                                                    |                         |             |                          |                |     |                |
|     | $\lambda_8 = + 0.3378$       | 8            |                |                         |                            |                     | $[\mathbf{w}\mathbf{x}^{\mathbf{s}}] = \mathbf{s}$ | 32.21                   |             |                          |                |     |                |

| <b>Figure</b> 1 | Vo. 12. |
|-----------------|---------|
|-----------------|---------|

|     | Observed A   | Angles         |        | Equations to be satisfied Fa |                                   |                          |                                   |                  |                    |           |     |                |  |  |
|-----|--------------|----------------|--------|------------------------------|-----------------------------------|--------------------------|-----------------------------------|------------------|--------------------|-----------|-----|----------------|--|--|
|     |              |                | -      | x <sub>1</sub>               | + x,                              | l                        | + x <sub>3</sub>                  |                  | $= e_1 =$          | • + 0·678 | ,   | λ <sub>1</sub> |  |  |
|     |              | cal            |        | x,                           | + x,                              | i                        | + x <sub>6</sub>                  |                  | = e <sub>9</sub> = | - 0.101   | ,   | λ              |  |  |
| No. | Value        | sipro<br>/eigl |        | <b>x</b> 7                   | + x <sub>e</sub>                  | 5                        | + x,                              |                  | = e <sub>3</sub> = | - 0.524   | ,   | λ              |  |  |
|     |              | Rec            |        | <b>x</b> <sub>10</sub>       | + x <sub>1</sub>                  | 1                        | + x <sub>12</sub>                 |                  | = e <sub>4</sub> = | - 0.137   | ,   | λ,             |  |  |
|     |              |                | -      | <b>x</b> <sub>13</sub>       | + x <sub>1</sub>                  | 4                        | + x <sub>15</sub>                 |                  | = e <sub>6</sub> = | + 0.038   | ,   | λ              |  |  |
|     | 72 22 4      | "<br>8:06 :0r  |        | <b>x</b> <sub>16</sub>       | + x <sub>1</sub>                  | 7                        | + x <sub>18</sub>                 |                  | = e <sub>6</sub> = | - 0.104   | ,   | $\lambda_6$    |  |  |
| 2   | 52 12 A      | 7.50 .14       | x1     | + x4 -                       | + x <sub>7</sub> + x <sub>1</sub> | 0 +x                     | x <sub>13</sub> + x <sub>16</sub> |                  | $= e_{7} =$        | + 0.34,   |     | λ7             |  |  |
| 2   | 55 -4 4/     | / Jy +4        |        | 16 x <sub>3</sub>            | — 15 x <sub>2</sub>               |                          | + 2 x <sub>6</sub>                | )                |                    |           |     |                |  |  |
|     | 12 28 E      | 2.80 .00       |        | — 16 x <sub>5</sub>          | + 19 x9                           |                          | — 19 x <sub>8</sub>               | (                |                    |           |     |                |  |  |
| 5   | 52 2A 5      | 8.20 .07       |        | +21 x <sub>12</sub>          | — 7 x <sub>1</sub> ;              | L                        | + 1 1 x <sub>15</sub>             | (                | $= e_8 =$          | -51.2,    |     | λ <sub>8</sub> |  |  |
| 6   | <u> </u>     | 0.30 .04       |        | $-5 x_{14}$                  | $+ 7 x_{10}$                      | 3                        | -16 x <sub>17</sub>               | )                |                    |           |     |                |  |  |
| 7   | 84 42 5T     | 1.22 · CQ      |        |                              |                                   |                          | •                                 |                  |                    |           |     |                |  |  |
| 8   | 47 18 16     | 5·28 ·04       |        |                              | Eq                                | uations                  | between t                         | he factor        |                    |           |     |                |  |  |
| 9   | 47 58 52     | 2·55 •07       |        |                              |                                   |                          |                                   | Co-efficie       | nts of             |           |     |                |  |  |
| 10  | 63 22 13     | 8·72 ·06       | No. of | Value of                     |                                   |                          | <u> </u>                          |                  |                    |           |     |                |  |  |
| 11  | 72 20 52     | .44 .04        |        | e                            | λ <sub>1</sub>                    | λ                        | $\lambda_3$                       | λ <sub>4</sub> λ | -5 λ               | , λη      |     | λ <sub>8</sub> |  |  |
| 12  | 44 16 54     | .52 .07        | I      | + 0.678                      | +0.27                             |                          |                                   |                  |                    | +0.02     |     | 0.82           |  |  |
| 13  | 42 10 17     | •63 •06        | 2      | - 0.101                      | 4                                 | -0.12                    |                                   |                  |                    | +0.0Q     | -   | 1.04           |  |  |
| 14  | 76 48 39     | · 26 · 06      | 3      | - 0.224                      |                                   | -                        | +0.12                             |                  |                    | +0.0Q     | +   | 0.57           |  |  |
| 15  | 61 1 4       | •08 •04        | 4      | - 0.137                      |                                   |                          | + 0                               | 0.17             |                    | +0.06     | +   | 1.10           |  |  |
| 16  | 53 42 56     | •01 •10        | 5      | + 0.038                      |                                   |                          |                                   | +0               | • 16               | +0.06     | +   | 0.14           |  |  |
| 17  | 53 48 29     | .32 .02        | 6      | - 0.104                      |                                   | ;                        | ŧ                                 |                  | +0.                | 26 +0.10  | +   | 0.66           |  |  |
| 18  | 72 28 35     | ·62 ·14        | 7      | + 0.34                       |                                   |                          |                                   |                  |                    | +0.39     |     |                |  |  |
|     |              |                | 8      | -51.2                        |                                   |                          |                                   |                  |                    |           | + 1 | 60.92          |  |  |
| V   | alnes of the | Factors        |        |                              |                                   |                          | •                                 |                  |                    |           | ÷—  |                |  |  |
|     |              |                |        |                              |                                   | Ingular                  | errors in s                       | seconds          |                    |           |     |                |  |  |
| Х   | $y_1 = + I$  | 2381           |        | $x_1 = +$                    | • 135                             | <b>X</b> 7               | =06                               | 2                | $x_{13} = -$       | + .086    |     |                |  |  |
| λ   | $y_{3} = -3$ | 1290           |        | $x_{g} = +$                  | •866                              | <b>X</b> 8 :             | = + ·15                           | ſ                | $x_{14} = -$       | + •098    |     |                |  |  |
| λ   | -3 = -2      | 4916           |        | $x_3 = -$                    | • 323                             | X9                       | = - ·61                           | 3                | $x_{15} = -$       | 146       |     |                |  |  |
| У   | $h_4 = + 0$  | 9886           |        | $x_4 = -$                    | .100                              | <b>x</b> <sub>10</sub> : | = + •142                          | 7                | $x_{16} = -$       | + •134    |     |                |  |  |
| у   | -5 = -0.     | 0218           |        | $x_{5} = +$                  | • 151                             | <b>x</b> 11 :            | = + .13                           | 2                | $x_{17} = -$       | + .103    |     |                |  |  |
| λ   | $r_6 = - 0.$ | 1244           |        | $x_6 = -$                    | • 152                             | <b>X</b> 12 :            | =416                              | 5                | $x_{18} = -$       | - 341     |     |                |  |  |
| λ   | -7 = + 1.    | 4616           |        |                              |                                   |                          |                                   |                  |                    |           |     |                |  |  |
| λ   | $r_8 = - 0.$ | 3300           |        |                              |                                   | [wx <sup>9</sup>         | <sup>s</sup> ] = 19.7             | 3                |                    |           |     | •              |  |  |

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|        | Observed Angles        |                      |                          |                      |                      |            |                      |                  |                                     |                      |  |  |
|--------|------------------------|----------------------|--------------------------|----------------------|----------------------|------------|----------------------|------------------|-------------------------------------|----------------------|--|--|
| No.    |                        | Value                | Reciprocal<br>Weight     | No.                  | Val                  | ue         | Reciprocal<br>Weight | No.              | Value                               | Reciprocal<br>Weight |  |  |
| Ŧ      | 0<br>70                | · //                 | .07                      | 10                   |                      | "          |                      | 10 6             |                                     |                      |  |  |
| -      | 79                     | 25 5 70              | .01                      |                      | 05 47                | 35 00      | 10                   | 19 0             | 5 57 15 80                          | 10                   |  |  |
| ~      | *ر<br>مە               | 44 Jº 43             |                          |                      | 70 4<br>11 <b>-</b>  | 43 34      | 04                   | 20 0.            | 30 15 29                            | 03                   |  |  |
| 3      | 47                     | 41 59 44             |                          | 12                   | 44 7                 | 41.20      | -04                  | 21 5             | 20 29 07                            | .05                  |  |  |
| 4      | 00                     | 2 25.70              | •03                      | 13                   | 00 4                 | 20.48      | •07                  | 22 73            | 3 5 <sup>2</sup> 44 <sup>.</sup> 47 | •07                  |  |  |
| 5      | 45                     | 15 20.09             | •08                      | 14                   | 57 46                | 10.32      | •03                  | 23 5.            | 5 53 <del>2</del> 4·55              | •06                  |  |  |
| 6      | 74                     | 42 14.27             | •06                      | 15                   | 62 9                 | 23.44      | ·07                  | 24 50            | 5 13 49.72                          | ·05                  |  |  |
| 7      | 56                     | 49 15.65             | •04                      | 16                   | 37 21                | 10.02      | •04                  | 25 80            | 51 26.94                            | •10                  |  |  |
| 8      | 53                     | 56 55.09             | ` <b>•</b> 07            | 17                   | 81 56                | 24.10      | .13                  | 26 30            | 5 6 17.23                           | •04                  |  |  |
| 9      | 69                     | 13 48.90             | •05                      | 18                   | 60 42                | 26.01      | •05                  | 27 6             | 3 2 16.33                           | •06                  |  |  |
|        | •                      |                      |                          | Equati               | ons to be sa         | tisfied    |                      |                  |                                     | Factor               |  |  |
| :      | x <sub>1</sub>         | + x <sub>2</sub>     | + x <sub>3</sub>         | •••                  | •••                  | •••        | •••                  | = e <sub>1</sub> | = + 0.717,                          | λ <sub>1</sub>       |  |  |
| :      | X4                     | + x <sub>5</sub>     | + x <sub>6</sub>         | •••                  | •••                  | •••        | •••                  | = e <sub>2</sub> | = - 0.333,                          | $\lambda_2$          |  |  |
| :      | <b>x</b> 7             | + x <sub>8</sub>     | + x <sub>9</sub>         | •••                  | •••                  | •••        | •••                  | = e <sub>3</sub> | = - 0.639,                          | λ <sub>s</sub>       |  |  |
| :      | <b>x</b> <sub>10</sub> | + x <sub>11</sub>    | + x <sub>12</sub>        | •••                  |                      |            | •••                  | = e4             | = - 0.075,                          | λ4                   |  |  |
| :      | <b>x</b> <sub>18</sub> | + x <sub>14</sub>    | + x <sub>15</sub>        | •••                  | •••                  | •••        | •••                  | = e <sub>6</sub> | = - 0.195,                          | $\lambda_{g}$        |  |  |
| 3      | X <sub>16</sub>        | + x <sub>17</sub>    | + <b>x</b> <sub>18</sub> |                      | •••                  | •••        |                      | = e <sub>6</sub> | = - 0.131,                          | λ <sub>6</sub>       |  |  |
| :      | x <sub>19</sub>        | + x <sub>20</sub>    | + x <sub>21</sub>        | •••                  |                      |            |                      | = e <sub>7</sub> | = - 0.281,                          | λ <sub>7</sub>       |  |  |
| 3      | X23                    | + x <sub>98</sub>    | + X 94                   | •••                  | •••                  | •••        |                      | $= e_{s}$        | = -1.890,                           | λ <sub>8</sub>       |  |  |
| 3      | Xos                    |                      | + Xar                    |                      |                      |            |                      | = e,             | = + 0.030                           | λ                    |  |  |
| · .    | Σ,                     | +x.                  | + X.                     | + X10                | + x,,                | + x.,      |                      | = 6.0            | = - 0.66.                           | λιο                  |  |  |
| 3      | -1<br>Xo               | + <b>x</b> .,        | + X                      | + X-0                | + Xar                | . —10      |                      | = 6              | = - 0.40                            | )<br>)               |  |  |
| 201    | -,<br>T.               | - 16 -               | , ~19<br>T V A           | 23                   | 1 8 <del>1</del> 2   | <u> </u>   |                      |                  |                                     |                      |  |  |
| + 21 1 | ~8<br>K <sub>19</sub>  | $-8x_{11}$           | $+ 12 x_{15}$            | $-13 x_{14}$         | + 12 X <sub>18</sub> | $-3x_{17}$ | •••                  | $= e_{12}$       | = +33.8,                            | λ <sub>13</sub>      |  |  |
| 93     | <b>x</b> <sub>10</sub> | — 21 x <sub>19</sub> | + 16 x <sub>8</sub> ·    | — 14 X <sub>7</sub>  | + 29 X <sub>26</sub> |            |                      | _                | - 1.0010                            |                      |  |  |
| -105   | x <sub>27</sub>        | + 14 X <sub>23</sub> | — 18 x <sub>24</sub>     | + 11 X <sub>20</sub> | $-16 x_{g1}$         | •••        | •••                  | $= e_{13}$       | = +29.3,                            | ^ <u>13</u>          |  |  |

Figure No. 13.

| Figure No. | 18—( | Contin | ued). |  |
|------------|------|--------|-------|--|
|------------|------|--------|-------|--|

|        |                    |                      |       |       | Equa       | tions b     | etween t              | he factor   | :8                   |               |                 |                   |                 |                              |  |  |
|--------|--------------------|----------------------|-------|-------|------------|-------------|-----------------------|-------------|----------------------|---------------|-----------------|-------------------|-----------------|------------------------------|--|--|
| No. of | Value of           | f Co-efficients of . |       |       |            |             |                       |             |                      |               |                 |                   |                 |                              |  |  |
| e      | e                  | λ <sub>1</sub>       | λ     | λ     | λ4         | $\lambda_5$ | <b>λ</b> <sub>6</sub> | λη          | λ <sub>8</sub>       | λ             | λ <sub>10</sub> | λ <sub>11</sub>   | λ <sub>13</sub> | λ <sub>13</sub>              |  |  |
| I      | + 0.111            | +0.30                |       |       |            |             |                       |             |                      |               | +0.01           |                   | + 1.10          |                              |  |  |
| 2      | - 0.333            |                      | +0.12 |       |            |             |                       |             |                      |               | + 0.03          |                   | - 1.32          |                              |  |  |
| 3      | - 0.639            |                      |       | +0.10 |            |             |                       |             |                      |               | +0.04           | +0.02             | - 0.72          | + 0.26                       |  |  |
| 4      | - 0.022            |                      |       |       | +0.18      |             |                       |             |                      |               | +0.10           | +0.04             | + 0.23          | + 0.00                       |  |  |
| 5      | - 0.192            |                      |       |       |            | +0.12       |                       |             |                      |               | + 0.07          |                   | + 0.42          |                              |  |  |
| 6      | - 0.121            |                      |       |       |            |             | +0.33                 |             |                      |               | +0'04           |                   | + 0.31          |                              |  |  |
| 7      | - 0.281            |                      |       |       |            |             |                       | +0.18       |                      |               |                 | +0.10             |                 | - 0.47                       |  |  |
| 8      | - 1.890            |                      |       |       |            |             |                       |             | +0.18                |               |                 | +0.02             |                 | - 0.06                       |  |  |
| 9      | + 0.039            |                      |       |       |            | *           |                       |             |                      | +0.30         |                 | +0.10             |                 | + 0.26                       |  |  |
| 10     | - 0.66             |                      |       |       |            |             |                       |             |                      |               | +0.32           |                   |                 | + 0.34                       |  |  |
| 11     | - 0.49             |                      |       |       |            |             |                       |             |                      |               |                 | +0.36             | + 0.08          |                              |  |  |
| 12     | + 33 · 8           |                      |       |       |            |             |                       |             |                      |               |                 |                   | + 148.52        | <b>- 3</b> 5 <sup>.</sup> 56 |  |  |
| 13     | + 29.3             |                      |       |       |            |             |                       |             |                      |               |                 |                   |                 | + 135.23                     |  |  |
| v      | alues of the       | Factors              |       |       |            |             |                       | Angular     | errors i             | n second      | 8               |                   |                 |                              |  |  |
| λ      | 1 = +              | 2.6042               |       |       | X.         | = +         | •065                  | <br>X.,     | = + •                | 011           | x               |                   | •043            |                              |  |  |
| λ      | <sub>2</sub> = +   | 0.4294               |       |       | -1<br>T.   | = -         | •068                  | -10<br>X-1  |                      | 018           |                 |                   | •022            |                              |  |  |
| λ      | s = -              | 4.2697               |       |       | -3<br>T.   | = +         | • 720                 | ~11<br>T    |                      | 010           |                 |                   | •257            |                              |  |  |
| λ      | 4 = -              | 0.9689               |       | •     |            | — -<br>— _  | •007                  | *19<br>•    | ·                    | 100           | ~;<br>•         |                   | .619            |                              |  |  |
| λ      | 5 = -              | 1.1747               |       |       | -4<br>     |             | •37                   | <u>≁</u> 18 | · ·                  | 199           | •<br>•          | 20                |                 |                              |  |  |
| λ      | s = -              | 0.6407               |       |       | - A5       |             | 419                   | ^14<br>-    |                      | 140           | •<br>•          |                   | 431             |                              |  |  |
| λ      | n = -              | 2 • 2597             |       |       | 6<br>      | T           | 123                   | ×15         | — T                  | 144           | •<br>•          | u — -             | 1040            |                              |  |  |
| λ      | <sub>8</sub> = - 1 | 1 • 4442             |       |       | Χη<br>     |             | 400                   | ×16         |                      | 192           |                 | ks = +<br>        | - 009           |                              |  |  |
| λ      | , = -              | 2.0023               |       |       | <b>x</b> 8 | = -         | - 200                 | <b>X</b> 17 | = - ·                | 109           | x,              | <sub>16</sub> = + | - 273           |                              |  |  |
| λ      | 10 = -             | 1.6667               |       |       | X9         | = +         | -029                  | <b>X</b> 18 | = + ·                | 130           | X,              | m = -             | .303            |                              |  |  |
| λ      | n = +              | 2.6889               |       |       |            |             |                       |             |                      |               |                 |                   |                 |                              |  |  |
| λ      | 12 = +             | 0.2697               |       |       |            |             |                       | [w]         | <sup>(8</sup> ] = 44 | <b>4 · 86</b> |                 |                   |                 |                              |  |  |
| λ      | 18 = +             | 0•3046               |       |       |            | -           |                       |             |                      |               |                 |                   |                 |                              |  |  |
|        |                    |                      |       |       |            |             |                       |             |                      |               |                 |                   |                 |                              |  |  |

September 1878.

J. B. N. HENNESSEY, In charge of Computing Office. Digitized by

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### PRINCIPAL TRIANGULATION. TRIANGLES.

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| No. of t | riangle         | Station .         | rical<br>xea                              | Cor                                | rections to (                           | Observed A          | ngle                                                                                                                         | Corrected Plane                                                                                                                                             | Distance                                  |                                     |                            |  |  |
|----------|-----------------|-------------------|-------------------------------------------|------------------------------------|-----------------------------------------|---------------------|------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------|-------------------------------------|----------------------------|--|--|
| Circuit  | Non-<br>circuit | Station           | Sphe<br>Exc                               | Figure                             | Circuit                                 | Non-<br>circuit     | Total                                                                                                                        | Angle                                                                                                                                                       | Log. feet                                 | Feet                                | Miles                      |  |  |
| I        |                 | XLI<br>XLIV<br>I  | *<br>1 * 545<br>1 * 546<br>1 * 546        | *<br>- ` 193<br>- ` 190<br>- ` 110 | + • • • • • • • • • • • • • • • • • • • | "                   | "<br>- '132<br>- '190<br>- '171                                                                                              | 38 58 34 °073<br>67 46 16 °374<br>73 15 9 °553                                                                                                              | 5°0716171,6<br>5°2394300,7<br>5°2541461,0 | 117928.06<br>173552.19<br>179533.76 | 22°335<br>32°870<br>34°003 |  |  |
| 2        |                 | XLI<br>I<br>II    | * 896<br>*895<br>*896                     | + °032<br>- °227<br>- °028         | + .090<br>118<br>+ .010                 |                     | $+ \cdot 131$<br>$- \cdot 345$<br>$- \cdot 009$                                                                              | 42 I 19°015<br>32 57 38°300<br>105 I 2°685                                                                                                                  | 5`0802173,1<br>4`9901706,7<br>5`2394300,7 | 120286.62<br>97762.13<br>173552.19  | 22°782<br>18°516<br>32°870 |  |  |
|          | 49              | XLI<br>XLIV<br>II | 1°368<br>1°367<br>1°367                   | - · 161<br>+ · 050<br>- · 087      |                                         | +.160<br>121<br>039 | $ \begin{array}{r} - \cdot \infty 1 \\ - \cdot 071 \\ - \cdot 126 \\ \end{array} $                                           | 80 59 54 161<br>30 27 7 162<br>68 32 58 677                                                                                                                 | 5°2799381,5<br>4°9901706,7<br>5°2541461,0 | 190518*93<br>97762*13<br>179533*76  | 36°083<br>18°516<br>34°003 |  |  |
| 3        |                 | I<br>II<br>III    | 4°102<br>1°152<br>1°153<br>1°152          | + · 183<br>+ · 244<br>· 000        | + °026<br>+ °075<br>- ° 101             |                     | + 209 + 319 - 101                                                                                                            | 180         0         0'000           62         5         14'337           65         16         14'276           52         38         31'387             | 5`1262127,6<br>5`1381529,7<br>5`0802173,1 | 133725°05<br>137452°62<br>120286°62 | 25°327<br>26°033<br>22°782 |  |  |
| 4        |                 | II<br>III<br>V    | 3 457<br>1 448<br>1 448<br>1 447<br>4 343 | `164<br>`438<br>`045               | + ·079<br>- ·047<br>- ·032              |                     | $ \begin{array}{r} + & \cdot & 427 \\ - & \cdot & 085 \\ - & \cdot & 485 \\ - & \cdot & 077 \\ - & \cdot & 647 \end{array} $ | 180       0       0.0000         81       14       27.237         50       38       45.987         48       6       46.776         180       0       0.0000 | 5°2492748,6<br>5°1426862,7<br>5°1262127,6 | 177531°25<br>138894°89<br>133725°05 | 33`623<br>26`306<br>25`327 |  |  |

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NOTES.--1. The values of the side are given in the same line with the opposite angle.
2. Stations XLI and XLIV appertain to the Karáchi Longitudinal Series.

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| No. of  | triangle        | <b>6</b> 4 - 1    | rical                                                                        | Cor                             | rections to (                  | Observed A                    | ngle                                                                                                          | Corrected Plane                                                                                                                                    |                                                                                  | Distance                                  |                                  |
|---------|-----------------|-------------------|------------------------------------------------------------------------------|---------------------------------|--------------------------------|-------------------------------|---------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------|-------------------------------------------|----------------------------------|
| Circuit | Non-<br>circuit | Station           | Sphe<br>Exc                                                                  | Figure                          | Circuit                        | Non-<br>circuit               | Total                                                                                                         | Angle                                                                                                                                              | Log. feet                                                                        | Feet                                      | Miles                            |
| 5       |                 | III<br>V<br>VII   | "<br>1,402<br>1,400<br>1,400                                                 | "<br>+ `019<br>+ `199<br>+ `139 | "<br>`092<br>+`088<br>+`004    | "                             | "<br>- °073<br>+ °287<br>+ °143                                                                               | ° ' "<br>43 5 42 962<br>55 2 24 631<br>81 51 52 407                                                                                                | 5 <sup>.0882240,5</sup><br>5 <sup>.1672452,2</sup><br>5 <sup>.2492748,6</sup>    | 122524 · 82<br>146975 · 60<br>177531 · 25 | 23 · 205<br>27 · 836<br>33 · 623 |
| б       |                 | III<br>VII<br>VI  | 4 <sup>217</sup><br>1 <sup>259</sup><br>1 <sup>259</sup><br>1 <sup>260</sup> | 003<br>+ .020<br>+ .101         | + °026<br>+ °064<br>- °090     |                               | $\begin{array}{ c c c c c c c c c c c c c c c c c c c$                                                        | 180 0 0.000<br>59 58 57.375<br>52 14 10.424<br>67 47 12.201                                                                                        | 5`1381661,9<br>5`0986612,2<br>5`1672452,2                                        | 137456°80<br>125505°06<br>146975°60       | 25.033<br>23.770<br>27.836       |
|         | 50              | I<br>III<br>IV    | 3.778<br>1.663<br>1.663<br>1.662                                             | + '399<br>+ '007<br>+ '132      |                                | - °010<br>+ ° 127<br>- ° 117  | $+ \cdot 158$<br>+ $\cdot 389$<br>+ $\cdot 134$<br>+ $\cdot 015$                                              | 180 0 0.000<br>52 40 50.016<br>82 22 27.451<br>44 56 42.533                                                                                        | 5`1895975,8<br>5`2852201,9<br>5`1381529,7                                        | 154738°21<br>192852°92<br>137452°62       | 29.306<br>36.525<br>26.033       |
|         | 51              | III<br>IV<br>VI   | 4 988<br>1 451<br>1 450<br>1 450                                             | + .060<br>+ .504<br>+ .167      |                                | + · 111<br>- · 001            | $+ \cdot 538$<br>+ $+ \cdot 171$<br>+ $\cdot 493$<br>+ $\cdot 067$                                            | 180       0       0       000         71       15       46       460         46       5       17       383         62       38       56       1.57 | 5°2174339,4<br>5°0986612,2<br>5°1895975,8                                        | 164981 °00<br>125505 °06<br>154738 °21    | 31 ° 246<br>23 ° 770<br>29 ° 306 |
| 7       |                 | VI<br>VII<br>VIII | 4 351<br>988<br>988<br>988                                                   | - °073<br>- °072<br>+ °049      | + · 046<br>+ · 045<br>- · 091  |                               | $\begin{vmatrix} + & 731 \\ - & 027 \\ - & 027 \\ - & 042 \end{vmatrix}$                                      | 48 42 30 585<br>57 47 49 925<br>73 29 39 490                                                                                                       | 5.033201311<br>2.08389830<br>2.138100190                                         | 107718°74<br>121310°45<br>137456°80       | 20°401<br>22°975<br>26°033       |
| 8       |                 | VII<br>VIII<br>X  | 2°964<br>°994<br>°994<br>°993                                                | + .000<br>+ .101<br>+ .011      | + °089<br>°043<br>°046         |                               | $ \begin{array}{r} - \cdot 090 \\ + \cdot 098 \\ + \cdot 058 \\ - \cdot 035 \\ \end{array} $                  | 78 52 36 014<br>54 5 19 984<br>47 2 4 002                                                                                                          | 5`1596842,2<br>5`0763667,8<br>5`0322912,1                                        | 144438 ° 91<br>119224 ° 86<br>107718 ° 74 | 27 · 356<br>22 · 580<br>20 · 401 |
| 9       |                 | VIII<br>X<br>XII  | 2.981<br>.919<br>.920<br>.920                                                | + ·200<br>+ ·091<br>+ ·158      | - 090<br>+ 089<br>+ 1001       |                               | $\begin{array}{r rrrrr} + & \cdot & 121 \\ + & \cdot & 110 \\ + & \cdot & 180 \\ + & \cdot & 159 \end{array}$ | 180 0 0.000<br>40 23 2.581<br>58 28 48.720<br>81 8 8.699                                                                                           | 4 <sup>.</sup> 9764158,6<br>5 <sup>.</sup> 0955763,7<br>5 <sup>.</sup> 1596842,2 | 94714°36<br>124616°74<br>144438°91        | 17 ° 938<br>23 ° 602<br>27 ° 356 |
| 10      |                 | VIII<br>XII<br>XI | 2°759<br>•839<br>•838<br>•839                                                | + .059<br>040<br>047            | + •045<br>+ •046<br>- •091     |                               | + '449<br>+ '104<br>'000<br>- '138                                                                            | 180 0 0.000<br>54 17 18.545<br>53 27 47.712<br>72 14 53.743                                                                                        | 5 <sup>.0263010,9</sup><br>5 <sup>.0217355,9</sup><br>5 <sup>.0955763,7</sup>    | 106243 ° 18<br>105132 ° 15<br>124616 ° 74 | 20°122<br>19°911<br>23°602       |
|         | 52              | VI<br>VIII<br>IX  | 2.516<br>.952<br>.953<br>.953                                                | - °005<br>+ °110<br>- °017      |                                | + · 030<br>+ · 085<br>- · 115 | $ \begin{array}{r} - \cdot 034 \\ + \cdot 025 \\ + \cdot 195 \\ - \cdot 132 \\ \end{array} $                  | 180 0 0.000<br>47 51 11.333<br>72 36 55.272<br>59 31 53.395                                                                                        | 5.0185059,2<br>5.1281314,8<br>5.0838982,0                                        | 104353°23<br>134317°15<br>121310°45       | 19°764<br>25°439<br>22°975       |
|         | 53              | VIII<br>IX<br>XI  | 2 · 858<br>• 785<br>• 785<br>• 784                                           | - '089<br>- '113<br>- '124      |                                | + °094<br>+ °013<br>- °107    | + .088<br>+ .002<br>100<br>231                                                                                | 180       0       0       000         65       7       38       650         57       46       11       585         57       6       9       765    | 5 <sup>.0</sup> 521346,8<br>5 <sup>.0217355,9</sup><br>5 <sup>.018</sup> 5059,2  | 112754°70<br>105132°15<br>104353°23       | 21°355<br>19°911<br>19°764       |
| 11      |                 | XI<br>XII<br>XIII | 2 354<br>•613<br>•612<br>•613                                                | - ·118<br>- ·119<br>- ·055      | + '035<br>+ '054<br>- '089     |                               | $ \begin{array}{r} - 320 \\ - 083 \\ - 065 \\ - 144 \\ \end{array} $                                          | 58 35 3.604<br>49 54 37.113<br>71 30 19.283                                                                                                        | 4 <sup>-</sup> 9804877,8<br>4 <sup>-</sup> 9330134,9<br>5 <sup>-</sup> 0263010,9 | 95606*58<br>85706*45<br>106243*18         | 18.107<br>10.335<br>20.135       |
| 13      |                 | XII<br>XIII<br>XV | 1.838<br>.530<br>.531<br>1.501                                               | - '139<br>+ '103<br>+ '017      | + · 1 16<br>- · 081<br>- · 035 |                               | $ \begin{array}{r} - & 202 \\ - & 023 \\ + & 022 \\ - & 018 \\ - & 010 \end{array} $                          | 55 52 6.427<br>55 44 31.812<br>68 23 21.761<br>180 0 0.000                                                                                         | 4 93004 I I,0<br>4 9293907,2<br>4 9804877,8                                      | 85121*86<br>84994*47<br>95606*58          | 16.133<br>16.091<br>18.102       |

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## PRINCIPAL TRIANGULATION. TRIANGLES.

| No. of  | of triangle     |                      | rical<br>eas                         | Cor                             | rections to                        | Observed A                 | ngle                                                                                            | Corrected Plane                                                           | Distance                                                                         |                                  |                            |  |
|---------|-----------------|----------------------|--------------------------------------|---------------------------------|------------------------------------|----------------------------|-------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------|----------------------------------------------------------------------------------|----------------------------------|----------------------------|--|
| Circuit | Non-<br>circuit | Station              | Spher                                | Figure                          | Circuit                            | Non-<br>circuit            | Total                                                                                           | Angle                                                                     | Log. feet                                                                        | Feet                             | Miles                      |  |
| 13      |                 | XIII<br>XV<br>XVII   | "<br>387<br>387<br>387<br>387        | "<br>+ '088<br>- '078<br>+ '031 | "<br>- · 102<br>+ · 159<br>- · 057 | "                          | $ \begin{array}{c}     " \\     - \cdot 014 \\     + \cdot 081 \\     - \cdot 026 \end{array} $ | ° / "<br>71 51 28.429<br>41 2 28.394<br>67 6 3.177                        | 4`9435461,4<br>4`7829932,9<br>4`9300411,0                                        | 87810°44<br>60672°69<br>85121°86 | 16.631<br>11.491<br>16.132 |  |
| 14      |                 | XIII<br>XVII<br>XVI  | 1.101<br>.308<br>.309<br>.308        | + °041<br>- °052<br>- °004      | + °050<br>+ °084<br>- °134         |                            | + '041<br>+ '091<br>+ '032<br>- '138                                                            | 180 0 0.000<br>62 58 19.073<br>66 39 51.303<br>50 21 49.624               | 4 <sup>.</sup> 8462130,0<br>4 <sup>.</sup> 8593774,0<br>4 <sup>.</sup> 7829932,9 | 70179°94<br>72339°82<br>60672°69 | 13°292<br>13°721<br>11°491 |  |
|         | 54              | XI<br>XIII<br>XIV    | <u>925</u><br>359<br>358<br>359      | + · 174<br>+ · 128<br>+ · 044   |                                    | + ·213<br>+ ·057<br>- ·270 | $\begin{array}{r} - & \cdot 015 \\ + & \cdot 387 \\ + & \cdot 185 \\ - & \cdot 226 \end{array}$ | 180 0 0.000<br>53 27 44.078<br>48 51 26.297<br>77 40 49.625               | 4 <sup>.</sup> 8480578,0<br>4 <sup>.</sup> 8199682,4<br>4 <sup>.</sup> 9330134,9 | 70485*18<br>66064*51<br>85706*45 | 13°349<br>12°512<br>16°232 |  |
|         | 55              | XIII<br>XIV<br>XVI   | 1.076<br>.3c3<br>.304<br>.304        | + °095<br>+ °030<br>- °024      |                                    | + '165<br>+ '136<br>- '301 | $+ \cdot 346$<br>+ $\cdot 260$<br>+ $\cdot 166$<br>- $\cdot 325$                                | 180 0 0'000<br>49 3 52'607<br>67 5 50'602<br>63 50 16'791                 | 4`7732438,0<br>, 4`8593773,9<br>4`8480978,0                                      | 59325*82<br>72339*82<br>70485*18 | 11°236<br>13°701<br>13°349 |  |
| 15      |                 | XVI<br>XVII<br>XVIII | ·911<br>·293<br>·292<br>·293         | - · 107<br>+ ·022<br>+ ·043     | + '036<br>+ '063<br>- '099         |                            | $ + 071 \\ + 085 \\ - 056 $                                                                     | 61 47 49 406<br>51 41 39 533<br>66 30 31 061                              | 4 <sup>.</sup> 8289003,0<br>4 <sup>.</sup> 7784986,6<br>4 <sup>.</sup> 8462130,0 | 67437°32<br>60048°02<br>70179°94 | 12°772<br>11°373<br>13°292 |  |
| 16      |                 | XVII<br>XVIII<br>XX  | ·878<br>·312<br>·312<br>·312         | - °098<br>+ °074<br>+ °020      | + ·124<br>- ·073<br>- ·051         |                            | $\begin{array}{c} - & 0.042 \\ + & 0.026 \\ + & 0.001 \\ - & 0.031 \end{array}$                 | 58 51 57°144<br>61 22 36°719<br>59 45 26°137                              | 4 <sup>.82489c2,3</sup><br>4 <sup>.8358276,0</sup><br>4 <sup>.8289003,0</sup>    | 66817°50<br>68521°62<br>67437°32 | 12.655<br>12.978<br>12.772 |  |
| 17      |                 | XVIII<br>XX<br>XXII  | ·936<br>·322<br>·321                 | + .030<br>133<br>001            | - •061<br>+ •115<br>- •054         |                            | - '004<br>- '022<br>- '018<br>- '055                                                            | 180 0 0.000<br>57 22 36.426<br>65 34 7.310<br>57 3 16.264                 | 4 <sup>.</sup> 8264635,6<br>4 <sup>.</sup> 8602905,7<br>4 <sup>.</sup> 8248902,3 | 67060°01<br>72492°08<br>66817°50 | 12.701<br>13.730<br>12.655 |  |
| 18      |                 | XVIII<br>XXII<br>XXI | <u>    965</u><br>269<br>270<br>270  | + :074<br>- :102<br>- :003      | + °068<br>+ °039<br>- °107         |                            | $\begin{array}{r} - \cdot 095 \\ + \cdot 142 \\ - \cdot 063 \\ - \cdot 110 \end{array}$         | 49 1 44 853<br>56 13 29 677<br>74 44 45 470                               | 4.7538389,3<br>4.7955865,4<br>4.8602905,7                                        | 56733°42<br>62457°78<br>72492°08 | 10°745<br>11°829<br>13°730 |  |
|         | 56              | XVI<br>XVIII<br>XIX  | *809<br>*239<br>*239<br>*239         | + °023<br>+ °072<br>- °078      |                                    | + °050<br>+ °072<br>- °122 | $\begin{array}{c} - & \cdot 031 \\ + & \cdot 073 \\ + & \cdot 144 \\ - & \cdot 200 \end{array}$ | 180 0 0'000<br>55 56 1'804<br>62 50 44'855<br>61 13 13'341                | 4.7539932,1<br>4.7850410,2<br>4.7784986,6                                        | 56753*57<br>60959*45<br>60048*02 | 10°749<br>11°545<br>11°373 |  |
|         | 57              | XVIII<br>XIX<br>XXI  | ·717<br>·249<br>·249<br>·248         | + '098<br>- '041<br>- '201      |                                    | + :093<br>+ :044<br>- :137 | $+ \cdot 017$<br>+ $\cdot 191$<br>+ $\cdot 003$<br>- $\cdot 338$                                | 180 0 0.000<br>62 51 44.402<br>63 2 44.264<br>54 5 31.334                 | 4`7948772,2<br>4`795,5865,4<br>4`7539932,1                                       | 62355-86<br>62457-78<br>56753-57 | 11.810<br>11.829<br>10.749 |  |
| 19      |                 | XXI<br>XXII<br>XXIV  | ·746<br>·213<br>·213<br>·213         | + '036<br>- '015<br>- '012      | - °054<br>+ °099<br>- °045         |                            | - '144<br>- '018<br>+ '084<br>- '057                                                            | 180 0 0.000<br>49 40 9.539<br>71 6 25.091<br>59 13 25.370                 | 4.7018973,2<br>4.7957073,2<br>4.7538389,3                                        | 50338°15<br>62475°15<br>56733°42 | 9°534<br>11°832<br>10°745  |  |
| 20      |                 | XXI<br>XXIV<br>XXIII | ·639<br>·186<br>·186<br>·187<br>·550 | - · 166<br>+ · 055<br>- · 200   | + '067<br>+ '034<br>- '101         |                            | $ + \cdot 009$<br>$ - \cdot 099$<br>$ + \cdot 089$<br>$ - \cdot 301$<br>$ - \cdot 311$          | 180 0 0.000<br>49 15 47.685<br>51 43 55.133<br>79 0 17.182<br>180 0 0.000 | 4.6832601,5<br>4.6986909,8<br>4.7957073,2                                        | 48223°66<br>49967°88<br>62475°15 | 9°133<br>9°464<br>11°832   |  |

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| No. of  | triangle        | 64.1°                         | rical<br>888                              | Cor                                                                                     | rections to                                                    | Observed A                                                                            | ngle                                                                                                            | Corrected Plane                                                                                                                                            |                                                                                  | Distance                               |                            |
|---------|-----------------|-------------------------------|-------------------------------------------|-----------------------------------------------------------------------------------------|----------------------------------------------------------------|---------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------|----------------------------------------|----------------------------|
| Circuit | Non-<br>circuit | Station                       | Spher                                     | Figure                                                                                  | Circuit                                                        | Non-<br>circuit                                                                       | Total                                                                                                           | Angle                                                                                                                                                      | Log. feet                                                                        | Feet                                   | Miles                      |
|         | 58              | XXI<br>XXII<br>XXIII<br>XXIII | "<br>* 22 I<br>* 220<br>* 22 I            | $ \begin{array}{r} " \\ - & 130 \\ - & 251 \\ + & 023 \\ \end{array} $                  | "                                                              | "<br>+ '013<br>+ '041<br>- '054                                                       | "<br>- '117<br>- '210<br>- '031                                                                                 | 98 55 57°402<br>37 25 48°850<br>43 38 13°748                                                                                                               | 4`9096344,2<br>4`6986909,8<br>4`7538389,3                                        | 81214°66<br>49967°88<br>56733°42       | 15°382<br>9°464<br>10°745  |
| 21      |                 | XXIII<br>XXIV<br>XXV          | •662<br>•247<br>•246<br>•246              | + .081<br>355<br>+ .123                                                                 | + °055<br>+ °116<br>- °171                                     |                                                                                       | $ \begin{array}{r} - & \cdot 358 \\ + & \cdot 136 \\ - & \cdot 239 \\ - & \cdot 048 \end{array} $               | 180 0 0.000<br>75 11 12.069<br>64 22 53.505<br>40 25 54.426                                                                                                | 4 <sup>.8566423,2</sup><br>4 <sup>.8263806,9</sup><br>4 <sup>.6832601,5</sup>    | 71885°67<br>67047°20<br>48223°66       | 13.615<br>12.698<br>9.133  |
| 22      | -               | XXIV<br>XXV<br>XXVI           | ·739<br>·247<br>·247<br>·248              | + ·364<br>- ·079<br>- ·183                                                              | $+ \frac{142}{-110}$                                           |                                                                                       | $\begin{array}{r} - & \cdot 151 \\ + & \cdot 506 \\ - & \cdot 189 \\ - & \cdot 215 \end{array}$                 | 180 0 0.000<br>47 2 9.349<br>54 21 24.674<br>78 36 25.977                                                                                                  | 4`7296662,9<br>4`7751950,4<br>4`8566423,2                                        | 53661 • 92<br>59592 • 98<br>71885 • 67 | 10°163<br>11°287<br>13°615 |
|         | 59              | XXIII<br>XXIV<br>XXVI         | 742<br>211<br>211<br>211<br>211           | + '410<br>+ '009<br>- '576                                                              |                                                                | $\begin{vmatrix} - & \cdot & 117 \\ + & \cdot & 258 \\ - & \cdot & 141 \end{vmatrix}$ | $\begin{array}{r} + & \cdot 102 \\ + & \cdot 293 \\ + & \cdot 267 \\ - & \cdot 717 \end{array}$                 | 180 0 0.000<br>38 24 15.402<br>111 25 3.136<br>30 10 41.462                                                                                                | 4`7751950,4<br>4`9508827,8<br>4`6832601,5                                        | 59592°98<br>89306°44<br>48223°66       | 11°287<br>16°914<br>9°133  |
| 23      |                 | XXV<br>XXVI<br>XXVII          | 230<br>230<br>230                         | $ \begin{vmatrix} - & \cdot & 415 \\ + & \cdot & 289 \\ - & \cdot & 084 \end{vmatrix} $ | + <sup>•</sup> 059<br>+ <sup>•</sup> 086<br>- <sup>•</sup> 145 |                                                                                       | $ \begin{array}{r} - & \cdot & 157 \\ - & \cdot & 356 \\ + & \cdot & 375 \\ - & \cdot & 229 \end{array} $       | 65 53 51 424<br>61 40 28 585<br>52 25 39 991                                                                                                               | 4`7910041,2<br>4`7752348,0<br>4`7296662,9                                        | 61802°23<br>59598°42<br>53661°92       | 11°705<br>11°288<br>10°163 |
| 24      |                 | XXVI<br>XXVII<br>XXIX         | · 238<br>· 238<br>· 239                   | $ \begin{array}{r} - & \cdot 334 \\ + & \cdot 136 \\ + & \cdot 373 \end{array} $        | + ·144<br>- ·086<br>- ·058                                     |                                                                                       | $ \begin{vmatrix} - & \cdot & 190 \\ + & \cdot & 050 \\ + & \cdot & 315 \end{vmatrix} $                         | 52 36 19.082<br>63 28 54.442<br>63 54 46.476                                                                                                               | 4`7377444,7<br>4`7893888,8<br>4`7910041,2                                        | 54669 • 42<br>61572 • 80<br>61802 • 23 | 10°354<br>11°662<br>11°705 |
| 25      |                 | XXVII<br>XXIX<br>XXXI         | -715<br>-333<br>-333<br>-333              | $ \begin{vmatrix} - & 0.014 \\ - & 262 \\ + & 425 \end{vmatrix} $                       | - °029<br> + °154<br> - °125                                   |                                                                                       | $+ \cdot 175$<br>$- \cdot 043$<br>$- \cdot 108$<br>$+ \cdot 300$                                                | 180       0       0.000         76       38       51.224         64       49       25.789         38       31       42.987                                 | 4`9314209,2<br>4`8999729,0<br>4`7377444,7                                        | 85392°73<br>79427°87<br>54669°42       | 16°173<br>15°043<br>10°354 |
| 26 -    |                 | XXVII<br>XXXI<br>XXX<br>XXX   | ·999<br>·354<br>·355<br>·355              | - °057<br>- °781<br>+ °282                                                              | + '098<br>+ '039<br>- '137                                     |                                                                                       | $+ \cdot 149$<br>+ $\cdot 041$<br>- $\cdot 742$<br>+ $\cdot 145$                                                | 180 0 0.000<br>47 29 25 347<br>64 5 47 403<br>68 24 47 250                                                                                                 | 4.7991189,6<br>4.8855711,7<br>4.8999729,0                                        | 62967 * 86<br>76837 * 13<br>79427 * 87 | 11°926<br>14°552<br>15°043 |
|         | 60              | XXV<br>XXVII<br>XXVIII        | 1°004<br>276<br>276<br>276                | + <sup>•</sup> 508<br>- <sup>•</sup> 054<br>- <sup>•</sup> 246                          |                                                                | + '156<br>+ '065<br>- '221                                                            | $\begin{array}{r} - \cdot 556 \\ + \cdot 664 \\ + \cdot 011 \\ - \cdot 467 \\ \end{array}$                      | 180       0       0.000         59       47       10.538         66       37       26.725         53       35       22.737                                 | 4 <sup>.</sup> 8061453,4<br>4 <sup>.</sup> 8323596,4<br>4 <sup>.</sup> 7752348,0 | 63994°90<br>67976°63<br>59598°42       | 12°120<br>12°874<br>11°288 |
|         | 61              | XXVII<br>XXVIII<br>XXX        | 311<br>311<br>311<br>311                  | + <sup>•</sup> 053<br>+ <sup>•</sup> 227<br>- <sup>•</sup> 267                          |                                                                | + '097<br>+ '106<br>- '203                                                            | $+ \frac{150}{+333}$                                                                                            | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                                                      | 4 <sup>.</sup> 8077577,7<br>4 <sup>.</sup> 8855711,7<br>4 <sup>.</sup> 8061453,4 | 64232°94<br>76837°13<br>63994°90       | 12°165<br>14°552<br>12°120 |
| 27      |                 | XXX<br>XXXI<br>XXXII          | 933<br>232<br>231<br>232                  | - 1.030<br>821<br>264                                                                   | + °049<br>+ °064<br>- °113                                     |                                                                                       | $\begin{array}{ c c c c c c c c c c c c c c c c c c c$                                                          | 62 36 10.927<br>50 17 54.712<br>67 5 54.361                                                                                                                | 4.7831115,6<br>4.7209196,2<br>4.7991189,6                                        | 60689°22<br>52591°99<br>62967°86       | 11°494<br>9°961<br>11°926  |
| 28      | ,               | XXXI<br>XXXII<br>XXXV         | · 268<br>· 268<br>· 268<br>· 268<br>· 804 | + ·458<br>+ ·305<br>+ ·131                                                              | + '157<br>- '075<br>- '082                                     |                                                                                       | $ \begin{array}{r} 1 - 2 \cdot 115 \\ + \cdot 615 \\ + \cdot 230 \\ + \cdot 049 \\ + \cdot 804 \\ \end{array} $ | 180       0       0.000         54       41       13.517         69       27       16.832         55       51       29.651         180       0       0.000 | 4.7769581,3<br>4.8367231,2<br>4.7831115,6                                        | 59835°39<br>68663°05<br>60689°22       | 11°332<br>13°004<br>11°494 |

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### PRINCIPAL TRIANGULATION. TRIANGLES.

| No. of  | triangle        | 64_4?                    | rical<br>ess                          | Cor                                                                                | rections to                                                    | Observed A                                                     | ngle                                                                                            | Corrected Plane                                                                                                                                          |                                                                                  | Distance                                                  |                                 |
|---------|-----------------|--------------------------|---------------------------------------|------------------------------------------------------------------------------------|----------------------------------------------------------------|----------------------------------------------------------------|-------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------|-----------------------------------------------------------|---------------------------------|
| Oircuit | Non-<br>circuit | Station                  | Spher<br>Exc                          | Figure                                                                             | Circuit                                                        | Non-<br>circuit                                                | Total                                                                                           | Angle                                                                                                                                                    | Log. feet                                                                        | Feet                                                      | Miles                           |
| 29      |                 | XXXII<br>XXXV<br>XXXIV   | "<br>198<br>198<br>198                | "<br>+ '173<br>+ '064<br>- '103                                                    | "<br>+ °038<br>+ °066<br>- °104                                | "                                                              | "<br>+ '211<br>+ '130<br>- '207                                                                 | 0 / "<br>67 0 40°473<br>44 59 31°432<br>67 59 48°095                                                                                                     | 4`7738645,8<br>4`6592271,6<br>4`7769581,3                                        | 59410°68<br>45627°55<br>59835°39                          | 11°252<br>8°642<br>11°332       |
|         | 62              | XXX<br>XXXII<br>XXXIII   | • 594<br>• 180<br>• 180<br>• 180      | $ \begin{array}{r} - \cdot \infty 6 \\ + \cdot 425 \\ + \cdot 311 \\ \end{array} $ |                                                                | + '019<br>+ '074<br>- '093                                     | $\begin{array}{r rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$                                           | 180 0 0.000<br>55 50 14.913<br>61 59 21.869<br>62 10 23.218                                                                                              | 4.6920302,5<br>4.7201817,4<br>4.7209196,2                                        | 49207°38<br>52502°72<br>` 52591°99                        | 9°320<br>9°944<br>9°961         |
|         | 63              | XXXII<br>XXXIII<br>XXXIV | ·540<br>·177<br>·176<br>·176          | $+ \frac{.501}{- 007}$<br>+ $\frac{.285}{- 285}$                                   |                                                                | + <sup>•</sup> 076<br>+ <sup>•</sup> 056<br>- <sup>•</sup> 132 | $\begin{array}{r} + & \cdot 730 \\ + & \cdot 577 \\ + & \cdot 049 \\ + & \cdot 153 \end{array}$ | 180 0 0.000<br>94 26 45.410<br>40 46 36.033<br>44 46 38.557                                                                                              | 4.8429305,0<br>4.6592271,6<br>4.6920302,5                                        | 69651 • 50<br>45627 • 55<br>49207 • 38                    | 13°192<br>8°642<br>9°320        |
| 30      |                 | XXXIV<br>XXXV<br>XXXVI   | ·529<br>·285<br>·285<br>·284          | + ·220<br>+ ·468<br>+ ·076                                                         | - <sup>•</sup> 047<br>+ <sup>•</sup> 129<br>- <sup>•</sup> 082 |                                                                | + .779<br>+ .173<br>+ .597<br>006                                                               | 180 0 0.000<br>57 57 48.648<br>70 37 23.172<br>51 24 48.180                                                                                              | 4 <sup>.</sup> 8090908,1<br>4 <sup>.</sup> 8555191,1<br>4 <sup>.</sup> 7738645,8 | 64430°40<br>71699°99<br>59410°68                          | •<br>12°203<br>13°580<br>11°252 |
| 31      |                 | XXXIV<br>XXXVI<br>XXXVII | *854<br>*296<br>*295<br>*296          | $ \begin{array}{r} + & \cdot 194 \\ + & \cdot 274 \\ + & \cdot 299 \end{array} $   | + °046<br>+ °072<br>- °118                                     | ,                                                              | + .704<br>+ .240<br>+ .346<br>+ .181                                                            | 68 16 58 594<br>45 48 22 151<br>65 54 39 255                                                                                                             | 4 <sup>.</sup> 8631164,8<br>4 <sup>.</sup> 7506005,7<br>4 <sup>.</sup> 8555191,1 | 72965*32<br>56311*94<br>71699*99                          | 13.819<br>10.665<br>13.580      |
| 32      |                 | XXXVI<br>XXXVII<br>XXXIX | • 523<br>• 523<br>• 522               | - •049<br>+ •242<br>- •275                                                         | + '132<br>- '021<br>- '111                                     |                                                                | + '707<br>+ '083<br>+ '221<br>- '386                                                            | 76 14 23 930<br>60 49 55 038<br>42 55 41 032                                                                                                             | 5'01 <b>7272</b> 1,8<br>4'9710293,6<br>4'8631164,8                               | 104057°21<br>93546°89<br>72965°32                         | 19°708<br>17°717<br>13°819      |
| 33      |                 | XXXVII<br>XXXIX<br>XLI   | 1.568<br>.756<br>.755<br>.755         | + ·146<br>+ ·170<br>+ ·390                                                         | + °070<br>+ °076<br>- °146                                     |                                                                | $ \begin{array}{r} - \cdot 082 \\ + \cdot 216 \\ + \cdot 246 \\ + \cdot 244 \\ \end{array} $    | 180 0 0.000<br>62 27 54.030<br>58 40 37.311<br>58 51 28.659                                                                                              | 5:0326460,5<br>5:0164405,2<br>5:0172721,8                                        | 10780 <b>6 • 78</b><br>103858 • 14<br>10405 <b>7 • 21</b> | 20°418<br>19°670<br>19°708      |
| 34      |                 | XXXIX<br>XLI<br>XLIII    | 2 · 266                               | $ \begin{array}{r} + & \cdot 034 \\ - & \cdot 021 \\ + & \cdot 088 \end{array} $   | + °055<br>+ °148<br>- °203                                     |                                                                | $\begin{array}{r} + & .706 \\ + & .089 \\ + & .127 \\ - & .115 \end{array}$                     | 180       0       0.000         83       20       2.902         44       29       21.390         52       10       35.708                                | 5·1321256,3<br>4·9806505,1<br>5·0326460,5                                        | 135558°14<br>95642°42<br>107806°78                        | 25°674<br>18°114<br>20°418      |
| 35      |                 | XXXIX<br>XLIII<br>XLIV   | 2°421<br>•681<br>•682<br>•682         | + °076<br>+ °079<br>+ °160                                                         | + '198<br>- '076<br>- '122                                     |                                                                | $+ \cdot 101$<br>+ $\cdot 274$<br>+ $\cdot 003$<br>+ $\cdot 038$                                | 180 0 0.000<br>50 7 57 323<br>77 27 33 811<br>52 24 28 866                                                                                               | 4`9668150,0<br>5`0712328,4<br>4`9806505,1                                        | 92643°51<br>117823°75<br>95642°42                         | 17°546<br>22°315<br>18°114      |
|         | 64              | XXXV<br>XXXVI<br>XXXVIII | 2°045<br>286<br>285<br>285            | $+ : \infty 7$<br>- :018<br>+ :247                                                 |                                                                | + '137<br>- '095<br>- '042                                     | $\begin{array}{r} + & 315 \\ + & 144 \\ - & 113 \\ + & 205 \end{array}$                         | 180 0 0.000<br>73 44 28.598<br>49 28 9.252<br>56 47 22.150                                                                                               | 4 <sup>.</sup> 86881 <b>43,2</b><br>4.7673860,5<br>4.8090908,1                   | 73928°92<br>58531°02<br>64430°40                          | 14°002<br>11°085<br>12°203      |
|         | 65              | XXXVI<br>XXXVIII<br>XL   | *850<br>*297<br>*297<br>*297          | + <sup>•</sup> 288<br>+ <sup>•</sup> 219<br>+ <sup>•</sup> 334                     |                                                                | - ·125<br>+ ·139<br>- ·014                                     | + :230<br> + :163<br> + :358<br> + :320                                                         | 180       0       0.000         47       20       17.386         62       5       32.791         70       34       9.623                                 | 4.7607854,7<br>4.8405886,1<br>4.8688143,2                                        | 57648°17<br>69276°92<br>73928°92                          | 10°918<br>13°121<br>14°002      |
|         | 66              | XXXVI<br>XL<br>XXXIX     | -891<br>-511<br>-511<br>-510<br>1-532 | - `361<br>- `156<br>+ `049                                                         |                                                                | + `098<br>- `007<br>- `091                                     | $ \begin{array}{r} + & 841 \\ - & 263 \\ - & 163 \\ - & 042 \\ - & 468 \\ \end{array} $         | 180       0       0.000         89       43       56.906         53       39       2.716         36       37       0.378         180       0       0.000 | 5`0650027,1<br>4`9710293,6<br>4`8405886,1                                        | 116145°59<br>93546°89<br>69276°92                         | 21°997<br>17°717<br>13°121      |

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| No. of ( | triangle        | <b>a</b>              | rical<br>ese                         | Cor                                                                              | rections to                   | Observed A                         | ngle                                                                                                    | Corrected Plane                                                                                                                                            |                                                                                  | Distance                               |                            |
|----------|-----------------|-----------------------|--------------------------------------|----------------------------------------------------------------------------------|-------------------------------|------------------------------------|---------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------|----------------------------------------|----------------------------|
| Circuit  | Non-<br>circuit | Station               | Sphe<br>Exc                          | Figure                                                                           | Circuit                       | Non-<br>circuit                    | Total                                                                                                   | Angle                                                                                                                                                      | Log. feet                                                                        | Feet                                   | Miles                      |
|          | 67              | XL<br>XXXIX<br>XLII   | "<br>•642<br>•641<br>•642            | "<br>+ `139<br>+ `109<br>+ `077                                                  | "                             | "<br>+ · 365<br>- · 188<br>- · 177 | "<br>+ •504<br>- •079<br>- •100                                                                         | ° ' "<br>51 +4 39`442<br>49 I 11`780<br>79 I4 8`778                                                                                                        | 4`9677234,5<br>4`9506238,0<br>5`0650027,1                                        | 92837°50<br>89253°20<br>116145°59      | 17°583<br>16°904<br>21°997 |
|          | 68              | XXXIX<br>XLII<br>XLIV | 1·925<br>•546<br>•546<br>•546        | + · 167<br>+ · 236<br>+ · 065                                                    |                               | + · 061<br>+ · 202<br>- · 263      | $\begin{array}{r} + & \cdot_{325} \\ + & \cdot_{228} \\ + & \cdot_{438} \\ - & \cdot_{198} \end{array}$ | 180 0 0.000<br>39 17 24.812<br>88 44 4.782<br>51 58 30.406                                                                                                 | 4`8729131,7<br>5`0712328,4<br>4`9677234,5                                        | 74629 96<br>117823 75<br>92837 50      | 14°134<br>22°315<br>17°583 |
| 36       |                 | XLIII<br>XLIV<br>XLV  | 1.638<br>.559<br>.559<br>.560        | + ·365<br>- ·304<br>+ ·157                                                       | - '071<br>+ '139<br>- '068    |                                    | $+ \cdot 468$<br>+ $\cdot 294$<br>- $\cdot 165$<br>+ $\cdot 089$                                        | 180 0 0 <sup>0</sup> 000<br>56 5 3 <sup>1</sup> 435<br>61 46 57 <sup>1</sup> 916<br>62 7 58 <sup>1</sup> 649                                               | 4`9393501,4<br>4`9654010,0<br>4`9668150,0                                        | 86966 • 13<br>92342 • 36<br>92643 • 51 | 16°471<br>17°489<br>17°546 |
| 37       |                 | XLIII<br>XLV<br>XLVI  | 1.078<br>.423<br>.423<br>.423        | - °052<br>+ °114<br>+ °477                                                       | + · 106<br>+ · 021<br>- · 127 |                                    | + .054<br>+ .135<br>+ .350<br>+ .520                                                                    | 46 42 57 62 1<br>57 7 5 062<br>76 9 57 317                                                                                                                 | 4 <sup>.</sup> 8402953,2<br>4 <sup>.</sup> 9023565,3<br>4 <sup>.</sup> 9654010,0 | 69230°16<br>79865°01<br>92342°36       | 13°112<br>15°126<br>17°489 |
| 38       |                 | XLV<br>XLVI<br>XLVIII | 1 200<br>240<br>240<br>240           | $ \begin{array}{r} + & \cdot 242 \\ - & \cdot 547 \\ + & \cdot 165 \end{array} $ | + °051<br>+ °057<br>– ° 108   |                                    | $\begin{array}{r} + & 339 \\ + & 293 \\ - & 490 \\ + & 057 \\ - & 140 \end{array}$                      | 43 59 57 513<br>61 41 27 700<br>74 18 34 787                                                                                                               | 4`6985532,8<br>4`8014690,2<br>4`8402953,2                                        | 49952°04<br>63309°52<br>69230°16       | 9°461<br>11°990<br>13°112  |
| 39       |                 | XLV<br>XLVIII<br>XLIX | ·389<br>·389<br>·389<br>·388         | - °064<br>- °667<br>- °003                                                       | + · 190<br>- · 033<br>- · 157 |                                    | + ·126<br>- ·700<br>- ·160                                                                              | 60 54 9 997<br>75 38 7 061<br>43 27 42 942                                                                                                                 | 4'9053711,5<br>4'9501666,8<br>4'8014690,2                                        | 80421°31<br>89159°30<br>63309°52       | 15.231<br>16.886<br>11.990 |
|          | 69              | XLIV<br>XLV<br>XLVII  | 460<br>460<br>460<br>460             | + 359<br>+ 173<br>- 392                                                          |                               | + · 250<br>- · 136<br>- · 114      | + .609<br>+ .037<br>506                                                                                 | 42 38 49 709<br>78 6 52 427<br>59 14 17 864                                                                                                                | 4 <sup>.</sup> 8361016,5<br>4 <sup>.</sup> 9957923,9<br>4 <sup>.</sup> 9393501,4 | 68564*87<br>99035*84<br>86966*13       | 12.986<br>18.757<br>16.471 |
|          | 70              | XLV<br>XLVII<br>XLIX  | 1°380<br>*407<br>*408<br>*407        | + '758<br>+ '080<br>- '616                                                       |                               | - · 058<br>+ · 155<br>- · 097      | $\begin{array}{r} + & .700 \\ + & .235 \\ - & .713 \end{array}$                                         | 57 43 53 873<br>74 27 35 947<br>47 48 30 180                                                                                                               | 4 <sup>.</sup> 8934831,4<br>4.9501666,8<br>4.8361016,5                           | 78249°79<br>89159°30<br>68564°87       | 14.820<br>16.886<br>12.986 |
| 40       |                 | XLVIII<br>XLIX<br>L   | 1 · 222<br>· 347<br>· 347<br>· 348   | $ \begin{array}{r} - & \cdot 866 \\ + & \cdot 323 \\ - & \cdot 135 \end{array} $ | 099<br>+ .154<br>055          |                                    | + ·222<br>- ·965<br>+ ·477<br>- ·190                                                                    | 180 0 0.000<br>53 12 46.278<br>54 14 25.300<br>72 32 48.422                                                                                                | 4 <sup>.8</sup> 293997,4<br>4 <sup>.8</sup> 351155,5<br>4 <sup>.</sup> 9053711,5 | 67514°91<br>68409°37<br>80421°31       | 12°787<br>12°956<br>15°231 |
| 41       |                 | XLVIII<br>L<br>LI     | 1.042<br>.352<br>.351<br>.351        | $+ \cdot 341$<br>$- \cdot 134$<br>$- \cdot 103$                                  | + °068<br>+ °099<br>- ° 167   |                                    | $\begin{array}{r} - & \cdot 678 \\ + & \cdot 409 \\ - & \cdot 035 \\ - & \cdot 270 \end{array}$         | 180 0 0.000<br>72 28 35.677<br>53 42 55.624<br>53 48 28.699                                                                                                | 4 <sup>.</sup> 9075826,0<br>4 <sup>.</sup> 8346015,3<br>4 <sup>.</sup> 8351155,5 | 80831 • 87<br>68328 • 44<br>68409 • 37 | 15°309<br>12°941<br>12°956 |
| 42       |                 | L<br>LI<br>LIII       | 1.054<br>•310<br>•311<br>•311        | - :086<br>+ :146<br>- :098                                                       | + °049<br>+ °057<br>- °106    |                                    | $+ \cdot 104$<br>$- \cdot 037$<br>$+ \cdot 203$<br>$- \cdot 204$                                        | 180 0 0.000<br>42 10 17.283<br>61 1 3.972<br>76 48 38.745                                                                                                  | 4`7461423,8<br>4`8610862,0<br>4`9075826,0                                        | 55736°84<br>72625°02<br>80831°87       | 10°556<br>13°755<br>15°309 |
| 43       |                 | L<br>LIII<br>LIV      | •932<br>•272<br>•272<br>•273<br>•817 | - '147<br>+ '416<br>- '132                                                       | + · 136<br>- · 087<br>- · 049 |                                    | $- \cdot 038$ $- \cdot 011$ $+ \cdot 329$ $- \cdot 181$ $+ \cdot 137$                                   | 180       0       0.000         63       22       13.437         44       16       54.577         72       20       51.986         180       0       0.000 | 4 <sup>.</sup> 83333321,9<br>4.7260047,2<br>4.8610862,0                          | 68129`03<br>53211`40<br>72625`02       | 12°903<br>10°078<br>13°755 |

#### PRINCIPAL TRIANGULATION. TRIANGLES.

| No. of  | triangle        | -                   | rical<br>ess                              | Cor                                        | rections to                                                    | Observed A                                                                                           | ngle                                                                                                               | Corrected Plane                                                                                                                                  |                                                                                               | Distance                         |                               |
|---------|-----------------|---------------------|-------------------------------------------|--------------------------------------------|----------------------------------------------------------------|------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------|----------------------------------|-------------------------------|
| Circuit | Non-<br>circuit | Station             | Sphe<br>Exc                               | Figure                                     | Circuit                                                        | Non-<br>circuit                                                                                      | Total                                                                                                              | Angle                                                                                                                                            | Log. feet                                                                                     | Feet                             | Miles                         |
|         | 71              | XLIX<br>L<br>LII    | "<br>197<br>197<br>197                    |                                            | "                                                              | $ \begin{array}{c}     " \\     + \cdot 128 \\     - \cdot 131 \\     + \cdot \infty 3 \end{array} $ | $ \begin{array}{c}     " \\     - \cdot 023 \\     - \cdot 031 \\     + \cdot 155 \\     + \cdot 001 \end{array} $ | 0 / "<br>52 24 58 080<br>43 28 52 572<br>84 6 9 348                                                                                              | 4 <sup>-7</sup> 306825,0<br>4 <sup>-66</sup> 93669,3<br>4 <sup>-82</sup> 93997,4              | 53787`64<br>46705`38<br>67514`91 | 10°187<br>8°846<br>12°787     |
|         | 72              | L<br>LII<br>LIV     | <u> </u>                                  | $ + \cdot 062 - \cdot 151 + \cdot 613 $    |                                                                | - ·098<br>+ ·180<br>- ·082                                                                           | 036<br>+ .029<br>+ .531                                                                                            | 84 42 50 959<br>47 18 16 185<br>47 58 52 856                                                                                                     | 4 <sup>.8</sup> 578855,6<br>4 <sup>.72600</sup> 47,2<br>4 <sup>.7</sup> 306825,0              | 72091°75<br>53211°40<br>53787°64 | 13.654<br>10.078<br>10.187    |
| 44      |                 | LIII<br>LIV<br>LV   | · 074<br>· 218<br>· 217<br>· 218          | + •068<br>- •720<br>- •065                 | + '090<br>+ '028<br>- '118                                     |                                                                                                      | $+ \cdot 158$<br>$- \cdot 692$<br>$- \cdot 183$                                                                    | 52 22 56·370<br>47 41 58·331<br>79 55 5·299                                                                                                      | 4`7388713,6<br>4`7091025,0<br>4`8333321,9                                                     | 54811°46<br>51180°26<br>68129°03 | 10°381<br>9°693<br>12°903     |
| 45      |                 | LIV<br>LV<br>LVII   | · 653<br>· 151<br>· 151<br>· 151          | + '419<br>+ '037<br>- '123                 | + <sup>•</sup> 200<br>- <sup>•</sup> 127<br>- <sup>•</sup> 073 |                                                                                                      | $- \cdot 619$<br>$- \cdot 090$<br>$- \cdot 196$                                                                    | 45 15 20°558<br>60 2 25°519<br>74 42 13°923                                                                                                      | 4 <sup>.60</sup> 59499,7<br>4 <sup>.6922427,2</sup><br>4 <sup>.7</sup> 388713,6               | 40359°89<br>49231°46<br>54811°46 | 7°644<br>9°324<br>10°381      |
| 46      |                 | LV<br>LVII<br>LIX   | ·453<br>·093<br>·093<br>·093              | + '408<br>+ '260<br>- '029                 | + °092<br>+ °049<br>- °141                                     |                                                                                                      | $\begin{array}{r} + & \cdot 333 \\ + & \cdot 500 \\ + & \cdot 309 \\ - & \cdot 170 \end{array}$                    | 180         0         0.000           56         49         16.057           53         56         55.306           69         13         48.637 | 4`5578404,4<br>4`5428074,2<br>4`6059499,7                                                     | 36127°71<br>34898°56<br>40359°89 | 6.842<br>6.610<br>7.644       |
| 47      |                 | LVII<br>LIX<br>XXI  | - 279<br>- 154<br>- 154<br>- 153          | + · 303<br>- ·069<br>- ·273                | + '210<br>- '005<br>- '205                                     |                                                                                                      | $\begin{array}{ }+ & \cdot 639 \\ + & \cdot 513 \\ - & \cdot 074 \\ - & \cdot 478 \end{array}$                     | 180       0       0.000         63       2       16.689         80       51       26.712         36       6       16.599                         | 4·7375598,9<br>4·7819798,8<br>4·5578404,4                                                     | 54646°19<br>60531°29<br>36127°71 | 10°350<br>11°464<br>6°842     |
| 48      |                 | LIX<br>XXI<br>XIX   | · 401<br>· 210<br>· 210<br>· 210<br>· 210 | $+ \frac{613}{+ 846}$<br>+ $\frac{431}{-}$ | + '059<br>+ '099<br>- '158                                     |                                                                                                      | $ \begin{array}{r} - & 672 \\ + & 945 \\ + & 273 \\ + & 1.800 \\ \end{array} $                                     | 73 52 44 932<br>50 13 50 455<br>55 53 24 613                                                                                                     | 4 <sup>.</sup> 8021262,9<br>4 <sup>.</sup> 7052635,0<br>4 <sup>.</sup> 737559 <sup>8</sup> ,9 | 63405°40<br>50729°84<br>54646°19 | 12°009<br>9°608<br>10°350     |
|         | 73              | LIII<br>LV<br>LVI   | ·110<br>·110<br>·111                      | - '130<br>+ '092<br>+ '189                 |                                                                | + ·163<br>- ·040<br>- ·123                                                                           | + .033<br>+ .052<br>+ .066<br>+ .151                                                                               | 60 42 25 933<br>37 21 10 012<br>81 56 24 055                                                                                                     | 4.6539955,0<br>4.4964028,1<br>4.7091025,0                                                     | 45081°21<br>31361°93<br>51180°26 | 8 · 538<br>5 · 940<br>9 · 693 |
|         | 74              | LV<br>LVI<br>LVIII  | 145<br>145<br>145<br>145                  | + '199<br>- '144<br>+ '140                 |                                                                | $\begin{array}{c} + & \cdot 023 \\ + & \cdot 227 \\ - & \cdot 250 \end{array}$                       | $+ \cdot 222$<br>+ $\cdot 083$<br>- $\cdot 110$<br>+ $\cdot 105$                                                   | 60 4 26 557<br>62 9 23 378<br>57 46 10 065                                                                                                       | 4 <sup>.</sup> 6645259,9<br>4.6732353,7<br>4 <sup>.6</sup> 539955,0                           | 46187°66<br>47123°27<br>45081°21 | 8°748<br>8°925<br>8°538       |
|         | 75              | LV<br>LVIII<br>LIX  | +35<br>118<br>119                         | - '011<br>+ '068<br>+ '018                 |                                                                | + '170<br>- '117<br>- '053                                                                           | + .159<br>049<br>035                                                                                               | 65 47 35 721<br>44 7 41 093<br>70 4 43 186                                                                                                       | 4.6600620,7<br>4.5428074,2<br>4.6732353,7                                                     | 45715°35<br>34898°56<br>47123°27 | 8.658<br>6.610<br>8.925       |
|         | 76              | LVIII<br>LIX<br>XIX | 355<br>167<br>167<br>167<br>.167<br>.501  | - '033<br>- '043<br>+ '357                 |                                                                | + <sup>•</sup> 230<br>+ <sup>•</sup> 140<br>- <sup>•</sup> 370                                       | + '197<br>+ '097<br>- '013<br>+ '281                                                                               | 61 36 15 320<br>65 57 15 790<br>52 26 28 890<br>180 0 0 000                                                                                      | 4`7052635,0<br>4`7215129,4<br>4`6600620,7                                                     | 50729 84<br>52663 90<br>45715 35 | 9`608<br>9`974<br>8`658       |

NOTE.-Stations XIX and XXI appertain to the Sutlej Series.

September 1878.

J. B. N. HENNESSEY,

In charge of Computing Office.

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# PRINCIPAL TRIANGULATION. LATITUDES, LONGITUDES AND AZIMUTHS.

|                    |                                          | Station A                                                                                                                      |                                                                                                                                                                                                                              |                                                                                                                                                                                                 | Station B                                                                                                                                                                                                                                                                                                                                                                                                                 |                                                                                                                                                                                                 |                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |                                                                      |
|--------------------|------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------|
| Circuit<br>No.     | Series No.                               | Name                                                                                                                           | Latitude North                                                                                                                                                                                                               | Longitude East<br>of Greenwich                                                                                                                                                                  | Asimuth at A                                                                                                                                                                                                                                                                                                                                                                                                              | Log. Feet                                                                                                                                                                                       | Azimuth at B                                                                                                                                                                                                                                                                                                                                                                                                                                                                 | Series No.                                                           |
| I<br>,,<br>,,<br>2 | XLI<br>" XLIV " I " I " II " III " " III | Bonik<br>,,<br>Súnda<br>,,<br>Borta<br>,,<br>Dhaula<br>,,<br>Kundal<br>,,<br>,,<br>,,<br>,,<br>,,<br>,,<br>,,<br>,,<br>,,<br>, | <ul> <li>3 51.50</li> <li>3 51.50</li> <li>3 51.50</li> <li>3 51.50</li> <li>25 3 51.50</li> <li>3 51.50</li> <li>3 50.77</li> <li>25 5 49.53</li> <li>3 30.85</li> <li>3 30.85</li> <li>3 30.85</li> <li>3 30.85</li> </ul> | <ul> <li>o</li> <li>72 54 21.85</li> <li>y</li> <li>72 27 44.54</li> <li>y</li> <li>72 22 58.39</li> <li>y</li> <li>72 42 2.97</li> <li>y</li> <li>72 22 26.38</li> <li>y</li> <li>y</li> </ul> | 0       4       15.67         94       2       51.29         136       4       11.20         167       6       44.65         204       25       54.05         240       51       53.70         178       46       38.21         126       5       46.53         126       16       16.06         207       30       44.75         81       8       53.65         255       29       4.56         152       24       41.56 | 5.2541461,0<br>5.2394300,7<br>4.9901706,7<br>5.0716171,6<br>5.2799381,5<br>5.0802173,1<br>5.1381529,7<br>5.2852261,9<br>5.1262127,6<br>5.1426862,7<br>5.1895975,8<br>5.2492748,6<br>5.0986612,2 | o       ,         234       53       2.57         273       49       32.90         315       58       57.05         347       4       43.99         24       31       57.10         61       0       0.63         358       46       24.54         305       53       41.41         306       7       52.00         27       35       45.70         260       56       57.21         75       42       33.92         332       20       6.50         232       20       6.50 | XLIV<br>I<br>II<br>II<br>II<br>II<br>IV<br>III<br>V<br>IV<br>V<br>VI |
|                    | IV                                       | Mandaula                                                                                                                       | ,,<br>25 24 32·35                                                                                                                                                                                                            | ,,<br>71 54 38·69                                                                                                                                                                               | 214 51 38.38                                                                                                                                                                                                                                                                                                                                                                                                              | 5.2174339,4                                                                                                                                                                                     | 34 59 4.11                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | VI                                                                   |

Norz.-Stations XLI and XLIV sppertain to the Karáchi Longitudinal Series.

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## PRINCIPAL TRIANGULATION. LATITUDES, LONGITUDES AND AZIMUTHS.

| Circuit<br>No.         Beries No.         Name         Latitude North<br>of Greenwich         Longitude East<br>of Greenwich         Azimuth at A         Log. Feet         Azimuth at B         Series No.           3         V         Bhádrájau         25 35 48 29<br>25 46 52 33         72 53 43 89<br>72 53 43 89<br>72 11 50 44         130 44 59 96<br>26 43 2 53 0 4 51 381661.9<br>26 43 2 53 0 4 51 381661.9<br>84 43 44 81         VII           y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y         y                                                                  |                |                       | Station A     |                     |                                         |              | Side <b>AB</b>             |                | Station B   |
|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------|-----------------------|---------------|---------------------|-----------------------------------------|--------------|----------------------------|----------------|-------------|
| 3       V       Bhádrájan       25 35 48 29       72 53 43 89       130 44 59 96       5 0882240,5       310 37 39 31       VII         y       Nagar       25 35 48 29       72 53 43 89       130 44 59 96       5 0882240,5       310 37 39 31       VII         y       y       y       y       y       25 46 52 33       72 11 50 44       264 32 53 04       5 1381661,9       84 43 44 81       VII         y       y       y       y       y       y       y       25 46 52 33       72 11 50 44       264 32 53 04       5 1381661,9       84 43 44 81       VII         y       y       y       y       y       y       y       215 50 21 47       5 0838982,0       35 56 1 90       VIII         y       y       y       y       y       y       y       167 59 9 18       5 1281314,8       347 56 54 86       IX         y       y       y       y       y       y       221 24 12 73       5 0763667,8       41 30 30 99       X         y       y       y       y       y       26 3 5 85       72 24 49 35       108 32 58 12       5 0185059,2       288 25 0 51       IX         y       y       y       y                                                                                                                                                                         | Circuit<br>No. | Series No.            | Name          | Latitude North      | Longitude East<br>of Greenwich          | Azimuth at A | Log. Feet                  | Azimuth at B   | Series No.  |
| 3       V       Bhádrájan       25 35 48 · 29       72 53 43 · 89       130 44 59 · 96       5 · 0882240,5       310 37 39 · 31       VII         VI       Nagar       25 46 52 · 33       72 11 50 · 44       264 32 53 · 04       5 · 1381661,9       84 43 44 · 81       VII         n       n       n       n       n       215 50 21 · 47       5 · 0838982,0       35 56 1 · 90       VIII         n       n       n       n       n       167 59 9 · 18       5 · 1281314,8       347 56 54 · 86       IX         4       VII       Samdari       26 3 5 · 85       72 36 48 · 02       142 31 35 · 72       5 · 032291 · 2,1       322 26 21 · 42       VIII         n       n       n       n       n       n       n       n       n       n         y       n       n       n       n       n       n       n       n       n       n         n       n       n       n       n       n       n       n       n       n       n         n       n       n       n       n       n       n       n       n       n       n         n       n       n       n       n                                                                                                                                                                                                                        |                |                       |               | 0 / //              | 0 1 11                                  | 0 / //       |                            | 0 1 11         |             |
| VI       Nagar       25 46 52 33       72 11 50 44       264 32 53 04       5 1381661,9       84 43 44 81       VII         y,       y,       y,       y,       y,       215 50 21 47       5 0838982,0       35 56 1 90       VIII         y,       y,       y,       y,       y,       167 59 9 18       5 1281314,8       347 56 54 86       IX         4       VII       Samdari       25 48 59 55       72 36 48 02       142 31 35 72       5 0763667,8       41 30 30 99       X         y,       y,       y,       y,       211 2 73       5 0763667,8       41 30 30 99       X         y,       y,       y,       y,       21 2 4 12 73       5 0763667,8       41 30 30 99       X         y,       y,       y,       y,       y,       221 24 12 73       5 0763667,8       41 30 30 99       X         y,       y,       y,       y,       y,       26 3 5 85       y,       y,       268 21 0 44       5 1596842,2       88 32 35 99       X         y,       y,       y,       y,       y,       y,       y,       227 57 56 94       5 0955763,7       48 5 25 41       XII                                                                                                                                                                                                           | 3              | v                     | Bhádrájau     | 25 35 48.29         | 72 53 43.89                             | 130 44 59.96 | 5.0882240,5                | 310 37 39.31   | VII         |
| " $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$ $"$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                | VI                    | Nagar         | 25 46 52.33         | 72 11 50.44                             | 264 32 53.04 | 5.1381661,9                | 84 43 44.81    | VII         |
| """       """       """"       """"""""""""""""""""""""""""""""""""                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   |                | <b>33</b>             |               | >>                  | 22                                      | 215 50 21.47 | 5.0838982,0                | 35 56 1.90     | VIII        |
| 4       VII       Samdari       25 48 59 55       72 36 48 02       142 31 35 72       5 0322912,1       322 26 21 42       VIII         ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       "" <t< td=""><td></td><td>39</td><td>&gt;&gt;</td><td>,,,</td><td>,,</td><td>167 59 9.18</td><td>5.1281314,8</td><td>347 56 54.86</td><td>IX</td></t<>                                                                                     |                | 39                    | >>            | ,,,                 | ,,                                      | 167 59 9.18  | 5.1281314,8                | 347 56 54.86   | IX          |
| """       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       """       """       ""       ""       ""       ""       ""       ""       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """ <th"""< th=""> <th"""< th=""> <th"""< td="" th<=""><td>4</td><td>VII</td><td>Samdari</td><td>25 48 59.55</td><td>72 36 48.02</td><td>142 31 35.72</td><td>5.0322912,1</td><td>322 26 21.42</td><td>VIII</td></th"""<></th"""<></th"""<> | 4              | VII                   | Samdari       | 25 48 59.55         | 72 36 48.02                             | 142 31 35.72 | 5.0322912,1                | 322 26 21.42   | VIII        |
| """       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       """       """       """       ""       ""       ""       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """       """"       """       """ <th"< td=""><td></td><td></td><td></td><td></td><td></td><td></td><td></td><td>•</td><td></td></th"<>                                                                                                           |                |                       |               |                     |                                         |              |                            | •              |             |
| VIII       Thob       26 3 5.85       72 24 49.35       108 32 58.12       5.0185059,2       288 25 0.51       IX         ,,       ,,       ,,       ,,       ,,       268 21 0.44       5.1596842,2       88 32 35.99       X         ,,       ,,       ,,       ,,       173 40 37.56       5.0217355,9       353 39 41.37       XI         ,,       ,,       ,,       ,,       227 57 56.94       5.0955763,7       48 5 25.41       XII                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | "              | 33                    | ,,            | ,,                  | ,,                                      | 221 24 12.73 | 5.0763667,8                | 41 30 30.99    | x           |
| ""       ""       ""       268 21 0.44       5.1596842,2       88 32 35.99       X         ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""                                                                                                                                                                                                                                                   |                | V1II                  | Thob          | 26 3 5.85           | 72 24 49.35                             | 108 32 58.12 | 5.0185059,2                | 288 25 0.51    | IX          |
| """       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       ""       "" <th""< th="">       ""       ""       <th< td=""><td></td><td>,,</td><td>,,</td><td>22</td><td>22</td><td>268 21 0.44</td><td>5.1596842,2</td><td>88 32 35.99</td><td>x</td></th<></th""<>                                                                                            |                | ,,                    | ,,            | 22                  | 22                                      | 268 21 0.44  | 5.1596842,2                | 88 32 35.99    | x           |
| " " " " " " 227 57 56 <sup>.</sup> 94 5 <sup>.</sup> 0955763,7 48 5 25 <sup>.</sup> 41 XII                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |                | ,,                    | <i>))</i>     | ,,                  | ,,                                      | 173 40 37.56 | 5.0217355,9                | 353 39 41.37   | XI          |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |                | ,,                    | <b>))</b>     | , ,,                | >>                                      | 227 57 56.94 | 5.0955763,7                | 48 5 25.41     | XII         |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |                |                       |               |                     |                                         |              |                            |                |             |
| IX Borla 26 8 33.54 72 6 43.60 230 38 48.14 5.0521346,8 50 45 51.92 XI                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                | IX                    | Borla         | 26 8 33.54          | 72 6 43.60                              | 230 38 48.14 | 5.0521346,8                | 50 45 51.92    | XI          |
| 5 X Dodo 26 3 44.63 72 51 12.79 147 1 25.63 4.9764158,6 326 57 15.80 XII                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | 5              | x                     | Dodo          | 26 3 44 . 63        | 72 51 12.79                             | 147 1 25.63  | 4 • 97641 58,6             | 326 57 15.80   | XII         |
| XI Adori 26 20 20.83 72 22 42.07 281 24 46.79 5.0263010,9 101 33 13.96 XII                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            |                | XI                    | Adori         | 26 20 20.83         | 72 22 42.07                             | 281 24 46.79 | 5.0263010,9                | 101 33 13.96   | XII ·       |
| ", ", ", ", ", 222 49 42·57 4·9330134,9 42 54 28·04 XIII                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |                | 23                    | >>            | ,,,                 |                                         | 222 49 42.57 | 4 • 93301 34,9             | 42 54 28.04    | XIII        |
| ,, ,, ,, ,, ,, 169 21 58·14 4·8199682,4 349 20 58·40 XIV                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |                | "                     | 29            | ,,                  | 22                                      | 169 21 58.14 | 4.8199682,4                | 349 20 58.40   | XIV         |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |                |                       |               |                     |                                         |              |                            |                |             |
| 6 XII Dugur 26 16 51 33 72 41 46 35 151 27 51 69 4 9804877,8 331 24 8 15 XIII                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | 6              | XII                   | Dugur         | 26 16 51.33         | 72 41 46.35                             | 151 27 51.69 | 4.9804877,8                | 331 24 8.15    | XIII        |
| " " " " " " " " 207 19 58.65 4.9293907,2 27 23 9.55 XV                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | "              | >>                    | >>            | >>                  | >>                                      | 207 19 58.65 | 4.9293907,2                | 27 23 9.55     | XV          |
| XIII Ketu 26 30 43 00 72 33 23 52 91 45 54 70 4 8480978,0 271 40 8 41 XIV                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             |                | XIII                  | Ketu          | 26 30 43.00         | 72 33 23.52                             | 91 45 54.70  | 4.8480978,0                | 271 40 8.41    | XIV         |
| " " " " " 275 39 35·81 4·9300411,0 95 46 31·84 XV                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                | >>                    | >>            | "                   | >>                                      | 275 39 35.81 | 4.9300411,0                | 95 46 31.84    | XV          |
| " " " " " " " 140 49 47°61 4°8593774,0 320 46 2°15 XVI                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                | "                     | "             | >>                  | 33                                      | 140 49 47.61 | 4.8593774,0                | 320 46 2.15    | XVI         |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |                |                       |               |                     |                                         |              |                            |                |             |
| """"""""""""""""""""""""""""""""""""""                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                | »»                    | <i>"</i>      | 23 ·                | >>                                      | 203 48 6.99  | 4.7829932,9                | 23 50 7.80     |             |
| XIV Sulkia Thalau 26 31 3.92 72 20 27.84 204 34 17.51 4.7732438,0 24 36 19.25 XVI                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                |                       | Sulkia Thalau | 26 31 3.92          | 72 20 27.84                             | 204 34 17.51 | 4.7732438,0                | 24 36 19.25    | XVI         |
| 7 XV Malunga 26 29 19.00 72 48 55.92 136 49 0.62 4.9435461,4 316 44 4.24 XVII                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | 7              | XV                    | Malunga       | 26 29 19.00         | 72 48 55.92                             | 136 49 0.62  | 4.9435461,4                | 316 44 4.24    | XVII        |
| XVI Loharan 20 39 58.22 72 24 59.81 270 24 12.22 4.8462130,0 90 29 59.42 XVII                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |                | XVI                   | Loharan       | 26 39 58.22         | 72 24 59.81                             | 270 24 12.22 | 4.8462130,0                | 90 29 59.42    |             |
| ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,, ,,                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                | <b>,,</b>             | >>            | >>                  | >>                                      | 208 36 22.52 | 4.7784986,6                | 28 38 45.30    | XVIII       |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |                |                       |               |                     |                                         |              |                            |                | VIV         |
| y         y         y         152 40 20.48         4.7850410,2         332 38         1.48         XIX           9         WIII         Champ                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |                | איז <del>א</del> יזיד | "             | »»                  | <b>"</b>                                | 152 40 20.48 | 4.7050410,2                | 332 38 1.48    | AIA<br>VUIT |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 | o              |                       |               | 20 39 52 74         | 72 37 53.40                             | 142 11 39.24 | 4.8289003,0                | 322 0 13.95    |             |
| """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """         """ <th""< th=""> <th"""< th=""> <th"""< th=""></th"""<></th"""<></th""<>                                                                 | <b>"</b>       | »<br>VVIII            | y<br>Dolm     | <i>"</i>            | "                                       | 201 3 30.70  | 4.0320270,0                | 21 5 39.07     | AA<br>VIV   |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |                | AVIII                 | relu          | 20 40 40 25         | 72 30 17-10                             | 91 29 30.40  | 4.7539932,1                | 271 24 47 90   | AIA<br>VV   |
| <i>"""" "" " "" "" "" "" "" ""</i>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |                | <b>23</b>             | **            | "                   | >>                                      | 200 45 30.92 | 4-0240902,3                | 00 51 5.52     | ла          |
| The at the second second and the second SVI                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                |                       |               |                     |                                         |              | <br>                       | 1 004 18 50100 | XXI         |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       |                | >>                    | >>            | "                   | , ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | 154 21 15:05 | 4 7955005,4                | 334 10 59 92   | XXII        |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |                | "<br>XIX              | "<br>Daichn   | »»<br>»6 48 5 4 5 5 | »»                                      | 203 23 0.17  | 4 0002905,7                | 25 25 24 10    | XXI         |
| $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 |                | XX                    | Soran         | 26 50 2500          | 14 19 50.09                             | 146 05 10.16 | 4 /940/72,2<br>A·806260r 6 | 20 24 31 30    | XXII        |
| <b>XXI</b> Jalore $2657.8172.25314025131040204035,0320227751 AATT$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | Г <sup>У</sup> | XXI                   | Jalora        | 06 57 57.81         | 1 44 45 33                              | 140 25 13 10 | 4.7528280 0                | 70 28 54.04    | XXII        |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 1              |                       |               | a 3/ 3/ 01          | /~ ~ 3 10 30                            | ~JY J# 14 10 | ליליטיטיטיט                | /> 5º 34 04    |             |

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|                |                                             | Station A                                 |                                         |                                | Station B     |             |               |                                     |
|----------------|---------------------------------------------|-------------------------------------------|-----------------------------------------|--------------------------------|---------------|-------------|---------------|-------------------------------------|
| Circuit<br>No. | Series No.                                  | Name                                      | Latitude North                          | Longitude East<br>of Greenwich | Azimuth at A  | Log. Feet   | Azimuth at B  | Series No.                          |
|                |                                             |                                           | 0 / //                                  | 0 / 11                         | o / #         |             | 0 1 11        |                                     |
|                | XXI                                         | Jalora                                    | 26 57 57.81                             | 72 25 18.36                    | 160 38 16.55  | 4.6986909,8 | 340 36 53.24  | XXIII                               |
|                | "                                           | 33                                        | 33                                      | "                              | 209 54 4.42   | 4.7957073,2 | 29 56 41.13   | XXIV                                |
| 10             | XXII                                        | Loháwat                                   | 26 59 39.15                             | 72 35 35 25                    | 117 4 43.11   | 4.9096344,2 | 296 58 39.27  | XXIII                               |
| "              | ,,                                          | 33                                        | رو                                      | 22                             | 150 45 19.35  | 4.7018973,2 | 330 43 15.55  | XXIV                                |
|                | XXIII                                       | Ekka                                      | 27 5 44.66                              | 72 22 15.04                    | 261 36 35.87  | 4.6832601,5 | 81 40 36.45   | XXIV                                |
|                |                                             | •                                         |                                         |                                |               |             |               |                                     |
|                | "                                           | 22                                        | 33                                      | ۰ در                           | 186 25 23.55  | 4.8263806,9 | 6 26 1.54     | XXV                                 |
|                | ,,                                          |                                           | "                                       | در                             | 223 12 20.26  | 4.9508827,8 | 43 17 29.86   | XXVI                                |
| 11             | XXIV                                        | Omlo                                      | 27 6 54.07                              | 72 31 3.07                     | 146 3 30.20   | 4.8566423,2 | 326 0 6.87    | XXV                                 |
| 22             | "                                           | <b>))</b>                                 | ,,,                                     | ,,                             | 193 5-39.80   | 4.7751950,4 | 13 6 48.19    | XXVI                                |
|                | XXV                                         | Khirwa                                    | 27 16 44.49                             | 72 23 38.18                    | 271 38 41 95  | 4.7296662,9 | 91 43 14.41   | XXVI                                |
|                |                                             |                                           |                                         |                                |               |             |               |                                     |
|                | <b>33</b>                                   | <b>39</b>                                 | ,,                                      | 22                             | 205 44 50.29  | 4.7752348,0 | 25 47 2.32    | XXVII                               |
|                | ,,                                          | "                                         | ,,                                      | ,,,                            | 145 57 39.48  | 4.8323596,4 | 325 54 25.40  | XXVIII                              |
| 12             | XXVI                                        | Jambo                                     | 27 16 28.88                             | 72 33 32.71                    | 153 23 43.23  | 4.7910041,2 | 333 21 22.10  | XXVII                               |
| "              | ,,                                          | ,,,                                       | 23                                      | ,,                             | 206 0 2.55    | 4.7893888,8 | 26 2 20.19    | XXIX                                |
|                | XXVII                                       | Sirad                                     | 27 25 36.03                             | 72 28 25.53                    | 92 24 29.32   | 4.8061453,4 | 272 19 2.39   | XXVIII                              |
|                |                                             |                                           |                                         |                                |               |             |               |                                     |
|                | <b>3</b> 2                                  |                                           | >>                                      | ,,,                            | 269 52 27.42  | 4.7377444,7 | 89 57 6.90    | XXIX                                |
|                | >>                                          | در                                        | ,,                                      | "                              | 145 44 10.16  | 4.8855711,7 | 325 40 28.00  | · XXX                               |
|                | **                                          | ))                                        | >>                                      | 22                             | 193 13 35.86  | 4.8999729,0 | 13 15 9.28    | XXXI                                |
|                | XXVIII                                      | Harban                                    | 27 26 2.16                              | 72 16 35.84                    | 198 41 19.99  | 4.8077577,7 | 18 43 5.70    | . XXX                               |
| 13             | XXIX                                        | Bintli                                    | 27 25 36.85                             | 72 38 32.30                    | 154 46 .33.02 | 4.9314209,2 | 334 43 25.96  | XXXI                                |
|                |                                             |                                           |                                         |                                |               |             |               | <b>V</b> V V T                      |
|                | XXX                                         | Nok                                       | 27 36 4.67                              | 72 20 24.63                    | 257 15 40.40  | 4.7991189,0 | 77. 20 57.03  | . AAAI                              |
| 1              | ,,                                          | <i>))</i>                                 | . ,,                                    | 33                             | 194 39 29.24  | 4.7209190,2 | 14 40 38.03   | XXXII                               |
|                | ,,                                          | >>                                        | رر                                      | ))                             | 138 49 14.15  | 4.7201817,4 | 318 40 15.00  | ΧΛΛΙΙΙ                              |
| 14             | XXXI                                        | Mongolia                                  | 27 38 21.71                             | 72 31 47.62                    | 127 38 51.98  | 4.7831115,6 | 307 34 43.44  | XXXII                               |
| "              | 22                                          | "                                         | >>                                      | <b>77</b> -                    | 182 20 5.76   | 4.8307231,2 | 2 20 20.20    | XXXV                                |
|                | <b>T</b> 7 <b>T</b> 7 <b>T</b> 7 <b>T</b> 7 |                                           |                                         |                                |               |             |               | VVVIII                              |
|                | XXXII                                       | Pabusar                                   | 27 44 28.51                             | 72 22 52.77                    | 70 40 0.08    | 4.0920302,5 | 250 35 52.21  | <b>XXXIV</b>                        |
|                | در                                          | <i>))</i>                                 | >>                                      | 22                             | 171 0 45.07   | 4.0592271,0 | 351 0 9.03    |                                     |
|                | »»                                          | "                                         | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | >>                             | 238 7 20.34   | 4.7709581,3 | 58 11 50.18   | ··· AAAV<br>VVVIV                   |
|                | XXXIII                                      | Bikampur                                  | 27 42 35.85                             | 72 13 59.97                    | 215 49 10.00  | 4.8429305,0 | 35 52 47.70   | AAAIV<br>VVVV                       |
|                | XXXIV                                       | Phulasar                                  | 27 51 54.92                             | 72 21 34.22                    | 283 6 20.74   | 4.7738045,8 | 103. 11 21.81 | . <b>ЛЛД</b> V                      |
|                |                                             |                                           |                                         |                                |               |             | 4             | YYYVI                               |
|                | "                                           | دد                                        | "                                       | <b>33</b> ···                  | 225 0 31.80   | 4 0555191,1 | 45 12 57 40   | XXXVII<br>XXXVII                    |
|                | ))<br>VVVT                                  | <i>"</i>                                  | >>                                      | "                              | 150 51 32.91  | 4 7500005,7 | 330. 49 37 23 | , <u>лаатіі</u><br>Таатіі<br>Таатіі |
| - 5            | ΔΔΔΫ                                        | Girondi                                   | 27 49 41.10                             | 72 32 18.78                    | 173 40 45.27  | 4.0000000,1 | 353 40 0.99   | XXXVIII<br>VVVVIII                  |
| <i>»</i>       | ))<br>TT 37 TT T T                          | ,,,<br>,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | "                                       | >>                             | 247 33 14.15  | 4.7073000,5 | 07 37 55.91   | AAAVIII<br>VVVVII                   |
| 10             | XXXVI                                       | Mankasar                                  | 28 0 15.40                              | 72 31 1.30                     | 91 1 19.90    | 4.9031194'8 | 270 54 57.08  | ΔλΔΥΠ                               |
|                |                                             |                                           | l                                       |                                |               |             |               |                                     |

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# PRINCIPAL TRIANGULATION. LATITUDES, LONGITUDES AND AZIMUTHS.

|                |            | Station A      |                                         |                                              |                     | Side AB      |                                                                      | Station <b>B</b> |
|----------------|------------|----------------|-----------------------------------------|----------------------------------------------|---------------------|--------------|----------------------------------------------------------------------|------------------|
| Circuit<br>No. | Series No. | Name           | Latitude North                          | Longitude East<br>of Greenwich               | Azimuth at A        | Log. Feet    | Azimuth at B                                                         | Series No.       |
|                |            |                | 0 / //                                  | o ' "                                        |                     |              | 0 1 11                                                               |                  |
| 16             | XXXVI      | Mankasar       | 28 0 15.40                              | 72 31 1.30                                   | 304 19 59.46        | 4.8688143,2  | 124 25 18.34                                                         | XXXVIII          |
| "              | "          | "              | ,,                                      | ,,                                           | 167 15 44.36        | 4.9710293,6  | 347 13 55.60                                                         | XXXIX            |
| "              | 22         | 32             | ,,                                      | 22                                           | 256 59 41.77        | 4.8405886,1  | 77 5 35.79                                                           | XL               |
|                | XXXVII     | Uperthal       | 28 0 27.62                              | 72 17 27.29                                  | 210 5 2.12          | 5.0172721,8  | 30 9 37.16                                                           | XXXIX            |
|                | "          | 22             |                                         |                                              | 147 37 7.33         | 5.0164405,2  | 327 32 14.09                                                         | XLI              |
| · ·            | XXXVIII    | Bithnok        | 27 53 22.03                             | 72 42 21:73                                  | 186 30 51.43        | 4.7607854.7  | 6 31 25.67                                                           | XL               |
| 17             | XXXIX      | Modia          | 28 15 18.87                             | 72 27 10.63                                  | 310 36 54.72        | 5.0650027.1  | 120 44 20.01                                                         | XL               |
| ,,             | 23         |                | , ,,                                    |                                              | 88 50 15.22         | 5.0326460.5  | 268 40 44.68                                                         | XLI              |
| ,,             |            |                |                                         |                                              | 261 35 42.20        | 1.0677234.5  | 81 42 48.08                                                          | XLII             |
|                |            |                |                                         |                                              | 172 10 18.02        | 4.08065051   |                                                                      | XLIII            |
|                | ,,         |                | , ,,                                    |                                              | 1/2 10 10 95        | 4 9000505,1  | <u> 304 9 9 5'</u>                                                   |                  |
| <i></i>        | <b>33</b>  | ·              | . در                                    |                                              | 222 18 16.94        | 5.0712328,4  | 42 25 19.37                                                          | XLIV             |
|                | XL         | Ronesar        | 28 2 49.20                              | 72 43 34.73                                  | 182 29 19.10        | 4.9506238,0  | 2 29 39.56                                                           | XLII             |
|                | XLI        | Sachu          | 28 14 55.74                             | 72 7 5.29                                    | 224 11 22.48        | 5-1321256,3  | 44 10 46.02                                                          | XLIII.           |
|                | XLII       | Jodasar        | 28 17 32.17                             | 72 44 18.09                                  | 170 27 54.31        | 4.8720131.7  | 350 26 48.42                                                         | XLIV             |
|                | XLIII      | Mugrala        | 28 30 57.06                             | 72 24 44 .59                                 | 274 41 35.02        | 4.0668150.0  | 04 40 48.02                                                          | XLIV             |
|                |            |                |                                         | 1 11 307                                     | -/+ +- 30           | + ,          | ייד ד <del>י</del> ע איז דיע איז |                  |
|                |            | >>             | >>                                      | 53                                           | 218 36 31.02        | 4.9654010,0  | . 38 41 40.98                                                        | XLV              |
|                | · ,,       | » ·            | ,,                                      |                                              | 171 53 32.98        | 4.9023565,3  | 351 52 32.36                                                         | XLVI             |
| 18             | XLIV       | Khirsar        | 28 29 40.91                             | 72 41 59.52                                  | 156 36 47.40        | 4.9393501,4  | 336 33 41.77                                                         | XLV              |
| ,,             | ,,         | <b>3</b> 2     | >>                                      | ••                                           | 199 15 37.57        | 4.9957923,9  | 19 18 33.40                                                          | XLVII            |
| 19             | XLV        | Bhad <b>a</b>  | 28 42 51.12                             | 72 35 31.79                                  | 95 48 46.46         | 4.84029.53,2 | 275 42 34.62                                                         | XLVI             |
|                |            |                |                                         |                                              |                     |              | /0 . 0.                                                              |                  |
|                | <b>33</b>  | <b>))</b>      | ,,                                      | "                                            | 258 26 48 88        | 4.8361016,5  | 78 32 51.73                                                          | XLVII            |
| ,,             | >>         |                | "                                       | ,,                                           | 139 48 44.21        | 4.8014690,2  | 319 45 3.02                                                          | XLVIII           |
| · ,,           |            | 29 <sup></sup> | "                                       | >>                                           | 200 42 54.60        | 4.9501666,8  | 20 45 45.78                                                          | XLIX             |
|                | XLVI       | Habib          | 28 43 59.93                             | 72 22 38.06                                  | 214 1 6.68          | 4.6985532,8  | 34 3 38.04                                                           | XLVIII           |
|                | XLVII      | Karamala       | 28 45 6.50                              | 72 48 6.58                                   | 153 0 28.08         | 4.8934831,4  | 332 57 15.20                                                         | XLIX             |
|                |            |                |                                         |                                              |                     |              |                                                                      |                  |
|                | XLVIII     | Phogala        | 28 50 49.77                             | 72 27 52.35                                  | 244 6 55·57         | 4.9053711,5  | 64 13 29.11                                                          | XLIX             |
|                | >>         | "              |                                         | <b>))</b> .                                  | 1 <u>90.54</u> 8.94 | 4.8351155,5  | 10 55 19.47                                                          | $\mathbf{L}$     |
|                | "          | <b>3</b> 3     | 22                                      | ,,                                           | 118 25 32.91        | 4.8346015,3  | 298 20 6.12                                                          | LI               |
| 20             | XLIX       | Bhulan         | 28 56 36.70                             | 72 41 26.80                                  | 118 27 54.76        | 4.8293997,4  | 298 22 30.70                                                         | L                |
| "              | <b>)</b> ) | >>             | 22                                      | <i>"</i>                                     | 170 52 53.04        | 4.6693669,3  | 350 52 12.59                                                         | LII              |
| 21             | L          | Soma           | 20 1 51.85                              | 72 30 18.12                                  | 64 28 15°AE         | 1.0075826 0  | 244 21 27.07                                                         | T.T              |
| ,,             | 22         | 99             | , ,,                                    | ,                                            | 254 52 27.02        | 4.720682=0   | 74 58 00.10                                                          |                  |
| ,              |            |                | ,,,                                     | <i>,,,</i> ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | 106 48 22.04        | 4.86108620   | 286 40 10-32                                                         | LITT             |
|                |            |                | ,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,, | 33                                           |                     | 4.706002,0   | 400 44 14 30                                                         | T.137            |
|                | LI         | Telu           | 28 56 11.24                             | 72 16 25.08                                  | 182 20 20.75        | 4 /20004/,2  | 55° 9 5° 95                                                          | T.ITT            |
|                |            |                | ,- ,- ,4                                | /~ · · 55 90                                 | 105 30 32 79        | 4 /401423,0  | 3 30 31 44                                                           | 14111            |
|                |            |                | J                                       |                                              |                     |              |                                                                      |                  |

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|                |                                | Station A                                    |                                                     |                                                       | Station <b>B</b>                                                                          |                                                                                        |                                                                                                                                                                                          |                                             |
|----------------|--------------------------------|----------------------------------------------|-----------------------------------------------------|-------------------------------------------------------|-------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------|
| Circuit<br>No. | Series No.                     | Name                                         | Latitude                                            | Longitude East<br>of Greenwich                        | Azimuth at A                                                                              | Log. Feet                                                                              | Azimuth at <b>B</b>                                                                                                                                                                      | Series No.                                  |
|                | LII<br>LIII<br>"               | Aukli<br>Mansa •                             | o , , , , , , , , , , , , , , , , , , ,             | o , , , , , , , , , , , , , , , , , , ,               | 0 / 10<br>122 16 38.54<br>242 25 17.53<br>190 2 20.94<br>129 19 54.90                     | 4 · 8578855,6<br>4 · 8333321,9<br>4 · 7091025,0<br>4 · 4964028,1                       | 0 / //<br>302 11 3.87<br>62 30 49.21<br>10 3 10.01<br>309 17 41.77                                                                                                                       | LIV<br>LIV<br>LV<br>LVI                     |
| 22<br>"        | LIV<br>"<br>LV<br>"            | Marot<br>,,<br>Hasan<br>,,<br>,,<br>,,<br>,, | 29 10 33·95<br>"<br>29 13 41·10<br>"<br>"           | 72 28 35·73<br>"<br>72 18 55·14<br>"                  | 110 12 47.75<br>155 28 8.46<br>47 24 20.13<br>230 5 38.82<br>107 28 46.83<br>173 16 22.67 | 4.7388713,6<br>4.6922427,2<br>4.6539955,0<br>4.6059499,7<br>4.6732353,7<br>4.5428074,2 | 290       8       4.49         335       26       15.69         227       21       17.61         50       8       29.77         287       24       38.86         353       16       0.09 | LV<br>LVII<br>LVII<br>LVIII<br>LVIII<br>LIX |
| 23<br>"        | LVI<br>LVII<br>"<br>LVIII<br>" | Sultán<br>Bijli<br>"<br>Panchkot             | 29 8 38·88<br>29 17 57·32<br>,,<br>29 16 0·97<br>,, | 72 12 40°84<br>72 24 44°85<br>,,<br>72 10 27°60<br>,, | 165 11 54.08<br>104 5 25.17<br>167 7 42.01<br>243 16 57.65<br>181 40 42.16                | 4 • 664,52,59,9<br>4 • 5578404,4<br>4 • 7819798,8<br>4 • 6600620,7<br>4 • 721,5129,4   | 345 10 49.07<br>284 2 11.36<br>347 6 27.17<br>63 20 43.39<br>1 40 50.71                                                                                                                  | LVIII<br>LIX<br>XXI<br>LIX<br>XIX           |
|                | LIX<br>"<br>XIX<br>XXI         | Randu<br>,,<br>Kaimsir<br>Kanda              | 29 19 24·24<br>"<br>29 24 42·15<br>29 27 41·52      | 72 18 8·95<br>"<br>72 10 45·04<br>72 22 12·29         | 129 17 59.35<br>203 10 44.49<br>253 20 56.83                                              | 4`7052635,0<br>4`737559 <sup>8</sup> ,9<br>4`8021262,9                                 | 309 14 21.65<br>23 12 43.92<br>73 26 34.58                                                                                                                                               | XIX<br>XXI<br>XXI                           |

NOTE .- Stations XIX and XXI appertain to the Sutlej Series.

September 1878.

J. B. N. HENNESSEY, In charge of Computing Office.


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#### JODHPORE MERIDIONAL SERIES.

#### PRINCIPAL TRIANGULATION. HEIGHTS ABOVE MEAN SEA LEVEL.

The following table gives, first, the usual data of the observed vertical angles and the heights of the signal and instrument, &c., in pairs of horizontal lines, the first line of which gives the data for the 1st or the fixed station, and the second line the data for the 2nd or the deduced station. This is followed by the arc contained between the two stations, and then by the terrestrial refraction, and the height of the 2nd station above or below the 1st, as computed from the vertical angles in the usual manner. This difference of height applied to the given height above mean sea level of the fixed station, gives that of the deduced station. Usually there are two or three independent values of the height of the deduced station; the details are so arranged as to show these consecutively and their mean in the columns of "Trigonometrical Results". The mean results thus obtained are however liable to receive corrections for the errors generated in the trigonometrical operations, which are shown up by the spirit leveling operations, whenever a junction between the two has been effected. The spirit leveled determinations, when available, are always accepted as final, and the trigonometrical heights of stations, lying between other stations fixed by the leveling operations, are adjusted—usually by simple proportion—to accord with the latter.

The heights of Jodhpore Meridional Series have been adjusted between the final values of Bonik and Súnda the fixed points of the Karáchi Longitudinal Series, and those of the fixed stations of Kaimsir and Kanda of the Sutlej Series. The heights of the fixed points are as follows :--

| XLI, Bonik<br>XLIV, Súnda  | ••• | 2098<br>325:2 | } feet above Mean S | ea Level at | Karáchi from | Karáchi I   | ongitudinal | Series |
|----------------------------|-----|---------------|---------------------|-------------|--------------|-------------|-------------|--------|
| XIX, Kaimsir<br>XXI. Kauda | ••• | 461<br>478    | <b>,</b> "          | "           | from         | n Sutlej Se | ries.       |        |

The trigonometrical heights always refer to the upper mark-stone, or to the upper surface of the pillar on which the theodolite stood. When the pillar of the station is perforated, the height given in the last column, is that between the upper surface of pillar and ground level mark-stone in floor of passage; otherwise it is the approximate height of the structure above the ground at the base of the station.

| Astronor     | nical    | Date               |           |                                                     | tions      | Height       | in feet      |         | Terre<br>Refra | estrial<br>action | ation                     | Height ir            | n feet of 2n     | d Station | Tower   |
|--------------|----------|--------------------|-----------|-----------------------------------------------------|------------|--------------|--------------|---------|----------------|-------------------|---------------------------|----------------------|------------------|-----------|---------|
|              |          | Mean of            | Station   | Observed                                            | obeerva    |              | nt           | ied Arc | 8              | of<br>Aro         | ht of<br>- 1st St<br>feet | above                | e Mean Sea       | Level     | llar or |
| 1873         |          | Times<br>of obser- | Station   | Vertical Angle                                      | ber of a   | Signal       | et rume      | Contain | າ ອອດເປ        | cimals<br>tained  | Heig<br>Station-          | Trigono<br>Res       | metrical<br>ults | Final     | t of Pi |
|              |          | vation             |           |                                                     | Num        |              | In           |         | Ir             | Con               | 2nd S                     | By each<br>deduction | Mean             | Result    | Heigh   |
|              |          | h. m.              | XI.       | 0 / 7                                               |            |              |              | 7       |                |                   |                           |                      |                  |           | feet    |
| Feb.         | 15       | 3 45               | I         | EO 252.8                                            | 12         | 4.10         | 5.52         | 1715    | 113*           | •066 <b>*</b>     | - 772.7                   | 1325.3               |                  |           |         |
| Jan.<br>Feb. | 31<br>15 | 3 24<br>3 23       | XLIV<br>I | D I 4 43 <sup>.</sup> 3<br>E o 47 33 <sup>.</sup> 9 | I 2<br>I 2 | 2·70<br>2·69 | 5°25<br>5°25 | 1165    | 72             | ·062              | - 1926 . 3                | 1325.7               | 1326.0           | 1326      | 3.1     |
| ))<br>))     | 11<br>15 | 3 20<br>3 19       | II<br>I   | Do 416.7<br>Do 1259.8                               | 12<br>12   | 2.69<br>2.56 | 5°25<br>5°25 | 1188    | 80             | •068              | + 152.5                   | 1326.9               |                  |           |         |
| 33<br>39     | 8<br>10  | 2 45<br>2 46       | XLI<br>II | D 0 39 31 2<br>E 0 25 26 2                          | I 2<br>I 2 | 2·56<br>4·42 | 5°25<br>5°25 | 966     | 64             | •066              | — 922·8                   | 1175°2               |                  |           |         |

• Estimated.

| Astronomical                 | Date                          |                   |                                    | tions         | Height       | in feet      | 0            | Terre<br>Refra | strial<br>ction        | station                                | Heigfeet             | of 2nd Stat<br>n Sea Level | ion . |                |              |
|------------------------------|-------------------------------|-------------------|------------------------------------|---------------|--------------|--------------|--------------|----------------|------------------------|----------------------------------------|----------------------|----------------------------|-------|----------------|--------------|
| 1873                         | Mean of<br>Times<br>of obser- | Station           | Observed<br>Vertical Angle         | ег об орвегти | lignal       | trument      | contained Ar | econde         | cimals of<br>ained Arc | Height of<br>tation – 1st 5<br>in feet | Trigono<br>Res       | metrical                   |       | ght of Filling |              |
|                              | vation                        |                   |                                    | Numb          |              | Ine          | J            | In             | De<br>Cont             | 2nd S                                  | By each<br>deduction | Mean                       | Rel   |                |              |
| Jany. 31, Feb. 1<br>Feb. 11  | h. m.<br>3 14<br>3 13         | XLIV<br>II        | 0 1 "<br>D 0 51 9 5<br>E 0 23 50 6 | I 2<br>I 2    | 2·56<br>2·74 | 5°25<br>5°25 | "<br>1882    | 125            | ·066                   | - 2078 . 5                             | 1173.5               | 1173'9                     |       | 4              | fed<br>2 · 8 |
| " 15<br>" 11                 | 3 19                          | III               | D o 12 59.8<br>D o 4 16.7          | 12            | 2.56         | 5.25         | 1188         | 80             | •068                   | - 152.2                                | 1173.0               |                            |       |                |              |
| ,, 15<br>,, 27,28            | 2 57<br>2 58                  | I<br>III          | E o 25 19.7<br>D o 45 6.4          | 12<br>12      | 2.57         | 5°25<br>5°25 | 1358         | 90             | •066                   | + 1408.4                               | 2734*4               | 2735'I                     | 273   | 5              | 3.3          |
| " 11<br>" <sup>.</sup> 27    | 3 24                          |                   | E o 30 34.7<br>D o 49 42.8         | 12            | 2·57<br>2·56 | 5.25         | 1321         | 91             | •069                   | + 1561.9                               | 2735.8               |                            |       |                |              |
| ,, 15<br>,, 20,21            | 2 48<br>3 5                   | I<br>IV           | D o 30 50.0<br>E o 3 6.7           | 12<br>20      | 2.71         | 5°25<br>5°25 | 1905         | 124            | •૦ઈઽ                   | - 952.3                                | 373-8                | 375.0                      | 37.   | 4              | 3.3          |
| " 27,28<br>" 21              | 3 14                          | 111<br>1 <b>V</b> | D 1 3 31.2<br>E 0 41 16.8          | 12<br>12      | 2·71<br>2·57 | 5°25<br>5°25 | 1529         | 101            | •066                   | -2359.0                                | 376 . 1              |                            |       |                |              |
| ,, 11<br>Mar. 5              | 3 29<br>3 20                  | II<br>V           | E 0 13 14 2<br>D 0 33 11 7         | 12<br>12      | 2·57<br>2·57 | 5°25<br>5°25 | 1372         | 91             | •067                   | + 938.1                                | 3113.0               | 3113.1                     | 211   | ı              | 3.2          |
| Feb. 27,28<br>Mar. 5         | 2 45<br>2 47                  | III<br>V          | D o 24 47 · 8<br>D o 040·4         | 12<br>12      | 2.57<br>2.56 | 5.25         | 1754         | 110            | •066                   | - 622.9                                | 2112.3               |                            |       |                |              |
| Feb. 26,27<br>Mar. 12        | 2 59<br>2 59                  | III<br>VI         | D 0 46 52.7<br>E 0 28 48.8         | 12<br>12      | 2.21         | 5°25<br>5°25 | 1240         | 82             | •066                   | -1381.9                                | 1353.2               |                            |       |                |              |
| Feb. 20,21<br>Mar. 12        | 3 IO<br>3 12                  | IV<br>VI          | E o 825.7<br>D o 3222.6            | 12<br>12      | 2.71<br>2.71 | 5°25<br>5°25 | 1630         | 100            | ·061                   | + 979'2                                | 1354.3               | 1353.0                     | 135:  | 2              | 3            |
| " 8<br>" 12                  | 3 34<br>3 34                  | VII<br>VI         | E 0 2 49'2<br>D 0 22 31'6          | 12<br>12      | 2°71<br>2°58 | 5°25<br>5°25 | 1358         | 92             | •067                   | + 506.2                                | 1353.5               |                            |       |                |              |
| Feb. 27,28<br>Mar. 8         | 3032                          | III<br>VII        | D 0 54 45 0<br>E 0 33 32 2         | 16<br>16      | 2·57<br>2·55 | 5°25<br>5°25 | 1452         | 93             | •064                   | -1887.0                                | 847.5                |                            |       |                |              |
| ,, 5<br>,, 8                 | 3 2<br>3 2                    | v<br>vii          | D 0 44 22 0<br>E 0 26 39 7         | 12<br>12      | 2·58<br>2·58 | 5°25<br>5°25 | 1210         | 79             | •065                   | - 1265.9                               | 846.2                | 846.9                      | 840   | 5 3            |              |
| , 12<br>, 8                  | 3 34                          | VI<br>VII         | D o 22 31.6<br>E o 249.2           | 12<br>12      | 2.58         | 5°25         | 1358         | 92             | •067                   | - 506.7                                | 847 .0               |                            |       |                |              |
| ,, <b>12</b> ,13<br>,, 17,19 | 2 50<br>2 50                  | VI<br>VIII        | D 0 22 52'1<br>E 0 5 14'5          | 12<br>12      | 2°58<br>2°71 | 5°25<br>5°25 | 1198         | 75             | ·062                   | - 495 9                                | 857.7                | 857.2                      | 856   | 3              |              |
| " 8<br>" 17,18,19            | 3 19                          | VII<br>VIII       | Do 729.0<br>Do 86.2                | 12<br>12      | 2·58<br>2·57 | 5.25         | 1064         | 70             | •065                   | + 9.1                                  | 856.6                |                            |       |                |              |
| ,, 12,13<br>,, 25            | 2 54<br>2 55                  | VI<br>1X          | D o 25 28.5<br>E o 5 53.4          | 12<br>12      | 2.68         | 5.25         | 1327         | 80             | •060                   | - 612.8                                | 740.8                | 740'4                      | 739   | 3              |              |
| 1                            | 1                             |                   |                                    | 1             | 1            |              | l.           |                | 1                      |                                        |                      |                            |       |                | -            |

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#### PRINCIPAL TRIANGULATION. HEIGHTS ABOVE MEAN SEA LEVEL.

|      |            | Astrono                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                 | mical Date                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                |                      |                               | tions                 | Height       | in feet      |               | Terr<br>Refr | estrial<br>action    | tation                             | Height i                   | n feet of 2r  | nd Station      | Tower     |
|------|------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------|-------------------------------|-----------------------|--------------|--------------|---------------|--------------|----------------------|------------------------------------|----------------------------|---------------|-----------------|-----------|
|      |            |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | Mean<br>Tim                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | of Station           | Observed<br>Vertical Angle    | of observe            | la           | ment         | tained Arc    | onde         | als of<br>ed Arc     | eight of<br>on — 1st B(<br>in feet | Trigono                    | metrical      | Level           | Pillar or |
| 't.  |            | 1878                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | of obe<br>vatu                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | ər-<br>n             |                               | Number                | Sign         | Instru       | Cont          | In sec       | · Decime<br>Containe | H<br>2nd Stati                     | Re<br>By each<br>deduction | sults<br>Mean | Final<br>Result | Height of |
|      | I          |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | ·                    |                               |                       |              |              |               |              |                      |                                    |                            |               |                 |           |
| 74   | fe.<br>2.8 | Mar. 1'<br>"                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | h.         h. <thh.< th="">         h.         h.         h.<!--</td--><td>•.<br/>3 VIII<br/>4 IX</td><td>0 1 11 35 2<br/>D 0 3 52 8</td><td>I 2<br/>I 2</td><td>2°71<br/>2°56</td><td>5°25<br/>5°25</td><td>"<br/>1031</td><td>57</td><td>•055</td><td>- 117.1</td><td>740'1</td><td></td><td></td><td>feet</td></thh.<> | •.<br>3 VIII<br>4 IX | 0 1 11 35 2<br>D 0 3 52 8     | I 2<br>I 2            | 2°71<br>2°56 | 5°25<br>5°25 | "<br>1031     | 57           | •055                 | - 117.1                            | 740'1                      |               |                 | feet      |
|      |            | "<br>Apr.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 8 3<br>6 3 2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | 9 VII<br>c X         | D 0 11 54 2<br>D 0 5 27 8     | 12                    | 2·56<br>2·71 | 5°25<br>5°25 | 1178          | 72           | .001                 | - 111.0                            | 735`3                      |               |                 |           |
|      |            | Mar.<br>Apr.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | 18 3<br>6,7 3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | 4 VIII<br>9 X        | D o 13 22.8<br>D o 7 40.0     | 8<br>8                | 2·55<br>2·58 | 5°25<br>5°25 | 1427          | 86           | •060 <sup>.</sup>    | - 120.0                            | 737 2                      | 736.3         | 735             | 3.3       |
| 35   | 3.3        | Mar. I                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | 7,18 3<br>28 3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | 5 VIII<br>5 XI       | Do 139.5<br>Do 13 48.9        | 13                    | 2.69<br>2.59 | 5°25<br>5°25 | 1039          | 60           | •058                 | + 185.8                            | 1043.0                     |               |                 |           |
|      |            | > <b>&gt;</b><br>> <b>&gt;</b>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 25 2 g<br>28 2 g                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 7 IX<br>8 XI         | Ео 049°4<br>D01736°5          | 12<br>12              | 2.68<br>2.70 | 5°25<br>5°25 | 1114          | 58           | .023                 | + 302.3                            | 1042.7                     | 1043.6        | 1042            | 2.1       |
| 4    | 3.3        | >><br>>>                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 81 3 2<br>28 3 2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 7 XII<br>7 XI        | D o 3 30' 1<br>D o 12 5' 2    | 16<br>16              | 2.69<br>2.56 | 5°25<br>5°25 | 1050          | 62           | •059                 | + 132.0                            | 1045.0                     |               |                 |           |
|      |            | " 14<br>"                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | 7,18 3<br>31 3                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | 8 VIII<br>8 XII      | D o 7 32.3<br>D o 10 34.5     | 12<br>12              | 2·56<br>2·58 | 5°25<br>5°25 | 1231          | 77           | ·062                 | + 55.1                             | 912.3                      |               |                 |           |
| ·  . | 3.7        | Apr.<br>Mar.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | 5,6 3 1<br>31 3 1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | 3 X<br>3 XII         | D0 034'3<br>D0 13 22'0        | 12<br>12              | 2.26<br>2.26 | 5°25<br>5°25 | 935           | 56           | •059                 | +.176.3                            | 912.5                      | 911.2         | 910             | I         |
|      |            | "<br>"                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | 28 3 2<br>81 3 2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 7 XI<br>7 XII        | D 0 12 5.2<br>D 0 3 30.1      | 16<br>1б              | 2.26<br>2.69 | 5°25<br>5°25 | 1050          | 62           | •059                 | - 132.0                            | 910.3                      |               |                 |           |
| 3    |            | Dec. 1<br>" 2 <sup>5</sup> ,2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | 3,17 3 2<br>9,30 3 2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      |                      | E 0 0 20'8<br>D 0 12 55'8     | 12<br>12              | 2.29<br>2.69 | 5°25<br>5°25 | 847           | 53           | •063                 | + 165.0                            | 1209.2                     | 1208.8        | 1207            | ,         |
|      |            | " 10<br>" ⊑2:                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | ),11 3 1<br>7,30 3 1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      | 3 XII<br>5 XIII      | E o 343.0<br>D o 1736.7       | 16<br>12              | 2.28<br>2.69 | 5°25<br>5°25 | , <b>94</b> 5 | 62           | •066                 | + 296.6                            | 1208.3                     | 1200 0        |                 | 5         |
|      |            | 39<br>39                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                | 16 3 I<br>22 3 I                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | 5 XI<br>4 XIV        | Do 737'1<br>Do 219'9          | 12<br>12              | 2.28<br>2.69 | 5°25<br>5°25 | 653           | 37           | •057                 | - 50.2                             | 992.9                      | 002.2         | 000             | ot        |
| ,/   |            | ", 27,29     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27     ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 27    ", 2 | 9,30 3<br>2,23 2 4<br>4                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | 5 XIII<br>5 XIV      | D 0 15 47 2<br>E 0 5 20 2     | 12<br>12              | 2°59<br>2°57 | 5°25<br>5°25 | 696           | 42           | .000                 | - 216.9                            | 992.2                      | <b>99</b> - J | <b>,</b>        |           |
| /    |            | Dec.<br>Jan.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | 11 2 5<br>2 2 5                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | XII<br>XV            | E 0 8 31 · 2<br>D 0 20 51 · 3 | 12 <sup>°</sup><br>12 | 2.58<br>2.70 | 5°25<br>5°25 | 840           | 57           | °068                 | + 363.3                            | 1275.0                     | 1075.0        | 1272            | 2         |
|      |            | Dec. 25,27<br>Jan.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                      | 7,80 3 2<br>2,3 3 2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                       | 3 XIII<br>5 XV       | D o 3 23 · 1<br>D o 8 47 · 4  | 12<br>12              | 2.62<br>3.57 | 5°25<br>5°25 | 841           | 63           | •075                 | + 66.9                             | 1275.7                     | /3 3          | 12              | 3         |
|      |            | Dec.<br>Jan.                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                            | 29 3 1<br>13 3 1                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          | XIII<br>XVI          | D0128.0<br>E0130.1            | 12<br>12              | 2·57<br>2·57 | 5°25<br>5°25 | 715           | 47           | •066                 | - 143.5                            | 1065.3                     |               |                 |           |
|      |            | Dec.<br>Jan. 19                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                         | 20 3 2<br>3,14 3 2                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        | XIV<br>XVI           | D o o 11'9<br>D o 845'4       | 12<br>12              | 2.27<br>2.62 | 5°25<br>5°25 | 586           | 34           | •058                 | + 73.8                             | 1066.3                     | 1062.2        | 1063            | ó†        |

+ Pillar 3 feet in height is sunk having its upper surface flush with the ground.

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| Astronomical                   | Date         |               |                           | ions       | Height       | in feet      |             | Terro<br>Refri | estrial<br>ection | ttion                       | Height i             | n feet of 2n     | d Station | ower              |
|--------------------------------|--------------|---------------|---------------------------|------------|--------------|--------------|-------------|----------------|-------------------|-----------------------------|----------------------|------------------|-----------|-------------------|
|                                | Mean of      | Station       | Observed                  | observat   |              | ent          | ned Aro     | ds             | s of<br>Aro       | rht of<br>– 1st Sta<br>feet | above                | ) Mean Sea       | Level     | illar or <b>]</b> |
| 1873-74                        | of obser-    |               | Vertical Angle            | aber of    | Signal       | Istrum       | Contai      | n secun        | ccimal            | Hei<br>Stution<br>in        | Trigono<br>Res       | metrical<br>ults | Final     | it of P           |
|                                | vation       |               |                           | Nun        |              |              |             |                | Con               | 2nd 8                       | By each<br>deduction | Mean             | Result    | Heigl             |
| Jan 8910                       | h m          | TVII          |                           |            |              |              | "           |                |                   |                             |                      |                  |           | feet              |
| <b>, 13,15,16</b>              | 3 20         | XVI           | Do 5 6.8                  | 10         | 2.69         | 5.25         | 693         | 41             | •059              | - 2.3                       | 1064.9               |                  |           |                   |
| Dec. 31<br>Jan. 8,9            | 3 0<br>3 0   | XIII<br>XVII  | D 0 12 36.8<br>E 0 3 27.2 | 12<br>12   | 2°70<br>2°57 | 5°25<br>5°25 | 599         | 34             | ·057              | - 141.9                     | 1066.9               |                  |           |                   |
| ,, 3<br>,, 8,9                 | 3 18<br>3 17 | XV<br>XVII    | D 0 14 27 9<br>E 0 1 47 9 | I 2<br>I 2 | 2·70<br>2·73 | 5°25<br>5°25 | 867         | 60             | ·069              | - 207.7                     | 1067.6               | 1067.5           | 1065      | ot                |
| " <b>13</b> ,15,16<br>" 8,9,10 | 3 20<br>3 11 | XVI<br>XVII   | Do 5 6.8<br>Do 5 20.7     | 12<br>16   | 2.69<br>2.57 | 5°25         | 693         | 41             | ·059              | + 2.3                       | 1068.1               |                  |           |                   |
| " 15,16<br>" 24,28             | 3 8<br>3 2   | XVI<br>XVIII  | Do 5 4.7<br>Do 3 54.2     | 12<br>12   | 2.62<br>2.58 | 5°25<br>5°25 | 59 <b>3</b> | 36             | ·061              | - 10.3                      | 1055.2               |                  |           |                   |
| ,, 9,10<br>,, 24,29            | 3 12<br>3 31 | XVII<br>XVIII | Do 540.9<br>Do 423.3      | 12<br>12   | 2·59<br>2·71 | 5°25<br>5°25 | 666         | 39             | ·059              | - 12.0                      | 1054.9               | 1055-1           | 1052      | ot                |
| " 14,15<br>" 19,20,22          | 3 2<br>3 2   | XVI<br>XIX    | Do 651.9<br>Do 228.7      | 12<br>12   | 2·71<br>2·58 | 5°25<br>5°25 | 603         | 31             | ·051              | - 39.0                      | 1026.2               |                  |           |                   |
| ", 29,31<br>", 20,22           | 3 28<br>3 24 |               | Do 558.5<br>Do 230.3      | 8<br>12    | 2.69<br>2.62 | 5°25<br>5°25 | 561         | 37             | •066              | - 28.7                      | 1026.4               | 1020 4           | 1023      |                   |
| ,, 8,10<br>Feb. 2,5            | 2 57<br>2 55 | XVII<br>XX    | E 0 0 13.2<br>D 0 10 25.4 | 12<br>12   | 2·73<br>2·71 | 5°25<br>5°25 | 677         | 41             | ·061              | + 106.1                     | 1173.6               |                  |           |                   |
| Jan. 28<br>Feb. 2,5            | 3 23<br>3 22 | XVIII<br>XX   | E O I 6'0<br>D.O II 2'3   | I 2<br>I 2 | 2·72<br>2·67 | 5°25<br>5°25 | 660         | 40             | ·061              | + 118.0                     | 1173.1               | 1173-3           | 1170      |                   |
| Jan. 29<br>Feb. 11,12          | 3 9<br>3 8   | XVIII<br>XXI  | Do 346.8<br>Do 538.6      | 8<br>12    | 2°59<br>2°55 | 5°25<br>5°25 | 617         | 35             | •057              | + 16.0                      | 1072.0               |                  |           |                   |
| Jan. 19,22<br>Feb. 11,13       | 3 12<br>3 11 | XIX<br>XXI    | Do 2 9.6<br>Do 711.7      | 12<br>12   | 2·58<br>2·70 | 5°25<br>5°25 | 616         | 36             | ·058              | + 45.8                      | 1072.2               | 1072.2           | 1069      | 4                 |
| " 6,7<br>" 11,12               | 3 33<br>3 32 | XXII<br>XXI   | D 0 15 30'0<br>E 0 7 5'6  | 12<br>12   | 2·57<br>2·58 | 5°25<br>5°25 | 561         | 39             | •070              | - 186.4                     | 1072.4               |                  |           |                   |
| Jan. 24,28,29<br>Feb. 7        | 2 46<br>2 48 | XVIII<br>XXII | E 0 4 17.4<br>D 0 15 1.7  | 12<br>12   | 2·56<br>2·56 | 5°25<br>5°25 | 716         | 44             | ·061              | + 203.7                     | 1258.8               |                  |           |                   |
| ", 2,5<br>", 6,7               | 3 7<br>3 6   | XX<br>XXII    | Do 036.3<br>Do 922.6      | I 2<br>I 2 | 2.25<br>2.71 | 5°25<br>5°25 | 662         | 40             | •060              | + 85.6                      | 1258.9               | 1258.7           | 1255      | 3                 |
| ,, 11,12<br>,, 6,7             | 3 32<br>3 33 | XXI<br>XXII   | E 0 7 5.6<br>D 0 15 30.0  | I 2<br>I 2 | 2·58<br>2·57 | 5°25<br>5°25 | 561         | 39             | •070              | + 186.4                     | 1258.5               |                  |           |                   |
| " 13<br>" 16,17                | 3 13<br>3 14 | XXI<br>XXIII  | D 0 14 22 1<br>E 0 6 26 9 | I 2<br>I 2 | 2·78<br>2·57 | 5°25<br>5°25 | 493         | 19             | ·039              | - 151.4                     | 920.8                |                  |           |                   |
|                                |              |               |                           |            |              |              |             |                |                   | ,                           |                      |                  |           |                   |

**†** Pillar 3 feet in height is sunk having its upper surface flush with the ground.

#### PRINCIPAL TRIANGULATION. HEIGHTS ABOVE MEAN SEA LEVEL.

| Astronomical                       | Date               |                 |                              | one       | Height       | in feet      |         | Terre<br>Refra | strial<br>ction | tion                        | Height in            | n feet of 2nd    | d Station        | Cower      |
|------------------------------------|--------------------|-----------------|------------------------------|-----------|--------------|--------------|---------|----------------|-----------------|-----------------------------|----------------------|------------------|------------------|------------|
|                                    | Mean of            | Station         | Observed                     | observati |              | nt           | ned Aro | đ              | of<br>Are       | ght of<br>– 1st Sta<br>feet | above                | Mean Sea         | Level            | illar or 7 |
| 1874                               | Times<br>of obser- |                 | Vertical Angle               | ber of    | Signal       | ıstrume      | Contai  | n secon        | ecimal          | Heit<br>Station<br>in       | Trigono<br>Res       | metrical<br>ulte | Final            | it of Pi   |
|                                    | vation             |                 |                              | Nur       |              | н<br>        |         |                | e o             | 2nd                         | By each<br>deduction | Mean             | Kesult           | Heigl      |
|                                    |                    |                 | 0 <i>1</i> 11                |           |              |              | "       |                |                 |                             |                      |                  |                  | feet       |
| Feb. 9<br>" 16,17,18               | 3 30<br>3 33       | XXII<br>XXIII   | D o 20 17.5<br>E o 8 17.6    | 12<br>12  | 2°71<br>2°57 | 5°25<br>5°25 | 802     | 48             | •050            | - 337.8                     | 920.9                | 921.5            | 918              | 0          |
| " 20,23<br>" 17,19                 | 3 3<br>3 0         | XXIV<br>XXIII   | Do 412.3<br>Do 323.9         | 12<br>12  | 2.77<br>2.56 | 5°25<br>5°25 | 476     | 21             | •044            | - 5.8                       | 922.9                |                  |                  | •          |
| " 14<br>" 20, <b>2</b> 3,24        | 3 I2<br>3 9        | XXI<br>XXIV     | D o 12 44 · o<br>E o 3 5 · o | 12<br>12  | 2·58<br>2·55 | 5°25<br>5°25 | 617     | 28             | ·045            | - 143.7                     | 928.5                |                  |                  |            |
| " 6,7<br>" 21,24                   | 3 6<br>3 3         | XXII<br>XXIV    | D o 26 29.8<br>E o 18 32.7   | 12<br>12  | 2.26<br>2.25 | 5°25<br>5°25 | 497     | 21             | •042            | - 329.8                     | 928.9                | 928.0            | 9 <sup>2</sup> 4 | 3          |
| " <b>1</b> 7,19<br>" <b>2</b> 0,23 | 3 O<br>3 3         | XXIII<br>XXIV   | Do 323.9<br>Do 412.3         | 12<br>12  | 2·56<br>2·77 | 5°25<br>5°25 | 476     | 21             | •044            | + 5.8                       | 926.7                |                  | -                |            |
| ,, 17,18<br>Mar. 10,11,12          | 3 16<br>3 16       | XXIII<br>XXV    | Do14 6.0<br>Eo349.4          | 12<br>12  | 2·57<br>2·74 | 5°25<br>5°25 | 662     | 3 I            | •047            | - 174.7                     | 746.8                |                  |                  |            |
| Feb. 21,23,24<br>Mar. 11,12        | 3 28<br>3 26       | XXIV<br>XXV     | Do14 3.0<br>Eo311.9          | 12<br>12  | 2°58<br>2°58 | 5°25         | 710     | 37             | .023            | - 180.3                     | 747.7                | 747*4            | 743              | 3‡         |
| " 8<br>" 10,12                     | 37<br>310          | XXVI<br>XXV     | Do 559.3<br>Do 216.9         | 12<br>12  | 2.21<br>2.65 | 5.25<br>5.25 | 530     | 28             | •053            | - 28.8                      | 747 . 8              |                  |                  |            |
| Feb. 16,18,19<br>" 28, Mar. 3,5    | 37<br>37           | XXIII<br>XXVI   | D o 12 20.6<br>D o 1 12.9    | 12<br>12  | 2°71<br>2°74 | 5°25<br>5°25 | 882     | 40             | ••45            | - 144.0                     | 776.9                |                  |                  |            |
| " 20,,21,23<br>" 28, Mar. 5        | 3 16<br>3 13       | XXIV<br>XXVI    | D 0 13 21 ° 0<br>E 0 4 8 ° 1 | 12<br>12  | 2°71<br>2°54 | 5.25<br>5.25 | 589     | 29             | .040            | - 151.0                     | 776.4                | 776.2            | 772              | 3‡         |
| Mar. 10,12<br>" 8                  | 3 10<br>3 7        | XXV<br>XXVI     | Do 216.9<br>Do 559.3         | 12<br>12  | 2.65<br>2.57 | 5°25<br>5°25 | 530     | 28             | •053            | + 28.8                      | 776.1                |                  |                  |            |
| " 10,12<br>" <b>14,16</b> ,18,19   | зт<br>257          | XXV<br>XXVII    | D o 4 56 o<br>D o 4 38 2     | 16<br>16  | 2·73<br>2·57 | 5.25<br>5.25 | 589     | 18             | .031            | - 2.7                       | 7+4.2                | 74.06            |                  |            |
| "5,6<br>"14                        | 3 15<br>3 13       | XXVI<br>XXVII   | D o 6 56.8<br>D o 3 23.7     | 6<br>4    | 5°86<br>5'71 | 5°25<br>5°25 | 611     | - 2            | .003            | - 32.0                      | 744.5                | /++ *            | 740              |            |
| " 13,16<br>" 30, Apr. 2            | 39<br>39           | XXVII<br>XXVIII | D o 5 59 3<br>D o 4 40 9     | 12<br>12  | 2·58<br>2·58 | 5°25<br>5°25 | 632     | 5              | •008            | - 12.3                      | 732.4                | 732°4            | 728              | 3          |
| Feb. 27<br>Mar. 20,23              | 3 19<br>3 19       | XXVI<br>XXIX    | E o 1 7.7<br>D o 10 37.8     | 12<br>12  | 2°57<br>2°58 | 5°25<br>5°25 | 608     | 28             | .040            | + 105.3                     | 881.8                | 881.0            | 876              | 2+         |
| " 13,18,19<br>" 20,21,23           | 3 4<br>3 7         | XXVII<br>XXIX   | E o 3 59'1<br>D o 13 5'2     | 18<br>14  | 2·58<br>2·56 | 5°25         | 540     | 7              | .013            | + 135.7                     | 880.3                |                  | 5,5              | 3+         |
| "16,17,18<br>"28                   | 3 20<br>3 21       | XXVII<br>XXX    | Do 9 8.9<br>Do 356.0         | 16<br>12  | 2°71<br>2°58 | 5°25<br>5°25 | 759     | - 5            | •007            | - 58.4                      | 686.3                |                  |                  |            |
|                                    |                    |                 | 1                            |           | l            |              | Į       |                | 1               |                             |                      | ł                |                  |            |

1 Approximate, see Description of the Station.

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| Astronomical                           | Dațe                |                 |                           | ione     | Height       | in feet      |          | Terre<br>Refre | estrial   | ation                      | Height is            | n feet of 2n     | d Station   | OWer    |
|----------------------------------------|---------------------|-----------------|---------------------------|----------|--------------|--------------|----------|----------------|-----------|----------------------------|----------------------|------------------|-------------|---------|
|                                        | Mean of             | <b>m</b>        | Observed                  | beervat  |              | 4            | od Aro   |                | - 2       | nt of<br>- let St<br>eet   | above                | Mean Sea         | Level       | ar or T |
| 1874                                   | Times<br>of obser-  | Station         | Vertical Angle            | er of o  | Signal       | trumen       | lontaine | seond          | cimals of | Heigh<br>tation -<br>in fe | Trigono<br>Res       | metrical<br>ults | Final       | of Pill |
|                                        | vation              |                 |                           | Numb     | _            | Ē            | 0        | 4              | Cont      | 2nd S                      | By each<br>deduction | Mean             | Result      | Height  |
|                                        | 2                   |                 |                           |          |              |              | ,,       |                |           |                            |                      |                  | •           | feet    |
| Mar. 30                                | n. m.<br>246<br>246 | XXVIII<br>XXX   | Do 733.3<br>Do 242.0      | 12<br>12 | 2.28         | 5.25         | 635      | 19             | .030      | - 45'2                     | 687 • 2              | 686.6            | 682         | 3‡      |
| " 25<br>97                             | 2 52                | XXXI            | D o 10 47.5               | 12       | 2.71         | 5.25         | 622      | I              | .003      | - 100.0                    | 686.5                |                  |             |         |
| " <sup>27</sup><br>14.16.17            | 3 52                | XXVII           | Do 4 54.6                 | 12       | 2.08         | 5.25         |          |                |           |                            |                      |                  |             |         |
| " 25                                   | 3 16                | XXXI            | Do 831.8                  | 12       | 2.28         | 5.52         | 784      | - 4            | •005      | + 41.8                     | 786.4                |                  |             |         |
| " 23<br>" 25                           | 3 15<br>3 15        | XXIX<br>XXXI    | D o 10 29.2<br>D o 2 58.9 | 12<br>12 | 2.68<br>2.59 | 5°25<br>5°25 | 843      | 25             | •030      | - 93.2                     | 787.8                | 787.2            | 782         | 3‡      |
| " 27<br>" 25                           | 2 52<br>2 52        | XXX<br>XXXI     | E 0 0 11.5<br>D 0 10 47.5 | 12<br>12 | 2.68         | 5°25<br>5°25 | 622      | I              | .003      | <b>+ 100.</b> Q            | 787.3                |                  |             |         |
| Dec. 18,19<br>" 23,24                  | 2 41<br>2 40        | XXX<br>XXXII    | Do 249'4<br>Do 537'0      | 16<br>16 | 2.72         | 5.25         | 519      | 18             | .032      | + 31.3                     | 707.9                |                  |             |         |
| " 21,22<br>" 23,24                     | 3 13                | XXXI<br>XXXII   | Do 845.3                  | 16<br>16 | 2.71         | 5.25         | 599      | 31             | .023      | - 72.9                     | 714.3                | 711.1            | 706         | 3       |
| " 18,19<br>28                          | 2 46                | XXX             | Do 514.3                  | 16       | 2.72         | 5.32         | 518      | 23             | •044      | - 17.3                     | 669.3                |                  |             |         |
| " 24                                   | 2 40<br>2 48        | XXXII           | Do 540.1                  | 10       | 3.24         | 5 25<br>5 25 |          |                |           |                            |                      | 670.4            | 665         | 3       |
| " 28                                   | 2 53                | XXXIII          | Do 1 8.0                  | 12       | 3.73         | 5.32         | 480      | 19             | .030      | - 39'0                     | 071-5                |                  |             |         |
| ,, 23,24<br>1874-75<br>Dec. 31, Jan. 1 | 2 48<br>2 56        | XXXII<br>XXXIV  | Do 729.6<br>Eo 021.9      | 12<br>16 | 2°58<br>2°71 | 5°25<br>5°25 | 45 I     | 24             | •053      | - 52.3                     | 658.8                |                  |             |         |
| " 28<br>" 31, Jan. 2                   | 3 1<br>3 32         | XXXIII<br>XXXIV | Do 555.0<br>Do 435.3      | 12<br>16 | 2·58<br>2·73 | 5°25<br>5°25 | 688      | 37             | •054      | - 13.0                     | 656 <b>·8</b>        | 658.2            | 65 <b>3</b> | 3       |
| Jan. 4,5<br>Dec. 81, Jan. 1,2          | 2 52<br>2 51        | XXXV<br>XXXIV   | Do 745.7<br>Do 120.3      | 12<br>12 | 2°74<br>2°59 | 5.25<br>5.25 | 587      | 31             | •053      | - 55.6                     | 660.4                |                  |             |         |
| " 21,22<br>Jan. 4,5                    | 3 1<br>3 1          | XXXI<br>XXXV    | Do 922.0<br>Do 222.4      | 20<br>20 | 2.28         | 5.25         | 678      | - 5            | .002      | - 69.7                     | 717.2                |                  |             |         |
| Dec. 23,24<br>Jan. 4,5                 | 2 42<br>2 22        | XXXII<br>XXXV   | Do 421.0<br>Do 443.4      | T2<br>(2 | 2.60         | 5.25         | 591      | 33             | •056      | + 3.3                      | 714.4                | 715.1            | 709         | 2       |
| Dec. 81, Jan. 1,2<br>Jan. 4,5          | 2 51<br>2 52        | XXXIV<br>XXXV   | Do 120.3<br>Do 745.7      | 12<br>12 | 2.59         | 5.25         | 587      | 31             | •053      | + 55.6                     | 713.4                |                  |             |         |
| Dec. 31, Jan. 1                        | 2 57                | XXXIV           | Do 622.5                  | 12       | 2.28         | 5.25         | 200      |                |           |                            | 64010                |                  |             |         |
| Jan. 14,15<br>1875                     | 2 56                | XXXVI           | Do 434.6                  | 12       | 3.08         | 5.32         | /00      | 33             | •47       | - 10 7                     | 040 0                | 639.6            | 633         | 2       |
| Jan. 4,5<br>,, 14,16                   | 3 17<br>3 17        | XXXV<br>XXXVI   | Do 856.4<br>Do 049.9      | 12<br>12 | 2.28<br>2.71 | 5°25<br>5°25 | 636      | 34             | °54       | - 75'9                     | 639.3                |                  |             |         |
|                                        |                     |                 |                           |          |              |              |          |                |           |                            |                      |                  |             |         |

\$ Approximate, see Description of the Station.



# PRINCIPAL TRIANGULATION. HEIGHTS ABOVE MEAN SEA LEVEL.

| Astronomical               | Date               |                  |                           | tions      | Height       | in foot        | 8            | Terre<br>Refra | etrial<br>action  | ation                         | Height in            | n feet of 2n | d Station | Tower     |
|----------------------------|--------------------|------------------|---------------------------|------------|--------------|----------------|--------------|----------------|-------------------|-------------------------------|----------------------|--------------|-----------|-----------|
|                            | Mean of            | Station          | Observed                  | observa    | _            | ont            | ined An      | abi            | s of<br>I Aro     | ight of<br>1- let 8<br>1 feet | 800Y6                |              |           | Pillar or |
| 1874-75                    | Times<br>of obser- |                  | Vertical Angle            | iber of    | Bigne        | netrum         | Conta        | n secor        | ecimal<br>itained | Hei<br>Statior<br>in          | Trigono<br>Res       | ults         | Final     | ht of ]   |
|                            | vation             |                  |                           | Nun        |              | Я              |              | н              | A 00<br>0         | 2nd                           | By each<br>deduction | Mean         | Result    | Heig      |
|                            | 1 -                |                  | 014                       |            |              |                | "            |                | ,                 |                               |                      |              |           | feet      |
| Dec. 81, Jan. 1<br>Jan. 18 | 3 2                | XXXIV<br>XXXVII  | Do 6 7.3<br>Do 210.4      | I 2<br>I 2 | 2°57<br>2°70 | 5.25           | 556          | 35             | •063              | - 31.0                        | 627.7                |              |           |           |
| 1875<br>" 14<br>" 18,19    | 2 47<br>2 46       | XXXVI<br>XXXVII  | Do 5 56.1<br>Do 4 54.8    | I 2<br>I 2 | 2°57<br>2°66 | 5°25<br>5°25   | 721          | 44             | ·061              | - 10.2                        | 628.9                | 628.3        | 622       | 3         |
| » 4,5<br>» 7,8             | 2 57<br>2 57       | XXXV<br>XXXVIII  | Do 039'1<br>Do 814'4      | 16<br>16   | 2°57<br>2°71 | 5°25<br>5°25   | 578          | 32             | •055              | + 64.7                        | 779.8                | 780.0        | 774       | 9.5       |
| ,, 14,15,16<br>,, 7        | 3 16<br>3 6        | XXXVI<br>XXXVIII | E 0 1 1.6<br>D 0 12 3.3   | 16<br>12   | 2·58<br>2·58 | 5°25<br>5°25   | 7 <b>3</b> 0 | 42             | ·058              | + 140.7                       | 780.3                | 780 0        | //4       | 3 3       |
| " 14,15,16<br>" 9,11       | 3 I4<br>3 I3       | XXXVI<br>XL      | Do 236.2<br>Do 88.1       | I 2<br>I 2 | 2·58<br>2·70 | 5°25<br>5°25   | 684          | 28             | <b>.</b> 041      | + 55'9                        | 695.2                | 605.5        | 680       | 2         |
| ,, 7<br>,, 9               | 3 16<br>3 18       | XXXVIII<br>XL    | Do 926.6<br>Eo 037.4      | 12<br>12   | 3.00<br>3.28 | 5°25<br>5°25   | 570          | 29             | ·051              | - 84.6                        | 695.4                | °93 J        | ,         | 3         |
| ,, 15<br>,, 25,26          | 2 48<br>2 47       | XXXVI<br>XXXIX   | Do 756.8<br>Do 616.5      | 12<br>12   | 7°26<br>2°66 | 5°25<br>5°25   | 924          | 36             | ·039              | - 25.1                        | 614.5                |              | •         |           |
| " 18<br>" <b>2</b> 5,26    | 3 22<br>3 23       | XXXVII<br>XXXIX  | Do 755'7<br>Do 721'3      | I 2<br>I 2 | 2°59<br>2°57 | 5°25<br>5°25   | 1028         | 60             | •058              | - 8.7                         | 619.6                | 617.2        | 610       | 4         |
| " 11<br>" 25,26            | 2 57<br>2 59       | XL<br>XXXIX      | D o 10 55.7<br>D o 6 23.5 | 12<br>12   | 5°67<br>4°58 | 5°25<br>5°25   | 1147         | 54             | •047              | - 77.2                        | 618.3                |              |           |           |
| " 19<br>" 21               | 2 54<br>2 55       | XXXVII<br>XLI    | Do 10 15.0<br>Do 516.0    | 12<br>12   | 2·75<br>2·57 | 5°25<br>5°25   | 1026         | 52             | <b>.</b> 021      | - 75.4                        | 552.9                | 551.3        | 544       | 2.8       |
| " 25<br>" 21,22            | 2 57<br>2 57       | XXXIX<br>XLI     | Do 10 2.4<br>Do 543.2     | 12<br>12   | 2°72<br>2°59 | 5°25<br>5°25   | 1065         | 65             | .001              | - 67.8                        | 549°7                | <u> </u>     | J++       | 5 -       |
| " 26<br>" 80               | 2 34<br>2 33       | XXXIX<br>XLII    | Do 526.7<br>Do 826.8      | 16<br>12   | 3.63<br>5.60 | 5°25<br>5°25   | 917          | 44             | •048              | + 41.6                        | 659.1                | 660°3        | 653       | 2.1       |
| , 12<br>, 30               | 2 55<br>2 55       | XL<br>XLII       | Do 8 3.4<br>Do 5 26.2     | 12<br>12   | 2·73<br>2·57 | 5°25<br>5°25   | 881          | 42             | •048              | - 34.1                        | 661 • 4              |              |           |           |
| " 25,26<br>" 15,16         | 2 44<br>2 50       | XXXIX<br>XLIII   | D 0 10 27.4<br>D 0 3 36.6 | 12<br>12   | 2°71<br>2°50 | 5°25<br>5°25   | 944          | 56             | •059              | - 95.3                        | 522.2                |              |           |           |
| " 21,22<br>Feb. 16         | 3 30<br>4 12       | XLI<br>XLIII     | D 0 10 40.4<br>D 0 9 24.8 | 20<br>8    | 5.85<br>5.83 | 5°25<br>5°25   | 1339         | 68             | <b>.</b> 021      | - 24.9                        | 526.4                | 524.7        | 517       | 5.3       |
| ,, 7<br>,, 16              | 3 4<br>3 7         | XLIV<br>XLIII    | D 0 10 2.0<br>D 0 3 42.1  | 12<br>12   | 2°70<br>2°60 | 5°25<br>5°25 - | 915          | 52             | ·057              | - 85.4                        | 525.6                | -            |           |           |
| Jan. 25,26<br>Feb. 7       | 2 43<br>2 44       | XXXIX<br>XLIV    | Do 9 2.9<br>Do 8 29.7     | 12<br>12   | 2.29<br>2.60 | 5°25<br>5°25   | 1164         | 58             | °050              | — 8·o                         | 609.2                |              |           |           |

103

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| Astr        | onomical       | Date                  |               |                       | tions    | Height       | in feet      |         | Terre<br>Refr | estrial<br>action |          | ation            | Height in            | n feet of 2n     | d Station | lower      |
|-------------|----------------|-----------------------|---------------|-----------------------|----------|--------------|--------------|---------|---------------|-------------------|----------|------------------|----------------------|------------------|-----------|------------|
|             |                | Mean of               | Station       | Observed              | observa  |              | ent          | ned Arc | da            | of<br>Aro         | ht of    | - let St<br>feet | above                | e Mean Sea       | Level     | llar or 1  |
| 1           | 875            | Times<br>of obser-    |               | Vertical Angle        | ber of   | Bignal       | strum        | Contai  | 1 BOCOIL      | ecimals<br>tained | Heio     | tation<br>in     | Trigono<br>Res       | metrical<br>ults | Final     | t of Pi    |
|             |                | vation                |               |                       | Num      |              | I            |         | Ц             | Son D             |          | 2nd 8            | By each<br>deduction | Mean             | Result    | Heigh      |
|             |                | 1                     |               |                       |          |              |              | ,       |               |                   |          |                  |                      |                  |           | feet       |
| Jan.        | <b>3</b> 0     | <i>n. m.</i><br>3 2 I | XLII          | Do 7 52.9             | 12       | 2.29         | 5.52         | 737     | 36            | .010              | _        | 47 0             | 612.4                | 610.2            | 603       | 5.2        |
| Feb.        | 5              | 3 23                  | XLIV          | Do 317.3              | 12       | 6.20         | 5.52         |         |               |                   |          | ., ,             |                      |                  |           | <b>J</b> - |
| "           | 16<br>7        | 37                    |               | Do 342.1<br>Do 10 2.0 | J2<br>12 | 2.60         | 5.25         | 915     | 52            | ·057              | +        | 85.4             | 609.7                |                  |           |            |
|             | 16.17          | 2 5 3                 | XLIII         | Do 644.1              | 12       | 2.26         | 5.52         |         |               |                   |          |                  |                      |                  |           |            |
| , " .<br>"  | 28             | 2 52                  | XLV           | Do 744.2              | 12       | 2.71         | 5.25         | 912     | 28            | .031              | +        | 13.0             | 538.3                |                  |           |            |
| "           | 5,6            | 3 5                   | XLIV          | Do 939.4              | 12       | 2.25         | 5.32         | 810     | 40            | .047              | _        | 76.7             | 522.8                | 530.1            | 528       | 3          |
| "           | -27            | 37                    | XLV           | Do 335.2              | 12       | 2.28         | 5.32         | 039     | <b>4</b> 0    |                   |          | /0 /             | 333 0                |                  |           | ļ          |
| "           | 15,16<br>22.23 | 36                    | XLIII         | Do 819.0              | 12       | 2.26         | 5.25         | 789     | 2             | .003              | -        | 38.3             | 486.5                |                  |           | 1          |
| "           | 27.28          | 3 3                   | XI.V          |                       | 16       | 2 /2         | 5 45         |         |               |                   |          |                  |                      | 483.9            | 476       | 5.3        |
| "<br>"      | 22,23          | 3 12                  | XLVI          | Do 256.1              | 12       | 2.26         | 5 25<br>5 25 | 684     | 10            | .012              | -        | 54.9             | 481.2                |                  |           |            |
| "           | 6,7            | 3 14                  | XLIV          | Do 920.0              | 12       | 2.73         | 5.25         | ~~~     |               |                   |          |                  |                      |                  |           |            |
| Mar.        | 2              | 3 15                  | XLVII         | Do 535.0              | 12       | 2.28         | 5.52         | 978     | 47            | 1040              | -        | 54 0             | 550 5                | 558.7            | 661       |            |
| Feb.        | <b>27,</b> 28  | 2 53                  | XLV<br>XLV    | Do 4 1.8              | 12       | 2.73         | 5.25         | 677     | 30            | .044              | +        | 24.9             | 561.0                | 5507             | 55.       | 3          |
| Diar.       | 2              | 2 53                  | XLVII<br>WIW  | Do 031.4              | 12       | 2.20         | 5'25         |         | -             |                   |          |                  |                      |                  |           |            |
| reb.        | 27<br>24       | 2 48<br>2 47          | XLV<br>XLVIII | Do 647.0<br>Do 321.4  | 12       | 2°73<br>2°56 | 5.25         | 625     | 18            | .029              | -        | 31.2             | 504.4                |                  |           |            |
|             | 22,23          | 2 52                  | XLVI          | Do 242.7              | 12       | 2.72         | 5.25         |         |               |                   |          |                  |                      |                  |           |            |
| "           | 24             | 2 52                  | XLVIII        | Do 536.8              | 12       | 2.76         | 5.25         | 493     | 7             | ·014              | +        | 31.3             | 202.1                | 504.8            | 496       | °          |
| Mar.        | 21             | 2 58                  | XLIX          | Do 745.5              | 12       | 4.32         | 5.25         | 704     | - 15          | .010              | _        | 20.3             | 504.0                |                  |           |            |
| Feb.        | 24,25          | 2 58                  | XLVIII        | Do 6 5.9              | 12       | 3.00         | 5.52         |         | -,            |                   |          | 5                | J-+ y                |                  |           |            |
| . "<br>Mar. | 28<br>4        | 3 27<br>3 26          | XLIX          | Do 7 54.6             | 12       | 2.60         | 5.25         | 881     | - 7           | •008              | -        | <b>9</b> .0      | 527.1                |                  |           |            |
|             | 2              | 3 20                  | XLVII         | Do 7507               | 12       | 2.60         | 5.32         |         |               | 1                 |          |                  |                      |                  |           |            |
| >><br>>>    | <b>4</b> ,6    | 2 39<br>2 39          | XLIX          | D o 4 48.4            | 12       | 2.28         | 5.25         | 773     | 12            | .010              | -        | 35.2             | 523.2                | 525.1            | 517       | 3          |
| Feb.        | <b>2</b> 4,25  | 2 58                  | XLVIII        | Do 6 5.9              | 12       | 2.60         | 5.25         |         | - 15          |                   | L _      | 30.3             | 505.1                |                  |           |            |
| Mar.        | 21             | 2 58                  | XLIX          | Do 745.5              | 12       | 4.32         | 5.52         | 794     | -12           | 019               | <b>–</b> | <u>4</u> 03      | 525 1                |                  |           |            |
| Feb.        | 24,25          | 3 4                   | XLVIII        | Do 427'2              | 16       | 2.69         | 5.25         | 676     | 36            | ·024              | +        | 21.0             | 525.8                |                  |           |            |
| mar.        | 7,8            | 3 5                   |               |                       | 10       | 2.71         | 5 25         |         |               |                   |          |                  |                      | 526.0            | 517       | 3.3        |
| "<br>"      | 4<br>7,8       | 2 53<br>2 53          |               | Do 5 23.8             | 12       | 2.21         | 5-25         | 667     | 15            | .023              | +        | 1,0              | 520.1                |                  |           |            |
| Feb.        | 25             | 2 58                  | XLVIII        | Do 7 5.2              | 12       | 2.57         | 5.25         |         | _             |                   |          |                  |                      |                  |           |            |
| Mar.        | 12             | 2 58                  | LI            | Do 428.9              | 12       | 2.73         | 5.25         | 075     | - I           | 1001              | -        | 25.8             | 479'0                | 478.6            | 470       | 5          |
| 1           |                |                       | 1             |                       |          | l            |              |         |               |                   |          |                  |                      |                  |           | 1          |

# PRINCIPAL TRIANGULATION. HEIGHTS ABOVE MEAN SEA LEVEL.

| Astr            | onomical    | Date                                    |              |                                                   | tions           | Height       | in feet      | _             | Terre<br>Refre | estrial<br>action           | ation                                       | Height in               | n feet of 2m | d Station       | Tower            |
|-----------------|-------------|-----------------------------------------|--------------|---------------------------------------------------|-----------------|--------------|--------------|---------------|----------------|-----------------------------|---------------------------------------------|-------------------------|--------------|-----------------|------------------|
| 1               | 875         | Mean of<br>Times<br>of obser-<br>vation | Station      | Observed<br>Vertical Angle                        | mber of observa | Bignal       | Instrument   | Contained Arc | In seconds     | Decimals of<br>intained Aro | Height of<br>I Station – 1 st St<br>in feet | abovo<br>Trigono<br>Res | metrical     | Final<br>Result | ght of Pillar or |
|                 |             |                                         |              |                                                   | Nu              |              |              |               |                | ိ                           | Suc.                                        | By each<br>deduction    | Mean         |                 | Hei              |
|                 |             | h. m.                                   |              |                                                   |                 |              |              | 4             |                |                             |                                             |                         |              |                 | feet             |
| Mar.            | 9<br>12     | 3 I3<br>3 I3                            |              | Do 839.6<br>Do 434.5                              | 12<br>12        | 5.58<br>5.86 | 5.25         | 798           | 3              | .004                        | - 47.8                                      | 478.2                   |              |                 |                  |
| "               | 4           | 3 12                                    | XLIX         | Do 437.5                                          | 12              | 2.27         | 5.25         | 461           |                | .003                        | - 7.0                                       | 517.2                   |              |                 | -                |
| "               | 19          | 3 13                                    |              | Do 328.4                                          | 12              | 2.25         | 5.52         | 401           |                |                             |                                             | 5-7 -                   | 510.2        | 507             | 1.1              |
| 97<br>37        | 7,8<br>19   | 3 27<br>3 28                            |              | Do 456.3<br>Do 338.8                              | J2<br>12        | 2·75<br>2·58 | 5°25<br>5°25 | 531           | 18             | •034                        | - 10.3                                      | 515.8                   |              |                 |                  |
| "<br>"          | 9<br>15     | 2 43<br>2 44                            | L<br>LIII    | Do 758.1<br>Do 356.5                              | 12<br>12        | 2·58<br>2·58 | 5°25<br>5°25 | 717           | 10             | .014                        | - 42.5                                      | 483.2                   |              |                 |                  |
| <b>39</b><br>33 | 12,13<br>15 | 3'10<br>3 13                            | LI<br>LIII   | Do 418.6<br>Do 456.2                              | 12<br>12        | 2·58<br>3·58 | 5°25<br>5°25 | 551           | 7              | .013                        | + 5.0                                       | 484.3                   | 484.7        | 475             | 0                |
| ))<br>))        | 17<br>15    | 3 19<br>3 19                            | LIV<br>LIII  | Do 835.1<br>Do 158.9                              | 12<br>12        | 2·58<br>2·57 | 5°25<br>5°25 | 673           | 28             | .013                        | - 65.4                                      | 486.4                   |              |                 |                  |
| 17<br>12        | 8<br>· 17   | 3 16<br>3 16                            | L<br>LIV     | D o 2 43 <sup>.</sup> 2<br>D o 6 2 <sup>.</sup> 9 | J2<br>I2        | 2·56<br>2·58 | 5°25<br>5°25 | 526           | 11             | ·021                        | + 25.8                                      | 551.8                   |              |                 |                  |
| 11<br>17        | 19<br>17    | 2 44<br>2 44                            | LII<br>LIV   | D o 4 10.6<br>D o 7 31.9                          | 12<br>12        | 2·73<br>2·75 | 5°25<br>5°25 | 712           | 12             | .012                        | + 35.3                                      | 551.8                   | 551.0        | 542             | +                |
| ))<br>))        | 15<br>17    | 3 19<br>3 19                            | LIII<br>LIV  | Do 158.9<br>Do 835.1                              | 12<br>12        | 2·57<br>2·58 | 5°25<br>5°25 | 673           | 28             | •042                        | + 65.4                                      | 549.3                   |              |                 |                  |
| Dec.<br>"       | 6<br>15     | 3 23<br>3 23                            | LIII<br>LV   | Do 353.6<br>Do 45.1                               | 12<br>12        | 2°54<br>2°60 | 5°25<br>5°25 | 505           | 25             | •050                        | + 1.4                                       | 486.1                   | 487.1        | 478             | 0                |
| 33<br>32        | 18<br>15    | 2 52<br>2 50                            | LIV<br>LV    | Do 8 3.2<br>Do 014.6                              | 12<br>12        | 2.67<br>2.57 | 5°25<br>5°25 | 541           | 32             | •059                        | - 62.4                                      | 488.6                   |              |                 |                  |
| 17<br>77        | 6<br>10,11  | 3 18<br>3 19                            | LIII<br>LVI  | Do 433.2<br>Do 050.8                              | 12<br>12        | 2·70<br>2·58 | 5.25<br>5.25 | 310           | 11             | •035                        | - 17.0                                      | 467.7                   | 167.8        | 478             |                  |
| "<br>"          | 15<br>10    | 34<br>33                                | LV<br>LVI    | Do 5 3.0<br>Do 2 5.3                              | 12<br>12        | 2°70<br>2°54 | 5°25<br>5°25 | 445           | 22             | .040                        | - 19.2                                      | 467.9                   | 407 0        |                 |                  |
| ))<br>))        | 18<br>21    | 36<br>35                                | LIV<br>LVII  | Do 6 6.7<br>Do 132.4                              | 12<br>12        | 2·55<br>2·58 | 5°25<br>5°25 | 486           | 24             | ••49                        | - 32.7                                      | 518.3                   | 617.0        | 607             | 1                |
| <b>17</b><br>27 | 16<br>21    | 3 I<br>2 55                             | LV<br>LVII   | Do 049.3<br>Do 543.4                              | 12<br>[2        | 2.27         | 5°25<br>5°25 | 398           | 17             | •043                        | + 28.8                                      | 510.3                   | J*/ *        | 5~/             |                  |
| >><br>>>        | 16<br>13,14 | 3 II<br>3 II                            | LV<br>LVIII  | Do 413.3<br>Do 315.0                              | 12<br>12        | 2·70<br>2·55 | 5°25<br>5°25 | 466           | 31             | .042                        | - 6.8                                       | 480.0                   | 480.18       |                 |                  |
| 27<br>72        | 11<br>13    | 2 57<br>2 56                            | LVI<br>LVIII | D o 243'I<br>D o 440'9                            | 12<br>12        | 2.70<br>2.70 | 5.35<br>5.35 | 456           | 17             | •037                        | + 13.3                                      | 481.0                   |              | 4/1             |                  |

† For particulars, see Description of the Station.

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| Astronomical                                 | Date               |              |                       | tions    | Height        | in feet      |         | Terre<br>Refre | estrial<br>action | ation                     | Height in            | n feet of 2n     | d Station | Ower      |
|----------------------------------------------|--------------------|--------------|-----------------------|----------|---------------|--------------|---------|----------------|-------------------|---------------------------|----------------------|------------------|-----------|-----------|
|                                              | Mean of            | Station      | Observed              | observal |               | nt           | ed Aro  |                | of<br>Aro         | ht of<br>– 1st St<br>feet | above                | Mean Sea         | Level     | llar or 1 |
| 1875                                         | Times<br>of obser- | Bration      | Vertical Angle        | ber of   | Signal        | etrumeı      | Contain | brooet 1       | scimals<br>tained | Heig<br>Station -<br>in 1 | Trigono<br>Res       | metrical<br>ults | Final     | ht of Pil |
|                                              | vation             |              |                       | Num      |               | In           |         | I              | Ğ ö               | 2nd f                     | By each<br>deduction | Mean             | Result    | Heigl     |
|                                              | h. m.              |              | o , ,                 |          |               |              | *       |                |                   |                           |                      |                  |           | feet      |
| Mar. 15<br>" 24                              | 2 34<br>2 34       | LV<br>LIX    | Do 2 4.9<br>Do 3 55.9 | 12<br>12 | 2·58<br>2·67  | 5°25<br>5°25 | 345     | 9              | ·026              | + 9.4                     | 496.8                |                  |           |           |
| " 21<br>" 24,25,28                           | 2 58<br>3 3        | LVII<br>LIX  | Do 452.3<br>Do 111.5  | 16<br>20 | 2°57<br>2°60  | 5°25<br>5°25 | 357     | 13             | •036              | - 19.3                    | 497 <b>`9</b>        | 49 <b>7°4</b>    | 487       | 1.9       |
| " 13<br>" 25                                 | 3 12<br>3 12       | LVIII<br>LIX | Do 228.9<br>Do 457.8  | 12<br>12 | 2·58<br>2·70  | 5°25<br>5°25 | 452     | 15             | .033              | + 16.0                    | 497 • 4              |                  |           |           |
| Dec. 14<br>1876<br>Jan. 1                    | 2 29<br>2 30       | LVIII<br>XIX | Do 437.9<br>Do 351.9  | 12<br>12 | 13·43<br>2·70 | 5°25<br>5°25 | 520     | 15             | ·029              | - 5'9                     | 474 . 9              |                  |           |           |
| 1875<br>Dec. 25,28<br>1876<br>Jan. 1<br>1875 | 3 4<br>3 5         | LIX<br>XIX   | Do 6 9.4<br>Do 248.6  | 16<br>16 | 13·30<br>2·57 | 5°25<br>5°25 | 501     | - 8            | .019              | - 24.6                    | 472.8                | 473.8            | 401       | 10.8      |
| Dec. 22<br>,, 29                             | 2 43<br>2 50       | LVII<br>XXI  | Do 654.9<br>Do 329.3  | 12<br>12 | 22.90<br>2.60 | 5°25<br>5°25 | 598     | - 4            | .002              | - 30.5                    | <b>4</b> 87°0        | 186.6            | 478       | 20.1      |
| " 25<br>" 29                                 | 2 30<br>2 32       | LIX<br>XXI   | Do 522.7<br>Do 356.6  | 12<br>12 | 22°90<br>2°57 | 5°25<br>5°25 | 540     | - I            | ·002              | - 11.3                    | 486°I                | 400 U<br>-       | 470       | 20 4      |
|                                              |                    |              |                       |          | ]             |              | 1       |                |                   |                           |                      |                  | -         |           |

NOTE.-Stations XIX and XXI appertain to the Sutlej Series.

October 1878.

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#### J. B. N. HENNESSEY,

In charge of Computing Office.

#### PRINCIPAL TRIANGULATION. AZIMUTHAL OBSERVATIONS.

## At VIII (Thob)

Lat. N. 26° 3′ 5″ 85; Long. E. 72° 24′ 49″ 35 = 4 49 39 3; Height above Mean Sea Level, 856 feet. March 1873; observed by Lieutenant M. W. Rogers, R. E., with Barrow's 24-inch Theodolite No. 2.

Stars observed Mean Right Ascension 1873.0 Mean North Polar Distance 1873.0 Local Mean Times of Elongation, Mar. 16

| a Ursæ  | Minoris (West)                                 | and No. 1612+ (East)                           |
|---------|------------------------------------------------|------------------------------------------------|
|         | 1 <sup>h</sup> 12 <sup>m</sup> 18 <sup>s</sup> | 13 <sup>h</sup> 46 <sup>m</sup> 4 <sup>s</sup> |
|         | 1° 22′ 4″·30                                   | 6° 36′ 38″ 70                                  |
| Western | 7 <sup>h</sup> 32 <sup>m</sup>                 | Eastern 8 <sup>h</sup> 18 <sup>m</sup>         |

| ato            |            | te of<br>.k)                              | 7.                                                                                                                                                                                                                            | ACE LEFT                                                                                                                                                                                                                                                                                                                                                                         | JACE BIGHT                                             |                                                                                               |
|----------------|------------|-------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------|-----------------------------------------------------------------------------------------------|
| Astronomical D | Elongation | Zeros<br>(Circle Reading<br>Referring Maı | Observed<br>Horizontal Angle:<br>Diff. of Readings<br>Ref. Mark-Star                                                                                                                                                          | Reduction in<br>Arc to Time of<br>Elongation<br>Ref. Mark—Star<br>at Elongation                                                                                                                                                                                                                                                                                                  | Observed                                               | ed Observation<br>Mark — Star<br>Elongation                                                   |
| <b>Mar.</b> 16 | w.         | • ,<br>180 0<br>&<br>0 0                  | • ' " m *<br>+ 143 57 36 94 6 50<br>57 38 80 3 5<br>57 31 70 11 22<br>57 29 50 13 28                                                                                                                                          | $\begin{array}{c ccccc} & & & & & & & \\ & & & & & & \\ + & \circ & 2^{\circ}43 & + 143 & 57 & 39^{\circ}37 \\ & \circ & \circ^{\circ}50 & & & & \\ & & & & & & & \\ 0 & \circ & 6^{\circ}73 & & & & & & \\ & & & & & & & & \\ 0 & 0 &$                                                                                                                                          | $\begin{array}{c c c c c c c c c c c c c c c c c c c $ | • • "<br>35 <sup>-</sup> 42<br>34 <sup>-</sup> 08<br>36 <sup>-</sup> 78<br>36 <sup>-</sup> 13 |
| " <b>1</b> 7   | E.         | 180 0<br>&<br>0 0                         | $\begin{array}{c ccccc} + & 135 & 5 & 6 \cdot 38 & 11 & 51 \\ & 4 & 53 \cdot 70 & 9 & 50 \\ & 4 & 32 \cdot 04 & 1 & 40 \\ & 4 & 31 \cdot 32 & 0 & 38 \\ & 6 & 44 \cdot 52 & 23 & 13 \\ & 7 & 7 \cdot 08 & 25 & 1 \end{array}$ | $\begin{array}{c ccccc} - & 0 & 35 & 0.4 \\ & 0 & 24 & 12 \\ & 0 & 0 & 70 \\ & 0 & 0 & 70 \\ & 0 & 0 & 10 \\ & 2 & 15 & 74 \\ & 2 & 37 & 50 \\ & 2 & 37 & 50 \end{array} + \begin{array}{c} + & 135 & 4 & 31 & 34 \\ & 2 & 9 & 58 \\ & 31 & 34 \\ & 31 & 22 \\ & 31 & 22 \\ & 31 & 22 \\ & 31 & 22 \\ & 31 & 22 \\ & 31 & 34 \\ & 28 & 78 \\ & 29 & 58 \end{array}$              | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  | 5 4 26.21<br>26.62<br>25.32<br>25.13<br>23.81<br>23.87                                        |
| " 18           | <b>w</b> . | 259 13<br>&<br>79 13                      | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                                                                                                                         | $\begin{array}{c cccc} + & \circ & \circ \circ \circ \circ & \circ \\ \circ & \circ \circ \circ \circ & & & + 143 57 44^{\circ}58 \\ \circ & \circ \circ \circ \circ & & & 42^{\circ}53 \\ \circ & 11^{\circ}25 & & & 43^{\circ}37 \\ \circ & 16^{\circ}23 & & & 43^{\circ}93 \\ \circ & 35^{\circ}95 & & & 43^{\circ}93 \\ \circ & 40^{\circ}40 & & & 42^{\circ}12 \end{array}$ | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  | 3 57 32 88<br>31 99<br>33 89<br>30 86                                                         |
| " 18           | E.         | 259 13<br>&<br>79 13                      | + 135 4 37 38 4 28<br>4 31 20 1 47<br>5 16 78 13 17<br>5 33 78 15 51                                                                                                                                                          | $\begin{array}{c ccccc} - & 0 & 4 \cdot 98 \\ \hline & 0 & 0 \cdot 80 \\ 0 & 0 \cdot 44 \cdot 32 \\ 1 & 3 \cdot 17 \\ \end{array} \begin{array}{c} + & 135 & 4 & 32 \cdot 40 \\ 30 \cdot 40 \\ 32 \cdot 40 \\ 30 \cdot 61 \end{array}$                                                                                                                                           | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  | 5 <b>4 24 °71</b><br>19 °97<br>22 °84<br>20 °59                                               |

† Of Greenwich New Seven-Year Catalogue of 2760 Stars for 1864.

|                |    |            | a of<br>tk)                               |                                                                       | 74                                          | CE LEFT                                             |                                                        |                                                                            | FACE BIGHT                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                          |                                                             |
|----------------|----|------------|-------------------------------------------|-----------------------------------------------------------------------|---------------------------------------------|-----------------------------------------------------|--------------------------------------------------------|----------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------|
| Astronomical I |    | Elongation | Zeros<br>(Cirole Reading<br>Referring Max | Observed<br>Horizontal Angle :<br>Diff. of Readings<br>Ref. Mark—Star | Interval in<br>Time from<br>Elongation      | Reduction in<br>Arc to Time of<br>Elongation        | Reduced Observation<br>Ref. Mark-Star<br>at Elongation | Observed<br>Horizontal Angle :<br>Diff. of Readings<br>Ref. Mark – Star    | H H H H<br>Te L J H<br>L J | Reduced Observation<br>Ref. Mark – Star<br>at Elongation    |
| Mar.           | 19 | W.         | • ,<br>338 24<br>&<br>158 24              | • / *<br>+ 143 57 39 40<br>57 32 28<br>57 24 02<br>57 16 64           | <i>m 8</i><br>5 5<br>2 27<br>16 51<br>19 41 | , ,<br>+ 0 1.35<br>0 0.31<br>0 14.78<br>0 20.13     | • , *<br>+143 57 40°75<br>32°59<br>38°80<br>36°77      | + 143 57 31.60<br>57 34.96<br>57 35.92<br>57 34.76                         | m     s     ,     ,       13     50     +     0     9.98       12     1     0     7.53       6     3     0     1.90       9     45     0     4.95                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                   | • , "<br>+ 143 57 41 • 58<br>42 • 49<br>37 • 82<br>39 • 71  |
| 33             | 19 | <b>E.</b>  | 338 24<br>&<br>158 25                     | +135 4 31.18<br>4 27.88<br>5 48.28<br>6 7.82                          | 4 3<br>0 39<br>17 53<br>20 8                | - 0 4.09<br>0 0.11<br>1 20.35<br>1 41.95            | +135 4 27.09<br>27.77<br>27.93<br>25.87                | +135 5 27.62<br>5 7.68<br>4 47.28<br>4 57.12                               | 14       55        0       55       55         12       21       0       38       07         8       14       0       17       02         10       21       c       26       93                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | +135 4 32.07<br>29.61<br>30.26<br>30.19                     |
| 33             | 20 | w.         | 57 36<br>&<br>237 36                      | + 143 57 34 °08<br>57 34 °84<br>57 36 °52<br>57 32 °48                | 9 36<br>7 12<br>7 54<br>9 33                | + 0 4.81<br>0 2.70<br>0 3.25<br>0 4.75              | + 143 57 38·89<br>37`54<br>39`77<br>37`23              | + 143 57 22.92<br>57 27.66<br>57 40.72<br>57 39.50                         | 18       7       + 0 17.10         15       50       0 13.08         0       59       0 0.05         2       39       0 0.37                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        | + 143 57 40°02<br>40°74<br>40°77<br>39°87                   |
| <b>)</b> }     | 20 | E.         | 57 36<br>&<br>237 36                      | +135 4 32.90<br>4 30.90<br>5 24.70<br>5 48.82                         | 3 22<br>I I<br>I4 57<br>I7 49               | - 0 2.83<br>0 0.26<br>0 56.19<br>1 19.73            | +135 4 30°07<br>30°64<br>28°51<br>29°09                | +135 5 8.10<br>4 58.08<br>4 36.12<br>4 46.10                               | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | +135 4 28·58<br>29·61<br>28·40<br>29·70                     |
| "              | 21 | W.         | 136 49<br>&<br>316 49                     | + 143 57 39°26<br>57 38°14<br>57 32°16<br>57 27°46                    | 5 41<br>3 29<br>11 32<br>13 21              | + 0 1.69<br>0 0.63<br>0 6.92<br>0 9.28              | +143 57 40°95<br>38°77<br>39°08<br>36°74               | + 143 57 34 78<br>57 31 76<br>57 42 48<br>57 42 40<br>57 20 04<br>57 12 84 | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | + 143 57 43 29<br>38 26<br>42 72<br>43 28<br>43 21<br>41 38 |
| 25             | 21 | E.         | 136 48<br>&<br>316 49                     | +135 4 39'04<br>4 32'50<br>5 6'74<br>5 25'72<br>6 49'08               | 5 52<br>3 29<br>11 55<br>14 51<br>23 23     | - 0 8.61<br>0 3.02<br>0 35.63<br>0 55.42<br>2 17.69 | +135 4 30'43<br>29'48<br>31'11<br>30'30<br>31'39       | + 135 5 26.66<br>5 10.74<br>4 35.60<br>4 39.02<br>7 14.10                  | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | +135 4 33.56<br>32.26<br>32.83<br>28.77<br>30.43            |
| 23             | 22 | <b>w</b> . | 180 I<br>&<br>0 I                         | + 143 57 34 50<br>57 34 94<br>57 26 42<br>57 22 34                    | 5 0<br>3 I<br>15 I<br>17 6                  | + 0 1.30<br>0 0.47<br>0 11.73<br>0 15.22            | +143 57 35.80<br>35.41<br>38.15<br>37.56               | +.143 57 31 80<br>57 33 14<br>57 44 06<br>57 38 18<br>57 8 64              | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | + 143 57 42 15<br>41 03<br>44 82<br>40 48<br>44 34          |
| 33             | 22 | E.         | 180 I<br>&<br>0 I                         | + 135 4 31 °02<br>4 27 °34<br>5 28 °64<br>5 43 ° 90                   | 3 3 <sup>2</sup><br>1 3<br>15 37<br>17 30   | - 0 3'12<br>0 0'28<br>1 1'32<br>1 17'08             | +135 4 27.90<br>27.06<br>27.32<br>26.82                | +135 5 7.68<br>4 53.06<br>4 39.28<br>4 51.86                               | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                               | +135 4 32'54<br>28'11<br>32'52<br>29'35                     |

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#### PRINCIPAL TRIANGULATION. AZIMUTHAL OBSERVATIONS.

#### Abstract of Astronomical Azimuth observed at VIII (Thob) 1873.

| Face                                                                                                         | L                                                                                                                                   | R                                                                                          | L                                | R                                           | L                                | R                                    | L                                | R                                        | L                                         | R                                                   |
|--------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------|----------------------------------|---------------------------------------------|----------------------------------|--------------------------------------|----------------------------------|------------------------------------------|-------------------------------------------|-----------------------------------------------------|
| . Zero                                                                                                       | 180°                                                                                                                                | 0°                                                                                         | <b>2</b> 59°                     | 79°                                         | <b>8</b> 38°                     | 158°                                 | <b>5</b> 8°                      | <b>2</b> 38°                             | 137°                                      | 817°                                                |
| Date                                                                                                         | Mar                                                                                                                                 | ch 17                                                                                      | Marc                             | h 18                                        | Mar                              | ch 19                                | Marc                             | ch 20                                    | Mar                                       | ch 21                                               |
|                                                                                                              | *                                                                                                                                   | •                                                                                          | *                                | •                                           | *                                | •                                    | •                                |                                          | •                                         | •                                                   |
| Observed difference<br>of Circle-Readings,<br>Ref. M.—Star<br>reduced to Elongation                          | 31 34<br>29 58<br>31 34<br>31 22<br>28 78<br>29 58<br>*26 36<br>*25 52<br>*25 78<br>*25 28                                          | 26 21<br>26 62<br>25 32<br>25 13<br>23 81<br>23 87<br>*31 00<br>*26 57<br>*30 98<br>*27 81 | 32,40<br>30,40<br>32,40<br>30,01 | 24°71<br>19°97<br>22°84<br>20°59            | 27.09<br>27.77<br>27.93<br>25.87 | 32°07<br>29°61<br>30°26<br>30°19     | 30°07<br>30°64<br>28°51<br>29°09 | 28 · 58<br>29 · 61<br>28 · 40<br>29 · 70 | 30°43<br>29°48<br>31°11<br>30°30<br>31°39 | 33 · 56<br>32 · 26<br>32 · 83<br>28 · 77<br>30 · 43 |
| Means                                                                                                        | 28.48                                                                                                                               | 26.73                                                                                      | 31.42                            | 22.03                                       | 27.17                            | 30.23                                | 29.58                            | 29.07                                    | 30.24                                     | 31.22                                               |
| Means of both faces<br>Level Corrections<br>Corrected Means<br>Az. of Star fr. S., by W.<br>Az. of Ref. M. " | $\begin{array}{c} & & & \\ & +135 & 4 & 27 \\ & +135 & 4 & 27 \\ & +135 & 4 & 27 \\ & 187 & 21 & 57 \\ & 322 & 26 & 27 \end{array}$ | 7 • 61<br>• • 8<br>7 • 53<br>5 • 96<br>4 • 49                                              | 26<br>+ 1<br>28<br>56<br>25      | •<br>• 75<br>• 61<br>• 36<br>• 65<br>• • 65 | _28<br>_28<br>56<br>24           | *<br>*85<br>*21<br>*64<br>*35<br>*99 | _29<br>_29<br>50<br>29           | *<br>* 11<br>5* 22<br>5* 04<br>5* 26     |                                           | • 06<br>• 59<br>• 47<br>• 74<br>• 21                |

#### 1. By Eastern Elongation of No. 1612<sup>+</sup>.

#### 2. By Western Elongation of a Ursæ Minoris.

| Face<br>Zero                                                                                                 | L<br>180°                                                                                                                     | k<br>0°                                                            | L<br>259°                                                                      | R<br>79°                                      | I.<br>338°                            | R<br>158°                                 | L<br>58°                              | R<br>238°                             | L<br>137°                    | R<br>817°                                                           |
|--------------------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------|--------------------------------------------------------------------------------|-----------------------------------------------|---------------------------------------|-------------------------------------------|---------------------------------------|---------------------------------------|------------------------------|---------------------------------------------------------------------|
| Date                                                                                                         | Mar                                                                                                                           | ch 16                                                              | Mar                                                                            | ch 18                                         | Mar                                   | ch 19                                     | Mar                                   | ch 20                                 | Marc                         | eh 21                                                               |
| Observed difference<br>of Circle-Readings,<br>Ref. M.—Star<br>reduced to Elongation                          | "<br>39`37<br>39`30<br>38`43<br>38`95<br>*33`80<br>*33`41<br>*36`15<br>*35`56                                                 | " 31'73 35'42 34'08 36'78 36'13 *40'15 *39'03 *42'82 *38'48 *42'34 | "<br>44 * 58<br>42 * 53<br>43 * 37<br>43 * 93<br>43 * 93<br>43 * 93<br>42 * 12 | "<br>32 * 88<br>31 * 99<br>33 * 89<br>30 * 86 | "<br>40`75<br>32`59<br>38`80<br>36`77 | "<br>41`58<br>42`49<br>37`82<br>39`71     | "<br>38*89<br>37*54<br>39*77<br>37*23 | "<br>40`03<br>40`74<br>40`77<br>39`87 | "<br>38`77<br>39`08<br>36`74 | "<br>43 * 29<br>38 * 26<br>42 * 72<br>43 * 28<br>43 * 21<br>41 * 38 |
| Means                                                                                                        | 36.87                                                                                                                         | 37°70                                                              | 43*41                                                                          | 32.41                                         | 37 23                                 | 40.40                                     | 38.30                                 | 40.32                                 | 38.89                        | 42.03                                                               |
| Means of both faces<br>Level Corrections<br>Corrected Means<br>Az. of Star fr. S., by W.<br>Az. of Ref. M. " | $\begin{array}{r} & & & \\ & & & \\ + & 143 & 57 & 37 \\ + & 143 & 57 & 37 \\ & 178 & 28 & 40 \\ & 322 & 26 & 24 \end{array}$ | "<br>* 29<br>* 03<br>* 26<br>* 78<br>* 04                          | 37<br>+ 1<br>39<br>46<br>25                                                    | "<br>• 38<br>• 29<br>• 11<br>• 40             | 38<br>+ 1<br>40<br>45<br>25           | "<br>* 26<br>* 26<br>* 08<br>* 78<br>* 86 | 39<br>                                | "<br>"04<br>"32<br>"45<br>"77         | 40<br>+<br>40<br>45<br>25    | "<br>'46<br>'02<br>'48<br>'11<br>'59                                |

† Of Greenwich New Seven-Yeur Catalogue of 2760 Stars for 1864. NOTR.—Where observations occurred on the same pair of zeros on different nights they are reduced in this abstract to one date—the most convenient—by allowing for star's change of place. The date so adopted appears at the head of the column, and the reduced observation is preceded by an asterisk.

| At V                                                       | VIII (Th | 10b)—( <i>Con</i>      | tinued).     |         |             |        | 0           |                |
|------------------------------------------------------------|----------|------------------------|--------------|---------|-------------|--------|-------------|----------------|
| Astronomical Azimuth of Referring Mark on<br>VII (Samdari) | by H     | Eastern Elo<br>Western | ngation<br>" | •••     |             | •••    | 322 26<br>" | 25.13<br>25.13 |
| Astronomical Azimuth of VII (Samdari) by                   | observat | tion, mean             | of abov      | е       | •••         | •••    | 322 26      | 25.16          |
| Geodetical Azimuth of " by                                 | calculat | ion from th            | hat adopt    | ted (Vo | l. II, page | e 141) |             |                |
| at Kaliánpur, see page 93 ante                             | •••      | •••                    | •••          | •••     | •••         | •••    | 322 26      | 21.42          |
| Astronomical-Geodetical Azimuth at VIII                    | (Thob)   | •••                    | •••          | •••     | •••         |        | F           | 3.24           |

# At XXVI (Jambo)

Lat. N. 27° 16′ 28″ 88; Long. E. 72° 83′  $32'' \cdot 71 = 4$  50 14.2; Height above Mean Sea Level, 772 feet. February and March 1874; observed by Lieutenaut J. Hill, R. E., with Barrow's 24-inch Theodolite No. 2.

| Stars observed                          | a Ursæ Minoris (West) a                        | nd 1612† (East).                               |
|-----------------------------------------|------------------------------------------------|------------------------------------------------|
| Mean Right Ascension 1874.0             | 1 <sup>h</sup> 12 <sup>m</sup> 38 <sup>s</sup> | 13 <sup>h</sup> 46 <sup>m</sup> 2 <sup>s</sup> |
| Mean North Polar Distance 1874.0        | 1° 21′ 45 <b>″ · 24</b>                        | 6° 36′ 56″·74                                  |
| Local Mean Times of Elongation, Feb. 26 | Western 8 <sup>h</sup> 44 <sup>m</sup>         | Eastern 9 <sup>h</sup> 35 <sup>m</sup>         |

| ate            |            | e of<br>k)                                | 1                                                                                   | ACE LEFT                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     | FACE LIGHT                                                                                                                  |                                                                                                                                                                           |  |  |  |
|----------------|------------|-------------------------------------------|-------------------------------------------------------------------------------------|----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--|--|--|
| Astronomical D | Elongation | Zeros<br>(Circle Reading<br>Referring Mat | Observed<br>Horizontal Angle:<br>Diff. of Readings<br>Ref. Mark-Star                | Reduction in<br>Arc to Time of<br>Elongation<br>Ref. Mark-Star<br>at Elongation                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              | Observed<br>Horizontal Angle:<br>Diff. of Readings<br>Ref. Mark-Star                                                        | Reduction in<br>Arc to Time of<br>Elongation<br>Ref. Mark-Star<br>at Elongation                                                                                           |  |  |  |
| Feb. 26        | w.         | 。 ,<br>323 36<br>&<br>143 36              | • • • • m 8<br>- 21 45 23 90 0 22<br>45 24 54 4 I<br>46 0 08 25 24<br>46 9 88 29 29 | $\begin{array}{c cccc} & & & & & & \\ & & & & & \\ + & 0 & 0.01 \\ & 0 & 0.84 \\ & 0 & 33.71 \\ & 0 & 33.71 \\ & 26.37 \\ & 0 & 45.37 \end{array} \qquad \begin{array}{c} & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ & & & & & & \\ & & &$ | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                       | + 0 11.69<br>0 5.11<br>0 10.09<br>0 10.09<br>0 14.93<br>- 21 45 22.57<br>20.69<br>22.85<br>24.07                                                                          |  |  |  |
| "26            | E.         | 323 36<br>&<br>143 36                     | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                               | $\begin{array}{ c c c c c c c c } \hline & \bullet & 43 \cdot 44 \\ \hline & \bullet & 25 \cdot 57 \\ \hline & \bullet & 28 \cdot 54 \\ \hline & \bullet & 46 \cdot 04 \end{array} \begin{array}{ c c c c c c c } \hline & 30 & 44 & 16 \cdot 66 \\ \hline & 19 \cdot 71 \\ \hline & 19 \cdot 68 \\ \hline & 0 & 46 \cdot 04 \end{array}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | - 30 44 19 <sup>•</sup> 24 1 57<br>44 20 <sup>•</sup> 22 0 28<br>41 58 <sup>•</sup> 06 23 38<br>41 10 <sup>•</sup> 12 27 17 | $\begin{array}{c ccccc} - & 0 & 0.97 \\ \hline 0 & 0.06 \\ 2 & 22.33 \\ 3 & 9.72 \end{array} \begin{array}{c} - & 30 & 44 & 20.21 \\ 20.28 \\ 20.39 \\ 19.84 \end{array}$ |  |  |  |

† Of Greenwich New Seven-Year Catalogue of 2760 Stars for 1864.

#### PRINCIPAL TRIANGULATION. AZIMUTHAL OBSERVATIONS.

| - a                |            | ra of<br> k)                              |                                                                                                                          | 74                                      | CE LEFT                                          |                                                                                                  | 1                                                                                   | ACB BIGHT                                                                                                       |                                                                     |
|--------------------|------------|-------------------------------------------|--------------------------------------------------------------------------------------------------------------------------|-----------------------------------------|--------------------------------------------------|--------------------------------------------------------------------------------------------------|-------------------------------------------------------------------------------------|-----------------------------------------------------------------------------------------------------------------|---------------------------------------------------------------------|
| Astronomical D     | Elongation | Zeros<br>(Circle Reading<br>Referring Man | Observed<br>Horizontal Angle :<br>Diff. of Readings<br>Ref. Mark – Star                                                  | Interval in<br>Time from<br>Elongation  | Reduction in<br>Arc to Time of<br>Elongation     | Reduced Observation<br>Ref. Mark-Star<br>at Elongation                                           | Observed<br>Horizontal Angle :<br>Diff. of Readings<br>Ref. Mark-Star               | Reduction in<br>Are to Time of<br>Elongation                                                                    | Reduced Observation<br>Ref. Mark-Star<br>at Elongation              |
| Feb. 27            | w.         | • ,<br>42 48<br>&<br>222 48               | • / "<br>- 21 45 36 44<br>45 33 04<br>45 39 60<br>45 45 44                                                               | m 8<br>14 12<br>11 13<br>15 11<br>18 46 | , "<br>+ 0 10.55<br>0 6.59<br>0 12.06<br>0 18.40 | • ' "<br>21 45 25 <sup>.8</sup> 9<br>26 <sup>.45</sup><br>27 <sup>.54</sup><br>27 <sup>.04</sup> | • ' " m 8<br>- 21 46 4.68 28 15<br>45 52.24 24 28<br>45 32.32 1 26<br>45 33.20 2 15 | + 0 41 80<br>0 31 37<br>0 0 11<br>0 0 27                                                                        | • ' "<br>- 21 45 22 88<br>20 87<br>22 21<br>21 93                   |
| " 27               | E.         | 42 48<br>&<br>222 48                      | - 30 42 1 22<br>42 48 14<br>44 12 40<br>43 59 32                                                                         | 23 34<br>19 3<br>6 19<br>9 23           | - 2 19'74<br>1 31'47<br>0 10'13<br>0 22'33       | - 30 44 20.96<br>19.61<br>22.53<br>21.65                                                         | - 30 43 57 82 8 43<br>44 11 16 5. 7<br>42 27 54 21 1<br>41 38 16 24 50              | $ \begin{array}{c} - & \circ & 19.16 \\ \circ & 6.61 \\ 1 & 52.58 \\ 2 & 38.48 \end{array} $                    | - 30 44 16 98<br>17 77<br>20 12<br>16 64                            |
| <mark>,,</mark> 28 | <b>W</b> . | 122 I<br>दे<br>302 I                      | - 21 45 32 52<br>45 29 90<br>45 43 76<br>45 51 18                                                                        | 12 29<br>9 8<br>18 19<br>21 15          | + 0 8.16<br>0 4.37<br>0 17.55<br>0 23.60         | - 21 45 24°36<br>25°53<br>26°21<br>27°58                                                         | - 21 46 0.26 26 12<br>45 52.76 22 48<br>45 24.60 2 53<br>45 26.34 6 35              | + 0 35 96<br>0 27 25<br>0 0 43<br>0 2 32                                                                        | - 21 45 24 30<br>25 51<br>24 17<br>24 02                            |
| <b>,, 2</b> 8      | E.         | 122 I                                     | - 30 42 57 68<br>43 24 68                                                                                                | 17 57<br>14 53                          | - 1 21°23<br>0 55°97                             | - 30 44 18 91<br>20 65                                                                           |                                                                                     |                                                                                                                 |                                                                     |
| Mar. 3             | w.         | 201 14<br>&<br>21 14                      | - 21 45 40°94<br>45 35°78<br>45 32°76<br>45 40°10                                                                        | 17 33<br>14 31<br>14 26<br>18 3         | + 0 16°15<br>0 11°04<br>0 10°90<br>0 17°06       | - 21 45 24°79<br>24°74<br>21°86<br>• 23°04                                                       | - 21 46 14.66 31 38<br>46 3.14 27 32<br>45 24.62 2 29<br>45 22.66 1 7               | + 0 52 40<br>0 39 72<br>0 0 32<br>0 0 06                                                                        | - 21 45 22°26<br>23°42<br>24°30<br>22°60                            |
| <mark>,,</mark> 8  | E.         | 201 14<br>&<br>21 14                      | $\begin{array}{r} - 30  41  59.86 \\ 42  37.18 \\ 44  12.34 \\ 44  0.92 \end{array}$                                     | 23 31<br>20 13<br>5 28<br>8 40          | - 2 19'13<br>1 43'01<br>0 7'58<br>0 19'04        | - 30 44 18 99<br>20 19<br>19 92<br>19 96                                                         | - 30 43 56 80 9 36<br>44 7 96 6 15<br>42 41 78 19 32<br>41 57 78 23 42              | - 0 23.33<br>0 9.88<br>1 37.19<br>2 23.12                                                                       | - 30 44 20°13<br>17°84<br>18°97<br>20°90                            |
| "5                 | <b>w</b> . | 280 23<br>&<br>100 23                     | - 31 45 33 96<br>45 31 60                                                                                                | 14 56<br>11 42                          | + 011.68<br>0 7.18                               | - 21 45 22°28<br>24°42                                                                           | - 21 46 10.24 30 33<br>45 59.10 27 0<br>45 20.82 0 4                                | + 0 48.92<br>0 38.19<br>0 0.00                                                                                  | - 21 45 21 32<br>20 91<br>20 82                                     |
| "6                 | <b>w</b> . | 280 23<br>&<br>100 23                     | - 21 45 27 98<br>45 25 64<br>45 41 98                                                                                    | 9 20<br>5 43<br>19 26                   | + 0 4.56<br>0 1.72<br>0 19.75                    | - 21 45 23.42<br>23.92<br>22.23                                                                  | - 21 45 53 28<br>45 44 14<br>45 23 92<br>45 27 14<br>9 21                           | $\begin{array}{c} + & 0 & 31 \cdot 51 \\ & 0 & 21 \cdot 30 \\ & 0 & 2 \cdot 12 \\ & 0 & 4 \cdot 58 \end{array}$ | - 21 45 21.77<br>22.84<br>21.80<br>22.56                            |
| "6                 | E.         | 280 23<br>&<br>100 23                     | $\begin{array}{r} - 30 \ 42 \ 44^{\circ} 72 \\ 43 \ 6^{\circ} 00 \\ 44 \ 15^{\circ} 12 \\ 44 \ 4^{\circ} 00 \end{array}$ | 19 21<br>17 7<br>4 56<br>8 11           | - 1 34.35<br>1 13.83<br>0 6.18<br>0 16.97        | - 30 44 19 07<br>19 83<br>21 30<br>20 97                                                         | - 30 44 2.60 8 13<br>44 13.30 4 47<br>42 48.68 18 43<br>42 9.62 22 31               | - 0 17.08<br>0 5.78<br>1 29.21<br>2 9.12                                                                        | - 30 44 19 68<br>19 08<br>17 89<br>18 74                            |
| "7                 | E.         | 122 I<br>&<br>302 2                       | 30 44 5°94<br>43 34°30                                                                                                   | 5 7<br>12 28                            | - • 6·65<br>• 39·55                              | - 30 44 12 59<br>13 85                                                                           | - 30 43 20°24 15 22<br>43 41°66 12´21<br>38 1°18 38 22                              | - 0 59 59<br>0 38 48<br>6 15 89                                                                                 | - 30 44 19 <sup>.83</sup><br>20 <sup>.14</sup><br>17 <sup>.07</sup> |
| I                  | 1          |                                           |                                                                                                                          |                                         |                                                  | j                                                                                                |                                                                                     | 1                                                                                                               |                                                                     |

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## Abstract of Astronomical Azimuth observed at XXVI (Jambo) 1874.

| Face                                          | L                 | ĸ                    | L                | R                        | L               | R            | L            | R           | L           | R                |
|-----------------------------------------------|-------------------|----------------------|------------------|--------------------------|-----------------|--------------|--------------|-------------|-------------|------------------|
| Zero                                          | 824 <sup>•</sup>  | 144°                 | <b>43°</b>       | 223°                     | 122°            | 302°         | <b>2</b> 01° | <b>2</b> 1• | 280°        | 100 <sup>•</sup> |
| Date                                          | Febru             | ary 26               | Febru            | ary 27                   | Mar             | ch 7         | Mar          | rch 3       | Mar         | ch 6             |
|                                               | "                 | "                    | "                | "                        | "               | "            | "            | "           | "           |                  |
| Observed difference                           | 16.62             | 20.31                | 20.06            | 10.08                    | #17.27          | 10.83        | 18.00        | 20.13       | 10.02       | 10.08            |
| of Circle-Readings,                           | 10.21             | 20.28                | 10.01            | 17.77                    | *10.01          | 20.14        | 20.19        | 17.84       | 19.83       | 19.08            |
| Ref. MStar                                    | 19.68             | 20.39                | 22.53            | 20.13                    | 12.59           | 17.07        | 19.92        | 18.02       | 21.30       | 17.89            |
| reduced to Elongation                         | 19.40             | 19.84                | 21.62            | 16.64                    | 13.85           |              | 19.96        | 20.00       | 20.97       | 18.74            |
| Means                                         | 18.80             | 20.18                | 31.10            | 17.88                    | 15.68           | 10.01        | 19.77        | 19.46       | 20.29       | 18.85            |
|                                               | <b>)</b>          | •                    |                  | •                        |                 | •            | ·            | •           |             |                  |
| Means of both faces - 30<br>Level Corrections | 44_ <sup>19</sup> | · 5 <b>2</b><br>· 27 | _ <sup>1</sup> 5 | ) <sup>•</sup> 54<br>•39 | _ <sup>17</sup> | · 35<br>· 62 | 19<br>+      | •62<br>•40  | 19<br>1 + 1 | · 57<br>· 26     |
| Corrected Means - 30                          | 44 19             | . 79                 | 19               | .93                      | 17              | ·97          | 19           | . 22        | 18          | .31              |
| Az. of Star fr. S., by W. 187                 | 27 12             | · 29                 | 12               | • 05                     | 10              | . 10         | 11           | .13         | 10          | ·42              |
| Az. of Ref. M. " 156                          | 42 52             | . 20                 | 52.13            |                          | 52.22           |              | 51.90        |             | 52.11       |                  |

| 1. | By | Eastern | Elongation | of | No. | 1612†. |
|----|----|---------|------------|----|-----|--------|
|----|----|---------|------------|----|-----|--------|

|  | 2. | By | Western | Elongation | of | a Ursæ | Minoris. |  |
|--|----|----|---------|------------|----|--------|----------|--|
|--|----|----|---------|------------|----|--------|----------|--|

| Face                                          | $\mathbf{L}$           | R                      | $\mathbf{L}$                     | R         | $\mathbf{L}$ | R            | $\mathbf{L}$                                                | R          | L              | R                                   |
|-----------------------------------------------|------------------------|------------------------|----------------------------------|-----------|--------------|--------------|-------------------------------------------------------------|------------|----------------|-------------------------------------|
| Zero                                          | 824°                   | 1 <b>44°</b>           | 43°                              | 223°      | 122°         | <b>3</b> 02° | <b>2</b> 01°                                                | <b>21°</b> | <b>280°</b>    | 100°                                |
| Date                                          | Febru                  | ary 26                 | Febru                            | 1ary 27   | Febru        | ary 28       | Ma                                                          | rch 3      | Ma             | urch 6                              |
|                                               | -                      | -                      | •                                |           | •            | •            | •                                                           | •          | •              | *                                   |
|                                               | 23.89                  | 22.57                  | 25.89                            | 22.88     | 24.30        | 24.30        | 24.79                                                       | 22.30      | <b>*</b> 22°05 | <b>#</b> 21°09                      |
| Observed difference                           | 23.70                  | 20.69                  | 26.45                            | 20.87     | 25.53        | 25.51        | 24.74                                                       | 23.45      | *24°19         | <b>*</b> 20*68                      |
| of Circle-Readings,                           | 20.37                  | 22.85                  | 27:54                            | 22.31     | 20.21        | 24.17        | 31.90                                                       | 24.30      | 23.42          | =20.59                              |
| Ref. M - Star                                 | 24 51                  | 24 07                  | 37 04                            | 21 93     | 2/ 50        | 24 02        | 23 04                                                       | 22 00      | 23 92          | 21.77                               |
| reduced to Elongation                         |                        |                        |                                  |           |              |              |                                                             |            | 22 23          | 21.30                               |
|                                               |                        |                        |                                  |           | -            |              |                                                             |            |                | 22.55                               |
| Means                                         | 24.62                  | 22.55                  | 26.73                            | 21.97     | 25.92        | 24.20        | 23.01                                                       | 23.15      | 23.10          | 21.03                               |
|                                               | o /                    | •                      |                                  | •         |              | •            |                                                             | •          |                | •                                   |
| Means of both faces -                         | - 21 45 23             | 21 45 23.59            |                                  | • 35      | 25°21<br>    |              | <b>23</b> 38<br>+ 34<br>23 04<br>15 59<br>5 <sup>2</sup> 55 |            | 23             | • 39                                |
| Level Corrections                             |                        | • 27                   | - '59<br>24'94<br>16'71<br>51'77 |           |              |              |                                                             |            | +              | •77                                 |
| Corrected Means -                             | - 21 45 23             | .80                    |                                  |           |              |              |                                                             |            | 2              | 1.03                                |
| Az. of Star fr. S., by W.<br>Az. of Ref. M. " | 178 28 10<br>156 42 53 | '9 <del>1</del><br>'08 |                                  |           |              |              |                                                             |            | 53             | 3.18<br>1.90                        |
|                                               |                        | :                      |                                  |           |              |              |                                                             |            |                | o, , ,,                             |
|                                               |                        |                        | (by Eas                          | tern Elo  | ngation      | ••• •        | ••                                                          | •••        | 15             | 6 42 52.1                           |
| Astronomical Azimuth                          | of Referrin            | g Mark                 | { by We                          | stern     | »            | •••          | ••                                                          | •••        | •••            | » 52°30                             |
|                                               |                        |                        | l                                | Me        | an .         | •• •         | ••                                                          | •••        | •••            | " 52.2                              |
| Angle Referring Mark                          | and XXVI               | I (Sirad)              | ) see page                       | e 34      |              |              | ••                                                          | •••        | ··· —          | 3 19 9.6                            |
| Astronomical Azimuth                          | of Sirad by            | observa                | ntion                            | •••       |              | •••          | ••                                                          | •••        | 15             | 3 23 42.5                           |
| Geodetical Azimuth                            | of "by                 | 7 calcula              | tion fron                        | n that ad | lopted ()    | vol. II, j   | page 141                                                    | ) at       |                |                                     |
| Kaliánpur, se                                 | e page 94 a            | inte                   | • • •                            | •••       |              |              | ••                                                          |            | 15             | 3 23 43.2                           |
| Astronomical _ Geodet                         | ical Azimut            | h at XX                | VI (Jan                          | nho)      |              |              |                                                             |            |                | · · · · · · · · · · · · · · · · · · |
| asu ononnear — Geouer                         | ioar Azimuu            | n av AA                | LAT LOUT                         | 1001      | ••           | • •          | •••                                                         | •••        | ••• —          | 0.0                                 |

+ Of Greenwich New Seven-Year Catalogue of 2760 Stars for 1864. NOTK.—Where observations occurred on the same pair of zeros on different nights they are reduced in this abstract to one date—the most convenient—by allowing for star's change of place. The date so adopted appears at the head of the column, and the reduced observation is preceded by an asteriak.

#### At XLIII (Mugrala)

Lat. N. 28° 80' 57''.06; Long. E. 72° 24' 44".59 = 4 49 39.0; Height above Mean Sea Level, 517 feet. February 1875; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Stars observed Mean Right Ascension 1875.0 Mean North Polar Distance 1875.0 Local Mean Times of Elongation, Feb. 15

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| a Ursæ M | lind           | oris (           | West) ai       | nd No. 1612†            | (Eas            | t).    |
|----------|----------------|------------------|----------------|-------------------------|-----------------|--------|
|          | Ih             | 1 2 <sup>m</sup> | 59 <b>°</b>    | 13 <sup>h</sup>         | 46 <sup>m</sup> | 08     |
|          | 1,             | 21'              | <b>2</b> 6″·18 | 6°                      | 37              | 14".77 |
| Western  | 9 <sup>h</sup> | 28 <sup>m</sup>  |                | Eastern 10 <sup>h</sup> | 19 <sup>m</sup> |        |

|                 | 8  |            | s of<br>it)                                       |                                                                                                                                                                                                                                                                                                                       | FACE LEFT                                                                                                                      |                                                                        | PACE BIGHT                                                                               |                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                                                                                                                              |  |  |
|-----------------|----|------------|---------------------------------------------------|-----------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------|------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------------|--|--|
| Astronomics 1   |    | Klongation | Zeroe<br>Zeroe<br>(Circle Reading<br>Referring Ma | Observed .H E<br>Horizontal Angle : E<br>Diff. of Readings<br>Ref. Mark-Star                                                                                                                                                                                                                                          | Reduction in<br>Aro to Time of<br>Elongation                                                                                   | Reduced Observation<br>Ref. Mark – Star<br>at Elongation               | Observed<br>Horizontal Angle :<br>Diff. of Readings<br>Ref. Mark-Star                    | Beduction in<br>Arc to Time of<br>Elongation                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           | Reduced Observation<br>Ref. Mark-Star<br>at Elongation                                                                       |  |  |
| Feb.            | 15 | w.         | • ,<br>180 25<br>&<br>0 25                        | $\begin{array}{c cccc} \bullet & \bullet & \bullet & & m \\ \hline & \bullet & \bullet & \bullet & & \\ \bullet & \bullet & \bullet & \bullet & \\ & 45 & 58^{\circ} & 40 & & 12 \\ & 45 & 51^{\circ} & 22 & 9 \\ & 45 & 50^{\circ} & 42 & 6 \\ & 45 & 52^{\circ} & 62 & 9 \\ & 40 & 6^{\circ} & 22 & 17 \end{array}$ | *     , *       19     + 0 7'99       17     0 5'05       13     0 2'49       18     0 4'72       14     0 16'55               | • • • •<br>- 61 45 50 • 41<br>46 • 17<br>47 • 93<br>47 • 90<br>49 • 67 | • , , , , , , , , , , , , , , , , , , ,                                                  | i     i       i     +       i     +       i     +       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i     -       i <td>- 61 45 54 12<br/>53 25<br/>50 22<br/>49 57<br/>52 74</td> | - 61 45 54 12<br>53 25<br>50 22<br>49 57<br>52 74                                                                            |  |  |
| <b>))</b>       | 15 | E.         | 180 25<br>&<br>0 25                               | - 70 50 55 68 2<br>50 54 50 0<br>50 14 42 12<br>50 3 64 13<br>49 18 78 19                                                                                                                                                                                                                                             | 7     -     0     1.34       8     0     0.00       0     38.08       0     50.11       7     1     37.65                      | - 70 50 57 02<br>54 50<br>52 50<br>53 75<br>56 43                      | - 70 48 52 54 22 2<br>49 16 24 20<br>50 53 66 5<br>50 47 54 7<br>48 33 80 23 5           | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | - 70 50 61 45<br>58 80<br>60 38<br>60 20<br>61 47                                                                            |  |  |
| >>              | 16 | <b>W</b> . | 259 37<br>&<br>79 37                              | - 61 45 51 22 4<br>45 48 68 1<br>45 53 92 11<br>45 56 70 13<br>46 11 58 20                                                                                                                                                                                                                                            | 6 + 0 0.89<br>2 0 0.18<br>5 0 6.86<br>2 0 9.64<br>7 0 21.29                                                                    | - 61 45 50 33<br>48 50<br>47 06<br>47 06<br>50 29                      | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                    | +     •     8.95       •     •     •       •     •     1.08       •     •     2.10       •     •     31.67                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | $\begin{array}{r} - & 61 & 45 & 51 \cdot 37 \\ & 56 \cdot 35 \\ & 56 \cdot 08 \\ & 56 \cdot 00 \\ & 55 \cdot 03 \end{array}$ |  |  |
| 33              | 16 | E.         | 259 37<br>&<br>79 37                              | - 70 50 53 50 4<br>50 53 06 2<br>50 11 38 12<br>49 57 66 14<br>48 55 28 21                                                                                                                                                                                                                                            | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                          | - 70 50 59 53<br>54 72<br>54 47<br>54 53<br>54 42                      | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                    | $\begin{array}{c} -1 & 11 & 18 \\ 0 & 42 & 90 \\ 0 & 31 & 14 \\ 0 & 3 & 61 \\ 0 & 9 & 90 \end{array}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                  | - 70 50 67 · 16<br>64 · 06<br>63 · 38<br>63 · 23<br>63 · 14                                                                  |  |  |
| "               | 18 | <b>W</b> . | 338 49<br>&<br>158 49                             | 61 46 0.02 3 :<br>45 53.14 0<br>46 0.70 14<br>46 5.78 17<br>46 20.26 22                                                                                                                                                                                                                                               | 0     + 0     0.59       2     0     0.00       2     0     11.65       3     0     15.30       1     0     27.05              | - 61 45 59'43<br>53'14<br>49'05<br>50'48<br>53'21                      | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                    | $\begin{array}{c} + \ 0 \ 12 \cdot 20 \\ 0 \ 6 \cdot 82 \\ 0 \ 5 \cdot 13 \\ 0 \ 1 \cdot 81 \\ 0 \ 3 \cdot 01 \end{array}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                             | - 61 45 55 60<br>53 84<br>51 71<br>58 29<br>56 45                                                                            |  |  |
| <b>39</b>       | 18 | E.         | 338 49<br>&<br>158 49                             | - 70 50 49 12 5<br>50 52 40 3<br>50 36 88 9<br>50 28 38 10<br>49 37 50 16                                                                                                                                                                                                                                             | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                                                          | - 70 50 57 47<br>56 28<br>58 15<br>58 19<br>51 50                      | - 70 49 50'32 16 54<br>50 20'86 12 32<br>50 27'22 10 47<br>51 1'90 1 41<br>50 57'84 3 39 | - 1 12.94<br>0 40.22<br>0 29.77<br>0 0.73<br>0 3.42                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | - 70 50 63 · 26<br>61 · 08<br>56 · 99<br>62 · 63<br>61 · 26                                                                  |  |  |
| <b>&gt;&gt;</b> | 19 | ₩.         | 22 I<br>&<br>202 I                                | - 61 45 50 86 5<br>45 46 34 3<br>45 51 20 9<br>45 52 60 11<br>46 4 30 17                                                                                                                                                                                                                                              | $\begin{array}{c ccccc} 7 & + & 0 & 1.67 \\ 3 & & 0 & 0.73 \\ 6 & & 0 & 5.02 \\ 0 & & 0 & 7.38 \\ 6 & & 0 & 16.92 \end{array}$ | - 61 45 49'19<br>45'61<br>46'18<br>45'22<br>47'38                      | - 61 46 6 28<br>46 1 02<br>45 56 00<br>45 48 88<br>45 49 76<br>3 29                      | $\begin{array}{c} + & 0 & 16 \cdot 33 \\ & 0 & 10 \cdot 00 \\ & 0 & 6 \cdot 52 \\ & 0 & 0 \cdot 14 \\ & 0 & 0 \cdot 64 \end{array}$                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | - 61 45 49°95<br>51°02<br>49°48<br>48°74<br>49°12                                                                            |  |  |

† Of Greenwich New Seven-Year Catalogue of 2760 Stars for 1864.

|               | ana.        |            | rk)                                      | ]                                                                                          | FACE LEFT                                                                                                                                                                                                                      | FACE BIGHT                                             |  |  |  |  |  |
|---------------|-------------|------------|------------------------------------------|--------------------------------------------------------------------------------------------|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|--------------------------------------------------------|--|--|--|--|--|
| T lesimonte A | ABUTUUUUUUU | Elongation | Zeros<br>(Circle Reading<br>Beferring Ma | Observed<br>Horizontal Angle :<br>Diff. of Readings<br>Ref. Mark-Star                      | Reduction in<br>Aro to Time of<br>Elongation<br>Reduced Observation<br>Bef. Mark-Star<br>at Elongation                                                                                                                         | Observed                                               |  |  |  |  |  |
| Feb.          | . 19        | E.         | o /<br>22 I<br>&<br>202 I                | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$                                      | - 1 21 27<br>- 70 50 59 69<br>0 0.75<br>0 3.18<br>1 22.43<br>1 40.28<br>- 70 50 59.69<br>- 60.65<br>- 58.90<br>- 59.69<br>- 58.42                                                                                              | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  |  |  |  |  |  |
| "             | 20          | <b>w</b> . | 101 13<br>&<br>281 13                    | - 61 45 45.62 0 47<br>45 57.86 10 38<br>45 56.02 13 26<br>46 35.38 29 21<br>46 50.04 34 12 | $\begin{array}{c ccccc} + & 0 & 0 & 0 & 3 \\ 0 & 5 & 96 \\ 0 & 9 & 52 \\ 0 & 45 & 30 \\ 1 & 1 & 44 \end{array} \begin{array}{c} - & 61 & 45 & 45 & 59 \\ 51 & 90 \\ 46 & 50 \\ 50 & 08 \\ 48 & 60 \end{array}$                 | $\begin{array}{c c c c c c c c c c c c c c c c c c c $ |  |  |  |  |  |
| "             | 20          | E.         | 101 13<br>ds<br>281 13                   | - 70 49 19 42 19 19<br>50 57 30 0 27<br>50 53 92 2 58<br>48 38 96 23 1                     | $\begin{array}{c cccc} - & 1 & 35 \cdot 28 \\ & 0 & 0 \cdot 05 \\ & 0 & 2 \cdot 27 \\ & 2 & 16 \cdot 69 \end{array} \begin{array}{c} - & 70 & 50 & 54 \cdot 70 \\ & 57 \cdot 35 \\ & 56 \cdot 19 \\ & 55 \cdot 65 \end{array}$ | $\begin{array}{c ccccccccccccccccccccccccccccccccccc$  |  |  |  |  |  |

Abstract of Astronomical Azimuth observed at XLIII (Mugrala), 1875.

1. By Eastern Elongation of No. 1612†.

|                                                                                                                                | _                                                                           |                                                     |                                           |                                           |                                           |                                           |                                                   |                                           |                                      |                                                     |
|--------------------------------------------------------------------------------------------------------------------------------|-----------------------------------------------------------------------------|-----------------------------------------------------|-------------------------------------------|-------------------------------------------|-------------------------------------------|-------------------------------------------|---------------------------------------------------|-------------------------------------------|--------------------------------------|-----------------------------------------------------|
| Face                                                                                                                           | L                                                                           | R                                                   | L                                         | R                                         | L                                         | R,                                        | L                                                 | R                                         | L                                    | R                                                   |
| Zero                                                                                                                           | 18 <b>0°</b>                                                                | 0°                                                  | <b>260°</b>                               | 80°                                       | <b>8</b> 39°                              | 15 <b>9°</b>                              | <b>22°</b>                                        | 202°                                      | 101°                                 | <b>2</b> 81°                                        |
| Date February 15                                                                                                               |                                                                             | ary 15                                              | February 16                               |                                           | February 18                               |                                           | February 19                                       |                                           | February 20                          |                                                     |
|                                                                                                                                |                                                                             |                                                     |                                           |                                           |                                           |                                           |                                                   |                                           |                                      | "                                                   |
| Observed difference<br>of Circle-Readings,<br>Ref. MStar<br>reduced to Elongation                                              | 57°02<br>54°50<br>52°50<br>53°75<br>56°43                                   | 61 ° 45<br>58 ° 80<br>60 ° 38<br>60 ° 20<br>61 ° 47 | 59°53<br>54°72<br>54°47<br>54°53<br>54°42 | 67°16<br>64°06<br>63°38<br>63°23<br>63°14 | 57°47<br>56°28<br>58°15<br>58°19<br>51°50 | 63°26<br>61°08<br>56°99<br>62°63<br>61°26 | 59°69<br>60°65<br>58°90<br>59°69<br>58° <b>42</b> | 60.72<br>61.69<br>63.11<br>58.21<br>60.08 | 54°70<br>57°35<br>56°19<br>55°65     | 61 · 52<br>61 · 42<br>59 · 05<br>60 · 82<br>59 · 96 |
| Means                                                                                                                          | 54.84                                                                       | 60°46                                               | 55*53                                     | 64.19                                     | 56.32                                     | 61.04                                     | 59°47                                             | 60.76                                     | 55*97                                | 60.22                                               |
| Means of both faces - 70<br>Level Correctiona<br>Corrected Means - 70<br>Az. of Star fr. S., by W. 187<br>Az. of Ref. M. , 116 | $50 50 57^{\circ}$<br>$50 59^{\circ}$<br>$32 48^{\circ}$<br>$41 49^{\circ}$ | 65<br>05<br>70<br>85<br>15                          | 59<br>60<br>48<br>48                      | 86<br>21<br>07<br>69<br>62                | 58<br>59<br>59<br>48<br>49                | 68<br>70<br>38<br>38<br>38                | 60<br>60<br>48<br>47                              | 12<br>18<br>30<br>22<br>92                | 58 -<br>58 -<br>58 -<br>48 -<br>49 - | 26<br>03<br>29<br>06<br>77                          |

† Of Greenwich New Seven-Year Catalogue of 2760 Stars for 1864.

#### PRINCIPAL TRIANGULATION. AZIMUTHAL OBSERVATIONS.

# Abstract of Astronomical Azimuth observed at XLIII (Mugrala) 1875-(Continued).

| Face                                                                                                         | Ĺ                                                                                                                      | R                                         | L                                         | R                                                   | L                                         | R                                         | Ĺ                                         | R                                         | L                                         | R                                         |
|--------------------------------------------------------------------------------------------------------------|------------------------------------------------------------------------------------------------------------------------|-------------------------------------------|-------------------------------------------|-----------------------------------------------------|-------------------------------------------|-------------------------------------------|-------------------------------------------|-------------------------------------------|-------------------------------------------|-------------------------------------------|
| Zero                                                                                                         | 180°                                                                                                                   | 0°                                        | 260°                                      | 80°                                                 | 839°                                      | 159°                                      | <b>2</b> 2°                               | 202°                                      | 101°                                      | 281°                                      |
| Date February 15                                                                                             |                                                                                                                        |                                           | Febru                                     | ary 16                                              | February 18                               |                                           | Febru                                     | ary 19                                    | February 20                               |                                           |
|                                                                                                              | n                                                                                                                      | "                                         | . <b>n</b>                                | "                                                   | "                                         | "                                         | n                                         | "                                         | "                                         | "                                         |
| Observed difference<br>of Circle-Readings,<br>Ref. MStar<br>reduced to Elongation                            | 50°41<br>46°17<br>47°93<br>47°90<br>49°67                                                                              | 54°12<br>53°25<br>50°22<br>49°57<br>52°74 | 50°33<br>48°50<br>47°06<br>47°06<br>50°29 | 51 · 37<br>56 · 35<br>56 · 08<br>56 · 00<br>55 · 03 | 59°43<br>53°14<br>49°05<br>50°48<br>53°21 | 55°60<br>53°84<br>51°71<br>58°29<br>56°45 | 49°19<br>45°61<br>46°18<br>45°22<br>47°38 | 49`95<br>51`02<br>49`48<br>48`74<br>49`12 | 45`59<br>51`90<br>46`50<br>50`08<br>48`60 | 49°19<br>53°94<br>54°32<br>54°24<br>53°65 |
| Means                                                                                                        | 48 • 42                                                                                                                | 51.98                                     | 48.65                                     | 54.97                                               | 53.00                                     | 55.18                                     | 46.72                                     | 49.66                                     | 48.53                                     | 53.02                                     |
| Means of both faces<br>Level Corrections<br>Corrected Means<br>Az. of Star fr. S., by W.<br>Az. of Ref. M. " | $\begin{array}{c} \circ & i \\ - & 6i \\ - & 5i \\ - & 1i \\ - & 6i \\ 178 \\ 27 \\ 176 \\ 16 \\ 4i \\ 49 \end{array}$ | "<br>*20<br>*21<br>*41<br>*43<br>*02      | + 51<br>51<br>40<br>48                    | 81<br>34<br>47<br>20<br>73                          | 54<br>+ 1<br>53<br>39<br>46               | 7<br>12<br>00<br>97<br>97                 | 48<br>,                                   | "<br>36<br>55<br>74<br>19                 | 50<br>50<br>39<br>48                      | "<br>80<br>03<br>83<br>51<br>68           |

2. By Western Elongation of a Ursæ Minoris.

|                                           |               |                                       |         |        |         |     | 0 /     | "     |
|-------------------------------------------|---------------|---------------------------------------|---------|--------|---------|-----|---------|-------|
| •                                         | (by Eastern   | Elongation                            | •••     | •••    | •••     | ••• | 116 41  | 48.89 |
| Astronomical Azimuth of Referring Mark    | } by Western  | 1 ,,                                  | •••     | •••    | •••     | ••• |         | 48.72 |
|                                           | (             | Mean                                  | •••     | •••    | •••     | ••• | 33      | 48.81 |
| Angle Referring Mark and XLVI (Habib)     | see page 47   | •••                                   | •••     | •••    | •••     | ••• | + 55 11 | 42.04 |
| Astronomical Azimuth of Habib by observat | io <b>n</b>   | • •••                                 | •••     | •••    | •••     | ••• | 171 53  | 30.85 |
| Geodetical Azimuth of " by calculati      | ion from that | adopted ( $\mathcal{V}_{\mathcal{C}}$ | ol. II, | page 1 | .41) at |     |         |       |
| Kaliánpur, see page 95 ante               | ••• ••        | ••••                                  | •••     | •••    | •••     | ••• | 171 53  | 32.98 |
| Astronomical-Geodetical Azimuth at XLII   | I (Mugrala)   | •••                                   | •••     | ***    | •••     | ••• | -       | 2.13  |
| •                                         |               |                                       |         |        |         |     |         |       |

October 1878.

J. B. N. HENNESSEY, In charge of Computing Office.



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PRINCIPAL TRIANGULATION. ALPHABETICAL LIST OF STATIONS.

| Arrabhit        | •       | •       | • | • | • | • | XXII.      | Máchka LIX.                                                |
|-----------------|---------|---------|---|---|---|---|------------|------------------------------------------------------------|
| Asu             | •       | •       | • | • |   | • | XXXI.      | (Of the Great Indus Series).                               |
| Badhor          | •       | •       | • | • | • | • | xv.        |                                                            |
| Bándri          | •       | •       | • | • | • | • | XXV.       | Malar XIV.                                                 |
| Bhádi           |         | •       |   |   |   |   | <b>v</b> . | Mangtor IX.                                                |
| Bhitala         |         |         |   |   |   |   | x.         | Mári XLI.                                                  |
| Bitri           | •       | •       | • | • | · |   | XXXII      | Máringra XXIX.                                             |
| Chánga          | •       | •       | • | • | • | • | TT         | Morgich XXXVII.                                            |
| Chauki          | •       | •       | • | • | • | • | XXXV       | Narhar XI.                                                 |
|                 | •       | •       | • | • | • | • | TVIT       | Narithal IV.                                               |
| (Of the Great ] | Indus S | erice). | • | • | • | • | LAII.      | Núrpír XLIII.                                              |
| Dewari          |         | •       | • | • | • | • | XLVIII.    | Parethal XXXIII.                                           |
| Dhanono         | •       | •       | • | • | • | • | XXIV.      | Patatonk III.                                              |
| Fulrár          | •       | •       | • | • | • | • | <b>I</b> . | Potanawári XVIII.                                          |
| Ghundi          | •       | •       | • | • | • | • | LI.        | Ramsar XVI.                                                |
| Girája          | •       | •       | • | • | • | • | XXVIII.    | Ráviláhu XXVI.                                             |
| Got Mír Mu      | iham    | mad     | • | • | • | • | XLVII.     | Rojhra LXXV.                                               |
| Harnáo          | •       | •       | • | • |   | • | XXIII.     | (Of the Karáchi Longitudinal Series).                      |
| Hatodan         | •       | •       | • | • | • | • | VI.        |                                                            |
| Jevsulmere      |         |         |   |   |   | • | XIII.      | Sanahu XXI.                                                |
| Joganali        | •       | •       | • | • | • | • | XIX.       | Sandohar LXXVIII.<br>(Of the Karáchi Longitudinal Series.) |
| Kanakotri       | •       | •       | • | • | • | • | VIII.      | Sinaba XVII.                                               |
| Kardo           | •       | •       | • |   | • | • | XX.        | Singra                                                     |
| Kháro           |         | •       |   | • | • | • | XXXVI.     | Thakur XII.                                                |
| Kiraríwáro      | •       | •       | • |   | • | • | XL.        | Thar Muhári XXXIX.                                         |
| Kolu            |         |         | • | • | • | • | XXXIV.     | Trisingh XXXVIII.                                          |
| Kot Sabzal      |         | •       | • | • | • | • | XLIX.      | Vijnot                                                     |
| Kubba           | •       |         | • |   | • | • | L.         | Vín XLVI.                                                  |
| Longwáli        | •       | •       | • | • | • | • | XLV.       | Yáru XLII.                                                 |

# PRINCIPAL TRIANGULATION. NUMERICAL LIST OF STATIONS.

| LXXV       | • | •  | • ( | Of the T | Taníski <sup>s</sup> | Rojhra.               |         | •   | • | • | • | •            | Máhu.                                |
|------------|---|----|-----|----------|----------------------|-----------------------|---------|-----|---|---|---|--------------|--------------------------------------|
| LYXVIII    |   | ·. | e   |          | Laraciii .           | Sandohar              | XXVIII  | •   | • | • | • | •            | Girája.                              |
|            | • | •  | •   | Of the R | aráchi ]             | Longitudinal Series). | XXIX    | •   | • | • | • | •            | Máringra.                            |
| I          | • | •  | •   | ٠        | •                    | Fulrár.               | XXX     | •   | • | • | • | •            | Singra.                              |
| 11         | • | •  | •   | •        | •                    | Chánga.               | XXXI    | •   | • | • | • | •            | Asu.                                 |
| 111        | • | •  | •   | •        | •                    | Patatonk.             | XXXII   | •   | • | • | • | •            | Bitri.                               |
| 1 <b>V</b> | • | •  | •   | •        | •                    | Narithal.             | XXXIII  | •   | • | • | • | •            | Parethal.                            |
| V          | • | •  | •   | •        | •                    | Bhádi.                | XXXIV   | •   | • | • | • | •            | Kolu.                                |
| VI         | • | •  | •   | •        | •                    | Hatodan.              | xxxv    | •   | • | • | • | •            | Chauki.                              |
| VII        | • | •  | •   | •        | •                    | Rupihar.              | XXXVI   | •   | • | • | • | •            | Kháro.                               |
| VIII       | • | •  | •   | •        | •                    | Kanakotri.            | XXXVII  | •   | • | • | • | •            | Morgich.                             |
| IX         | • | •  | •   | •        | •                    | Mangtor.              | XXXVIII | •   | • | • | • | •            | Trisingh.                            |
| X          | • | •  | •   | •        | •                    | Bhitala.              | XXXIX   | •   | • | • | • | •            | Thar Muhári.                         |
| XI         | • | •  | •   | •        | •                    | Narhar.               | XL      | •   | • | • | • | •            | Kiraríwáro.                          |
| XII        | • | •  | •   | •        | •                    | Thakur.               | XLI     | Ň   | • | • | • | •            | Mári.                                |
| XIII       | • | •  | •   | •        | •                    | Jeysulmere.           | XLII    | . • | • | • | • | •            | Yáru.                                |
| XIV        | • | •  | •   | •        | •                    | Malar.                | XLIII   | •   | • | • | • | •            | Núrpír.                              |
| XV         | • | •  | •   | •        | •                    | Badhor.               | XLIV    | •   | • | • | • | •            | Vijnot.                              |
| XVI        | • | •  | •   | •        | •                    | Ramsar.               | XLV     | •   | • | • |   | •            | Longwáli.                            |
| XVII       | • | •  | •   | •        | •                    | Sinaba.               | XLVI    | •   | • | • | • | •            | Vín.                                 |
| XVIII      | • | •  | •   | •        | •                    | Potanawári.           | XLVII   | •   | • | é |   | Got <b>L</b> | lír Muhammad.                        |
| XIX        | • | •  | •   | •        | •                    | Joganali.             | XLVIII  | •   | • | • | • | •            | Dewari.                              |
| XX         | • | •  | •   | •        | •                    | Kardo.                | XLIX    | •   | • | • |   | •            | Kot Sabzal.                          |
| XXI        | • | •  | •   | •        | •                    | Sanahu.               | L       |     | • | • |   | •            | Kubba.                               |
| XXII       | • | •  | •   | •        | •                    | Arrabhit.             | LI      | •   | • | • |   | •            | Ghundi.                              |
| XXIII      | • | •  | •   | •        | •                    | Harnáo,               | LIX     |     |   | • | • |              | Máchka.                              |
| XXIV       | • | •  | •   | •        | •                    | Dhanono.              |         | •   | · | · |   | (Of t        | he Great Indus Series).              |
| XXV        |   | •  | •   | •        | •                    | Bándri.               |         | •   | • | • | • | (Of 1        | Dáowála.<br>the Great Indus Series). |
| XXVI       | • | •  |     | •        | •                    | Ráviláhu.             |         |     |   |   |   | •            | · · · · · ·                          |

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#### DESCRIPTION OF PRINCIPAL STATIONS.

Of the 51 Principal Stations composing this Series, those numbered I to XLIII and XLVII are situated on sand hills. Each consists of a solid, circular, isolated pillar of masonry surrounded by an annular wall, the pillar being sunk to a depth of 3 feet, and having its upper surface flush with the hill top. In the centre and upper surface of the pillar a mark (circle and dot) engraved either on stone or brick, was imbedded in the normal of one or two other similar marks previously inserted within the pillar. Stations LXXV and LXXVIII of the Karáchi Longitudinal Series are similar in construction to those above described, with the exception that the pillars are not sunk but rise above the hill tops and are surrounded by platforms about 14 feet square for the observatory tent to stand on. The remainder with stations LIX and LXII of the Great Indus Series, on which this Series closes, are tower stations. Each consists of either a solid or perforated central pillar surrounded by solid towers of sun-dried bricks set in mud cement for the accommodation of the observatory tent: the pillars themselves are composed of rectangular blocks of masonry surmounting one another, each succeeding block being contracted, so as to leave a plinth at its base, the uppermost block, for the theodolite to stand on, is circular,  $3\frac{1}{3}$  feet in diameter, and isolated from the tower. The solid pillars have marks, as already described, at top and bottom and others intermediately, the perforated pillars have a mark imbedded at about the level of the floor and another below in the foundation. In the case of perforated pillars access to the upper mark is obtained by a vaulted passage, especially constructed for the purpose, through the tower and the central pillar. The upper mark-stones, where the pillars are solid, are protected by a rectangular pyramidal pillar of masonry erected after the completion of the observations, and bearing a sufficiently accurate mark for Topographical and Revenue Survey purposes—as shown at page 74 of Volume II of the Account of the Operations &c.

The following descriptions have been compiled from those given by the officers who executed the Series. The orthography of such names of parganas, districts &c., as has been fixed by Government for Rajputana and Sind has been adhered to. A few details, such as the name of a village or pargana within which a station is situated, have been obtained from the returns furnished by the political authorities to whose charge the stations have been committed.

LXXV.—(Of the Karáchi Longitudinal Series). Rojhra Hill Station, lat. 24° 57′, long. 70° 17′ observed at in 1851 and 1876—is situated on a high, narrow hill  $1\frac{1}{4}$  miles west of the road from Cháchra to Islámkot. The hill lies in that part of the Thar or little desert which appertains to Bhuj. It is in the lands of Rohrara village, taluka Cháchra, district Thar and Párkar.

The masonry pillar, which is surrounded by an annular wall, is solid and 3 feet high. It contains three mark-stones, one at the foundation, another 2 feet above it, and the third at the surface of the pillar. When visited in 1876 for originating the Eastern Sind Meridional Series, the pillar was found in good order and the upper mark-stone intact, and no alteration in the construction of the station was made. The azimuths and distances of the circumjacent villages are :—Pariara 143°, miles 3.4; and Dhakla 297°, miles 2.



LXXVIII.—(Of the Karáchi Longitudinal Series). Sandohar Hill Station, lat. 25° 3′, long. 70° 1′ observed at in 1851 and 1876—is situated on a narrow and extensive hill in that portion of the Thar or little desert appertaining to Bhuj, about 2 miles N. of the road from Cháchra to Chelár. It is in the lands of Akli village, taluka Cháchra, district Thar and Párkar.

The masonry pillar, which is surrounded by an annular wall, is solid and 3 feet high. It contains three mark-stones, one at the foundation, another 2 feet above, and the third at the upper surface of the pillar. When visited in 1876 for originating the Eastern Sind Meridional Series, the pillar was found in good preservation, but there was no upper mark : on cutting into the pillar the second mark on stone was found intact one foot below the surface. The pillar was then re-built to its original height and a new mark was placed in its upper surface one foot above and in the normal of the mark found. The azimuths and distances of the circumjacent villages are :—Sandohar 88°, mile 0.5; and Arnára 198°, mile 1.

I. Fulrár Hill Station, lat. 24° 53′, long. 70° 6′—observed at in 1876—is on a high and narrow sand hill in that portion of the Thar or little desert appertaining to Bhuj. It is in the lands of Fulrár village, taluka Cháchra, district Thar and Párkar.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains two mark-stones, one at the bottom and the other 3 feet above it at the surface of the pillar. This station is nearly identical with station LXXVI of the Karáchi Longitudinal Series established in 1851, which was found almost totally destroyed in 1876. The centre of the old pillar was determined from the lowest layer of bricks indicating its circumference. The azimuths and distances of the circumjaceut villages are :--Fulrár 157°, mile 1; Dhurio 10°, miles 2; and Bisasar 44°, miles 4.

II. Chánga Hill Station, lat. 24° 59′, long. 69° 54′—observed at in 1876—is situated on a sand hill bearing that name in that portion of the Thar or little desert appertaining to Bhuj. It lies  $1\frac{1}{2}$  miles S.W. of the road from Chelár to Nabisar. The nearest good water is at Asar 2.4 miles S.E. The station is in the lands of Chelár village, taluka Cháchra, district Thar and Párkar.

The masonry pillar, which is surrounded by an annular wall, is solid and 3½ feet deep. It contains three marks, two on stone, one at the foundation, the other 1½ feet above it, and the third on brick at the surface of the pillar. This station is nearly identical with station LXXX of the Karáchi Longitudinal Series established in 1851, which was found entirely destroyed. The present pillar is erected on the ruins of the base of the old pillar. The azimuths and distances of the circumjacent villages are :--Chelár 275°, miles 3.8; and Jojar 263°, miles 4.5.

III. Patatonk Hill Station, lat. 25° 10′, long. 69° 48′—observed at in 1876—is situated on a hill peak midway between the high roads from Umarkot to Nabisar and Chelár, 7 miles E. of the former and the same distance W. of the latter, and 4 miles E. of the plains of Sind. It is in the lands of Pata village, taluka Cháchra, district Thar and Párkar.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three marks, two on stone, one at the foundation, the other 1 foot above it, and the third on brick at the surface of the pillar. The station mark at the foundation was originally fixed in the course of the execution of the Umarkot Minor Series of the Karáchi Longitudinal Series. Pata (Ali Akbar) well azimuth 187°, mile 0.5.

IV. Narithal Hill Station, lat. 25° 16′, long. 69° 55′—observed at in 1876—is situated on a sand hill of the same name. The high road from Umarkot to Cháchra runs 1½ miles W. and that to Kesar 4 miles N. It is in the lands of Kacholi village, taluka Umarkot, district Thar and Párkar.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3½ feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar. The station is identical with that of the Umarkot Minor Series of the Karáchi Longitudinal Series, the marks being plumbed over the old station mark. The azimuths and distances of the circumjacent places are :—Ajba well 205°, mile ½; and Rojhra or Rodhar well 36°, miles 2.

V. Bhádi Hill Station, lat. 25° 15′, long. 70° 14′—observed at in 1876—is situated on a high, narrow and very long sand hill, 2 miles E.N.E. of Bhádi sweet-water well. Gatta village and well lie at the foot of the hill to the N.W. The road from Umarkot to Kesar runs about 7 miles N. It is in the lands of Bhádi village, taluka Cháchra, district Thar and Párkar.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three marks, the upper engraved on stone is let into the surface of the pillar, and two others on bricks are 2 and 3 feet respectively below it. The azimuths and distances of the circumjacent villages are :-Bhádi 75°, miles 2; and Gatta 230°, mile 1.

VI. Hatodan Hill Station, lat. 25° 30′, long. 69° 52′—observed at in 1876—is situated on the northern extremity of a long sand hill running in the usual direction and terminating abruptly towards the north, about  $1\frac{3}{4}$  miles W. of the road from Umarkot to Ranáhu village, 3 miles W. of the low ground inundated by the Nára river, and  $2\frac{1}{3}$  miles S.E. of Sínai (new) sweet-water wells. It is in the lands of Chor village, taluka Umarkot, district Thar and Párkar.

The masonry pillar, which is surrounded by an annular wall, is 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third on the surface of the pillar. The azimuths and distances of the circumjacent places are :--Kerlo sweet-water well 280°, miles 1<sup>1</sup>/<sub>3</sub>; Chor village old (Sinai) 134°, miles 4; and Chor village new 186°, miles 2.2.

VII. Rupihar Hill Station, lat. 25° 27', long. 70° 5'—observed at in 1876—is situated on a sand hill 1 mile north of the village so called on the high road from Umarkot to Gadra and Balmer. It is in the lands of Rupihar village, taluka Umarkot, district Thar and Párkar.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and  $3\frac{1}{3}$  feet in diameter. It contains three marks, the upper engraved on stone is flush with the surface of the pillar, and two others on brick are 2 and 3 feet respectively below it. Rupihar well azimuth  $23\frac{1}{3}^{\circ}$ , mile 0.9.

VIII. Kanakotri Hill Station, lat. 25° 30′, long. 70° 17′—observed at in 1876—is situated on a high sand hill about  $3\frac{1}{2}$  miles S. E. of the road from Umarkot to Kesar village. It is in the lands of Kanakotri village, taluka Umarkot, district Thar and Párkar.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three marks, the upper engraved on stone flush with the surface of the pillar, and two others on brick 2 and 3 feet respectively below it. The azimuths and distances of the circumjacent villages are :--Jagmal 174°, miles 1.5; and Silali 104°, mile 0.7.

IX. Mangtor Hill Station, lat. 25° 39′, long. 69° 57′—observed at in 1877—is situated on a low flat hill, about 2 miles S. of the well of the same name, and 5 miles E. of the road from Chor and Umarkot to Ránáhu. It is in the lands of Mangtor village, taluka Umarkot, district Thar and Párkar.

The masonry pillar, which is surrounded by an annular wall 1½ feet thick, is solid, 3 feet deep and 3½ feet in diameter. It contains three marks, one at the foundation, another 1 foot above it, and the third on the surface of the pillar. The azimuths and distances of the circumjacent wells are :—Goedani 48°, miles 4 (by road 4.7 miles); Bandho 48°, miles 6.7; and Mangtor 180°, miles 2.

X. Bhitala Hill Station, lat. 25° 39', long. 70° 11'—observed at in 1877—is situated on a long, narrow sand hill running N. E. and S. W., about 3 miles S. W. by S. of Khuiri or Khokro village, and 3 miles S. of Lapla well. It is in the lands of Khara Lapla village, taluka Umarkot, district Thar and Párkar.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third on the surface of the pillar. The azimuths and distances of the circumjacent wells are :--Datura 133°, miles 8.5; and Somo 157°, miles 8.9.

XI. Narhar Hill Station, lat. 25° 51′, long. 69° 57′—observed at in 1877—is situated on the hill on which the Revenue Survey station of Bamniwáro formerly existed, and about  $5\frac{1}{3}$  miles E. of the road from Umarkot and Chor to Ránáhu. It is in the lands of Narhar village, taluka Khipra, district Thar and Párkar.

The masonry pillar, which is surrounded by an annular wall 1½ feet thick, is solid, 3 feet deep and 3½ feet in diameter. It contains three mark-stones, one at the foundation, another one foot above it, and the third on the surface of the pillar. Narhar village distant 1.6 miles, azimuth 68°.

XII. Thakur Hill Station, lat. 25° 50′, long. 70° 10′—observed at in 1877—is situated on a sand ridge, about 3 miles W. of the boundary between Jodhpore and Sind. It is in the lands of Juma village, taluka Khipra, district Thar and Párkar.

The masonry pillar, which is surrounded by an annular wall 1½ feet thick, is solid, 3 feet deep and 3½ feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third on the surface of the pillar. The azimuths and distances of the circumjacent places are :—Katarlo well 345°, miles 3; Tar Rang Dahar (large village) 152°, miles 5½; Marwar village 258°, miles 5; and Juma well 69°, miles 2. It is identical with the Revenue Survey station of the same name.



XIII. Jeysulmere Hill Station, lat. 26° 5′, long. 69° 54′—observed at in 1877—was situated on the highest elevated sand knoll of the Jeysulmere draen (a tract of shifting sand) which extends for a space of about 50 square miles and has in parts sand knolls of considerable height. It was close to the Revenue Survey station of the same name. There are two wells of good water in the draen, about  $\frac{3}{4}$  and  $1\frac{1}{2}$  miles respectively W. of the site of the station, which is in the lands of Lodhar village, taluka Khipra, district Thar and Párkar.

The masonry pillar, which was surrounded by an annular wall, was solid, 5 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contained three mark-stones, one at the foundation, another 2 feet above it, and the third on the surface of the pillar. Lodhar village is distant 3.6 miles, azimuth 77°. This station was reported by the district officer in May 1879 to have been completely carried away by the shifting sand, the *debris* were collected and heaped together close to the original site.

XIV. Malar Hill Station, lat. 26° 2′, long. 70° 6′—observed at in 1877—is situated on the lowest and southernmost of three sand hills about a mile distant from each other, named after a hamlet about 2 miles to N.W., and 2 miles W. of the boundary between Sind and Marwar. It is in the lands of Saiadáhu village, taluka Khipra, district Thar and Párkar.

The masonry pillar, which is surrounded by an annular wall 1½ feet thick, is solid, 3 feet deep and 3½ feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third on the surface of the pillar. Saiadáhu village, on the road from Khipra to Jeysulmere town, is distant 4 miles, azimuth 128°.

XV. Badhor Hill Station, lat. 26° 0′, long. 70° 20′—observed at in 1877—is situated on a high sand hill in division Giraub, taluka Shiu, territory Jodhpore.

The masonry pillar, which is surrounded by an annular wall 1½ feet thick, is solid, 3 feet deep and 3½ feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third on the surface of the pillar. The azimuths and distances of the circumjacent places are :—Saijado well 217°, miles 3; and Sundra 143°, miles 10.

XVI. Ramsar Hill Station, lat. 26° 13′, long. 70° 2′—observed at in 1877—is situated on a hill 2 miles N. of the boundary between Thar and Párkar and Khairpur State. It is in lands of Wuriáhu village, Khairpur State, Sind.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>2</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third on the surface of the pillar which is flush with the hill top. The azimuths and distances of the circumjacent villages are :—Ramsar Bhil 325°, mile 1; and Wuriáhu 175°, miles 2.

XVII. Sinaba Hill Station, lat. 26° 12′, long. 70° 14′—observed at in 1877—is situated on the northern summit of a long sand ridge, about 4 miles N.E. of Khara well and a mile N.W. of the path from Saidáhu to Jeysulmere town, which passes by Khara. The nearest good water is at Saidáhu, 14 miles S:W. It is in village and division of Mehájliar, Jeysulmere State.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3½ feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third on the surface of the pillar which is flush with the hill top. The azimuths and distances of the circumjacent places are:—Badhi Baor hill (close to which is the quadri-junction pillar of Thar and Párkar, Jeysulmere, Khairpur and Jodhpore) 36°, miles 4; Sundra (in Jodhpore) 340°, miles 9; and Mehájliar (in Jeysulmere) 250°, miles 12.

XVIII. Potanawári Hill Station, lat. 26° 24′, long. 69° 56′—observed at in 1877—is situated on a low sand hill 2 miles W. 19° N. of Bakshiwári village. It is in the lands of Bakshiwári village, Khairpur State, Sind.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third on the surface of the pillar which is flush with the hill top. The azimuths and distances of the circumjacent places are :-Juma wells 332°, miles 2 and 3; Chanáhu well 116°, miles 1.6; Raknáhu well 255°, miles 3.3; and Bakshiwári village 289°, miles 2.3.

XIX. Joganali Hill Station, lat. 26° 25', long. 70° 6'-observed at in 1877—is situated on the second highest hill in the locality, about 1½ miles S.E. of Gauj Sing's wand and the same distance S.W. of Gagu hill which is the highest in this part of the country. It is in the lands of Sartanáhu village, Khairpur State, Sind.

The masonry pillar, which is surrounded by an annular wall, is solid,  $3\frac{1}{2}$  feet deep and  $3\frac{1}{2}$  feet in diameter. It contains three mark-stones, one at the foundation, another  $1\frac{1}{4}$  feet above it, and the third  $3\frac{1}{2}$  feet above, on the surface of the pillar which is flush with the ground. Azimuth and distance of Sartanáhu village are  $54^\circ$ , miles  $4^{\circ}8$ .



XX. Kardo Hill Station, lat. 26° 24', long. 70° 17'—observed at in 1877—is situated on a long sand ridge running N.E. and S.W. in the lands of Kardo (Karora) village, division Mehájliar, Jeysulmere State.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third on the surface of the pillar which is flush with the hill top. The azimuths and distances of the circumjacent places are :—Pochina well 850°, miles 2; and Komprajro Par 27°, miles 8<sup>1</sup>/<sub>3</sub>; and Kardo or Karora village 204°, miles 2.2.

XXI. Sanahu Hill Station, lat. 26° 34′, long 70° 1′—observed at in 1877—is situated on a sand hill conspicuous from its having several large trees on it, about  $\frac{1}{6}$  of a mile N. E. of a well so called, and 2 miles S. of the boundary between Khairpur and Jeysulmere. To the west, north and south there are extensive draens. It is in the lands of Sanahu village, Khairpur State, Sind.

The masonry pillar, which is surrounded by an annular wall, is solid, 8 feet deep and  $8\frac{1}{3}$  feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar. The azimuth and distance of Sumráhu village are 853°, miles  $5\frac{1}{3}$ .

XXII. Arrabhit Hill Station, lat. 26° 34′, long. 70° 12′—observed at in 1877—was situated on a long sand hill, about 200 yards N.E. of the boundary between Jeysulmere and Khairpur, and 4 miles N.E. of Sonhar village. It is in the lands of Shem village, Jeysulmere State.

The masonry pillar, which was surrounded by an annular wall, was solid, 8 feet deep and 8<sup>‡</sup> feet in diameter. It contained three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar which was flush with the hill top. The azimuths and distances of the circumjacent villages are :—Petrio 49°, miles 2<sup>‡</sup>; Sumráhu 61°, miles 12. This station was reported in 1880 by the District Officer as totally destroyed.

XXIII. Harnáo Hill Station, lat. 26° 44′, long. 69° 59′—observed at in 1877—was situated on the highest knoll of the draen called after the well of Harnáo about  $1\frac{1}{3}$  miles east. It was in the lands of Harnáo village, taluka Sháhgarh, Jeysulmere State.

The masonry pillar, which was surrounded by an annular wall, was solid, 5 feet deep and 3½ feet in diameter. It contained three mark-stones, one at the foundation, another 2 feet above it, and the third flush with the surface of the pillar. The directions and distances of the circumjacent places are :—Harnhár conspicuous sand-hill N.N.E., miles 4; Saunhar well E.N.E., miles 8; Kharodi well W., mile 1. This station was reported by Major Rogers in 1880 to have been completely carried away by the shifting sand.

XXIV. Dhanono Hill Station, lat. 26° 45′, long. 70° 13′—observed at in 1877—is situated on the highest part of a long sand ridge, about 5 miles N.W. of Dhanono well, 9 miles E.S.E. of Saunhar well, and 8 miles S.S.W. of Bhoiána well. It is in the lands of Dhanono village, division Shem, Jeysulmere State.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>4</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar.

XXV. Bándri Hill Station, lat. 26° 55′, long. 69° 52′—observed at in 1877—is situated on a sand hill, which, though low, is the highest for some miles around. It is in the midst of draens, the largest of which is to the west and extends to the foot of the station hill. Saira well is 4.7 miles to the west. The station is in the lands of Bándri well, division Sháhgarh, Jeysulmere State.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>2</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar.

XXVI. Ráviláhu Hill Station, lat. 26° 52′, long. 70° 5′—observed at in 1877 and 1880—is situated on the highest sand hill in the vicinity. Ráviláhu fresh water well is distant 1.5 miles and Saunhar well 5.7 miles. It is in the lands of Ráviláhu well, taluka Sháhgarh, Jeysulmere State.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar. When again visited in 1880 for continuing the Series northwards, the station was found in good order and the upper mark-stone intact, and no alteration in its construction is stated to have been made.

XXVII. Máhu Hill Station, lat. 27° 5′, long. 69° 48′—observed at in 1880—is situated on a sand hill which is also called Ramúwáribhit from the toba (or tank) of that name at its N.W. foot. About 31 miles W. of Máhu well. Maiha conspicuous Tar tree on a draen is distant 4 miles. The station is in the lands of Máhu well, taluka Sháhgarh, Jeysulmere State.

The masonry pillar, which is surrounded by an annular wall, is solid, 8 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar.

XXVIII. Girája Hill Station, lat. 27° 2′, long. 70° 3′—observed at in 1880—is situated on a high sand hill 8 miles S.S.W. of the village of Sháhgarh, and 3 miles E. of Girája well. It is in the lands of Girája well, taluka Sháhgarh, Jeysulmere State.

The masonry pillar, which is surrounded by an annular wall, is solid, 8 feet deep and 8<sup>1</sup>/<sub>2</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar.

XXIX. Máringra Hill Station, lat. 26° 59', long. 70° 15'—observed at in 1880—is situated on the highest part of a long sand hill, 4.6 miles S. of Mírwála well; and about 3 miles W. of Máringra well. It is in the lands of Máringra well, taluka Shem, Jeysulmere State.

The masonry pillar, which is surrounded by an annular wall, is solid, 8 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar.

XXX. Singra Hill Station, lat.  $27^{\circ}$  14', long.  $70^{\circ}$  1'—observed at in 1880—stands on a rather conspicuous sand hill midway between the villages of Sháhgarh and Gotaru, the road between them passing by the eastern base of the hill. The nearest fresh water is obtained from a small well on the north side of the Sháhgarh draen, distant about 6 miles. The station is in the lands of Sháhgarh village, taluka Sháhgarh, Jeysulmere State.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>4</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar. The directions and distances of the following places are :--Gotaru fort N., miles 8; and Sháhgarh village S., miles 8.

XXXI. Asu Hill Station, lat. 27° 11′, long. 70° 13′—observed at in 1880—is situated on a sand hill known in the neighbourhood as Báwalwála, which has several of equal or even greater height near it. The road from Gotaru to Jeysulmere, *vid* Khiwála, passes about 8 miles N. Asu well is distant about 5 miles. The station is in the lands of Asu well, taluka Khiwála (Kháro), Jeysulmere State.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar.

XXXII. Bitri Hill Station, lat. 27° 23', long. 69° 59'—observed at in 1880—is situated on a sand hill locally known as Saian-ki-Khabri, about  $1\frac{1}{3}$  miles S. of the path from Gotaru to Mitrau in Sind, and 4 miles E. of the Sind boundary. Gotaru fort and village, the nearest places for water, are about  $7\frac{1}{3}$  miles S.E. by E. The station is in the lands of Gotaru village, taluka Gotaru, Jeysulmere State.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar.

**XXXIII.** Parethal Hill Station, lat. 27° 22′, long. 70° 8′—observed at in 1880—is situated on the highest sand hill in the neighbourhood, which is not much above the general level of the country, about  $\frac{1}{2}$  mile E. of the path from Gotaru to Hingora well. Gotaru fort, at which fresh water is obtained, is distant 5 miles S.W. The station is in the lands of Gotaru village, taluka Gotaru, Jeysulmere State.

The masonry pillar, which is surrounded by an annular wall, is solid, 8 feet deep and 8<sup>1</sup>/<sub>2</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar.

XXXIV. Kolu Hill Station, lat. 27° 25′, long. 70° 20′—observed at in 1880—is situated on a low sand hill locally called Baurawála, about  $2\frac{1}{3}$  miles E. of Kolu well, and 7 miles distant in the same direction from Hassu and Hakara wells. It is in the lands of Kolu well, taluka Khiwála (Kháro), Jeysulmere State.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar. XXXV. Chauki Hill Station, lat. 27° 34′, long. 69° 56′—observed at in March and December 1880 is situated on the top of the sand hill which rises about 120 feet above the adjacent hollows. Fresh water is available from the Kiridi wells, 12 miles to N. The station is in Deh Sutiyáro, taluka Mirpur, district Shikárpur.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>2</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar. When again visited in December 1880 for continuing the Series northwards, "the station was evidently in perfect order, and the upper mark-stone intact," and no alteration in its construction is stated to have been made. The directions and distances of the circumjacent places are :--Ditta-ka-Toba N.E., mile <sup>2</sup>/<sub>2</sub>; Korárdara N.W., miles 3; Sháhbáz Khán Wali Toba S.S.W., miles 2; Bandli N, miles 9; and Sone-ka-Dara (Daro Sono) W.S.W., miles 2.

XXXVI. Kháro Hill Station, lat. 27° 33′, long. 70° 8′—observed at in 1880—is situated on a flattopped sand hill called by the natives Koudíwáladara from the tank at its northern base. The road from Kháro to Bandli in Sind passes 2 miles S. of the station. Kháro ruined fort is distant  $3\frac{3}{4}$  miles S.S.E., and Hingora well 7 miles S. Drinking water must be brought from Hassu well, about 12 miles S.E. It is in the lands of Hingora village, taluka Khiwála (Kháro), Jeysulmere State.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar.

XXXVII. Morgich Hill Station, lat. 27° 35′, long. 70° 17′—observed at in 1880—is situated on a small sand hill west of and close to the track from Kolu well to Khairgarh in Sind, and about 5 miles N. of the Karibhar well. It is in the lands of Karibhar well, taluka Khiwála (Kháro), Jeysulmere State.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar.

XXXVIII. Trising Hill Station, lat. 27° 42′, long. 70° 8′—observed at in March and December 1880 is situated on the northernmost of three high sand hills of that name lying together in the heart of the desert, far from any place. The station is built 200 yards S. of the declivity. The hill is a narrow ridge, 120 feet high, and steep except on the south side; a stone on the boundary of Sind and Jeysulmere, at the S.W. foot of the hill, is distant 1,105 feet W.S.W. from the station. Good water is available from the Kiridi and Sand (Khairgarh) wells in Sind, distant 16 and 14 miles respectively. The station is in the lands of Hingora well, taluka Khiwála (Kháro), Jeysulmere State.

The masonry pillar, which is surrounded by an annular wall, is solid, 8 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar. The approximate directions and distances of the circumjacent places are :—Islám-ka-Tarái S. by W., miles 8 or 4; Kardo W. by S., miles 8 or 4; and Band Lodi E.N.E., miles 8 or 4. When again visited in December 1880 for continuing the Series northwards, it is presumed from the absence of any remarks in the original records that the station was found in good order and the upper mark-stone intact; and that no alteration in its construction was made.

XXXIX. Thar Muhári Hill Station, lat. 27° 42′, long. 69° 43′—observed at in 1880—is situated on the northern summit of the sand hill of that name which rises to a height of about 100 feet above its base, 1½ miles S.S.W. from the present hamlet. It is in the lands of Saranwaro village, Deh Sutiyaro, taluka Mirpur, district Shikarpur.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>2</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar. The directions and distances of the circumjacent places are :--Saranwáro village N.N.E., miles 1<sup>1</sup>/<sub>2</sub>; Yáru Lund N.W., miles 9<sup>1</sup>/<sub>2</sub>; and Thar Bangáhu well W., miles 1<sup>1</sup>/<sub>2</sub>.

XL. Kiraríwáro Hill Station, lat. 27° 46', long. 69° 52'—observed at in 1880—is situated on the sand hill locally known as Kír-ri-wáro, about 80 feet high, which stands out from the more desert tract to the southeast, in the Patti or low ground which is still occasionally reached by the (Sind) inundation, and is called Kirari and Kanderawála. It is in Deh Sutiyáro, taluka Mirpur, district Shikárpur.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>2</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar. The directions and distances of the circumjacent places are :--Bandli S.S.E., miles 5; and Janganwáli N.N.E., miles 6.



XLI. Mári Hill Station, lat. 27° 51′, long. 69° 46′—observed at in 1880—is situated on the top of a large sand ridge about 70 feet above the plain, known as Daro Mári from an old deserted hamlet at its southwest foot. It is in the lands of Bhághibhit, Deh Sutiyáro, taluka Mirpur, district Shikárpur.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 8<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar. The directions and distances of the circumjacent places are:—Yáru Lund W.S.W., miles 8; Bhághibhit S.S.E., mile 1; Chanesar E.N.E., miles 5; Chándan N.N.W., miles 9; and Simna or Sinwála N.E., mile 1.

XLII. Yáru Hill Station, lat. 27° 55′, long. 69° 51′—observed at in 1880—is situated on a sand hill, locally known as Chor-ka-Dara, rising about 70 feet above the adjacent ground to its N. and W. It is in Deh Sutiyáro, taluka Mirpur, district Shikárpur.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar. The directions and distances of the circumjacent places are :—Reti Railway Station N. by E., miles 12<sup>1</sup>/<sub>3</sub>; Chándan Imámwáh W.N.W., miles 8<sup>1</sup>/<sub>3</sub>; Chanesar S.S.W., miles 2<sup>1</sup>/<sub>3</sub>; and Khenju N.E. by E., miles 5<sup>1</sup>/<sub>4</sub>.

XLIII. Núrpír Hill Station, lat. 27° 55′, long. 70° 2′—observed at in 1880—is situated on the present central summit of the somewhat isolated sand hill of that name which rises to a height of about 120 feet above the ground at its base, about  $1\frac{1}{2}$  miles W. by S. of Khairgarh fort, and 330 feet S.S.W. of the piles of old bricks supposed to mark the grave of Núrpír, after whom the place is named. It is in the lands of Deh Poh, taluka Mirpur, district Shikárpur.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar. The directions and distances of the circumjacent places are:—Khenju W.N.W., miles 7; Sand wells S.S.E., miles 2; and Khángarh village N., miles 2<sup>1</sup>/<sub>3</sub>.

XLIV. Vijnot Tower Station, lat. 28° 2′, long. 69° 53′—observed at in 1880 and 1881—stands on one of the highest mounds of the ruins of the ancient Hindu town of Vijnot, 3.8 miles S. by W. from the Railway Station of Reti. It is in Deh Vijnot, taluka Mirpur, district Shikárpur.

The station consists of a tower of sun-dried bricks set in mud cement, 20 feet square at base and 14 feet square at top, enclosing a central, perforated pillar of masonry 13 feet high. There are two marks, one engraved on stone is imbedded in the floor (15 feet above ground level) and the other, cut on a large brick, is 3 feet below it in the foundation of the pillar. A vaulted passage especially constructed for the purpose gives access to the upper mark. When again visited in 1881, the station was found in good preservation, the upper mark-stone intact, and no alteration in its construction is stated to have been made. The directions and distances of the circumjacent places are :--Reti village N.W., miles 4.2; and Reninadi W., miles 3<sup>‡</sup>.

XLV. Longwáli Hill Station, lat. 28° 2′, long. 70° 2′—observed at in 1881—is situated on the N.N.W. summit of the somewhat isolated sand ridge which rises to a height of 80 or 90 feet above the low ground at its base on three sides, *viz.*, the western, northern and eastern. The ridge is known as Rabbanwála Tibba, and among the Játs as Lániwáli Muhár, and is about  $1\frac{3}{4}$  miles N.E. by E. from the pond called Longwáli Talái, and 11 miles E.S.E. from the Reti Railway Station. The station is in the lands of Lakhíwáh village, tahsíl Sádikabad, Baháwalpur State.

The masonry pillar, which is surrounded by an annular wall, and a platform of earth and brushwood, is solid, 10 feet high and 3½ feet in diameter. It contains five mark-stones, one at its upper surface, and four others at 4, 7, 9 and 10 feet below it respectively.

XLVI. Vín Tower Station, lat. 28° 7′, long. 69° 57′—observed at in 1881—is built on a small mound on the northern edge of the southern branch of the rice fields, about a mile S.E. of the Indus Valley State Railway, and 750 yards S.E. by E. from the old masonry well of Vín deserted village. It is in the lands of Sabzalwáh village, tahsíl Sádikabad, Baháwalpur State.

The station consists of a tower of sun-dried bricks set in mud cement 16½ feet square at base and about 14 feet square at top, enclosing a central, perforated pillar of masonry 12.2 feet high. There are two mark-stones, one 0.2 foot below the floor level, and the other 2.75 feet below it in the foundation of the pillar. A vaulted passage especially constructed for the purpose gives access to the upper mark. The directions and distances of the circumjacent places are:—Reti Railway Station W.S.W., miles 3.8; Dhandi village N.N.W., miles 2.7; and Kalandar Sháh's tomb S.E. by S., miles 1.1.
XLVII. Got Mír Muhammad Hill Station, lat. 28° 8′, long. 70° 3′—observed at in 1881—is situated on the northern end of a low sand ridge, perhaps better known as Dhandhi Tálibwáli, from the slight hollow or low ground so called to the N.N.E., and otherwise named Wáhi Uhde Dás from a masonry well of that name about 1 mile to N.W. and  $1\frac{1}{3}$  miles E.N.E. of Got Jumma village. The station is named after Got Mír Muhammad, a hamlet about a mile N.W. by W. and near the brick well of Uhde Dás. The sand ridge may be about 20 feet above the adjacent low ground. Formerly it was called after Múša Máchi who occupied both ends of the ridge and a hamlet to the N.E. The station is in the lands of Got Mír Muhammad village, tahsíl Sádikabad, Baháwalpur State.

The masonry pillar, which is surrounded by an annular wall, is solid, 3 feet deep and 3<sup>1</sup>/<sub>3</sub> feet in diameter. It contains three mark-stones, one at the foundation, another 1 foot above it, and the third at the surface of the pillar. The azimuth and distance of Walhar Railway Station are 168° 38' and miles 4.4.

XLVIII. Dewari Tower Station, lat. 28° 9', long. 69° 50'—observed at in 1881—is built on the top of an old earthen watch-tower of Abdul Khair Dahar of Ubauro, which stands on an irregular mound long used for a graveyard, and named after one Mahmúd Bádala. It is in the lands of Dewari village, taluka Ubauro, district Shikárpur.

The masonry pillar, which is enclosed in a tower of sun-dried bricks set in mud cement, 18 feet square at base and 14 feet square at top, is solid, 16 feet high and 3½ feet in diameter at top. It carries a mark at its top and others below, the number and their distances are not forthcoming. The directions and distances of the circumjacent places are :—Dewari village S.E., 0.6 mile; Kádu Rind (Juna) hamlet W.N.W., about 500 yards; Ubauro W. by N., 3½ miles; and Reti Railway Station S.E., 6½ miles.

XLIX. Kot Sabzal Tower Station, lat. 28° 13', long. 69° 56'—observed at in 1881—is built on the mound which once formed the south-western round tower or bastion of the fort or fortified town of this name, and immediately over the new bridge across the Sabzalwáh canal at the S.W. corner of the place. The station is about 28 feet high above the level of the adjacent flat ground. It is in the lands of Kot Sabzal village, tahsíl Sádikabad, Baháwalpur State.

The isolated masonry pillar which is enclosed in a tower of sun-dried bricks set in mud cement, 14 feet square, is solid, 8 feet high and 3<sup>1</sup>/<sub>3</sub> feet in diameter at top, built on the top of the old tower which was cut down to afford a level platform. The pillar has a mark on its upper surface and others below it, the number and the relative distances apart of these are not forthcoming.

L. Kubba Tower Station, lat. 28° 12′, long. 69° 44′—observed at in 1881—is built on a low mound about 30 yards N.E. of another such mound said to be the site of a ruined kubba (tomb or mausoleum) of Walla Kalál. The remains of a well are to be seen between the two mounds. The station is a few yards E. of the road, 3.2 miles N.W. of Ubauro. It is in the lands of Lángha village, taluka Ubauro, district Shikárpur.

The perforated masonry pillar which is enclosed in a tower of sun-dried bricks set in mud cement, of the usual dimensions, is 21 feet high above the floor of the vaulted passage. It contains two marks engraved on bricks, one in the floor and the other in the foundation 2 feet below it. A vaulted passage especially constructed for the purpose gives access to the upper mark. The directions and distances of the circumjacent places are :--Basti Jiwan Sháh N.W., miles 3; and Ubauro S.E., miles 8.

LI. Ghundi Tower Station, lat. 28° 15′, long. 69° 50′—observed at in 1881—is built on the south bank of the canal called (Abul Khair) Dahrwáh, about 28 feet above its bed, and 150 yards S.E. of a rough stone set up on its N. bank, said to mark the tenth mile-stone. It lies 1 mile S.W. by S. from the old Ghundi graveyard. It is in the lands of Ghundi village, taluka Ubauro, district Shikárpur.

The station consists of a tower of sun-dried bricks set in mud cement, 21 feet square at base, 15 feet square at top, enclosing a central, perforated pillar of masonry 21 feet high. The upper surface of the pillar is 18.8 feet above the mark imbedded in the floor of the vaulted passage, this mark is 3 inches below the floor level, a second mark-stone is in the foundation 1 foot below the upper mark. A vaulted passage especially constructed for the purpose gives access to the upper mark.

LIX.—(Of the Great Indus Series). Máchka Tower Station, lat. 28° 20', long. 69° 42'—observed at in 1859, 1861 and 1881—is built on an island near the left bank of the Indus, or on a flat between the present main channel and the Kirár and Gudu branches, about 7 miles south of Kasmor. The flat is annually flooded during the inundation. The station is in the lands of Máchka village, tahsíl Sádikabad, Baháwalpur State.

The station as originally constructed in 1859 and 1861 consists of a tower of sun-dried bricks set in mud cement, enclosing a central, perforated pillar of masonry 24.6 feet high above the mark-stone at the ground level. When again visited in

#### EASTERN SIND MERIDIONAL SERIES.

1881, for the purpose of closing the Eastern Sind Meridional Series, the tower although somewhat settled and split, was found in a very serviceable condition, and the mark-stone at the floor level appeared unaltered. The pillar had however become inclined to the S.S.E., so that it was necessary to enlarge the perforation on the N.N.E. side to a depth of about 2 or 3 feet from the top of the pillar to allow of the mark-stone being plumbed over. The isolation and stability of the pillar were tested and seemed sufficiently perfect, and no alteration in the construction of the station was made. The directions and distances of the circumjacent places are :--Máchka (the present site of) S.E. by E., miles 1½; Daulatpur N.E., miles 1½; and Kharor W.S.W., mile 1.

LXII. (Of the Great Indus Series). Dáowála Tower Station, lat. 28° 20', long. 69° 53'—observed at in 1860-61 and 1881—is situated on low flat marshy ground of the Dhora Simna. It lies about  $1\frac{3}{4}$  miles N.E. from Dáowála village, the same distance N.N.W. of Mubárak Bhára, a mile E. from the head of the Sabzalwáh canal. It is in Mauza Dáowála, tahsíl Sádikabad, Baháwalpur State.

The station as originally constructed in 1860-61 consists of a tower of sun-dried bricks and mud cement built on an artificial basement 8 feet high and 23 feet square, enclosing a central, perforated pillar of masonry 22.4 feet high and 3½ feet in diameter at top, having a mark-stone at its floor level. The station was visited by Captain Rogers in 1880 who identified and restored it; but the records do not say in what condition it was found. When again visited in 1881, for the purpose of closing the Eastern Sind Meridional Series, the station was in the same state as left by Captain Rogers. The top of the pillar was found deflected a couple of inches to the north, but no alteration in the construction of the station was made. The directions and distances of the circumjacent places are :--Khambra S.W., miles 3½; and Kot Sabzal S.S.E., miles 9.3.

December, 1883.

W. H. COLE,

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## EASTERN SIND MERIDIONAL SERIES.

#### PRINCIPAL TRIANGULATION. OBSERVED ANGLES.

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	At	LXXV	(Rojhra)
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November 1876; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	0° 0′	180° 0′	Circle r 79°13′	eadings, 259° 13′	telescop 158° 25′	e being s 338° 24'	et on I ( 237° 37'	(Fulrár) 57° 37'	816° 49′	186° 49′	M = Mean of Groups to = Relative Weight C = Concluded Angle
·I (Fulrár) and LXXVIII (Sandohar)	*	γ λ 48 · 16 λ 48 · 28 λ 48 · 18 48 · 21	" 2 50.82 2 45.86 2 45.50 2 46.70 2 46.70 2 46.70 2 46.70 2 46.70 2 46.70 2 46.70 2 46.70 2 46.70 2 45.86 2 45.86 2 45.86 2 45.86 2 45.80 2 45.80 2 45.80 2 45.80 2 45.80 2 45.80 2 45.80 2 45.80 2 45.90 2 5.90 2 5	" \$ 50 · 16 \$ 47 · 60 \$ 46 · 86 \$ 47 · 38 \$ 47 · 78 47 · 96	h 47 · 58 h 49 · 68 h 48 · 88 h 49 · 22 48 · 84	ћ 49 · 86 ћ 48 · 06 ћ 47 · 16 ћ 46 · 92 48 · 00	n h 48 · 50 h 49 · 32 h 47 · 14 h 48 · 64 48 · 64	<sup>"</sup> <sup>k</sup> 48 · 56 <sup>k</sup> 47 · 78 <sup>k</sup> 47 · 76 48 · 07	к к 47 · 82 к 48 · 02 к 49 · 02 48 · 29	48.38 46.20 46.98 47.38 47.24	$M = 48'' \cdot 21$ $w = 18 \cdot 02$ $\frac{1}{w} = 0 \cdot 06$ $C = 46^{\circ} 47' 48'' \cdot 19$
LXXVIII (Sandohar) and V (Bhádi)	λ 38 · 68 λ 39 · 54 λ 38 · 68 λ 37 · 76 λ 40 · 98 39 · 13	h 37 · 76 h 37 · 60 h 38 · 58 37 · 98	2 34 · 84 2 37 · 08 2 36 · 28 2 35 · 96 3 35 · 96 3 38 · 44 36 · 10	h 34 · 76 h 34 · 76 h 35 · 48 h 37 · 84 h 37 · 82 36 · 13	h 36 · 94 h 36 · 20 h 38 · 04 37 · 06	h 36 · 94 h 37 · 52 h 39 · 88 h 99 · 78 38 · 53	h 37 · 38 h 38 · 88 h 37 · 54 37 · 93	h 37 · 22 h 37 · 12 h 36 · 64 36 · 99	h 37 · 56 h 38 · 12 h 38 · 06	h 37 · 38 h 37 · 58 h 36 · 74 37 · 23	$M = 37'' \cdot 50$ $w = 7 \cdot 96$ $\frac{1}{w} = 0 \cdot 13$ $C = 60^{\circ} 25' 37'' \cdot 49$

NOTE.-Stations LXXV (Bojhrs) and LXXVIII (Sandohar) apportain to the Karáchi Longitudinal Series of the North West Quadrilateral.

### At LXXVIII (Sandohar)

## November and December 1876; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch

Theodolite No. 2.

Angle between	0° 0′	Ci 180° 0′	rcle read 79°13'	ings, tele 259° 12′	escope be 158° 24′	oing set ( 338° 24′	on LXX 237° 37'	V (Rojh 57° 87′	ra) 816° 49'	136° 49′	<ul> <li>M - Mean of Groups</li> <li>Relative Weight</li> <li>C - Concluded Angle</li> </ul>
LXXV (Rojhra) and I (Fulrár)	" k 21 ° 46 k 22 ° 86 l 21 ° 60	" 2 21 · 18 2 24 · 82 7 21 · 78 2 22 · 48 2 22 · 98	*	n h 21 ° 04 h 21 ° 66 h 23 ° 74 h 21 ° 40	" h 20.68 h 21.58 h 21.12	# l 20·42 l 20·98 l 20·26	n h 20`86 h 22`66 h 23`64 h 20`64	* h 20°76 h 21°12 h 21°72 h 22°58	" h 21 · 44 h 22 · 54 h 21 · 52	" h 21 ° 68 l 24 ° 36 l 21 ° 80 l 20 ° 36 l 22 ° 06	$M = 21'' \cdot 80$ $w = 16 \cdot 33$ $\frac{1}{w} = 0 \cdot 06$
	21.92	22.65	22.34	21.96	21.13	<b>2</b> 0°55	<b>3</b> 1.95	31.24	21.83	22.05	$C = 44^{\circ} 57^{\prime} 21^{\prime\prime} \cdot 83$
I (Fulrár) and II (Chánga)	k 53°54 k 52°74 k 53°64	l 53°40 l 52°84 l 53°08	h 50°92 h 52°28 h 51°70	h 51 °68 h 52 °90 h 53 °78 h 52 °60	h 53°00 h 53°60 hl 52°90	l 52°94 l 54°78 l 52°94	k 51 ° 92 k 51 ° 64 k 53 ° 12	k 52°12 h 50°82 h 54°16 k 53°94 h 53°00	h 53°40 h 52°10 h 55°24	k 53°16 l 53°66 l 54°04	$M = 52'' \cdot 98$ $w = 16 \cdot 48$ $\frac{1}{w} = 0 \cdot 06$
	53.31	53.11	51.63	52.24	53.17	53°55	52.23	52.81	53.28	53.62	$C = 81^{\circ} 16' 52'' \cdot 98$
II (Chánga) and III (Patatonk)	k 5°76 k 9°24 k 7°72 l 5°96 l 6°96	l 8·20 l 6·76 l 7·10	አ 9°56 አ 9°36 አ 8°46	እ 8•84 እ 8•94 እ 8•68	k 9°18 k 9°50 lk 9°44	l 9°00 l 7°62 l 7°80 d 9°45	k 9.26 k 11.60 k 10.42 k 10.16	k 8.22 k 9.62 k 10.38 k 9.94	k 10°78 k 8°38 k 7°50 k 8°74	k 9°36 l 7°26 l 9°50 l 8°90	$M = 8'' \cdot 78'$ $w = 8 \cdot 80$ $\frac{1}{w} = 0 \cdot 11$
	7.13	3 7.35	9.13	8.82	9.37	8.47	10.36	9.24	8-85	8.76	$C = 60^{\circ}$ 1' 8".78
III (Patatonk) and IV (Narithal)	k 34 · 30 k 36 · 62 k 37 · 96 l 37 · 64 l 37 · 70	l 34°04 l 35°78 l 37°04 l 36°26 l 35°04	k 38 · 18 k 35 · 96 k 37 · 30 k 36 · 88	<b>h 37°74</b> h 37°68 h 36°76	k 36°74 k 36°22 k 36°06	l 37°10 l 37°76 l 36°82 d 38°54	h 37°04 h 35°80 h 37°88 h 36°46	k 37 · 38 k 36 · 10 k 36 · 64 k 36 · 12	ћ 36°34 ћ 35°70 ћ 36°70	k 36.62 l 36.12 l 36.40	$M = 36'' \cdot 68$ $w = 19 \cdot 90$ $\frac{1}{w} = 0 \cdot 05$
	36.84	35.63	37.08	37 * 39	36.34	37.56	36.29	36.26	36.22	36.38	$C = 38^{\circ} 25' 36'' \cdot 68$
IV (Narithal) and V (Bhádi)	h 1.10 h 3.90 h 0.16 l 2.68 l 2.32	2 3 · 14 2 2 · 56 2 4 · 88 2 1 · 62 2 4 · 22	h 2.74 h 3.24 h 0.60 h 4.58 h 1.86	h 3.62 h 3.28 h 2.22	h 2·40 h 2·42 hl 1·84	l 3.14 l 3.12 l 2.06 l 2.92	h 1.64 h 2.14 h 1.26	h 1.54 h 0.06 h 1.96	h 2.22 h 3.58 h 2.20	hl 2.52 l 2.04 l 3.12	$M = 2'' \cdot 41$ $w = 20 \cdot 65$ $\frac{1}{w} = 0 \cdot 05$
	2.03	3 · 28	2.60	3.04	2 . 22	2.81	1.98	1.19	2.67	2.26	$C = 66^{\circ} 39' 2'' \cdot 43$

NOTE.-Stations LXXV (Rojhrs) and LXXVIII (Sandohar) appertain to the Karáchi Longitudinal Series of the North-West Quadrilateral.

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#### PRINCIPAL TRIANGULATION, OBSERVED ANGLES.

	At LXXVIII (Sandohar)—(Continued).									
Angle between	Circle readings, telescope being set on LXXV (Rojhra) 0°0′ 180°0′ 79°13′ 259°12′ 158°24′ 338°24′ 237°37′ 57°37′ 316°49′ 186°49′	M - Mean of Groups w - Relative Weight C - Concluded Angle								
· V (Bhádi) and LXXV (Rojhra)	\$\$ 56 \cdot 08 \$\$ 1 57 \cdot 58 \$\$ \$ 55 \cdot 4 \$\$ 58 \cdot 38 \$\$ \$ 57 \cdot 02 \$\$ 1 56 \cdot 64 \$\$ \$ 56 \cdot 72 \$\$ 56 \cdot 08 \$\$ \$ 55 \cdot 70 \$\$ \$\$ \$ 55 \cdot 70 \$\$ \$ \$ \$ \$ 55 \cdot 70 \$\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	$M = 56'' \cdot 66$ $w = 28 \cdot 17$ $\frac{1}{w} = 0 \cdot 04$ $C = 68^{\circ} 26' z 6'' \cdot 60$								
	56.41 56.17 56.85 57.35 57.09 56.42 56.55 56.75 56.36 56.97	c = 08 39 50 09								
	At I (Fulrár)									
December 1876;	December 1876; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.									
Angle between	Circle readings, telescope being set on II (Chánga) 232° 32′ 52° 31′ 311° 44′ 131° 44′ 30° 56′ 210° 56′ 110° 8′ 290° 8′ 189° 20′ 9° 20′	M - Mean of Groups $\infty$ - Relative Weight C - Concluded Angle								
II (Chánga) and LXXVIII (Sandohar)	h 53 · 18 h 53 · 48 h 53 · 36 h 53 · 80 h 53 · 46 h 53 · 18 h 54 · 46 h 55 · 36 h 53 · 32 h 53 · 26 h 52 · 92 h 52 · 36 h 53 · 12 h 53 · 60 h 53 · 06 h 52 · 78 h 53 · 60 h 53 · 68 h 52 · 62 h 53 · 48 h 54 · 48 h 53 · 02 h 53 · 96 h 53 · 58 h 52 · 56 l 52 · 82 h 54 · 00 h 54 · 18 h 53 · 66 h 52 · 66	$M = 53'' \cdot 43$ $w = 32 \cdot 30$ $\frac{1}{w} = 0 \cdot 03$								
	53.53 52.95 53.48 53.66 53.03 52.93 54.02 54.41 53.20 53.13	$C = 39^{\circ} 13' 53'' \cdot 43$								
LXXVIII (Sandohar) and LXXV (Rojhra)	k 50.62 k 50.84 k 51.64 k 51.88 k 50.34 k 51.82 k 50.96 k 50.62 k 51.66 k 50.74 k 51.66 k 51.26 k 51.38 k 51.36 k 50.82 k 49.52 k 50.14 k 51.48 k 50.64 k 51.46 k 49.98 k 52.46 k 51.82 k 51.64 k 50.48 k 50.78 k 50.64 k 52.18 k 51.62 k 50.96 l 49.78	$M = 51'' \cdot 09$ $w = 31 \cdot 50$ $\frac{1}{w} = 0 \cdot 03$								
•	50.75 51.52 51.61 51.63 50.55 50.48 50.58 51.43 51.31 51.05	$C = 88^{\circ} 14' 51'' \cdot 09$								
	At II (Chánga)									
December 1876; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.										
Angle between	Circle readings, telescope being set on III (Patatonk) 0° 0′ 180° 0′ 79° 13′ 259° 13′ 158° 24′ 338° 24′ 237° 37′ 57° 37′ 316° 49′ 136° 49′	M = Mean of Groups $\omega$ = Relative Weight C = Concluded Angle								
III (Patatonk) and LXXVIII (Sandohar)	h 40.06 h 39.40 h 38.10 h 38.68 h 36.14 h 38.40 h 38.78 l 37.14 h 37.42 h 38.52 h 36.26 h 37.76 h 36.38 h 36.84 h 39.08 h 38.22 l 36.96 l 38.18 h 38.90 h 38.12 h 37.92 h 38.50 h 37.52 h 36.18 h 37.64 h 39.58 l 38.28 l 38.c2 h 38.02 h 37.40 h 39.24 h 38.14 h 38.76 h 38.62	$M = 38'' \cdot 03$ $w = 23 \cdot 03$ $\frac{1}{w} = 0 \cdot 04$								
	38.42 38.55 37.33 37.46 37.91 38.73 38.01 37.78 38.11 38.01	$C = 84^{\circ} 46' 38'' \cdot 03$								

Norz.-Stations LXXV (Rojhrs) and LXXVIII (Sandohar) appertain to the Karáchi Longitudinal Series of the North-West Quadrilateral.

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#### EASTERN SIND MERIDIONAL SERIES.

			At	II (Cł	nánga)-	—(Oon	tinued)	•			
Angle between	0° 0′	C 180° 0′	ircle read 79° 13′	lings, tel 259°13'	lescope b .158° 24'	eing set 338° 24'	on III 237° 37'	(Pataton 57° 37'	k) 316° 49'	136° 49′	M = Mean of Groupe w = Relative Weight C = Concluded Angle
LXXVIII (Sandohar) and I (Fulrár)	" \$ 12.90 \$ 13.40 \$ 14.18 13.49	" h 14 · 32 h 13 · 58 h 14 · 08	" k 14.08 k 14.16 k 14.34 14.19	*	" h 14·30 h 14·08 h 13·88 14·09	" h 14 · 22 h 14 · 72 h 14 · 54 14 · 49	" 1 14·24 1 14·18 1 13·68 14·03	2 14·44 2 14·76 2 13·94 14·38	" h 14·28 h 14·52 k 15·02 14·61	" h 12 · 56 h 15 · 38 h 14 · 34 h 13 · 56 13 · 96	$M = 14'' \cdot 07$ $w = 39 \cdot 00$ $\frac{1}{w} = 0 \cdot 03$ $C = 59^{\circ} 29' 14'' \cdot 07$

### At III (Patatonk)

December 1876; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	251° 7′	C 71° <i>7′</i>	circle rea 330° 19'	dings, te 150° 19′	lescope 49° 31'	being set 229°31′	; on IV 128° 44'	(Narithal) 808° 44′ 2	07° 55′ 27° 55′	M = Mean of Groups w = Relative Weight C = Concluded Angle
IV (Narithal) and LXXVIII (Sandohar)	" \$ 55.36 \$ 56.92 \$ 56.42 56.23	" h 54 · 66 h 56 · 62 h 55 · 48	* \$55.62 \$56.08 \$57.66 \$56.82 \$56.55	* \$54.30 \$55.28 \$55.16 54.91	<i>k</i> 56 · 84 <i>k</i> 56 · 06 <i>k</i> 55 · 64 56 · 18	π h 55.64 h 55.76 h 56.38	<i>k</i> 56 · 02 <i>k</i> 56 · 04 <i>k</i> 54 · 76 55 · 61	<i>k</i> 55 <sup>•</sup> 34 <i>k</i> <i>k</i> 55 <sup>•</sup> 80 <i>k</i> <i>k</i> 55 <sup>•</sup> 10 <i>k</i> <i>k</i> <i>k</i> <i>k</i> <i>k</i>	56 06 h 57 32 53 04 h 57 64 56 98 h 57 18 54 58 h 57 34 57 58 57 66 55 98 57 37	$M = 55'' \cdot 98$ w = 14 : 65 $\frac{1}{w} = 0 \cdot 07$ $C = 73^{\circ} 40' 56'' \cdot 00$
LXXVIII (Sandohar) and II (Chánga)	h 12 · 42 h 11 · 26 h 12 · 72	h 11 · 50 h 13 · 42 h 12 · 76	h 13 · 90 h 14 · 66 h 13 · 82 14 · 13	h 13.30 h 12.96 h 13.66	h 13 92 h 13 94 h 13 50 13 79	h 14.62 h 13.76 h 13.68	h 11 °92 h 13 °78 h 13 °58	h 12.70 h 1 h 12.34 h 1 h 13.30 h 1 12.78	13.38 k 13.96 13.34 k 12.34 14.30 k 13.46 13.67 13.25	$M = 13'' \cdot 27$ $w = 19 \cdot 20$ $-\frac{1}{w} = 0 \cdot 05$ $C = 35^{\circ} 12' 13'' \cdot 27$

At IV (Narithal)

December 1876; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	0° 0′	C 180°0′	ircle rea 79° 13'	dings, te 259°13′	blescope   158° 24'	being set 838°23'	on VI ( 237° 37'	Hatod <b>a</b> n 57° 37'	) 816° 49′	136° 49′	M = Mean of Groups w = Relative Weight C = Concluded Angle
VI (Hatodan) and VII (Rupihar)	" k 8.54 k 9.00 h 8.60 h 4.66 l 5.42 l 5.10 6.89	" h 5.68 h 7.10 h 7.58 h 6.46 6.71	" l 4.52 l 8.14 h 4.26 h 7.16 h 6.08 6.03	<i>h</i> 6 · 44 <i>h</i> 6 · 28 <i>h</i> 4 · 20 <i>h</i> 8 · 52 <i>h</i> 6 · 78 <i>h</i> 7 · 76 6 · 66	" h 4.80 h 6.32 h 5.12 5.41	n h 6·76 h 7·62 h 8·04 7·47	* h 6.66 h 8.18 h 7.76 7.53	κ 5·74 λ 4·48 λ 5·76 5·33	* h 7.78 h 8.90 h 7.16 7.95	* h 5 · 54 h 7 · 26 h 3 · 92 h 5 · 80 h 7 · 86 6 · 08	$M = 6^{"} \cdot 61$ $w = 8 \cdot 42$ $\frac{1}{w} = 0 \cdot 12$ $C = 49^{\circ} 24^{\prime} 6^{"} \cdot 60$

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NOTE.-Station LXXVIII (Sandohar) appertains to the Karáchi Longitudinal Series of the North-West Quadrilateral.

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PRINCIPAL TRIANGULATION. OBSERVED ANGLES.

-	At IV (Narithal)—(Continued).	
Angle between	Circle readings, telescope being set on VI (Hatodan) 0°0′ 180°0′ 79°13′ 259°13′ 158°24′ 838°23′ 237°37′ 57°37′ 816°49′ 186°49′	M = Mean of Groups w = Relative Weight C = Concluded Angle
VII (Rupih <b>ar)</b> and V (Bhádi)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$M = 57'' \cdot 00$ $w = 21 \cdot 61$ $\frac{1}{w} = 0 \cdot 05$ $C = 54^{\circ} 30' 56'' \cdot 98$
V (Bhádi) and LXXVIII (Sandohar)	\$\$ 26.90       \$\$ 27.60       \$\$ 27.76       \$\$ \$\$ 29.90       \$\$ \$\$ 26.78       \$\$ \$\$ 27.96       \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$	$M = 28'' \cdot 29$ $w = 16 \cdot 94$ $\frac{1}{w} = 0 \cdot 06$ $C = 63^{\circ} 27' 28'' \cdot 30$
LXXVIII (Sandohar) and III (Patatonk)	h 26 · 98       h 28 · 02       l 28 · 40       h 27 · 70       h 26 · 20       h 27 · 12       h 28 · 50       h 28 · 58       h 27 · 74       h 29 · 84         h 27 · 72       h 27 · 46       l 27 · 98       h 28 · 62       h 28 · 14       h 27 · 76       h 28 · 38       h 28 · 56       h 26 · 56       h 28 · 58       h 27 · 74       h 29 · 84         h 25 · 98       h 27 · 58       h 28 · 52       h 29 · 76       h 28 · 86       h 26 · 56       h 29 · 12       h 27 · 98       h 27 · 92       h 27 · 80         h 27 · 56       h 27 · 88       h 29 · 10       h 29 · 82       h 29 · 82         27 · 06       27 · 69       28 · 30       28 · 49       28 · 08       27 · 15       28 · 67       28 · 31       27 · 41       28 · 89	$M = 28'' \cdot 01$ $w = 18 \cdot 06$ $\frac{1}{w} = 0 \cdot 06$ $C = 67^{\circ} 53' 28'' \cdot 01$

At V (Bhádi)

December 1876; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	161 <b>° 54</b> ′	Ci 841° 54'	rcle read 241°6′	ings, tel 61°6′	escope be 320° 18'	9ing set ( 140°17'	m LXX' 89° 30'	V (Bojh: 219° 30'	ra) 118° 42′	298° 42′	M - Mean of Groups $\infty$ - Relative Weight C - Concluded Angle
LXXV (Rojhra) and LXXVIII (Sandohar)	" h 25.08 h 24.68 h 28.74 h 26.52 l 25.64 l 28.02 26.45	" h 26 · 90 h 27 · 88 h 27 · 28 27 · 35	" l 28.88 l 27.28 l 27.34 27.83	" l 28.06 l 28.58 l 27.74 28.13	" h 28 · 18 h 27 · 44 h 29 · 00 28 · 21	" h 28 · 18 h 26 · 84 h 29 · 00 h 28 · 32 28 · 09	" h 28 · 56 h 27 · 84 h 27 · 54 d 28 · 51 28 · 11	" h 26 · 62 h 28 · 54 h 27 · 34 27 · 50	" l 27·30 l 27·98 l 27·16 27·48	* l 26.68 l 28.60 l 27.38 27.55	$M = 27'' \cdot 67$ $w = 19 \cdot 93$ $\frac{1}{w} = 0 \cdot 05$ $C = 50^{\circ} 54' \cdot 27'' \cdot 65$

NOTE.-Stations LXXV (Rojhra) and LXXVIII (Sandohar) appertain to the Karáchi Longitudinal Series of the North-West Quadrilateral.

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At V (Bhádi)-(Continued).

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Angle between	Circle readings, telescope being set on LXXV (Rojhra) 161°54′ 341°54′ 241°6′ 61°6′ 320°18′ 140°17′ 39°30′ 219°30′ 118°42′ 298°42′	M - Mean of Groups w - Relative Weight C - Concluded Angle
LXXVIII (Sandohar) and IV (Narithal)	$\begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \end{array} \\ \begin{array}{c} \end{array} \end{array} \\ $	$M = 30'' \cdot 63$ $w = 53 \cdot 82$ $\frac{1}{w} = 0 \cdot 02$ $C = 49^{\circ} 53' 30'' \cdot 63$
IV (Narithal) and VII (Rupihar)	k 23.02 k 23.12 l 23.30 l 22.48 k 22.42 k 21.98 k 21.22 k 22.36 l 20.08 l 22.58 k 23.02 k 23.12 l 23.30 l 22.48 k 22.42 k 21.98 k 21.22 k 22.36 l 20.08 l 22.58 k 22.28 k 22.62 l 20.90 l 23.16 k 22.96 k 22.36 k 21.92 k 20.96 l 21.10 l 21.78 h 19.18 k 21.52 l 22.60 l 22.62 k 22.24 k 21.92 k 21.54 k 22.62 l 21.42 l 22.06 k 22.74 l 22.08 d 23.91 l 22.84 k 21.86 k 23.68 d 20.41 k 22.88 22.30 22.42 22.22 22.75 22.88 22.09 21.59 21.95 20.87 22.14	$M = 22'' \cdot 12$ $w = 19 \cdot 35$ $\frac{1}{w} = 0 \cdot 05$ $C = 51^{\circ} 49' 22'' \cdot 12$
VII (Bupihar) and VIII (Kanakotri)	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$M = 6'' \cdot 19$ $w = 17 \cdot 19$ $\frac{1}{w} = 0 \cdot 06$ $C = 45^{\circ} 20' \cdot 6'' \cdot 20$
	5.96 5.78 6.49 5.86 6.56 4.95 6.60 6.63 6.68 6.34	$0 = 45^{-}29^{-}0^{-}20$

At VI (Hatodan)

December 1876; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle hetween		C	ircle rea	dings, te	lescope b	eing set	on IX (	Mangton	•)		M = Mean of Groups
 Augre Dermeen	<b>2</b> 15° 2 <b>2</b> ′	85° 22′	294° 34′	114° 33′	13° <b>4</b> 6′	193° <b>46</b> ′	92° 58′	272° 58′	172° 11′	<b>352°</b> 11′	c = Kelative Weight C = Concluded Angle
IX (Mangtor) and VII (Rupihar)	k 35 · 30 h 32 · 82 h 33 · 86 h 33 · 50	" h 32 · 88 h 34 · 70 h 33 · 20	" h 33 · 08 h 32 · 22 h 34 · 34 h 33 · 76	" h 36 · 10 h 33 · 28 h 34 · 22 h 36 · 56 h 35 · 96	" 1 32 · 44 1 33 · 00 1 34 · 08	" 2 35 · 36 2 33 · 62 2 33 · 16 2 33 · 58	" l 36 · 30 l 34 · 22 l 33 · 62 l 34 · 28	" 1 33 · 86 1 30 · 56 1 31 · 98 1 31 · 00 1 34 · 98 1 33 · 68	n h 32 · 18 h 34 · 08 h 33 · 66	" h 33 · 26 h 34 · 62 h 35 · 46 h 34 · 60	$M = 33'' \cdot 82$ $w = 11 \cdot 38$ $\frac{1}{w} = 0 \cdot 09$
	33.87	33.29	33.35	35.22	33.17	33 . 93	34.61	32.68	33.31	34 · 48	$C = 76^{\circ} 1' 33'' \cdot 83$

NOTE.-Stations LXXV (Rojhrs) and LXXVIII (Sandohar) appertain to the Karáchi Longitudinal Series of the North-West Quadrilateral.

At VI (Hatodan)-(Continued).

<b>∆ng</b> le between	Circle readings, telescope being set on IX (Mangtor) 215° 22' 35° 22' 294° 34' 114° 33' 13° 46' 193° 46' 92° 58' 272° 58' 172° 11' 352° 11'	M = Mean of Groupe w = Relative Weight C = Concluded Angle
VII (Rupihar) and IV (Narithal)	#       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #	$M = 34'' \cdot 62$ $w = 23 \cdot 17$ $\frac{1}{w} = 0 \cdot 04$ $C = 68^{\circ} 36' 34'' \cdot 62$
	33.99 35.09 35.05 34.58 33.99 34.45 34.17 35.15 34.61 35.45	

At VII (Rupihar)

December 1876; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	Circle readings, telescope being set on VI (Hatodan) 0°1′ 180°1′ 79°12′ 259°12′ 158°24′ 838°24′ 237°37′ 57°37′ 816°48′ 136°48′	M - Mean of Groups w - Relative Weight C - Concluded Angle
VI (Hatodan) and IX (Mangtor)	h 37 · 04       h 36 · 56       h 37 · 26       h 37 · 80       h 38 · 04       h 37 · 40       h 37 · 44       l 37 · 60       h 36 · 70       h 36 · 34         h 36 · 78       h 39 · 70       h 36 · 38       h 36 · 64       h 37 · 14       h 37 · 68       l 40 · 50       h 37 · 06       h 36 · 78         h 38 · 42       h 36 · 80       h 38 · 46       h 37 · 06       h 36 · 12       h 36 · 60       l 37 · 44       h 36 · 70       h 36 · 78         h 38 · 42       h 36 · 80       h 38 · 46       h 37 · 06       h 36 · 12       h 36 · 60       l 37 · 44       h 36 · 70       h 36 · 78         h 37 · 02       h 37 · 64       l 37 · 52       .       h 39 · 20       l 38 · 94       h 36 · 06         l 36 · 80       l 38 · 94       h 36 · 06       l 38 · 94       h 36 · 06       l 37 · 44       h 36 · 06         37 · 41       37 · 38       37 · 44       37 · 17       37 · 10       37 · 23       38 · 37       37 · 12       37 · 02       36 · 64	$M = 37'' \cdot 29$ $w = 22 \cdot 72$ $\frac{1}{w} = 0 \cdot 04$ $C = 48^{\circ} 34' 37'' \cdot 32$
IX (Mangtor) and X (Bhitala)	h 31 · 92 h 34 · 38 h 34 · 26 h 33 · 44 h 36 · 04 h 33 · 58 h 33 · 60 l 34 · 74 h 34 · 40 h 34 · 24 h 34 · 42 h 34 · 84 h 33 · 72 h 33 · 64 h 33 · 48 h 33 · 02 l 34 · 14 h 33 · 28 h 33 · 64 h 34 · 80 h 35 · 60 h 36 · 04 h 34 · 16 h 32 · 80 h 33 · 28 h 34 · 02 l 35 · 00 h 34 · 48 h 33 · 82 h 33 · 94 h 35 · 10 h 36 · 60 h 34 · 46 h 35 · 24	$M = 34'' \cdot 19$ $w = 19 \cdot 52$ $\frac{1}{w} = 0 \cdot 05$
	34.30 35.42 34.05 33.29 34.27 33.54 34.60 34.17 33.95 34.33	$C = 58^{\circ} 5' 34'' \cdot 22$
X (Bhitala) and VIII (Kanakotri)	h 51 · 46 h 53 · 22 h 50 · 58 h 50 · 98 h 50 · 70 h 51 · 88 h 51 · 40 l 49 · 76 h 51 · 16 h 49 · 36 h 51 · 74 h 49 · 30 h 49 · 86 h 51 · 92 h 50 · 06 h 49 · 64 l 48 · 80 h 48 · 72 h 49 · 42 h 48 · 98 h 50 · 60 h 50 · 68 h 51 · 40 h 50 · 30 h 51 · 58 l 49 · 64 h 50 · 68 h 50 · 26 h 50 · 94 h 49 · 62 h 51 · 20 h 51 · 20	$M = 50'' \cdot 52$ $w = 16 \cdot 80$ $\frac{1}{w} = 0 \cdot 06$
	51.27 50.86 50.37 51.43 50.14 51.03 50.32 49.72 50.28 49.76	$C = 48^{\circ} 43' 5^{\circ''} \cdot 5^{2}$

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At VII (Rupihar)—(Continued).

Angle between	Circle readings, telescope being set on VI (Hatodan) 0°1′ 180°1′ 79°12′ 259°12′ 158°24′ 888°24′ 237°87′ 57°87′ 816°48′ 136°48′	M = Mean of Groups w = Relative Weight C = Concluded Angle
VIII (Kanakotri) and V (Bhádi)	h 56·32 h 55·56 h 55·66 h 56·90 h 55·88 h 56·80 h 57·46 l 56·60 h 56·68 h 57·02         h 55·72 h 55·50 h 55·66 h 57·58 h 58·04 h 56·86 l 56·62 l 56·04 h 58·02 h 54·68         h 56·24 h 54·76 h 55·44 h 55·86 h 56·66 h 56·92 l 57·30 h 57·36 h 56·86 h 56·40         h 55·34	$M = 56'' \cdot 45$ $w = 18 \cdot 60$ $\frac{1}{w} = 0 \cdot 05$
	55.91 55.27 55.59 56.78 56.76 56.86 57.13 56.70 57.19 56.35	$C = 68^{\circ} 56' 56'' \cdot 45$
V (Bhádi) and IV (Narithal)	$h_{38} \cdot 22 h_{40} \cdot 58 h_{41} \cdot 60 h_{41} \cdot 68 h_{41} \cdot 82 h_{41} \cdot 80 h_{42} \cdot 02 l_{40} \cdot 88 h_{41} \cdot 90 h_{42} \cdot 08 h_{42} \cdot 12 h_{42} \cdot 00 h_{43} \cdot 34 h_{43} \cdot 10 h_{41} \cdot 94 h_{42} \cdot 34 l_{41} \cdot 38 l_{42} \cdot 76 h_{41} \cdot 58 h_{42} \cdot 54 h_{40} \cdot 84 h_{41} \cdot 70 h_{42} \cdot 50 h_{40} \cdot 18 h_{41} \cdot 38 h_{40} \cdot 36 l_{41} \cdot 94 h_{41} \cdot 94 h_{42} \cdot 08 h_{42} \cdot 10 h_{43} \cdot 10 h_{41} \cdot 56 h_{4$	$M = 41w \cdot 78$ $w = 25 \cdot 95$ $\frac{1}{w} = 0 \cdot 04$
	41.41 41.43 42.48 41.63 41.71 41.50 41.78 41.75 41.85 42.24	$C = 73^{\circ} 39' 41'' \cdot 75$
IV (Narithal) and VI (Hatodan)	\$\$ 22.32       \$\$ 19.60       \$\$ 19.26       \$\$ 18.20       \$\$ 20.30       \$\$ 20.18       \$\$ 18.54       \$\$ 20.22       \$\$ 20.50       \$\$ 20.38         \$\$ 18.84       \$\$ 20.18       \$\$ 18.04       \$\$ 19.92       \$\$ 19.38       \$\$ 19.40       \$\$ 17.94       \$\$ 21.54       \$\$ 20.98       \$\$ 19.80         \$\$ 22.34       \$\$ 20.60       \$\$ 19.76       \$\$ 18.96       \$\$ 21.24       \$\$ 18.82       \$\$ 20.18       \$\$ 20.14       \$\$ 17.54       \$\$ 19.24         \$\$ \$\$ 19.84       \$\$ 20.54       \$\$ 19.76       \$\$ 18.96       \$\$ 21.22       \$\$ \$\$ 18.86       \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$ \$\$	$M = 19'' \cdot 82$ $w = 13 \cdot 58$ $\frac{1}{w} = 0 \cdot 07$
	21.12 20.13 10.02 10.03 20.31 10.47 10.30 20.42 10.26 10.81	$C = 61^{\circ} 59' 19'' \cdot 84$

# At VIII (Kanakotri)

December 1876; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	°° 0°	179° 59′	Circle 1 79° 13′	eadings, 259° 13'	telescop 158° 25′	e being a 838° 25'	et on V 237° 37'	(Bhádi) 57° 37′	<b>816° 49</b> ′	136° 49′	M - Mean of Groups w - Relative Weight C - Concluded Angle
V (Bhádi) aud VII (Rupihar)	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	k 57 · 14 h 58 · 32 h 59 · 34 h 58 · 94 58 · 44	* \$57.78 \$58.86 \$58.82 58.49	* \$ 55.86 \$ 58.12 \$ 55.32 \$ 57.66 56.74	и л 57 · 26 л 56 · 70 л 56 · 98 56 · 98	n h 57 · 50 h 58 · 34 h 57 · 74 57 · 86	x \$ 58.56 \$ 58.06 \$ 58.24 58.29	k 57 · 24 k 59 · 20 k 59 · 46 k 56 · 64 58 · 13	x x x x 58 · 20 58 · 67	* \$ 57 · 12 \$ 57 · 78 \$ 58 · 32 57 · 74	$M = 58'' \cdot \infty$ $w = 16 \cdot 01$ $\frac{1}{w} = 0 \cdot 06$ $C = 65^{\circ} 33' 58'' \cdot \infty$

#### PRINCIPAL TRIANGULATION. OBSERVED ANGLES.

At VIII (	(Kanakotri)—(	(Continued).
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Angle between	<b>0°0′</b>	179° 59′	Circle re 79° 13′	eadings, 1 259° 13'	telescope 158° 25'	being se 838° 25'	et on V 237° 37′	(Bhádi) 57° 37'	816° 49′	186° 49′	M = Mean of Groups w = Relative Wøight C = Concluded Angle
VII (Rupihar) and X (Bhitala)	* h 47 · 08 h 46 · 78 h 47 · 60 47 · 15	n h 46 · 10 h 47 · 56 h 47 · 42 47 · 03	*	k 44 · 16 k 46 · 98 k 48 · 76 k 45 · 94 k 47 · 12 k 46 · 40 46 · 56	* * 45.62 * 44.86 * 48.02 * 44.38 * 45.90 * 45.76	<b>h</b> 47 · 32 <b>h</b> 45 · 58 <b>h</b> 47 · 24 46 · 71	* h 48 · 86 h 47 · 88 h 48 · 80 48 · 51	* * * * * * * * * * * * * *	k 48 · 38 k 46 · 02 k 46 · 28 k 46 · 78 46 · 87	* * 47·38 * 46·78 * 47·04 47·07	$M = 46'' \cdot 96$ $w = 14 \cdot 17$ $\frac{1}{w} = 0 \cdot 07$ $C = 71^{\circ} 47' 46'' \cdot 93$

At IX (Mangtor)

January 1877; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	Circle readings, telescope being set on XI (Narhar) 0°1′ 180°1′ 79°12′ 259°12′ 158°24′ 338°24′ 237°37′ 57°37′ 816°49′ 186°49′	M = Mean of Groups $\omega$ = Relative Weight C = Concluded Angle
XI (Narhar) and XII (Thakur)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$M = 17'' \cdot 85$ $w = 11 \cdot 74$ $\frac{1}{w} = 0 \cdot 09$
	19.19 17.50 18.42 17.11 16.50 17.73 18.34 17.15 18.16 18.43	$C = 49^{\circ} 41' 17'' \cdot 86$
XII (Thakur) and X (Bhitala)	$\begin{array}{c} \begin{array}{c} \begin{array}{c} \lambda \ 35 \cdot 88 \ h \ 33 \cdot 40 \ h \ 33 \cdot 10 \ l \ 32 \cdot 60 \ l \ 33 \cdot 12 \ l \ 33 \cdot 18 \ h \ 33 \cdot 66 \ h \ 33 \cdot 18 \ l \ 33 \cdot 60 \ l \ 33 \cdot 30 \\ h \ 32 \cdot 88 \ h \ 34 \cdot 74 \ h \ 32 \cdot 76 \ l \ 33 \cdot 78 \ l \ 35 \cdot 38 \ l \ 35 \cdot 58 \ h \ 33 \cdot 00 \ l \ 33 \cdot 70 \ l \ 36 \cdot 76 \ l \ 32 \cdot 56 \\ h \ 32 \cdot 70 \ h \ 34 \cdot 68 \ h \ 33 \cdot 42 \ l \ 33 \cdot 00 \ l \ 33 \cdot 56 \ l \ 34 \cdot 28 \ h \ 33 \cdot 34 \ l \ 35 \cdot 50 \ l \ 33 \cdot 64 \\ h \ 34 \cdot 72 \ h \ 33 \cdot 20 \ l \ 34 \cdot 28 \ l \ 34 \cdot 38 \ l \ 33 \cdot 36 \ l \ 34 \cdot 58 \\ h \ 33 \cdot 34 \ h \ 33 \cdot 34 \ l \ 34 \cdot 58 \end{array}$	$M = 33'' \cdot 82$ $w = 20 \cdot 22$ $\frac{1}{w} = 0 \cdot 05$
	33 90 34 27 33 09 33 34 34 09 34 35 33 33 33 94 34 73 33 17	$C = 43^{\circ} 6' 33'' \cdot 84$
X (Bhitala) and VII (Rupihar)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$M = 5'' \cdot 28$ $w = 21 \cdot 84$ $\frac{1}{w} = 0 \cdot 05$
	5.96 5.23 5.40 5.23 4.28 5.04 5.13 5.31 5.96 4.99	$C = 57^{\circ} 15' 5'' 31$

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	At IX (Mangtor)—(Continued).	
Angle between	Circle readings, telescope being set on XI (Narhar) 0° 1' 180° 1' 79° 12' 259° 12' 158° 24' 338° 24' 237° 37' 57° 37' 316° 49' 136° 49'	M - Mean of Groups w - Belative Weight C - Concluded Angle
VII (Rupihar) and VI (Hatodan)	k 49.66       k 49.06       k 50.18       l 48.38       k 50.06       k 49.54       k 50.28       k 49.58       l 49.48       l 49.76         k 49.78       k 49.12       k 51.10       l 50.04       k 50.18       k 49.34       k 49.20       k 50.38       l 49.04       l 49.52         k 48.82       k 49.50       k 50.08       l 50.40       k 48.92       k 49.54       k 49.28       l 47.92       l 49.24       l 49.68         l 48.46       k 49.76       l 50.14       k 49.76       l 50.14       k 49.66       k 49.76       l 50.14	$M = 49'' \cdot 57$ $w = 43 \cdot 47$ $\frac{1}{w} = 0 \cdot 02$ $C = 55^{\circ} 23' \cdot 49'' \cdot 50$
	<u> </u>	L
	At X (Bhitala)	
January 1877;	observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theo	odolite No. 2.
Angle between	Circle readings, telescope being set on VIII (Kanakotri) 0° 1′ 180° 1′ 79° 13′ 259° 13′ 158° 24′ 838° 24′ 287° 36′ 57° 36′ 316° 49′ 136° 49′	M - Mean of Groups w - Relative Weight C - Concluded Angle
VIII (Kanakotri) and VII (Rupihar)	h 23.08 h 23.46 h 24.16 h 23.96 l 22.90 h 23.02 h 23.18 h 23.22 h 23.36 h 23.20 h 24.16 h 22.76 h 23.48 h 22.10 l 22.74 h 22.08 h 22.20 h 22.00 h 23.00 h 23.20 h 24.46 h 22.28 h 22.42 h 22.76 l 22.30 h 21.96 h 22.40 h 22.80 h 23.22 h 23.02 d 22.56	$M = 22'' \cdot 96$ $w = 34 \cdot 76$ $\frac{1}{w} = 0 \cdot 03$
	23.90 22.77 23.35 22.94 22.65 22.35 22.59 22.67 23.19 23.14	$C = 59^{\circ} 28' 22'' \cdot 9$
VII (Rupihar) and IX (Mangtor)	k 21 · 92 k 20 · 74 l 24 · 12 k 20 · 58 l 21 · 44 k 21 · 86 k 21 · 30 k 21 · 02 k 22 · 84 k 20 · 68 k 19 · 46 k 21 · 18 l 22 · 00 l 21 · 36 l 21 · 14 k 20 · 76 k 21 · 62 k 22 · 32 k 22 · 48 k 22 · 12 k 19 · 14 k 22 · 22 l 21 · 52 l 21 · 62 l 21 · 10 k 21 · 54 k 22 · 02 k 20 · 92 k 21 · 60 k 21 · 12 k 20 · 54 d 21 · 11 l 21 · 28 l 22 · 34 l 21 · 72 d 22 · 87	$M = 21'' \cdot 43$ $w = 21 \cdot 22$ $\frac{1}{w} = 0 \cdot 05$ $C = 64^{\circ} 30' 21'' \cdot 44$
	20.27 21.31 22.26 21.19 21.23 21.39 21.65 21.42 22.31 21.31	
IX (Mangtor) and XI (Narhar)	k 42 · 48 k 39 · 88 l 40 · 38 k 42 · 38 l 40 · 72 k 39 · 38 k 40 · 36 k 39 · 64 l 39 · 78 k 39 · 64 k 41 · 64 k 39 · 16 l 39 · 74 l 40 · 06 l 40 · 26 k 40 · 32 k 40 · 20 k 40 · 16 l 39 · 62 k 40 · 32 k 39 · 00 k 38 · 76 l 40 · 10 l 41 · 24 l 39 · 44 k 41 · 28 k 39 · 98 k 40 · 44 l 40 · 54 l 39 · 54 k 40 · 04 d 40 · 78 l 40 · 26 k 40 · 18 d 40 · 37	$M = 40'' \cdot 17$ $w = 28 \cdot 41$ $\frac{1}{w} = 0 \cdot 04$
	40.62 39.27 40.25 40.99 40.14 40.33 40.18 40.08 39.98 39.83	$C = 41^{\circ} 12' 40'' \cdot 1$

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#### PRINCIPAL TRIANGULATION. OBSERVED ANGLES.

At X (Bhitala)—(Continued).

Angle between	0° 1'	Cin 180° 1′	cle read 79° 13'	ings, tele 259° 13′	escope be 158° 24'	ing set o 338° 24'	n VIII ( 237° 36'	(Kanakot 57° 36'	tri) 316° 49′	136° 49′	M - Mean of Groups w - Relative Weight C - Concluded Angle
XI (Narhar) and XII (Thakur)	h 31 · 22 h 29 · 56 h 30 · 86 d 30 · 25	ћ 30°70 ћ 31°18 ћ 29°28	" l 29.00 l 29.68 l 30.60	n 29·26 230·52 29·64 230·10	" l 29°72 l 30°12 l 30°26	к 130°40 131°62 129°92	n h 28 · 66 h 30 · 68 h 29 · 90 h 29 · 26	n h 30 · 40 h 30 · 20 h 30 · 06	" 1 29·82 1 30·52 1 30·08	* h 29·56 h 29·68 l 29·74	$M = 30'' \cdot 08$ $w = 46 \cdot 85$ $\frac{1}{w} = 0 \cdot 02$
	30.42	30.39	<b>2</b> 9·76	<b>2</b> 9·88	30.03	<b>3</b> 0.65	<b>2</b> 9·63	30.22	30.14	<b>29</b> .66	$C = 41^{\circ} 19' 30'' \cdot 0$

## At XI (Narhar)

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January 1877; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	Circle readings, telescope being set on XIII (Jeysulmere) 0°0′ 180°0′ 79°12′ 259°12′ 158°25′ 338°25′ 237°36′ 57°37′ 316°49′ 136°49′	M - Mean of Groups w - Relative Weight C - Concluded Angle
XIII (Jeysulmere) and XIV (Malar)	n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n	$M = 47'' \cdot 05$ $w = 12 \cdot 80$ $\frac{1}{w} = 0 \cdot 08$
	48.29 47.47 46.57 47.10 48.24 46.64 45.93 47.12 46.83 46.33	$C = 46^{\circ} 38' 47'' \cdot 04$
XIV (Malar) and	k61.88 k61.68 k60.12 l 59.58 l 62.06 k61.42 k62.00 k60.26 k61.48 k60.18 k62.12 k59.96 l 61.40 l 60.34 l 60.10 k60.58 k60.18 k59.76 k60.74 l 60.98 k60.44 k61.34 l 61.96 l 59.64 l 60.32 k61.06 k62.26 k61.00 k61.36 l 61.26 k61.06	$M = 60'' \cdot 91$ $w = 26 \cdot 53$ $\frac{1}{w} = 0 \cdot 04$
	61.48 60.99 61.16 59.85 60.83 61.02 61.38 60.34 61.19 60.81	$C = 60^{\circ} 41' 0'' \cdot 90$
XII (Thakur) and X (Bhitala)	h 22 · 32 h 23 · 28 h 23 · 26 l 22 · 82 l 22 · 12 h 22 · 40 h 23 · 92 h 22 · 38 h 22 · 36 l 22 · 54 h 22 · 18 h 20 · 86 l 22 · 28 l 22 · 76 l 21 · 72 h 21 · 58 h 22 · 82 h 21 · 02 h 21 · 60 l 22 · 78 h 22 · 00 h 21 · 88 l 22 · 68 l 22 · 36 l 21 · 98 h 22 · 58 h 21 · 88 h 21 · 62 h 22 · 20 l 22 · 04 h 21 · 78 h 22 · 06	$M = 22'' \cdot 25$ $w = 46 \cdot 40$ $\frac{1}{w} = 0 \cdot 02$
	22.17 21.95 23.74 23.65 21.94 23.19 23.67 21.67 23.05 23.45	$C = 36^{\circ} 15' 22'' \cdot 25$
X (Bhitala) and IX (Mangtor)	h 29.56 h 27.88 l 29.72 l 30.74 l 29.52 h 29.58 h 30.14 h 28.90 h 29.72 l 29.00 h 28.64 h 28.52 l 27.96 l 29.38 l 29.88 h 29.86 h 29.94 h 30.38 h 29.24 l 28.62 h 29.64 h 28.30 l 29.42 l 29.16 l 28.56 h 29.82 h 29.24 h 29.92 h 30.54 l 29.28	$M = 29'' \cdot 37$ $w = 28 \cdot 60$ $\frac{1}{w} = 0 \cdot 03$
	<b>29</b> <sup>-</sup> 20 <b>20</b> <sup>-</sup> 23 <b>29</b> <sup>-</sup> 03 <b>29</b> <sup>-</sup> 70 <b>29</b> <sup>-</sup> 32 <b>29</b> <sup>-</sup> 75 <b>29</b> <sup>-</sup> 77 <b>29</b> <sup>-</sup> 73 <b>29</b> <sup>-</sup> 83 <b>28</b> <sup>-</sup> 97	$C = 45^{\circ} 59' 29''' 37$

### At XII (Thakur)

January 1877; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	133° 1′	Ciro 813° 1'	cle readi 212° 13′	ngs, tele 32°13′	291° 24'	ing set of 111°24'	n X (Bh 10°37'	it <b>ala)</b> 190° 37'	89° 48'	269° 48′	M = Mean of Groups w = Relative Weight C = Concluded Angle
X (Bhitala) and IX (Mangtor)	* \$ 17.32 \$ 16.50 \$ 16.32 16.71	" h 18 · 62 h 15 · 88 h 17 · 12 h 17 · 30 17 · 23	" l 19.96 l 16.68 l 18.04 l 18.82 l 18.02 h 15.38 h 17.96 h 18.18 17.88	" h 18 · 02 h 17 · 84 h 15 · 86 h 17 · 38 17 · 28	* h 15.92 l 16.26 l 17.78 16.65	* \$ 17.00 \$ 16.60 \$ 17.50 17.03	" l 18.04 l 16.00 l 17.20 l 18.46 17.42	* l 18.36 l l 15.72 l l 16.82 l l 15.90	16·34 16·32 15·48	16.61	$M = 16'' \cdot 96$ $w = 20 \cdot 37$ $\frac{1}{w} = 0 \cdot 05$ $C = 54^{\circ} 21' \cdot 17'' \cdot 01$
IX (Mangtor) and XI (Narhar)	h 51 · 28 h 52 · 52 h 54 · 44 h 51 · 64 h 52 · 52 52 · 48	h 52 · 38 h 53 · 14 h 52 · 18 h 54 · 08	l 48.82 l 54.56 l 54.72 l 49.92 h 49.54 h 49.14 51.12	h 53 °62 h 51 °38 l 52 °36 l 52 °42 52 °44	k 52°76 l 53°20 l 51°86	h 52.54 h 52.02 h 53.12 52.56	l 50°98 l 51°92 l 51°68	l 50.26 l l 52.70 l l 52.36 l l 51.76	51°94 51°72 52°42 52°03	l 50°94 l 50°78 l 51°28	$M = 52^{"} \cdot 05$ $w = 11 \cdot 74$ $\frac{1}{w} = 0 \cdot 09$ $C = 48^{\circ} 3' 52^{"} \cdot 04$
XI (Narhar) and XIV (Malar)	k 26 · 26 k 29 · 12 k 28 · 22 k 29 · 60 k 27 · 64 28 · 17	h 30.56 h 28.38 h 29.22 h 26.60 h 30.14 28.98	l 31 · 30 l 27 · 36 l 26 · 44 l 29 · 66 h 29 · 14 h 29 · 78 28 · 95	h 29°20 h 30°54 l 28°62 l 29°74 29°53	h 29°42 l 27°74 l 28°74 28°63	h 27.04 h 27.52 h 27.00 27.19	28.34 27.64 27.64 27.87	26.80	28.02 27.48 28.96 28.15	29.26 28.32 28.54 28.71	$M = 28^{"} \cdot 30$ $w = 10 \cdot 16$ $\frac{1}{w} = 0 \cdot 10$ $C = 67^{\circ} 31' 28^{"} \cdot 32$
XIV (Malar) and XV (Badhor)	k 27.86 k 27.06 k 25.72 k 23.76 k 26.48 k 27.14	h 27 · 20 h 26 · 16 h 27 · 90 27 · 09	l 28.90 l 29.80 l 26.64 l 28.58 h 25.84 h 26.06 h 25.08 27.27	k 28 · 24 l 26 · 66 l 26 · 66 l 27 · 88	k 25.04 k 25.28 k 26.30 25.54	Å 25 · 84 Å 24 · 78 Å 24 · 74	25.85	l 25 · 50 l l 28 · 34 l l 27 · 60 l l 27 · 80	25°10 26°34 25°66 25°70	27.46 26.32 26.83	$M = 26^{w} \cdot 64$ $w = 9 \cdot 48$ $\frac{1}{w} = 0 \cdot 11$ $C = 57^{\circ} 3' 26^{w} \cdot 65$
At XIII (Jeysulmere) January 1877; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.											
Angle between	<b>232°</b> 17′	C 52° 17′	ircle rea 811°29'	dings, te 131° 28′	lescope l 80°41'	0eing set	on XVI 109° 52'	(Ramsar) 289° 52′ 1	189° 5′	9° 5′	M - Mean of Groups w - Relative Weight C - Concluded Angle
XVI (Ramsar) and XIV (Malar)	* h 24.66 h 24.10 h 26.50 h 26.76 	* h 27·34 h 26·30 h 26·50 26·71	" h 27 · 70 h 26 · 92 h 26 · 96 27 · 19	* \$ 26.16 \$ 27.98 \$ 28.16 27.43	* \$ 26.74 \$ 26.02 \$ 26.88 26.55	* \$ 25.80 \$ 26.12 \$ 26.64 26.19	n h 26 ° 08 h 28 ° 94 h 25 ° 94 h 26 ° 20 h 26 ° 62 26 ° 76	" h 26.84 h h 27.10 h h 25.88 h h 26.61	24 · 16 25 · 74 25 · 74 25 · 42 25 · 26	* h 27 · 00 h 28 · 84 h 26 · 68 h 27 · 48 27 · 50	$M = 26'' \cdot 57$ $w = 13 \cdot 62$ $\frac{1}{w} = 0 \cdot 07$ $C = 61^{\circ} 11' 26'' \cdot 56$

	At XIII (Jeysulmere)—(Continued).	,
Angle between	Circle readings, telescope being set on XVI (Ramsar) 232° 17′ 52° 17′ 811° 29′ 131° 28′ 30° 41′ 210° 40′ 109° 52′ 289° 52′ 189° 5′ 9° 5′	M - Mean of Gro w - Relative Wei C = Concluded Ar
XIV (Malar) and XI (Narhar)	h 20.40 h 21.12 h 21.30 h 22.74 h 20.88 h 20.50 h 19.50 h 21.40 h 20.06 h 21.26 h 21.76 h 21.40 h 21.18 h 19.88 h 20.96 h 20.20 h 19.14 h 20.86 h 20.16 h 20.08 h 20.66 h 21.66 h 20.64 h 20.56 h 20.18 h 20.44 h 19.66 h 21.44 h 21.30 h 21.06 h 20.88	$M = 20'' \cdot 74$ $w = 25 \cdot 13$ $\frac{1}{w} = 0 \cdot 04$
	20.94 21.39 21.04 21.03 20.67 20.38 19.43 21.23 20.51 20.80	$C = 66^{\circ} 32' 20$
	At XIV (Malar)	<u> </u>
January 1877;	observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theod	olite No. 2.
Angle between	Circle readings, telescope being set on XVI (Ramsar) 0°1′ 180°1′ 79°13′ 259°13′ 158°25′ 338°25′ 237°36′ 57°36′ 316°48′ 136°48′	M = Mean of Gr w = Relative Wo C = Concluded A
XVI (Ramsar) and XVII (Sinaba)	h 31 · 60 h 32 · 00 h 29 · 34 l 29 · 70 h 31 · 06 h 30 · 58 h 31 · 06 h 32 · 30 h 31 · 70 h 31 · 58 h 30 · 68 l 33 · 76 l 28 · 32 l 31 · 74 h 31 · 76 l 31 · 08 h 31 · 36 h 30 · 12 l 31 · 62 h 31 · 18 h 32 · 04 l 34 · 60 l 31 · 38 h 30 · 56 l 31 · 44 l 32 · 86 h 32 · 20 h 30 · 74 l 32 · 16 h 31 · 60 h 32 · 60 l 31 · 46 l 33 · 12 h 31 · 76 l 32 · 16 h 32 · 16 h 32 · 74 l 30 · 30 l 31 · 34	$M = 31'' \cdot 55$ $w = 16 \cdot 77$ $\frac{1}{w} = 0 \cdot 06$
	31.23 32.01 30.63 30.04 31.42 31.67 31.24 31.33 31.83 31.45	$C = 56^{\circ} 8'31$
XVII (Sinaba) and XV (Badhor)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$M = 50'' \cdot 22$ $w = 13 \cdot 97$ $\frac{1}{w} = 0 \cdot 07$
	50.13 48.48 20.21 20.22 20.04 20.62 20.33 20.62 20.66 20.03	$C = 64^{\circ} 1' 50^{\circ}$
XV (Badhor) and XII (Thebur)	k 34 · 98 k 33 · 42 l 34 · 82 l 34 · 88 k 33 · 42 k 34 · 64 k 34 · 94 k 33 · 90 k 34 · 52 k 34 · 44 k 34 · 80 l 35 · 22 l 34 · 42 l 33 · 18 k 33 · 64 l 35 · 62 k 35 · 10 k 34 · 18 k 33 · 74 k 34 · 02 k 33 · 96 l 33 · 64 l 34 · 16 k 35 · 28 l 34 · 72 l 33 · 48 k 33 · 94 k 34 · 60 l 34 · 42 k 33 · 38 k 35 · 72	$M = 34'' \cdot 35$ $w = 46 \cdot 22$ $\frac{1}{w} = 0 \cdot 02$
	34.28 34.09 34.47 34.77 33.93 34.28 34.66 34.23 34.23 33.95	$C = 62^{\circ}44'34$
XII (Thakur) and XI (Narhar)	h 31 · 48 h 32 · 26 l 33 · 90 l 31 · 74 h 33 · 04 l 32 · 00 h 31 · 80 h 31 · 70 h 32 · 44 h 30 · 84 h 31 · 52 l 33 · 38 l 32 · 44 l 33 · 94 h 31 · 60 l 32 · 30 h 32 · 60 h 31 · 26 h 32 · 32 h 31 · 92 h 32 · 30 l 31 · 08 l 32 · 52 h 31 · 62 l 32 · 32 l 34 · 26 h 32 · 30 h 31 · 96 l 32 · 22 h 32 · 22 l 30 · 34 h 32 · 24 h 31 · 56 h 32 · 30 h 31 · 96 l 32 · 22 h 32 · 22 l 30 · 34 h 32 · 24 h 31 · 56 h 30 · 12 l 32 · 28	$M = 32'' \cdot 13$ $w = 24 \cdot 73$ $\frac{1}{w} = 0 \cdot 04$
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At XIV (Malar)—(Continued).

Angle between	Circle readings, telescope being set on XVI (Ramsar) 0° 1′ 180° 1′ 79° 13′ 259° 13′ 158° 25′ 338° 25′ 237° 36′ 57° 36′ 316° 48′ 136° 48′	M = Mean of Groups w = Relative Weight C = Concluded Angle
XI (Narhar) and XIII (Jeysulmere)	k       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x       x	$M = 52'' \cdot 68$ $w = 18 \cdot 32$ $\frac{1}{w} = 0 \cdot 05$ $C = 66^{\circ} 48' 52'' \cdot 68$
XIII (Jeysulmere) and XVI (Ramsar)	k 36 · 74 k 40 · 06 k 38 · 46 l 38 · 28 k 37 · 58 l 38 · 12 k 37 · 56 k 38 · 04 k 38 · 28 k 38 · 36 k 37 · 16 l 38 · 48 k 39 · 76 k 37 · 98 k 37 · 14 l 38 · 22 k 37 · 92 k 38 · 42 k 38 · 84 k 39 · 14 k 37 · 68 l 38 · 40 l 37 · 94 k 38 · 36 l 37 · 68 k 37 · 90 k 37 · 96 k 38 · 46 l 37 · 70 k 38 · 10 37 · 19 38 · 98 38 · 72 38 · 21 37 · 47 38 · 08 37 · 81 38 · 31 38 · 27 38 · 53	$M = 38^{"} \cdot 16$ $w = 27 \cdot 80$ $\frac{1}{w} = 0 \cdot 04$ $C = 58^{\circ} 28' 38^{"} \cdot 16$
XVI (Ramsar) and R. M.	$\begin{array}{c} k  42 \cdot 68  k  40 \cdot 74  k  41 \cdot 50  l  40 \cdot 76  k  43 \cdot 04  l  40 \cdot 70  k  41 \cdot 58  l  42 \cdot 36  k  42 \cdot 04  k  41 \cdot 66 \\ k  42 \cdot 62  l  42 \cdot 88  k  42 \cdot 36  l  42 \cdot 30  k  42 \cdot 46  l  41 \cdot 70  k  42 \cdot 32  l  41 \cdot 36  k  41 \cdot 96  k  43 \cdot 04 \\ k  45 \cdot 00  l  42 \cdot 70  l  42 \cdot 26  l  42 \cdot 58  l  42 \cdot 50  l  42 \cdot 32  k  41 \cdot 86  l  41 \cdot 52  l  42 \cdot 48  k  41 \cdot 66 \\ k  44 \cdot 82  l  42 \cdot 88 \end{array}$	$M = 42'' \cdot 22$ $w = 18 \cdot 48$ $\frac{1}{w} = 0 \cdot 05$ $C = 29^{\circ} 14' 42'' \cdot 23$

## At XV (Badhor)

February 1877; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	Circle readings, telescope being set on XII (Thakur) 0°0′ 180°0′ 79°12′ 259°12′ 158°25′ 338°25′ 237°37′ 57°37′ 316°48′ 136°48′	M = Mean of Groups so = Relative Weight C = Concluded Angle
XII (Thakur) and XIV (Malar)	h 59.84 h 61.16 h 59.34 h 59.60 l 60.32 l 60.72 l 60.32 l 59.06 h 60.04 h 58.96         h 61.90 h 60.38 h 60.00 l 59.94 l 60.62 l 60.18 l 61.24 h 59.64 h 60.82 h 59.40         h 61.12 h 60.46 h 60.30 l 59.32 l 59.90 l 60.36 l 60.02 h 60.32 h 60.68 h 60.18         h 61.18         61.01 60.67 59.88 59.62 60.28 60.42 60.53 59.67 60.51 59.51	$M = 60^{\circ} \cdot 21$ $w = 30 \cdot 50$ $\frac{1}{w} = 0 \cdot 03$ $C = 60^{\circ} 12'  0^{\circ} \cdot 22$
XIV (Malar) and XVII (Sinaba)	$ \begin{array}{c} k \ 57 \ 76 \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \ \$	$M = 56'' \cdot 45$ $w = 31 \cdot 68$ $\frac{1}{w} = 0 \cdot 03$ $C = 55^{\circ} 49' 56'' \cdot 45$

Norg.-R.M. denotes Referring Mark.

At XVI (Ramsar)

February 1877; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

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Angle between	Circle readings, telescope being set on XVIII (Potanawári) 0°0′ 180°0′ 79°12′ 259°12′ 158°24′ 338°24′ 237°37′ 57°36′ 316°49′ 136°48′	M - Mean of Groups $\omega$ = Relative Weight C = Concluded Angle
XVIII (Potanawári) and XIX (Joganali)	<i>k</i> 60·10 <i>k</i> 60·04 <i>k</i> 59·56 <i>l</i> 60·20 <i>l</i> 60·32 <i>k</i> 60·88 <i>k</i> 61·00 <i>k</i> 58·54 <i>k</i> 60·10 <i>k</i> 60·06 <i>k</i> 60·08 <i>k</i> 59·96 <i>k</i> 61·16 <i>l</i> 58·70 <i>l</i> 59·22 <i>k</i> 60·68 <i>k</i> 61·00 <i>k</i> 60·78 <i>l</i> 60·36 <i>k</i> 60·84 <i>k</i> 60·86 <i>k</i> 60·88 <i>l</i> 59·28 <i>l</i> 60·12 <i>k</i> 60·32 <i>k</i> 61·58 <i>k</i> 61·22 <i>k</i> 61·54 <i>l</i> 60·32 <i>k</i> 59·36 <i>k</i> 60·92	$M = 60'' \cdot 32$ $w = 30 \cdot 60$ $\frac{1}{w} = 0 \cdot 03$
	60.35 60.29 60.00 59.67 59.95 61.05 61.07 60.45 60.26 60.09	$C = 45^{\circ} 32^{\circ} 0^{\prime\prime} \cdot 32$
XIX (Joganali) and XVII (Sinaba)	$h_{26} \cdot 80 \ h_{25} \cdot 94 \ h_{24} \cdot 14 \ l_{23} \cdot 86 \ l_{25} \cdot 20 \ h_{24} \cdot 36 \ h_{23} \cdot 90 \ h_{24} \cdot 72 \ l_{24} \cdot 60 \ h_{25} \cdot 46 \ h_{26} \cdot 52 \ h_{26} \cdot 22 \ h_{25} \cdot 50 \ l_{25} \cdot 98 \ l_{24} \cdot 78 \ h_{25} \cdot 42 \ h_{24} \cdot 84 \ h_{24} \cdot 42 \ h_{23} \cdot 56 \ h_{24} \cdot 28 \ h_{26} \cdot 44 \ h_{25} \cdot 66 \ l_{25} \cdot 70 \ l_{24} \cdot 46 \ h_{25} \cdot 42 \ h_{25} \cdot 80 \ h_{24} \cdot 30 \ h_{24} \cdot 94 \ h_{24} \cdot 40 \ h_{24} \cdot 10 \ l_{25} \cdot 40 \ h_{24} \cdot 34 \ h_{25} \cdot 14$	$M = 25'' \cdot 08$ $w = 16 \cdot 85$ $\frac{1}{w} = 0 \cdot 06$
	26.59 25.94 25.11 24.93 25.13 25.19 24.34 24.81 24.19 24.61	$C = 77^{\circ} 11' 25'' \cdot 08$
XVII (Sinaba) and XIV (Malar)	k 26 · 90 k 27 · 12 k 27 · 10 l 27 · 36 l 28 · 84 k 28 · 84 k 26 · 70 k 28 · 24 l 27 · 18 k 27 · 62 k 27 · 72 k 27 · 34 k 27 · 50 l 29 · 22 l 28 · 16 k 27 · 80 k 28 · 82 k 26 · 32 k 27 · 54 k 27 · 44 k 27 · 34 k 27 · 42 k 27 · 62 l 28 · 02 k 27 · 16 k 27 · 44 k 27 · 50 k 28 · 54 k 28 · 00 k 27 · 50 k 27 · 82 k 29 · 16	$M = 27'' \cdot 72$ $w = 41 \cdot 10$ $\frac{1}{w} = 0 \cdot 02$
	27.32 27.29 27.41 28.20 28.05 28.03 27.71 28.07 27.57 27.52	$C = 66^{\circ} 30' 27'' \cdot 72$
XIV (Malar) and XIII (Invenimenc)	h 55 · 26 h 56 · 46 h 55 · 74 l 57 · 22 l 57 · 14 h 55 · 44 h 55 · 30 h 56 · 64 h 56 · 10 h 56 · 80 h 55 · 58 h 55 · 76 h 56 · 24 l 56 · 94 h 56 · 48 h 56 · 54 h 54 · 60 h 56 · 00 l 56 · 60 h 55 · 28 h 55 · 08 h 56 · 46 h 56 · 04 l 55 · 42 h 55 · 66 h 55 · 92 h 55 · 56 h 54 · 94 l 55 · 80 h 56 · 02	$M = 55'' \cdot 97$ $w = 35 \cdot 70$ $\frac{1}{w} = 0 \cdot 03$
AIII (Jeysuimere)	55.31 56.23 56.01 56.53 56.43 55.97 55.15 55.86 56.17 56.03	$C = 60^{\circ} 19' 55'' \cdot 97$

#### At XVII (Sinaba)

February 1877; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	0° 0′	( 180° 0′	Circle rea 79°12'	adings, t 259°12'	elescope 158° 24′	being se 838°24'	t on XV 237° 36′	(Badhor 57° 36'	c) 316° 49′	136° 49′	M - Mean of Groups w = Relative Weight C - Concluded Angle
XV (Badhor) and XIV (Malar)	" l 14·26 l 15·50 l 14·66	" l 14·32 l 14·56 l 15·16	" l 13·42 h 14·66 h 14·60	" h 12 · 46 h 14 · 14 h 13 · 94	" h 13°76 h 13°88 h 14°22	" h 13.88 h 13.62 h 14.08	" l 14·52 l 13·22 l 14·08	" l 13·74 l 15·76 l 13·46 l 14·14	" 14 · 18 14 · 40 13 · 58	" 1 15 · 66 h 14 · 18 h 13 · 98	$M = 14'' \cdot 19$ $w = 35 \cdot 98$ $\frac{1}{w} = 0 \cdot 03$
	14.81	14.68	14.33	13.21	13.95	13.86	13.94	14.38	14.02	14.61	$C = 60^{\circ} 8' 14'' \cdot 19$

At XVII (Sinaba)-(Continued)

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Angle between	ሆ ወ	1 <b>80° 0′</b>	Circle re 79°12′	adings, t 259°12'	elescope 158° 24'	being set 338° 24'	on XV 237° 36'	(Badhor) 57° 36'	<b>816° 49</b> ′	136° 49′	M - Mean of Groups w - Relative Weight C - Concluded Angle
XIV (Malar) and XVI (Ramsar)	\$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	k 62 · 54 k 60 · 38 k 61 · 02 k 62 · 12 61 · 52	k 62 · 36 k 60 · 56 k 61 · 24 61 · 39	* \$ 60 · 82 \$ 62 · 46 \$ 62 · 00 61 · 76	k 63 · 40 k 61 · 44 k 62 · 96 62 · 60	* \$ 61.00 \$ 62.46 61.69	2 61 · 56 2 62 · 34 2 61 · 40 61 · 77	4 1 61 · 92 1 62 · 52 1 62 · 02 62 · 15	, 2 62 • 96 2 61 • 96 2 61 • 86 62 • 26	, 1 60°00 1 60°88 1 60°34 60°41	$M = 61'' \cdot 82$ $w = 17 \cdot 30$ $\frac{1}{w} = 0 \cdot 06$ $C = 57^{\circ} 21' \cdot 1'' \cdot 82$
XVI (Ramsar) and XIX (Joganali)	h 21 · 54 h 21 · 18 h 20 · 38 h 21 · 00	k 21 · 34 k 19 · 92 k 19 · 66 k 20 · 18	k 19°14 k 22°36 k 20°46 k 20°24	k 20.18 k 19.28 k 20.00	k 20.08 k 19.94 k 19.60	k 20.16 k 19.60 k 20.60	l 21 · 38 l 19 · 76 l 21 · 56	l 19 <sup>.</sup> 44 l 19 <sup>.</sup> 74 l 20 <sup>.</sup> 52	2 21 · 32 2 19 · 48 2 19 · 32	2 19.44 2 19.12 2 21.32 2 19.66	$M = 20'' \cdot 24$ $w = 28 \cdot 32$ $\frac{1}{w} = 0 \cdot 04$
XIX (Joganali) and XX (Kardo)	21.03 1.60.92 1.60.72 1.61.10	20.27 k 64.36 k 62.12 k 62.96 k 60.56 k 63.34 k 60.86	20.55 \$61.80 \$60.32 \$60.32	19°82 262°10 259°66 261°26	19.87 \$61.40 \$61.52 \$60.44	20°12 \$62°38 \$61°00 \$61°12	20°90 260°90 260°94 261°10	19°90 161°50 161°36 160°46	20°04 1 60°44 1 60°40 1 59°88	19°89 261°32 261°72 260°66	$C = 55^{\circ} 32' 20'' \cdot 25$ $M = 61'' \cdot 13$ $w = 20 \cdot 50$ $\frac{1}{w} = 0 \cdot 05$
	60.91	62 · 37	60.78	61.07	61·12	61.50	60·98	61.11	60.24	61.53	$C = 41^{\circ} 55' 1'' \cdot 16$
At XVIII (Potanawári)											

February 1877; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	Circle readings, telescope being set on XXI (Sanahu) 0° 1' 180° 1' 79° 12' 259° 12' 158° 24' 338° 24' 237° 36' 57° 36' 816° 49' 136° 49'	M = Mean of Groups w = Relative Weight C = Concluded Angle
XXI (Sanahu) and XIX (Joganali)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$M = 26'' \cdot 57$ $w = 6 \cdot 49$ $\frac{1}{w} = 0 \cdot 15$ $C = 54^{\circ} 43' 26'' \cdot 53$
XIX (Joganali) and XVI (Ramsar)	$\begin{array}{c} k 56 \cdot 62 \ h 58 \cdot 80 \ h 57 \cdot 04 \ l 57 \cdot 64 \ l 57 \cdot 98 \ l 58 \cdot \infty \ l 55 \cdot 06 \ h 57 \cdot 38 \ h 56 \cdot 78 \ h 57 \cdot 12 \\ h 56 \cdot 30 \ h 58 \cdot 80 \ h 56 \cdot 56 \ l 56 \cdot 94 \ l 57 \cdot 80 \ l 58 \cdot 02 \ l 54 \cdot 76 \ h 57 \cdot 80 \ h 56 \cdot 04 \ h 55 \cdot 64 \\ h 56 \cdot 70 \ h 56 \cdot 94 \ h 57 \cdot 66 \ l 57 \cdot 76 \ l 57 \cdot 94 \ l 56 \cdot 30 \ l 58 \cdot 30 \ h 56 \cdot 38 \ h 56 \cdot 04 \ h 55 \cdot 64 \\ h 56 \cdot 70 \ h 56 \cdot 86 \ l 57 \cdot 76 \ l 57 \cdot 94 \ l 56 \cdot 30 \ l 58 \cdot 30 \ h 56 \cdot 38 \ h 58 \cdot 12 \ h 57 \cdot 02 \\ h 56 \cdot 86 \ l 58 \cdot 02 \ $	$M = 57'' \cdot 13$ $w = 23 \cdot 82$ $\frac{1}{w} = 0 \cdot 04$ $C = 72^{\circ} 4' 57'' \cdot 12$

At XIX (Joganali)

February 1877; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	0° 1′	C 180° 1′	Circle rea 79° 13′	ding <b>s,</b> te 259°13′	lescope t 158° 24'	eing set 338° 24'	on XXI 237° 37'	(Sanahu 57° 37'	1) 316° 48'	136° 48′	M - Mean of Groups to = Relative Weight C = Concluded Angle
XXI (Sanahu) and XXII (Arrabhit)	<pre>h 5 · 28 h 1 · 42 h 2 · 92 h 2 · 48 h 3 · 68</pre>	h 2·38 l 4·02 l 2·56	" l 2.60 h 2.72 h 4.98 h 1.98	" h 2·14 h 1·78 h 2·46	" h 3.66 h 2.02 h 3.28	" h 2·94 h 3·52 h 2·04	" h 2·16 h 3·36 h 3·02	n 3.40 h 2.98 h 2.46	" h 2`42 h 2`60 h 2`92		$M = 2'' \cdot 82$ $w = 34 \cdot 39$ $\frac{1}{w} = 0 \cdot 03$
	3.16	2.99	3.07	2.13	3.99	2.83	2.85	2.95	2.65	2.61	$C = 57^{\circ} 5' 2'' \cdot 84$
XXII (Arrabhit) and XX (Kardo)	h 8.52 h 6.66 h 6.42 h 7.86 h 8.14	h 7.58 l 7.66 l 8.28	l 7.26 h 7.42 h 4.46 h 7.18	h 5.88 h 7.86 h 5.30 h 7.18	h 6.16 h 8.10 h 6.26	h 7.38 h 6.78 h 7.56	h 6.54 h 7.90 h 7.14	h 6·18 h 7·60 h 7·28	h 6.96 h 7.32 h 7.16	k 6.82 l 6.44 l 6.68	$M = 7'' \cdot 07$ $w = 29 \cdot 49$ $\frac{1}{w} = 0 \cdot 03$
	7.52	7.84	6.28	6.26	6.94	7 . 24	7.19	7·02	7 . 1 2	6.62	$C = 69^{\circ} 3' 7'' \cdot 07$
XX (Kardo) and XVII (Sinaba)	h 20.88 h 24.76 h 24.82 h 24.12 h 23.36	26 · 52 23 · 06 22 · 72 26 · 14 23 · 56	l 22.48 l 25.04 h 25.20 h 23.86	h 24 · 18 h 26 · 58 h 24 · 64 h 27 · 48 h 24 · 80	h 22 · 38 h 24 · 76 h 23 · 12 h 24 · 86	h 23°90 h 25°18 h 25°10	h 24 · 56 h 24 · 28 h 23 · 36	h 23 · 44 h 24 · 40 h 24 · 24	h 23 · 24 h 24 · 16 h 24 · 06	h22.82 h23.94 h23.68	$M = 24'' \cdot 16$ $w = 14 \cdot 40$ $\frac{1}{w} = 0 \cdot 07$
	23.29	24.40	24.12	25.24	23.78	24.73	24.07	24.03	23.82	23.48	$C = 51^{\circ} 36' 24'' \cdot 18$
XVII (Sinaba) and XVI (Ramsar)	h 17 · 36 h 15 · 12 h 15 · 30 h 16 · 44 h 16 · 16	k 15·86 17·08 14·26 15·06	l 15.56 l 16.54 h 16.08	h 16 · 42 h 16 · 22 h 16 · 80	h 16.80 h 15.92 h 17.18	h 14 · 84 h 16 · 74 h 15 · 82	h 17 · 28 h 15 · 24 h 16 · 02 h 16 · 22	h 16 · 06 h 15 · 78 h 15 · 42	h 16 · 30 h 15 · 34 h 17 · 40 h 15 · 48	h 16 · 54 h 15 · 64 l 15 · 94	$M = 16'' \cdot 07$ $w = 41 \cdot 75$ $\frac{1}{w} = 0 \cdot 02$
	16.08	15.22	16.06	16.48	16.63	15.80	16.19	15.22	16.13	16.04	$C = 47^{\circ} 16' 16'' \cdot 06$
XVI (Ramsar) and XVIII (Potanawári)	h 3°26 h 5°66 h 4°12 h 1°48 h 4°10	h 2.86 h 4.24 l 4.30 l 5.30	l 4.74 l 4.36 h 3.98	h 2.58 h 1.92 h 2.60	h 3°34 h 2°96 h 3°52	h 3.00 h 2.60 h 2.24	h 2.84 h 2.70 h 2.78	h 3°26 h 2°34 h 3°72	h 2°54 h 2°74 h 2°58	h 3°26 h 2°94 l 3°34	$M = 3'' \cdot 22$ $w = 16 \cdot 69$ $\frac{1}{w} = 0 \cdot 06$
	3.72	4 · 18	4 · 36	2 · 37	3 · 27	2.61	<b>2</b> .77	3.11	2.62	3.18	$C = 62^{\circ} 23' 3'' \cdot 23$
XVIII (Potanawári) and XXI (Sanahu)	h 4.52 h 4.38 h 4.64 h 5.04 h 8.06	h 4.12 h 3.84 h 6.22 h 5.30 h 7.82	l 5°14 l 5°76 h 5°86	h 6.98 h 7.48 h 6.10	h 5.86 h 6.14 h 5.66	k 5.64 k 4.78 k 5.36	h 6.08 h 7.38 h 7.30	h 6.78 h 6.36 h 6.62	k 6.70 k 7.64 k 6.94	h 6·26 h 6·98 h 7·66	$M = 6'' \cdot 20$ $w = 12 \cdot 54$ $\frac{1}{w} = 0 \cdot 08$
	5.33	5.46	5.29	6.85	5.89	5 · 26	6·9 <b>2</b>	6.29	7.09	6.92	$C = 72^{\circ}36' 6'' \cdot 18$

## At XX (Kardo)

February 1877; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	Circle readings, telescope being set on XVII (Sinaba) 0° 0' 180° 0' 79° 13' 259° 10' 158° 24' 338° 24' 237° 37' 57° 37' 316° 49' 136° 49'	M = Mean of Groups w = Relative Weight C = Concluded Angle
XVII (Sinaba) and XIX (Joganali)	$\begin{array}{c} \textbf{1} 35 \cdot 48 \ \textbf{1} 35 \cdot 86 \ \textbf{1} 35 \cdot 46 \ \textbf{1} 34 \cdot 26 \ \textbf{1} 34 \cdot 48 \ \textbf{1} 35 \cdot 64 \ \textbf{1} 37 \cdot 10 \ \textbf{1} 35 \cdot 72 \ \textbf{1} 37 \cdot 22 \ \textbf{1} 36 \cdot 36 \\ \textbf{1} 36 \cdot 46 \ \textbf{1} 35 \cdot 90 \ \textbf{1} 36 \cdot 52 \ \textbf{1} 35 \cdot 82 \ \textbf{1} 37 \cdot 12 \ \textbf{1} 36 \cdot 66 \ \textbf{1} 36 \cdot 88 \ \textbf{1} 36 \cdot 86 \ \textbf{1} 37 \cdot 58 \ \textbf{1} 37 \cdot 50 \\ \textbf{1} 35 \cdot 48 \ \textbf{1} 37 \cdot 34 \ \textbf{1} 36 \cdot 20 \ \textbf{1} 36 \cdot 02 \ \textbf{1} 36 \cdot 66 \ \textbf{1} 35 \cdot 58 \ \textbf{1} 34 \cdot 24 \ \textbf{1} 35 \cdot 30 \ \textbf{1} 37 \cdot 58 \ \textbf{1} 37 \cdot 02 \ \textbf{1} 35 \cdot 42 \\ \textbf{1} 38 \cdot 62 \ \textbf{1} 36 \cdot 30 \ \textbf{1} 35 \cdot 72 \\ \textbf{1} 37 \cdot 58 \\ \textbf{1} 35 \cdot 28 \end{array}$	$M = 36^{w} \cdot 21$ $w = 24 \cdot 45$ $\frac{1}{w} = 0 \cdot 04$ $C = 86^{\circ} 28' 36'' \cdot 21$
XIX (Joganali) and XXII (Arrabhit)	$\begin{array}{c} k \ 44^{\circ} 88 \ h \ 46^{\circ} 12 \ h \ 43^{\circ} 94 \ h \ 45^{\circ} 08 \ h \ 44^{\circ} 62 \ h \ 46^{\circ} 02 \ h \ 45^{\circ} 74 \ h \ 44^{\circ} 38 \ h \ 45^{\circ} 94 \ l \ 42^{\circ} 50 \\ h \ 45^{\circ} 58 \ h \ 46^{\circ} 32 \ h \ 45^{\circ} 60 \ h \ 43^{\circ} 36 \ h \ 44^{\circ} 64 \ h \ 45^{\circ} 22 \ h \ 45^{\circ} 06 \ h \ 45^{\circ} 50 \ l \ 46^{\circ} 36 \ l \ 45^{\circ} 14 \\ h \ 46^{\circ} 36 \ h \ 45^{\circ} 56 \ h \ 45^{\circ} 36 \ h \ 44^{\circ} 58 \ h \ 44^{\circ} 84 \ h \ 46^{\circ} 30 \ h \ 46^{\circ} 22 \ h \ 45^{\circ} 04 \ l \ 45^{\circ} 20 \ l \ 45^{\circ} 92 \\ l \ 45^{\circ} 78 \\ l \ 45^{\circ} 78 \\ l \ 45^{\circ} 42 \\ l \ 45^{\circ} 44^{\circ} 97 \\ l \ 45^{\circ} 83 \ \ 44^{\circ} 95 \\ \end{array}$	$M = 45'' \cdot 29$ $w = 21 \cdot 10$ $\frac{1}{w} = 0 \cdot 05$ $C = 56^{\circ} 58' 45'' \cdot 29$

### At XXI (Sanahu)

February and March 1877; observed by Captain M. W. Bogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	Circle readings, telescope being set on XXIII (Harnáo) 143° 6′ 823° 6′ 222° 20′ 42° 20′ 301° 31′ 121° 31′ 20° 43′ 200° 43′ 99° 55′ 279° 55′	M = Mean of Groups w = Relative Weight C = Concluded Angle
XXIII (Harnáo) and XXIV (Dhanono)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$M = 39'' \cdot 99$ $w = 11 \cdot 47$ $\frac{1}{w} = 0 \cdot 09$ $C = 53^{\circ} 51' 39'' \cdot 98$
XXIV (Dhanono) and XXII (Arrabhit)	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$M = 39'' \cdot 95$ $w = 22 \cdot 28$ $\frac{1}{w} = 0 \cdot 04$ $C = 45^{\circ} 32' 39'' \cdot 93$

	At XXI (Sanahu)—(Continued).						
Angle between	Circle readings, telescope being set on XXIII (Harnáo) 143°6′ 823°6′ 222°20′ 42°20′ 301°31′ 121°31′ 20°43′ 200°43′ 99°55′ 279°55′	M = Mean of Groups w = Relative Weight C = Concluded Angle					
XXII (Arrabhit) and XIX (Joganali)	k 44 · 72 k 46 · 16 k 45 · 70 l 48 · 06 k 46 · 10 k 46 · 06 k 46 · 64 k 45 · 64 k 46 · 40 k 46 · 16 k 46 · 02 k 46 · 72 l 45 · 58 k 46 · 04 k 45 · 86 k 45 · 88 k 45 · 64 k 45 · 52 k 46 · 18 k 46 · 44 k 46 · 16 k 46 · 72 l 47 · 86 k 47 · 34 k 47 · 10 k 46 · 82 k 46 · 10 k 45 · 92 k 45 · 96 k 45 · 66 k 46 · 28 l 48 · 22 k 45 · 56 k 47 · 40	$M = 46'' \cdot 29$ $w = 37 \cdot 88$ $\frac{1}{w} = 0 \cdot 03$ $C = 64^{\circ} 48' 46'' \cdot 30$					
	46.12 46.53 46.84 46.75 46.35 46.25 46.13 45.69 46.18 46.09						
XIX (Joganali) and XVIII (Potanawári)	k 27 · 60 k 27 · 82 k 27 · 96 l 27 · 86 k 27 · 52 k 27 · 30 k 28 · 30 k 29 · 50 k 28 · 50 k 28 · 60 k 28 · 68 k 27 · 76 l 28 · 34 k 28 · 96 k 28 · 36 k 27 · 70 k 27 · 64 k 28 · 86 k 28 · 60 k 28 · 72 k 27 · 66 k 28 · 82 l 29 · 98 k 28 · 44 k 28 · 84 k 28 · 54 k 28 · 62 k 29 · 42 k 28 · 02 k 27 · 52 k 28 · 26 l 29 · 18 k 28 · 00	$M = 28'' \cdot 37$ $w = 40 \cdot 90$ $\frac{1}{w} \pm 0 \cdot 02$					
	28.04 28.13 28.87 28.42 28.24 27.85 28.19 29.26 28.37 28.28	$C = 52^{\circ} 40' 28'' \cdot 36$					
February 1877;	At XXII (Arrabhit) observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theo Circle readings, telescope being set on XX (Kardo)	M - Mean of Groups - Relative Weight					
	0° 0′ 180° 0′ 79° 13′ 259° 13′ 158° 24′ 338° 24′ 237° 37′ 57° 37′ 316° 48′ 136° 48′	C = Concluded Angle					
XX (Kardo) and XIX (Joganali)	k 9.46 k 9.08 k 6.98 l 5.32 l 7.48 k 7.14 k 8.36 k 7.64 k 7.58 k 7.40 k 8.10 k 6.94 k 8.20 l 7.76 l 7.88 k 8.56 k 8.10 k 7.94 k 8.06 k 7.80 k 6.94 k 7.32 k 8.06 l 7.72 l 8.48 k 7.28 k 7.24 k 7.56 k 7.4z k 7.38 k 7.94 l 6.44	$M = \gamma^{w} \cdot 69$ $w = 38 \cdot 34$ $\frac{1}{w} = 0 \cdot 03$					
	8.11 7.78 7.75 6.81 7.95 7.66 7.90 7.71 7.69 7.53	$C = 53^{\circ}58' 7'' \cdot 68$					
XIX (Joganali) and XXI (Sanahu)	h 8.74 h11.08 h12.42 l 11.08 l 11.00 h12.58 h10.96 h12.16 h13.56 h12.28 h11.72 h12.64 h10.82 l 11.00 l 12.10 h13.00 h13.66 h14.36 h11.34 h11.54 h13.22 h11.14 h11.66 l 12.14 l 12.46 h11.36 h10.76 h11.12 h12.84 h12.38 h14.24 h13.50 h11.54 h12.42 h12.72 h12.94 h12.52	$M = 11^{w} \cdot 99$ $w = 23 \cdot 15$ $\frac{1}{w} = 0 \cdot 04$					
	12.30 11.62 11.63 11.41 11.85 12.31 PI.89 12.24 12.54 12.07	$U = 55^{\circ} 0' 12'' \cdot 03$					
XXI (Sanahu) and XXIII (Harnáo)	h 29.72 h 28.56 h 27.14 l 28.04 l 26.88 h 28.56 h 27.80 h 27.46 h 29.18 h 27.80 h 26.80 h 27.96 h 27.86 l 28.30 l 27.60 h 28.32 h 28.92 h 29.40 h 28.32 h 27.00 h 28.94 h 27.50 h 28.46 l 29.22 l 26.58 h 29.60 h 28.86 h 27.96 h 28.94 h 27.52 h 28.40 h 27.48	$M = 28'' \cdot 16$ $w = 20 \cdot 66$ $\frac{1}{w} = 0 \cdot 05$					
······································	28.47 27.87 27.82 28.52 27.02 28.83 28.53 28.27 28.81 27.44	$C = 42^{\circ} 21' 28'' \cdot 16$					

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	At XXII (Arrabhit)—(Continued).	
Angle between	Circle readings, telescope being set on XX (Kardo) 0° 0′ 180° 0′ 79° 13′ 259° 13′ 158° 24′ 338° 24′ 237° 37′ 57° 37′ 316° 48′ 136° 48′	M = Mean of Groups w = Relative Weight C = Concluded Angle
XXIII (Harnáo) and XXIV (Dhanono)	k 25 · 42 k 23 · 08 k 25 · 48 l 25 · 32 l 23 · 86 k 24 · 14 k 25 · 28 k 24 · 74 k 25 · 84 k 24 · 16 k 26 · 84 k 23 · 00 k 24 · 50 l 23 · 40 l 24 · 84 k 23 · 38 k 23 · 68 k 25 · 90 k 23 · 38 k 23 · 38 k 23 · 74 k 24 · 18 k 23 · 44 l 23 · 42 l 23 · 38 k 24 · 54 k 26 · 04 k 24 · 84 k 24 · 24 k 23 · 56 k 23 · 76 l 23 · 96 k 23 · 70 k 22 · 88	$M = 24^{w} \cdot 24$ $w = 20 \cdot 65$ $\frac{1}{w} = 0 \cdot 05$
	24.53 23.42 24.35 24.05 24.03 24.02 24.67 25.16 24.49 23.70	$C = 54^{\circ} 26' 24'' \cdot 25$
March 1877; o	At XXIII (Harnáo) bserved by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theo	dolite No. 2.
Angle between	Circle readings, telescope being set on XXV (Bándri) 0°1′ 180°1′ 79°12′ 259°12′ 158°24′ 338°24′ 237°36′ 57°37′ 316°48′ 136°48′	M = Mean of Groups w = Relative Weight C = Concluded Angle
XXV (Bándri) and XXVI (Báviláhu)	h 57°52 h 54°62 h 56°12 h 52°62 l 53°62 h 53°90 h 53°68 h 52°64 h 54°46 h 54°70 h 56°14 h 53°56 h 54°02 h 52°82 h 53°48 h 54°04 h 53°90 h 53°02 h 54°42 h 53°02 h 56°20 h 52°34 h 55°22 h 54°42 h 54°84 h 54°42 h 52°52 h 53°16 h 53°82 h 53°86 h 54°88 h 53°54 h 55°02 h 55°28	$M = 54^{w} \cdot 04$ $w = 10 \cdot 34$ $\frac{1}{w} = 0 \cdot 10$
	56.00 23.25 25.09 23.29 23.98 24.12 23.37 22.94 24.23 23.86	$C = 59^{\circ} 41' 54'' \cdot 66$
XXVI (Ráviláhu) and XXIV (Dhanono)	h 46 · 46 h 48 · 04 h 46 · 90 h 45 · 36 l 47 · 54 h 46 · 80 h 45 · 86 h 44 · 24 h 46 · 84 h 45 · 24 h 47 · 60 h 47 · 32 h 47 · 16 h 46 · 22 h 49 · 88 h 46 · 12 h 44 · 70 h 46 · 46 h 45 · 52 h 46 · 02 h 46 · 78 h 48 · 30 h 45 · 18 h 45 · 80 h 46 · 34 h 47 · 10 h 45 · 94 h 44 · 28 h 47 · 12 h 45 · 60 h 46 · 76 h 47 · 62 h 46 · 10 h 45 · 94 h 44 · 28 h 47 · 12 h 45 · 60 h 46 · 10 h 45 · 22 h 46 · 10	$M = 46'' \cdot 35$ $w = 10 \cdot 74$ $\frac{1}{w} = 0 \cdot 09$
·	46.95 47.82 46.41 45.79 47.22 46.67 45.50 45.05 46.49 45.62	$C = 53^{\circ} 5' 46'' \cdot 36$
XXIV (Dhanono) and XXII (Arrabhit)	h 10·32 h 9·24 h 10·40 h 11·10 h 8·72 h 11·00 h 10·16 h 10·16 h 11·30 h 10·52 h 9·28 h 10·50 h 10·52 h 10·68 h 10·40 h 9·80 h 10·12 h 10·80 h 10·26 h 11·02 h 8·76 h 8·20 h 10·48 h 11·08 h 10·74 h 11·92 h 10·76 h 10·48 h 10·74 h 10·74 h 12·16 h 9·62	$M = 10'' \cdot 38$ $w = 26 \cdot 47$ $\frac{1}{w} = 0 \cdot 04$
	9.45 9.94 10.47 10.95 9.95 10.70 10.35 10.48 10.77 10.76	$C = 46^{\circ} 6' 10^{\circ} 37$
XXII (Arrabhit) and	h 11 · 86 h 12 · 08 h 11 · 92 h 12 · 00 h 12 · 18 h 12 · 08 h 12 · 72 h 11 · 96 h 12 · 66 h 12 · 66 h 13 · 36 h 11 · 78 h 12 · 40 h 12 · 12 h 12 · 80 h 11 · 68 h 13 · 02 h 12 · 36 h 12 · 10 h 11 · 28 h 11 · 94 h 12 · 46 h 12 · 72 h 12 · 34 h 12 · 46 h 12 · 48 h 12 · 00 h 12 · 72 h 11 · 92 h 12 · 80	$M = 12'' \cdot 30$ $w = 111 \cdot 50$ $\frac{1}{2} = 0 \cdot 01$
AAI (Sanahu)	12.39 12.11 12.35 12.15 12.48 12.08 12.28 12.35 12.23 12.25	$c = 38^{\circ} 14' 12'' \cdot 30$

At XXIV (	Dhanono)
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March 1877; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	Circle readings, telescope being set on XXII (Arrabhit) 179° 14' 359° 14' 258° 26' 78° 26' 337° 38' 157° 38' 56° 49' 236° 49' 136° 1' 316° 2'	M – Mean of Groups $\infty$ = Relative Weight C = Concluded Angle
XXII (Arrabhit) and XXI (Sanahu)	n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n	$M = 28'' \cdot 67$ $w = 30 \cdot 42$ $\frac{1}{w} = 0 \cdot 03$ $C = 37^{\circ} 39' 28'' \cdot 64$
XXI (Sanahu) and XXIII (Harnáo)	\$\$ 58.94       \$\$ 58.66       \$\$ 58.96       \$\$ 57.64       \$\$ 58.98       \$\$ 58.66       \$\$ 57.78       \$\$ 58.66       \$\$ 59.90       \$\$ 56.36         \$\$ 59.28       \$\$ 58.66       \$\$ 58.38       \$\$ 59.06       \$\$ 58.34       \$\$ 57.72       \$\$ 56.58       \$\$ 58.12       \$\$ 57.20       \$\$ 57.54         \$\$ 59.12       \$\$ 59.94       \$\$ 59.34       \$\$ 59.80       \$\$ 59.14       \$\$ 59.96       \$\$ 58.74       \$\$ 57.72       \$\$ 58.62         \$\$ 59.00       \$\$ 58.34       \$\$ 59.80       \$\$ 59.14       \$\$ 59.96       \$\$ 58.74       \$\$ 57.72       \$\$ 58.62         \$\$ 59.00       \$\$ 58.35       \$\$ 59.04       \$\$ 58.51       \$\$ 58.51       \$\$ 58.52       \$\$ 77.60	$M = 58'' \cdot 61$ $w = 26 \cdot 17$ $\frac{1}{w} = 0 \cdot 04$ $C = 41^{\circ} 47' 58'' \cdot 59$
XXIII (Harnáo) and XXVI (Ráviláhu)	h 6.74       h 7.36       h 7.80       l 7.52       h 6.94       h 6.68       h 7.14       h 6.78       h 7.22       h 7.00         h 6.90       h 7.34       h 7.52       h 6.14       h 6.28       h 6.30       h 8.04       h 6.90       h 8.00       h 6.34         h 6.68       h 7.96       l 7.92       h 7.56       h 6.62       h 6.72       h 6.98       h 7.84       h 7.50       h 6.36         6.77       7.55       7.75       7.07       6.61       6.57       7.39       7.17       7.57       6.57	$M = 7'' \cdot 10$ $w = 41 \cdot 70$ $\frac{1}{w} = 0 \cdot 02$ $C = 50^{\circ} 27' 7'' \cdot 10$
XXVI (Ráviláhu) and XXIX (Máringra)	k 7.06 k 7.76 k 7.02 l 6.76 k 7.02 k 6.14 k 7.32 k 7.88 k 7.06 k 5.56 k 7.98 k 6.60 l 6.22 k 5.74 k 5.76 k 5.66 k 5.92 k 7.80 k 7.68 k 7.16 k 9.62 k 5.54 l 5.30 k 6.36 k 7.32 k 6.48 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 4.42 k 5.92 k 6.10 k 9.54 k 5.68 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.59 k 6.10 k 9.54 k 5.68 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.59 k 6.10 k 9.54 k 5.68 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.58 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.58 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.58 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.58 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.58 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.58 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 5.68 k 7.58 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 6.10 k 9.54 k 9.558 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 9.558 k 7.58 k 7.46 k 7.62 k 6.10 k 9.54 k 9.558 k 9.5	$M = 6'' \cdot 73$ $w = 16 \cdot 20$ $\frac{1}{w} = 0 \cdot 06$ $C = 50^{\circ} 52' 6'' \cdot 74$

### At XXV (Bándri)

\*March 1877; and †January 1880; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	<b>239° 41′</b>	Cii 59° 41′	rcle read 318 53'	ings, tel 138°52'	escope b 88° 5′	eing set 218°5'	on XXV 117°17'	'II (Máb 297° 17'	iu) 196° 29'	16° 29′	M - Mean of Groups w - Relative Weight C - Concluded Angle
† XXVII (Máhu) and XXVIII (Girája)	*	* h 34 · 02 h 33 · 18 h 33 · 16 h 32 · 78 33 · 28	n h 32 · 84 h 32 · 80 h 33 · 00 32 · 88	<pre>h 31 · 30 h 33 · 86 h 31 · 98 h 32 · 66 32 · 45</pre>	2 30.70 2 34.16 2 31.78 2 32.76 2 33.50 32.58	* l 31 · 98 l 32 · 02 l 32 · 10 32 · 03	" h 31 · 48 h 32 · 36 h 31 · 48 31 · 77	* h 32 · 22 h 32 · 86 h 32 · 06 32 · 38	" h 33 · 02 h 33 · 14 h 32 · 44 32 · 87	* h 32 · 10 h 32 · 08 h 32 · 94 32 · 37	$M = 32^{"} \cdot 51$ $w = 30 \cdot 30$ $\frac{1}{w} = 0 \cdot 03$ $C = 70^{\circ} 10' 32^{"} \cdot 52$

#### EASTERN SIND MERIDIONAL SERIES.

	At XXV (Bándri)—(Continued).	
Angle between	Circle readings, telescope being set on XXVII (Máhu) 239° 41′ 59° 41′ 318° 53′ 138° 52′ 38° 5′ 218° 5′ 117° 17′ 297° 17′ 196° 29′ 16° 29′	M - Mean of Groups $\infty$ = Relative Weight C = Concluded Angle
† XXVIII (Girája) and XXVI (Ráviláhu)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$M = 3'' \cdot 74$ $w = 15 \cdot 56$ $\frac{1}{w} = 0 \cdot 06$ $C = 50^{\circ} 9' 3'' \cdot 74$
• XXVI (Ráviláhu) and XXIII (Harnáo)	k 16 °02 k 13 °12 k 13 °14 k 15 °14 k 15 °58 k 12 °66 k 15 °22 k 14 °70 k 14 °40 k 14 °14 k 15 °26 k 14 °10 k 15 °20 k 14 °80 k 14 °00 k 14 °48 k 14 °30 k 14 °20 k 14 °70 k 14 °08 k 15 °12 k 15 °66 k 13 °18 k 14 °88 k 14 °78 k 13 °86 k 15 °10 k 13 °60 k 14 °22 k 13 °74 k 17 °76 k 14 °34 k 15 °44 k 14 °12 k 13 °94 15 °47 14 °78 13 °97 14 °94 14 °79 14 °11 14 °87 14 °17 14 °44 13 °99	$M = 14'' \cdot 55$ $w = 22 \cdot 10$ $\frac{1}{w} = 0 \cdot 05$ $C = 49^{\circ} 49' 14'' \cdot 54$

# At XXVI (Ráviláhu)

\*March 1877; and +January 1880; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	0° 1′	Ci 180° 1'	ircle read 79° 13'	lings, te 259°13′	lescope b 158°25'	oeing set 338° 25'	on XXV 237°36'	7 (Bándr 57°37'	i) 816°49′	136°49′	M = Mean of Groups w = Relative Weight C = Concluded Angle
† XXV (Bándri) and XXVIII (Girája)	n h 30.84 h 31.44 h 31.06 h 30.66 31.00	" h 28 · 80 h 29 · 18 h 28 · 24 28 · 74	* l 29.58 l 26.70 l 28.36 l 25.54 l 29.66 h 29.02 28.14	" 1 30.08 h 28.22 h 27.90 h 28.38 28.65	" h 28 · 60 h 29 · 32 h 30 · 28 29 · 40	" l 28.70 l 28.90 l 29.24 28.95	" h 30°74 h 30°06 h 30°44 30°41	* h 31 °04 h 29 °52 h 31 °52 30 °69	* h 30 · 60 h 29 · 80 h 29 · 64 30 · 01	* h 30° 42 h 29° 44 h 27° 88 h 30° 20 29° 48	$M = 29'' \cdot 55$ $w = 8 \cdot 85$ $\frac{1}{w} = 0 \cdot 11$ $C = 66^{\circ} 17' 29'' \cdot 54$
† XXVIII (Girája) and XXIX (Máringra)	11.49	k 13.72 k 11.48 k 13.06 k 10.44 l 11.10	l 11 · 80 l 11 · 82 l 13 · 16	l 12.32 h 11.98 h 15.50 h 12.12 12.98	k 12°24 k 12°84 k 12°34	k 10.98 k 11.58 k 12.12	k 10.42 k 11.16 k 12.66 k 11.82	k 12.62 k 10.94 k 12.04	k 12.04 k 11.92 k 11.52	k 13.76 k 11.26 k 13.10 k 12.26	$M = 12^{\psi} \cdot 05$ $w = 20 \cdot 62$ $\frac{1}{w} = 0 \cdot 05$ $C = 64^{\circ} 59' 12^{\psi} \cdot 06$

At XXVI (Ráviláhu)—(Continued).											
Angle between	Circle readings, telescope being set on XXV (Bándri) 0° 1' 180° 1' 79° 18' 259° 13' 158° 25' 338° 25' 237° 36' 57° 37' 316° 49' 136° 49'	M = Mean of Groups $\omega$ = Relative Weight C = Concluded Angle									
† XXIX (Máringra) and XXIV (Dhanono)	k       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n	$M = 19'' \cdot 46$ $w = 14 \cdot 42$ $\frac{1}{w} = 0 \cdot 07$ $C = 81^{\circ} 47' 19'' \cdot 46$									
• XXIV (Dhanono) and XXIII (Harnáo)	$ \begin{array}{cccccccccccccccccccccccccccccccccccc$	$M = 7'' \cdot 44$ $w = 59 \cdot 68$ $\frac{1}{w} = 0 \cdot 02$ $C = 76^{\circ} 27' 7'' \cdot 44$									
• XXIII (Harnáo) and XXV (Bándri)	h 48.38       h 51.92       h 51.86       h 51.60       l 51.68       l 52.92       h 53.30       l 50.96       l 51.96       l 51.58         h 51.34       h 52.42       h 51.92       h 50.92       l 52.56       l 52.10       h 53.30       l 50.96       l 51.96       l 51.70         h 49.72       h 50.78       h 51.72       h 52.52       l 51.90       l 51.62       l 51.46       l 53.38       l 51.78       l 51.98         h 52.38       l 51.44       l 51.80       l 51.80       l 51.80       l 51.75       l 51.75	$M = 51'' \cdot 85$ $w = 22 \cdot 43$ $\frac{1}{w} = 0 \cdot 04$ $C = 70^{\circ} 28' 51'' \cdot 83$									

## At XXVII (Máhu)

February 1880; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	0° 0′	C 180° 0′	Vircle rea	dings, te	lescope l	eing set	on XXX	(Singra	s)	136° 48'	M - Mean of Groups $\infty$ - Relative Weight Q - Concluded Augle
XXX (Singra) and XXVIII (Girája)	λ     7.20       λ     6.18       λ     9.24       λ     5.48       λ     7.42	180°0 <i>k</i> 6°54 <i>k</i> 5°60 <i>k</i> 6°60	<i>h</i> 5.40 <i>h</i> 6.64 <i>h</i> 6.96 <i>d</i> 6.55	259°11°	158° 25° h 6°04 h 6°04 h 6°72 h 6°74	\$38*24 <b>h</b> 6·16 <b>h</b> 7·88 <b>h</b> 7·06	237-36 <b>h</b> 5.96 h 7.58 <b>h</b> 6.76	h 4.96 h 5.88 h 5.36	<i>k</i> 5 <sup>.82</sup> <i>h</i> 6 <sup>.60</sup> <i>l</i> 5 <sup>.58</sup>	l 4 · 18 l 6 · 74 l 5 · 20 l 6 · 38	$M = 6'' \cdot 30$ $w = 18 \cdot 13$ $\frac{1}{w} = 0 \cdot 06$
	7.10	6.32	6.39	5.91	6.20	7.03	6.77	5.40	6.00	5.63	$C = 51^{\circ} 10^{\circ} 0^{\circ} 30^{\circ}$
XXVIII (Girája) and XXV (Bándri)	\$\$ 41.98         \$\$ 40.86         \$\$ 37.68         \$\$ 39.76         \$\$ 40.44         \$\$ 39.84	h 40°78 h 39°90 h 39°22 39°97	h 39.04 h 39.10 h 36.92 h 37.04 d 38.25 38.07	h 36 · 82 h 40 · 22 h 41 · 16 h 36 · 74 h 38 · 30 h 38 · 82 38 · 68	k 39.62 k 37.94 k 37.26 k 39.24 38.52	h 39.68 h 38.28 h 37.40 h 41.34 h 41.08 39.56	4 38 30 h 38 58 h 37 18 38 02	k 39 · 18 k 42 · 12 k 39 · 94 k 40 · 44	h 39 °02 h 39 °30 l 39 °24 39 °19	l 39°04 l 39°32 l 40°30 l 40°38 39°76	$M = 39'' \cdot 23$ $w = 9 \cdot 38$ $\frac{1}{w} = 0 \cdot 11$ $C = 56^{\circ} 10' 39'' \cdot 23$

## At XXVIII (Girája)

February 1880; observed by Captain M. W. Rogers, B.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	0° 0′	Cir 180° 0′	cle readi 79°13′	ings, tele 259° 18′	scope bei 158° 24′	ing set o 838° 24'	n XXIX 237°36'	(Máring 57° 36'	g <b>ra)</b> 816° 48'	1 <b>86° 48</b> ′	
XXIX (Máringra) and XXVI (Ráviláhu)	12.34 1 12.20 1 12.20 1 12.22 1 12.49	• 12°78 11°98 12°02	# 12.04 12.26 111.98 12.50 12.20	l 13.08 l 11.54 l 11.92	k 13.02 k 12.28 k 12.16	k 11 °94 k 12 °42 k 12 °70	* * 11 * 86 * 13 * 14 * 11 * 46 12 * 15	* \$ 11.74 \$ 12.04 \$ 11.62 11.80	l 11 · 66 l 13 · 50 l 12 · 48	" l 10°32 k 12°12 k 11°52	$M = 12^{v} \cdot 18$ $v = 45 \cdot 95$ $\frac{1}{v} = 0 \cdot 02$ $C = 62^{\circ} 56' 12^{v} \cdot 18$
XXVI (Ráviláhu) and XXV (Bándri)	26.99	26.74 29.10 29.92 27.02 27.48 28.05	h 27 · 82 h 28 · 34 h 29 · 68 28 · 61	1 27 · 98 1 28 · 92 1 28 · 96 28 · 62	k 27.84 k 27.48 k 27.18 k 27.18	\$ 26.10 \$ 27.06 \$ 27.06 \$ 27.06	k 27 · 10 k 26 · 34 k 26 · 44	h 27 · 28 k 26 · 50 l 27 · 74 27 · 17	28.14 26.68 27.16	27.01	$M = 27'' \cdot 47$ $w = 14 \cdot 25$ $\frac{1}{w} = 0 \cdot 07$ $C = 63^{\circ} 33' \cdot 27'' \cdot 48$
XXV (Bándri) and XXVII (Máhu)	1 50°10 1 1 49°06 1 1 49°14 1 1 2 49°43	48.64 45.26 46.34 47.34 48.88 47.29	k 47 · 64 k 48 · 64 k 47 · 70 47 · 99	\$ 49.48 \$ 49.46 \$ 47.86 \$ 48.76 48.89	\$ 50.02 \$ 48.50 \$ 49.66 49.39	k 48 · 12 k 49 · 22 k 46 · 44 k 49 · 04 48 · 21	k 49 · 92 k 49 · 64 k 48 · 92 49 · 49	k 49°50 k 49°86 k 49°08	l 49°34 l 48°26 l 49°92 49°17	l 47°70 l 49°66 l 48°62 48°66	$M = 48'' \cdot 80$ $w = 12 \cdot 86$ $\frac{1}{w} = 0 \cdot 08$ $C = 53^{\circ} 38' 48'' \cdot 78$
XXVII (Máhu) and XXX (Singra)	h 25°34 h h 21°90 h h 23°08 h h 23°76 h h 22°28 h h 21°48 h 22°97	22°46	h 22 · 56 h 21 · 76 h 20 · 32 h 20 · 98	Å 19 · 36 Å 22 · 48 Å 20 · 46 Å 22 · 58 Å 20 · 90	\$ 21 · 12 \$ 21 · 36 \$ 22 · 08	k 20.62 k 22.02 k 21.74 21.46	k 22°12 k 20°82 k 21°50 21°48	λ 21 ° 80 λ 21 ° 18 λ 21 ° 18 λ 21 ° 12 21 ° 37	22.18	l 22°34 l 21°20 l 21°20 21°58	$M = 21^{w} \cdot 76$ $w = 16 \cdot 11$ $\frac{1}{w} = 0 \cdot 06$ $C = 68^{\circ} 17' 21^{w} \cdot 80$
XXX (Singra) and XXXI (Asu)	h 30°54 h h 29°42 h h 27°72 h h 31°44 h h 32°38 h h 30°02 h h 29°52 h 30°15	30 · 48 30 · 72 32 · 80 32 · 04 30 · 64 31 · 20 31 · 26 31 · 31	<b>k</b> 31 · 40 <b>k</b> 31 · 54 <i>l</i> 29 · 18 <i>l</i> 30 · 66 <i>l</i> 29 · 36 <b>3</b> 0 · 43	28.99	k 29 · 22 k 30 · 68 k 30 · 00 29 · 97	k 29°70 k 28°90 k 29°94 29°51	k 29.86 h 30.98 k 30.94 30.59	k 29°56 k 30°20 l 29°24 29°67	30°90 30°94 30°58 30°81	30°39	$M = 30'' \cdot 18$ $w = 15 \cdot 02$ $\frac{1}{w} = 0 \cdot 07$ $C = 55^{\circ} 22' 30'' \cdot 20$
XXXI (Asu) and XXIX (Máringra)	k 39.12 k k 38.30 k k 41.78 k k 37.66 k k 38.28 k 39.03	38.62 38.68 40.06 39.20 36.30 38.57	h 40 · 86 h 40 · 30 k 38 · 70 l 40 · 80 40 · 17	l 39·22 l 40·60 l 41·36 l 40·40 40·39	1 38.76 1 38.78 1 38.50 38.68	k 39.06 k 38.12 k 38.84 38.67	k 38.62 k 38.44 k 38.36 38.36	h 40 · 52 / h 39 · 50 l 38 · 34 l 40 · 02 39 · 60	40°06 140°90 139°18 40°05	k 38 · 48 k 39 · 68 k 38 · 42 38 · 86	$M = 39'' \cdot 25$ $w = 13 \cdot \infty0$ $\frac{1}{w} = 0 \cdot 08$ $C = 56'' 11' 39'' \cdot 26$

#### At XXIX (Máringra)

February 1880; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	0° 1′	Cin 180° 0'	rcle readi 79° 13'	ings, tele 259° 13'	escope be 158°25'	ing set o 838° 24'	n XXIV 237° 86'	(Dhanc 57° 36'	ono) 816° 49'	136° 48'	M = Mean of Groups w = Relative Weight C = Concluded Angle
XXIV (Dhanono) and XXVI (Ráviláhu)	n h 36 · 58 h 36 · 32 h 35 · 72	n h 33 · 64 h 34 · 30 h 34 · 76	" 1 33·38 1 34·80 1 33·44	" 2 36 · 10 2 35 · 30 2 37 · 16	" 1 36 · 08 1 34 · 88 1 35 · 56	" 1 34·28 1 34·66 1 34·30	" 1 34·76 1 36·30 1 34·72	* 1 34 · 86 1 35 · 40 1 34 · 96	" 1 33 · 76 1 35 · 16 1 35 · 22	l 33·76 l 33·68 l 34·56	$M = 34^{"} \cdot 95$ $w = 12 \cdot 20$ $\frac{1}{w} = 0 \cdot 08$
	36 · 21	34.33	33.87	36.19	35.21	34.41	35 • 26	35.07	34.21	34.00	$C = 47^{\circ} 20' 34'' \cdot 95$
XXVI (Ráviláhu) and XXVIII (Giráia)	h 37 · 60 h 36 · 46 h 38 · 98 h 36 · 22	h 38 · 26 h 36 · 46 h 37 · 50	l 37°20 l 35°42 l 36°60	l 35.68 l 36.90 l 34.40 l 36.62	l 35·72 l 35·20 l 36·50	l 35·92 l 36·72 l 35·42	1 36 · 90 1 36 · 22 1 36 · 38	l 34°94 l 35°52 l 35°00	l 37·10 l 36·72 l 36·30	l 35·52 l 35·42 l 35·20	$M = 36'' \cdot 26$ $w = 13 \cdot 86$ $\frac{1}{w} = 0 \cdot 07$
(	37.32	37.41	36.41	35.90	35.81	36.02	36.20	<b>3</b> 5 · 1 <b>5</b>	36.21	35.38	$C = 52^{\circ} 4' 36'' \cdot 26$
XXVIII (Girája) and XXXI (Asn)	h 36 · 76 h 35 · 66 h 35 · 30	h 37 °02 h 35 °82 h 37 ° 16	1 35·38 1 35·08 1 36·68	l 36.86 l 38.24 l 35.38 l 35.60	2 35°78 2 35°06 2 35°44	l 34·76 l 35·44 l 36·48	l 36 · 20 l 35 · 30 l 36 · 26	l 36 · 02 l 34 · 00 l 35 · 96 l 35 · 58	l 35·94 l 36·02 l 36·02	2 35°70 2 36°70 2 36°80	$M = 35'' \cdot 95$ $w = 28 \cdot 50$ $\frac{1}{w} = 0 \cdot 04$
	35.91	36.67	35.21	36.22	35.43	35.26	35.92	35°39	35.99	36.40	$C = 70^{\circ} 11' 35'' \cdot 95$

At XXX (Singra)

February 1880; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	Circle readings, telescope being set on XXXII (Bitri) 0° 0′ 180° 0′ 79° 13′ 259° 13′ 158° 25′ 838° 25′ 237° 36′ 57° 35′ 816° 49′ 186° 49′	M = Mean of Groups w = Relative Weight C = Concluded Angle
XXXII (Bitri) and XXXIII (Parethal)	h 12 · 50 h 12 · 54 h 12 · 66 h 13 · 32 l 12 · 74 l 11 · 66 l 13 · 34 h 11 · 56 h 10 · 32 h 11 · 42         h 12 · 50 h 12 · 54 h 12 · 66 h 13 · 32 l 12 · 74 l 11 · 66 l 13 · 34 h 11 · 56 h 10 · 32 h 11 · 42         h 12 · 34 h 12 · 52 h 13 · 78 h 12 · 48 l 11 · 30 l 11 · 54 l 12 · 78 h 10 · 68 h 12 · 44 h 11 · 82         h 14 · 02 h 15 · 76 h 12 · 86 h 11 · 96 l 11 · 74 l 10 · 42 l 11 · 38 h 11 · 10 h 12 · 46 h 9 · 18         h 13 · 64 h 13 · 28         h 15 · 68 h 11 · 96         13 · 64 i 3 · 21 i 3 · 10 i 2 · 59 i 1 · 93 i 1 · 21 i 2 · 11 i 1 · 11 i 1 · 99 i 1 · 30	$M = 12^{\psi} \cdot 22$ $w = 9 \cdot 67$ $\frac{1}{w} = 0 \cdot 10$ $C = 49^{\circ} 35' 12^{\psi} \cdot 23$
XXXIII (Parethal) and XXXI (Asu)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$M = 37^{"} \cdot 80$ $w = 12 \cdot 00$ $\frac{1}{w} = 0 \cdot 08$ $C = 67^{\circ} 44' 37'' \cdot 77$

At XXX (Singra)—(Continued).

At AAA (Singra)—(Communea):											
Angle between	0°0′ 1	Circle readings, telescope being set on XXXII (Bitri) 0°0′ 190°0′ 79°13′ 259°13′ 158°25′ 838°25′ 287°36′ 57°35′ 816°49′ 136°49′									
XXXI (Asu) and XXVIII (Girája)	* \$ 49.90 \$ \$ 51.26 \$ \$ 51.16 \$ \$ 50.77	*       50*96       51*80       50*86       52*50	h 51 · 70 h 51 · 30 h 50 · 96	* \$ 51.76 \$ 52.78 \$ 51.62 52.05	# 1 52*24 1 51*70 1 51*88 51*94	2 51.64 2 51.14 2 50.76 2 52.36 51.48	* 1 53.80 1 51.68 1 53.38 1 52.38 52.81	* \$ 51 • 28 \$ 51 • 20 \$ 50 • 76 51 • 08	n h 50.72 h 50.90 h 51.94 51.19	x h 52 · 52 h 52 · 38 52 · 51	$M = 51^{\psi} \cdot 67$ $w = 19 \cdot 56$ $\frac{1}{\psi} = 0 \cdot 05$ $C = 68^{\circ} 2' 51^{\psi} \cdot 68$
XXVIII (Girája) and XXVII (Máhu)	h 31 ° 96 h h 33 ° 56 h h 33 ° 80 h k 33 ° 11	33°10 35°66 34°80 34°18 34°44	h 33.06 h 33.92 h 32.72	h 34 · 08 h 33 · 92 h 33 · 98 33 · 99	1 33.80 1 32.34 1 32.90 33.01	l 32·38 l 32·04 l 34·64 l 31·88 32·73	1 33 · 30 1 33 · 64 1 33 · 94 33 · 63	h 34 · 74 h 33 · 02 h 34 · 10 33 · 95	h 33 · 32 h 32 · 86 h 33 · 76 33 · 31	h 31 · 74 h 32 · 32 h 32 · 02	$M = 33'' \cdot 34$ $w = 15 \cdot 82$ $\frac{1}{w} = 0 \cdot 06$ $C = 60^{\circ} 32' \cdot 33'' \cdot 34$

At XXXI (Asu)

February 1880; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	Circle readings, telescope being set on XXIX (Máringra) 153° 29′ 833° 29′ 232° 45′ 52° 45′ 811° 57′ 131° 57′ 81° 9′ 211° 9′ 110° 20′ 290° 20′	M - Mean of Groups w - Relative Weight C - Concluded Angle
XXIX (Máringra) and XXVIII (Girája)	k 42 · 26       k 45 · 04       l 43 · 68       l 44 · 34       k 46 · 36       l 45 · 62       l 45 · 14       l 45 · 96       k 46 · 04       k 47 · 54         k 43 · 72       l 46 · 84       l 45 · 76       l 42 · 98       l 45 · 36       l 46 · 46       l 44 · 44       k 43 · 92       k 46 · 08       k 44 · 38         k 46 · 30       l 43 · 24       l 42 · 54       k 43 · 82       l 46 · 62       l 44 · 54       l 46 · 90       k 46 · 20       k 44 · 90         k 43 · 44       l 43 · 84       l 43 · 82       l 46 · 62       l 44 · 54       l 46 · 42       k 46 · 24       k 44 · 38         k 43 · 56       l 43 · 52       l 44 · 54       l 46 · 42       k 46 · 24       k 44 · 38         k 43 · 56       l 43 · 52       l 44 · 54       k 46 · 24       k 44 · 38         k 43 · 82       k 45 · 58       k 45 · 58       k 45 · 58	$M = 45^{"} \cdot 05$ $w = 8 \cdot 86$ $\frac{1}{w} = 0 \cdot 11$ $C = 53^{\circ} 36' 45^{"} \cdot 02$
	43.85 44.50 44.08 43.71 46.11 45.54 45.73 45.64 46.11 45.24	
XXVIII (Girája) and XXX (Singra)	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$M = 38'' \cdot 77$ $w = 22 \cdot 16$ $\frac{1}{w} = 0 \cdot 05$
	38.32 39.89 38.42 39.47 38.63 38.37 38.18 38.78 38.71 38.93	$\int C = 56^{\circ} 34' 38'' \cdot 80$
XXX (Singra) and XXXIII (Parethal)	k 19.46 k 20.32 l 20.12 l 18.62 k 20.76 l 20.90 l 20.40 l 18.32 k 20.92 k 20.44 k 19.98 k 19.58 l 19.44 k 20.38 l 20.88 l 21.04 l 20.72 k 20.70 k 21.18 k 19.98 k 21.76 k 20.22 l 19.38 k 20.06 l 20.52 l 20.14 l 20.12 k 20.78 k 20.78 k 21.02 k 21.74 d 19.95 k 20.64	$M = 20^{w} \cdot 32$ $w = 29 \cdot 61$ $\frac{1}{w} = 0 \cdot 03$
	20.72 20.04 19.65 19.75 20.72 20.69 20.41 19.77 20.96 20.48	$\int C = 53^{\circ} 10' 20'' \cdot 32$

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At XXXI (Asu)—(Continued).											
Angle between	Ci 153° 29′ 333° 29	rcle readings, teles ′232°45′52°45′	cope being set on XXIX 811° 57′ 131° 57′ 81° 9′	(Máringra) 211°9′ 110°20′ 290°20′	M = Mean of Groups = Relative Weight C = Concluded Angle						
XXXIII (Parethal) and XXXIV (Kolu)	* * * k 11 · 16 k 12 · 0 k 8 · 02 k 13 · 1 k 11 · 10 k 12 · 6 k 10 · 96	8 2 14 46 2 11 94 2 2 10 88 2 10 44 0 2 11 76 2 10 10 2 12 30 2 11 58 2 11 36 2 11 04	k 9.02 l 11.06 l 13.74 l 10.12 l 11.76 l 12.78 l 12.72 l 11.96	l 13·14 k 11·34 k 10·86 k 11·12 k 8·98 k 11·72 k 12·78 k 11·42 k 11·94 k 10·32 k 10·40	$M = 11'' \cdot 59$ $w = 9 \cdot 88$ $\frac{1}{w} = 0 \cdot 10$ $C = 43^{\circ} 6' 11'' \cdot 57$						
	10.28 13.6	0 11.97 11.03	11.31 11.37 13.35	11.84 10.23 11.21							
XXXIV (Kolu) and B. M.	h 52.84 h 53.4 h 52.52 h 52.24 h 52.24 h 50.8	2 2 51.78 2 52.38 5 2 53.42 2 54.82 5 2 53.34 3 52.72 3 52.46	k 50°80 l 54°14 l 51°56 l 51°90 l 51°42 l 50°52 l 52°26 l 52°62 l 51°52 l 51°38	l 52.82 h 50.78 h 52.94 h 53.56 h 52.14 h 51.98 h 51.74 h 53.26 h 51.92 h 51.80	$M = 52'' \cdot 29$ $w = 18 \cdot 53$ $\frac{1}{w} = 0 \cdot 05$						
	52.23 52.1	5 52.85 53.10	51.65 52.39 51.30	52.71 51.99 52.28	$C = 21^{\circ} 32' 52'' \cdot 30$						
		At X	XXXII (Bitri)								
February 1880;	observed by C	aptain M. W.	Rogers, R.E., with	Barrow's 24-inch The	odolite No. 2.						
					1						
Angle between	179° 11′ 859° 11	258° 23′ 78° 23′	scope being set on XXX 837° 34′ 157° 84′ 56° 47′	V (Chauki) 236° 47′ 135° 58′ 315° 57′	M = Mean of Groups w = Relative Weight C = Concluded Angle						
Angle between XXXV (Chauki) and XXXVI (Kháro)	179°11′ 859°11	258°23′78°23′ 258°23′78°23′ 5 \$ 58.20 \$ 57.24 4 \$ 57.16 \$ 57.12 6 \$ 56.60 \$ 57.02	850000 being set on XXX 887°84' 157°84' 56°47'	V (Chauki) 236° 47' 135° 58' 315° 57' 1 56° 18 1 55° 22 1 57° 96 1 54° 60 1 56° 50 1 57' 76 1 56° 86 1 56° 44 1 56° 66 1 56° 16	$M = Mean \text{ of Groups}$ $w = Relative Weight$ $C = Concluded Angle$ $M = 56'' \cdot 69$ $w = 18 \cdot 72$ $\frac{1}{w} = 0 \cdot 05$						
Angle between XXXV (Chauki) and XXXVI (Kháro)	179°11′ 859°11	5 17 16 readings, tele 258° 23' 78° 23' 4 5 8 20 1 57 24 4 3 57 16 1 57 24 5 57 32 57 13	BBCOPE being set on XXX         887°84'       157°84'       56°47'         n       n       n         h 55'20       1 55'90       1 56'68         h 57'38       1 56'22       1 54'90         h 55'92       1 56'76       1 56'40         1 56'70       56'30       56'29       55'99	V (Chauki) 236° 47′ 135° 58′ 315° 57′ 1 56 · 18 1 55 · 22 1 57 · 96 1 54 · 60 1 56 · 50 1 57 · 76 1 56 · 86 1 56 · 44 1 56 · 66 1 56 · 16 55 · 95 56 · 05 57 · 46	M = Mean of Groups w = Relative Weight C = Concluded Angle $M = 56'' \cdot 69$ $w = 18 \cdot 72$ $\frac{1}{w} = 0 \cdot 05$ $C = 53'' \cdot 8' \cdot 56'' \cdot 68$						
Angle between XXXV (Chauki) and XXXVI (Kháro) XXXVI (Kháro) and XXXIII (Parethal)	179°11' 859°11 * " \$56.84 \$56.60 \$56.20 \$57.11 \$58.12 \$58.2 57.05 \$57.3 \$3.46 \$4.40 \$5.68 \$4.44 \$2.10 \$2.11 \$3.00 \$3.44 \$2.296	incle readings, tele         258° 23'       78° 23'         5       58° 20       57° 24         4       57° 16       57° 12         6       Å 57° 16       Å 57° 12         6       Å 50° 60       Å 57° 02         5       57° 32       57° 13         0       Å 5° 04       Å 3°00         2       Å 3° 50       Å 2°40         6       Å 3° 30       Å 3°08	887° 84'       157° 84'       56° 47'         887° 84'       157° 84'       56° 47'         n       n       n         h 55' 20       1 55' 90       1 56' 68         h 57' 38       1 56' 22       1 54' 90         h 55' 92       1 56' 76       1 56' 40         1 50' 70       56' 30       56' 29       55' 99         56' 30       56' 29       55' 99         h 2' 38       1 2' 26       1 2' 72         h 2' 38       1 3' 54       1 2' 72         h 2' 70       1 2' 66       1 2' 82	V (Chauki) 236° 47' 135° 58' 315° 57' 236° 47' 135° 58' 315° 57' 2 56 18 2 55 22 2 57 96 2 54 60 2 56 50 2 57 76 2 56 86 2 56 44 2 56 66 2 55 95 56 05 57 46 2 3 32 2 4 16 2 4 46 2 1 90 2 3 8 2 3 48 2 2 46 2 1 40 2 3 36 2 2 54	$M = Mean \text{ of Groups}$ $w = Relative Weight$ $C = Concluded Angle$ $M = 56'' \cdot 69$ $w = 18 \cdot 72$ $\frac{1}{w} = 0 \cdot 05$ $C = 53'' \cdot 8' 56'' \cdot 68$ $M = 3'' \cdot 12$ $w = 23 \cdot 24$ $\frac{1}{w} = 0 \cdot 04$						
Angle between XXXV (Chauki) and XXXVI (Kháro) XXXVI (Kháro) and XXXIII (Parethal)	179°11'       859°11         *       *         \$56.84       \$56.60         \$56.20       \$57.11         \$58.12       \$58.2         57.05       \$57.3         \$3.46       \$4.40         \$5.68       \$4.44         \$2.10       \$2.11         \$3.30       \$3.44         \$2.96       3.44	258° 23'       78° 23'         6 \$\lambda 58` 20 \$\lambda 57' 24         4 \$\lambda 57' 16 \$\lambda 57' 12         6 \$\lambda 56' 60 \$\lambda 57' 02         5 \$\lambda 5' 60 \$\lambda 57' 02         5 \$\lambda 5' 60 \$\lambda 57' 13         0 \$\lambda 5' 60 \$\lambda 57' 13         0 \$\lambda 5' 60 \$\lambda 2 \$\lambda 2 \$\lambda 0\$         5 \$\lambda 7' 32 \$\lambda 7' 13         0 \$\lambda 5' 60 \$\lambda 2 \$\lambda 2 \$\lambda 0\$         2 \$\lambda 3' 50 \$\lambda 2 \$\lambda 0\$         3 \$\lambda 5 \$\lambda 3 \$\lambda 3 \$\lambda 3\$         0 \$\lambda 5' 30 \$\lambda 3' 30\$         0 \$\lambda 3' 30 \$\lambda 3' 30\$         0 \$\lambda 3' 95 \$\lambda 2' 83\$	887° 84'       157° 84'       56° 47'         887° 84'       157° 84'       56° 47'         n       n       n         h 55° 20       1 55° 90       1 56° 68         h 57° 38       1 56° 22       1 54° 90         h 55° 92       1 56° 76       1 56° 40         56° 30       56° 29       55° 99         h 2° 38       1 2° 26       1 2° 50         h 2° 38       1 3° 54       1 2° 72         h 2° 70       1 2° 66       1 2° 82         2° 65       2° 82       2° 68	V (Chauki) 236° 47' 135° 58' 315° 57' 236° 47' 135° 58' 315° 57' 2 56 18 2 55 22 2 57 96 2 54 60 2 56 50 2 57 76 2 56 86 2 56 44 2 56 66 2 55 95 56 05 57 46 2 3 32 2 4 16 2 4 46 2 1 90 2 3 88 2 3 48 2 2 46 2 1 40 2 3 36 2 2 54 2 56 2 99 3 77	$M = Mean of Groups$ $w = Relative Weight$ $C = Concluded Angle$ $M = 56'' \cdot 69$ $w = 18 \cdot 72$ $\frac{1}{w} = 0 \cdot 05$ $C = 53'' \cdot 12$ $M = 3'' \cdot 12$ $w = 23 \cdot 24$ $\frac{1}{w} = 0 \cdot 04$ $C = 54'' \cdot 14' \cdot 3'' \cdot 13$						
Angle between XXXV (Chauki) and XXXVI (Kháro) XXXVI (Kháro) and XXXIII (Parethal) XXXIII (Parethal) and XXX (Singra)	$ \begin{array}{c} 179^{\circ}11' & 859^{\circ}11\\ & & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & & \\ & $	incle readings, tele         258° 23'       78° 23'         5       58' 20 h 57' 24         4 h 57' 16 h 57' 12         6 h 56' 60 h 57' 02         5       57' 32         5       57' 32         5       57' 32         6 h 3' 50 h 2' 40         6 h 41' 68 h 43' 12         6 h 42' 80	$\begin{array}{c} 887^{\circ}84' & 157^{\circ}84' & 56^{\circ}47' \\ \hline \\ 887^{\circ}84' & 157^{\circ}84' & 56^{\circ}47' \\ \hline \\ 887^{\circ}84' & 157^{\circ}84' & 56^{\circ}47' \\ \hline \\ 855^{\circ}20 & l 55^{\circ}90 & l 56^{\circ}68 \\ \hline \\ h 57^{\circ}38 & l 56^{\circ}22 & l 54^{\circ}90 \\ \hline \\ h 55^{\circ}92 & l 56^{\circ}76 & l 56^{\circ}40 \\ \hline \\ l 56^{\circ}70 \\ \hline \\ 56^{\circ}30 & 56^{\circ}29 & 55^{\circ}99 \\ \hline \\ h 2^{\circ}30 & 56^{\circ}29 & 55^{\circ}99 \\ \hline \\ h 2^{\circ}30 & 56^{\circ}29 & 55^{\circ}99 \\ \hline \\ h 2^{\circ}30 & 56^{\circ}29 & 55^{\circ}99 \\ \hline \\ h 2^{\circ}30 & 56^{\circ}29 & 55^{\circ}99 \\ \hline \\ h 2^{\circ}30 & 56^{\circ}29 & 55^{\circ}99 \\ \hline \\ h 2^{\circ}30 & 56^{\circ}29 & 55^{\circ}99 \\ \hline \\ h 2^{\circ}30 & 56^{\circ}29 & 55^{\circ}99 \\ \hline \\ h 2^{\circ}30 & 56^{\circ}29 & 55^{\circ}99 \\ \hline \\ h 2^{\circ}30 & 12^{\circ}66 & l 2^{\circ}82 \\ \hline \\ h 2^{\circ}30 & l 41^{\circ}46 \\ \hline \\ \end{array}$	V (Chauki) 236° 47' 135° 58' 315° 57' $l 56 \cdot 18 l 55 \cdot 22 k 57 \cdot 96$ $l 54 \cdot 60 l 56 \cdot 50 k 57 \cdot 76$ $l 56 \cdot 86 l 56 \cdot 44 k 56 \cdot 66$ $l 55 \cdot 95 56 \cdot 05 57 \cdot 46$ $l 3 \cdot 32 l 4 \cdot 16 k 4 \cdot 46$ $l 1 \cdot 90 l 3 \cdot 88 k 3 \cdot 48$ $l 2 \cdot 46 l 1 \cdot 40 k 3 \cdot 36$ $l 2 \cdot 54$ $2 \cdot 56 2 \cdot 99 3 \cdot 77$ $l 42 \cdot 80 l 41 \cdot 90 k 42 \cdot 38$ $l 42 \cdot 00 l 43 \cdot 92 k 41 \cdot 14$ $l 41 \cdot 02 l 41 \cdot 66 k 42 \cdot 04$ $l 41 \cdot 96$	$M = Mean of Groups$ $w = Relative Weight$ $C = Concluded Angle$ $M = 56'' \cdot 69$ $w = 18 \cdot 72$ $\frac{1}{w} = 0 \cdot 05$ $C = 53'' \cdot 12$ $w = 23 \cdot 24$ $\frac{1}{w} = 0 \cdot 04$ $C = 54'' \cdot 14' \cdot 3'' \cdot 13$ $M = 41'' \cdot 68$ $w = 17 \cdot 83$ $\frac{1}{w} = 0 \cdot 06$						

Nore.--R. M. denotes Referring Mark.

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# At XXXIII (Parethal)

March 1880; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	359° 59′	Ciro 179° 59′	cle readi 79° 12'	ngs, tele 259°12'	scope be 158°25'	ing set o 338° 24'	n XXX 237° 36'	7I (Khá 57° 86'	iro) 816°49′	136° 49'	M = Mean of Groups w = Relative Weight C = Concluded Angle
XXXVI (Kháro) and XXXIV (Kolu)	k 12 · 70 / k 14 · 16 / k 14 · 80 / k 15 · 16 k 13 · 70	" k 15.68 k 15.20 k 14.30	<i>k</i> 14.04 <i>l</i> 17.06 <i>l</i> 16.18 <i>l</i> 16.78 <i>l</i> 14.86	" l 17·14 l 14·94 l 15·34 l 14·20	k 13.92 h 13.02 h 12.34	k 13.14 h 14.30 h 13.94	k 14·44 h 15·76 k 15·28	k 14°36 k 13°98 k 16°60 k 15°48	k 15.90 k 15.64 k 15.32	* \$ 15.68 \$ 14.46 \$ 15.88	$M = 14^{w} \cdot 85$ $w = 10 \cdot 20$ $\frac{1}{w} = 0 \cdot 10$
	14.10	15.06	15.78	15.41	13.09	13.29	15.16	15.10	15.62	15.34	$C = 74^{\circ} 10^{\circ} 14^{\circ} \cdot 85$
XXXIV (Kolu) and XXXI (Asu)	\$\$ 55.76         \$\$ 58.30         \$\$ 59.04         \$\$ 59.04         \$\$ 58.34         \$\$ 59.20	k 57 · 82 k 59 · 18 k 60 · 70 k 57 · 38 k 57 · 22	h 58.58 l 58.90 l 57.32	l 59·48 l 57·72 l 59·10	k 57 · 38 k 59 · 06 k 57 · 74	k 56°90 k 58°42 h 59°74 k 58°92	h 56°72 h 59°42 h 58°08 h 58°44	k 57°96 h 58°44 k 57°94	h 57°08 h 57°42 h 57°44	h 58.64 h 57.78 h 58.04	$M = 58'' \cdot 19$ $w = 25 \cdot 80$ $\frac{1}{w} = 0 \cdot 04$
	58.13	58.46	58.27	58.77	58.06	58.20	58.16	58.11	57.31	58.12	$C = 84^{\circ} 38' 58'' 20$
XXXI (Asu) and XXX (Singra)	Å 3.68 Å 5.24 Å 3.08 Å 2.14 Å 3.16	h 2.26 h 1.70 h 1.24 h 4.42 h 3.10	<b>h</b> 3.04 <b>l</b> 5.08 <b>l</b> 1.60 <b>l</b> 3.68 <b>l</b> 2.84	2 2.14 2 2.76 2 3.50	k 3·32 k 4·16 k 2·82	h 3.46 h 2.28 h 3.66 d 3.11	h 3.38 h 2.60 h 3.20	h 3.02 h 3.04 h 3.10	<i>እ</i> 1.92 <i>እ</i> 2.42 <i>እ</i> 2.68	k 1°98 k 2°04 k 2°96	$M = 2^{w} \cdot 94$ $w = 28 \cdot 29$ $\frac{1}{w} = 0 \cdot 04$
	3.46	2.24	3°25	2.80	3*43	3.13	3.06	3.02	2.34	2.33	$C = 59^{\circ} 5' 2'' \cdot 95$
XXX (Singra) and XXXII (Bitri)	k 4.18 k 8.06 k 9.04 k 8.36	h 4.78 h 7.02 h 8.18 h 4.68 h 9.10 h 6.92	h 7.50 h 4.34 l 8.80 l 8.02 l 6.74 l 6.78	1 7.08 1 8.46 1 6.54	h 8.20 h 6.96 h 8.18	h 7°74 h 7°34 h 8°42 d 7°81	λ 6·86 λ 6·72 λ 6·76	h 6°14 h 7°52 h 6°34	k 8°20 k 7°84 k 6°58	k 7.64 k 7.60 k 6.24	$M = 7'' \cdot 23$ $w = 18 \cdot 96$ $\frac{1}{w} = 0 \cdot 05$
	7.41	6.78	7.03	7.36	7.78	7.83	6.78	6.67	7.54	7.16	$C = 56^{\circ} 58' 7'' \cdot 21$
XXXII (Bitri) and XXXVI (Kháro)	k 34 · 96 / k 37 · 70 / k 34 · 06 / k 35 · 44 / k 33 · 90	k 38 · 18 k 37 · 86 k 36 · 10 k 37 · 26	h 34 · 50 h 34 · 74 l 37 · 14 l 33 · 48 l 33 · 96	l 35°30 l 35°82 l 36°56	h 37 · 88 h 36 · 72 h 38 · 98 h 36 · 16	h 37.68 h 35.00 h 35.40 h 33.50 h 35.82 h 37.90	k 35.68 k 36.76 k 35.48	k 38.60 k 37.60 k 36.44 k 36.64	k 36°02 h 38°16 k 36°64 k 36°90	h 36 · 20 h 36 · 10 h 35 · 10	$M = 36'' \cdot 25$ $w = 8 \cdot 38$ $\frac{1}{w} = 0 \cdot 12$
	35.31	37.35	34.76	35.89	37.44	35.88	35.97	37.32	36.93	35.80	$C = 85^{\circ} 7' 36'' \cdot 24$

At XXXIV (Kolu) March 1880; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.										
Angle between	Circle readings, telescope being set on XXXI (Asu) 216°19′ 36°19′ 295°31′ 115°31′ 14°42′ 194°42′ 93°55′ 278°55′ 178°8′ 853°7′	M = Mean of Groups $\infty$ = Relative Weight C = Concluded Angle								
XXXI (Asu) and XXXIII (Parethal)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$M = 51'' \cdot 86$ $w = 8 \cdot 68$ $\frac{1}{w} = 0 \cdot 12$ $C = 52^{\circ} 14' 51'' \cdot 86$								
XXXIII (Parethal) and XXXVI (Kháro)	$\begin{array}{c} k \ 45^{\circ} 12 \ h \ 47^{\circ} 00 \ h \ 48^{\circ} 50 \ h \ 47^{\circ} 56 \ l \ 45^{\circ} 60 \ h \ 46^{\circ} 40 \ h \ 45^{\circ} 42 \ h \ 47^{\circ} 52 \ h \ 46^{\circ} 98 \ h \ 47^{\circ} 60 \\ h \ 47^{\circ} 06 \ h \ 46^{\circ} 94 \ h \ 48^{\circ} 50 \ h \ 45^{\circ} 94 \ l \ 47^{\circ} 04 \\ h \ 45^{\circ} 94 \ h \ 47^{\circ} 64 \ h \ 46^{\circ} 98 \ h \ 45^{\circ} 94 \ l \ 47^{\circ} 04 \\ h \ 45^{\circ} 94 \ h \ 47^{\circ} 64 \ h \ 46^{\circ} 98 \ h \ 46^{\circ} 34 \ l \ 46^{\circ} 36 \ h \ 46^{\circ} 86 \ h \ 47^{\circ} 68 \ h \ 48^{\circ} 12 \ h \ 45^{\circ} 98 \ h \ 47^{\circ} 88 \\ h \ 46^{\circ} 80 \ h \ 46^{\circ} 14 \ h \ 46^{\circ} 98 \ h \ 46^{\circ} 34 \ l \ 46^{\circ} 36 \ h \ 46^{\circ} 86 \ h \ 47^{\circ} 68 \ h \ 48^{\circ} 18 \ h \ 45^{\circ} 78 \ h \ 47^{\circ} 88 \\ h \ 46^{\circ} 90 \ \phantom 66^{\circ} 66^{\circ} 66^{\circ} 66^{\circ} 76 \ \ 48^{\circ} 11 \ \ 45^{\circ} 93 \ \ 47^{\circ} 51 \end{array}$	$M = 46'' \cdot 91$ $w = 14 \cdot 84$ $\frac{1}{w} = 0 \cdot 07$ $C = 52^{\circ} 32' 46'' \cdot 90$								
XXXVI (Kháro) and XXXVII (Morgich)	\$ 58 * 22 \$ \$ 59 * 96 \$ \$ 60 * 16 \$ \$ 59 * 12 \$ 160 * 38 \$ \$ 58 * 50 \$ \$ 58 * 60 \$ \$ 60 * 58 \$ \$ 61 * 18 \$ \$ 60 * 06 \$ \$ \$ \$ 60 * 56 \$ \$ 60 * 00 \$ \$ 59 * 74 \$ \$ 59 * 94 \$ \$ 59 * 76 \$ \$ 59 * 76 \$ \$ 50 * 56 \$ \$ 60 * 00 \$ \$ 59 * 74 \$ \$ 58 * 58 \$ \$ 60 * 34 \$ \$ 59 * 70 \$ \$ \$ 58 * 34 \$ \$ 60 * 14 \$ \$ 59 * 74 \$ \$ 59 * 94 \$ \$ \$ 58 * 56 \$ \$ 61 * 22 \$ \$ 60 * 34 \$ \$ 60 * 06 \$ \$ \$ \$ 59 * 64 \$ \$ \$ 60 * 64 \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ \$	$M = 59'' \cdot 85$ $w = 28 \cdot 02$ $\frac{1}{w} = 0 \cdot 04$ $C = 38^{\circ} 53' 59'' \cdot 85$								
	59.90 59.85 60.08 59.54 59.73 59.57 59.05 60.51 60.12 60.15									

### At XXXV (Chauki)

\*March 1880; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

†December 1880; observed by Lieut.-Colonel B. R. Branfill, with Troughton and Simm's 24-inch Theodolite No. 1.

Angle between	0° 1′	Circle 180° 1'	readings 79°18'	, telesco 259°13'	pe being 158°24'	set on 2 338° 24'	XXXIX 237° 37'	(Thar M 57° 37'	Iuhári) 816° 49′	136° 49′	M - Mean of Groups w - Relative Weight C - Concluded Angle
† XXXIX (Thar Muhári) and XL (Kiraríwáro)	<i>h</i> 36 ° 09 <i>h</i> 36 ° 79 <i>h</i> 36 ° 94	h 38.01 h 38.00 h 38.50 28.17	" 1 35.95 1 35.71 1 35.85 25.84	1 36·58 1 36·58 1 36·72	h 35.68 h 36.38 h 35.84	h 36.55 h 36.48 l 36.95	" 1 36·84 1 35·99 1 37·51 26·78	l 37.31 l 37.25 l 38.04	h 37.63 h 37.41 h 37.37	" \$ 37.08 \$ 37.65 \$ 37.43 37.30	$M = 36'' \cdot 91$ $w = 17 \cdot 90$ $\frac{1}{w} = 0 \cdot 06$ $C = 43^{\circ} 45' \cdot 36'' \cdot 91$

At	XXXV	(Chauki)	)(	(Continued)	).

Angle between	0° 1′	Cir 180° 0'	cle readi 79°18′	ings, tele 259° 12′	scope be 158° 25'	sing set ( 338°24'	on XL (1 237° 36'	Kiraríwá: 57° 86'	ro) 316° <del>4</del> 9'	136° <b>4</b> 8′	M = Mean of Groups $\omega$ = Relative Weight C = Concluded Angle
• XL (Kiraríwáro) and XXXVIII (Trisingh)	* \$ 46.26 \$ 44.40 \$ 44.40 45.04	<i>k</i> 45 · 80 <i>k</i> 46 · 32 <i>k</i> 45 · 32 45 · 81	* h 44 · 54 h 45 · 66 h 44 · 26 44 · 82	k 44 · 50 k 44 · 22 k 45 · 20 44 · 64	h 43 · 54 h 45 · 30 h 44 · 44 44 · 43	h 45°12 h 45°02 h 43°84 44°66	1 46.00 1 46.18 1 46.28 46.15	* 2 45 * 58 2 45 * 60 2 44 * 96 45 * 38	" 1 45°56 1 44°00 1 45°46 45°01	* 2 45.94 2 44.34 2 44.18 44.82	$M = 45'' \cdot 08$ $w = 23 \cdot 80$ $\frac{1}{w} = 0 \cdot 04$ $C = 67^{\circ} 48' 45'' \cdot 08$
• XXXVIII (Trisingh) and XXXVI (Kháro)	\$ 55.40 \$ 54.50 \$ 55.56	h 54 · 76 h 54 · 94 h 52 · 70 h 54 · 18	h 54 · 84 h 54 · 88 h 55 · 66	k 54.54 k 54.78 k 54.36	h 55.26 h 55.42 h 55.04	h 55°36 h 55°30 h 55°32	l 54 · 40 l 54 · 18 l 54 · 86	2 54 ° 90 2 54 ° 28 2 53 ° 88 54 ° 35	2 55°16 2 54°86 2 54°24	l 55.60 l 54.62 l 55.60	$M = 54^{"} \cdot 84$ $w = 38 \cdot 82$ $\frac{1}{w} = 0 \cdot 03$ $C = 44^{\circ} 21^{'} 54^{"} \cdot 82$
• XXXVI (Kháro) and	h'41'10 h 41'56 h 41'20	h 39.78 h 40.48 h 39.80	h 41 · 18 h 40 · 36 h 40 · 70	h 40.80 h 41.64 h 40.10	h 39.70 h 40.18 h 39.68	h 40.60 l 41.22 l 40.60	l 39.42 l 40.20 l 40.14	l 40.04 l 39.92 l 39.66	l 39°28 l 40°02 l 40°06	l 40.36 l 39.80 l 39.82	$M = 40'' \cdot 31$ $M = 29 \cdot 40$ $\frac{1}{2} = 0 \cdot 03$
XXXII (Bitri)	41.39	40.03	4° • 75	40.85	39.85	40.81	39.9 <b>2</b>	39.87	39.79	<b>3</b> 9.99	$\begin{array}{c} w \\ C = 69^{\circ}  15'  40'' \cdot 31 \end{array}$

# At XXXVI (Kháro)

March 1880; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Angle between	Circle readings, telescope being set on XXXIII (Parethal) 0° 0′ 180° 0′ 79° 12′ 259° 12′ 158° 24′ 338° 24′ 237° 36′ 57° 36′ 316° 48′ 186° 48′	M - Mean of Groups w = Relative Weight C = Concluded Angle
XXXIII (Parethal) and XXXII (Bitri)	h 21 · 54 h 18 · 76 h 21 · 98 l 20 · 72 h 21 · 40 h 20 · 62 h 20 · 46 h 20 · 50 h 24 · 22 l 20 · 84 h 20 · 52 h 20 · 82 h 20 · 62 l 20 · 30 h 20 · 82 h 21 · 34 h 21 · 60 h 20 · 52 h 20 · 82 l 20 · 28 h 21 · 18 h 20 · 52 l 20 · 36 l 20 · 64 h 20 · 16 h 21 · 28 h 20 · 58 h 20 · 54 h 20 · 46 l 20 · 98 h 19 · 50 d 20 · 17 h 20 · 50 d 20 · 03 h 20 · 80	$M = 20'' \cdot 75$ $w = 32 \cdot 36$ $\frac{1}{w} = 0 \cdot 03$ $C = 40^{\circ} 28' 20'' \cdot 75$
	21.08 19.90 20.99 20.55 20.79 20.69 20.88 20.52 21.36 20.70	- 40 30 40 75
XXXII (Bitri) and XXXV (Chauki)	k 26 · 76 k 25 · 52 k 23 · 10 l 24 · 74 k 23 · 50 k 24 · 76 k 23 · 56 k 24 · 20 k 22 · 12 l 23 · 12 k 26 · 14 k 23 · 88 k 26 · 40 l 24 · 08 k 24 · 06 k 25 · 10 k 24 · 44 k 23 · 88 k 23 · 94 l 23 · 54 k 26 · 88 k 25 · 14 l 24 · 28 l 25 · 24 k 24 · 00 k 25 · 20 k 24 · 72 k 25 · 12 k 24 · 12 l 23 · 80 k 25 · 04 k 24 · 46 l 23 · 28 k 23 · 72 l 24 · 20 k 24 · 02 d 25 · 47 25 · 43 24 · 75 24 · 25 24 · 69 23 · 85 25 · 02 24 · 24 24 · 40 23 · 39 23 · 49	$M = 24^{"} \cdot 35$ $w = 16 \cdot 22$ $\frac{1}{w} = 0 \cdot 06$ $C = 57^{\circ} 35' 24^{"} \cdot 38$

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At XXXVI (Kháro)—(Continued).									
Angle between	Circle readings, telescope being set on XXXIII (Parethal) 0°0′ 180°0′ 79°12′ 259°12′ 158°24′ 338°24′ 237°86′ 57°36′ 316°48′ 136°48′	M = Mean of Groups w = Relative Weight C = Concluded Angle							
XXXV (Chauki) and XXXVIII (Trisingh)	\$\$ 0.26       \$7.58       \$8.87       \$8.06       \$0.10       \$0.77       \$0.90       \$0.17       \$8.63       \$0.15	$M = 59'' \cdot 05$ $w = 15 \cdot 68$ $\frac{1}{w} = 0 \cdot 06$ $C = 80^{\circ} 54' 59'' \cdot 06$							
XXXVIII (Trisingh) and XXXVII (Morgich)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$M = 3'' \cdot 70$ $w = 15 \cdot 04$ $\frac{1}{w} = 0 \cdot 07$ $C = 73^{\circ} 21'  3'' \cdot 75$							
XXXVII (Morgich) and XXXIV (Kolu)	h 14 · 14 h 14 · 34 h 13 · 84 l 14 · 70 h 15 · 76 h 15 · 96 h 13 · 42 h 13 · 08 h 15 · 26 l 14 · 50 h 12 · 96 h 13 · 96 h 14 · 90 l 14 · 62 h 13 · 78 h 15 · 58 h 14 · 74 h 14 · 34 h 13 · 30 l 14 · 18 h 13 · 38 h 14 · 72 h 14 · 08 l 13 · 68 h 13 · 74 h 11 · 76 h 13 · 28 h 13 · 52 h 14 · 54 l 14 · 72 h 13 · 58 h 13 · 62 h 14 · 84 h 13 · 20         13 · 49 14 · 34 14 · 27 14 · 33 14 · 22 14 · 16 13 · 81 13 · 65 14 · 37 14 · 47	$M = 14'' \cdot 11$ $w = 31 \cdot 64$ $\frac{1}{w} = 0 \cdot 03$ $C = 54^{\circ} 13' 14'' \cdot 11$							
XXXIV (Kolu) and XXXIII (Parethal)	h 59 · 68 h 58 · 26 h 58 · 54 l 58 · 74 h 59 · 00 h 59 · 76 h 58 · 84 h 59 · 40 h 58 · 76 l 58 · 40 h 59 · 44 h 59 · 34 h 59 · 18 l 58 · 86 h 58 · 92 h 59 · 06 h 58 · 72 h 58 · 66 h 58 · 72 l 58 · 80 h 58 · 86 h 58 · 28 h 59 · 70 l 58 · 76 h 59 · 20 h 56 · 50 h 59 · 62 h 60 · 16 h 59 · 14 l 59 · 30 h 59 · 92 d 57 · 90 d 57 · 76 59 · 33 58 · 63 59 · 14 58 · 79 59 · 04 58 · 48 59 · 06 59 · 41 58 · 87 58 · 83	$M = 58'' \cdot 96$ $w = 47 \cdot 21$ $\frac{1}{w} = 0 \cdot 02$ $C = 53^{\circ} 16' 58'' \cdot 94$							
At XXXVII (Morgich) March 1880; observed by Captain M. W. Rogers. R.E., with Barrow's 24-inch Theodolite No. 2.									

Angle between	° 0° 0′	C 180° 0′	ircle read 79°12'	dings, tel 259°12′	евсоре b 158° 25′	eing set 338° 25'	on XXX 237° 37'	<b>IV (K</b> ol <b>57° 36</b> ′	u) 316° 49'	136° 48′	M - Mean of Groups w - Relative Weight C - Concluded Angle
XXXIV (Kolu) and XXXVI (Kháro)	# 48 · 46 # 46 · 74 # 46 · 68 47 · 29	* \$ 47 °04 \$ 46 °50 \$ 48 °46 \$ 48 °46 \$ 47 °33	* * 45 * 88 * 48 * 48 * 45 * 96 * 47 * 24 46 * 89	* k 47 · 80 k 47 · 98 k 47 · 30 47 · 69	* \$ 44 • 92 \$ 45 • 74 \$ 45 • 86 45 • 51	\$ \$46.14 \$46.94 \$47.00 46.69	* * 43.62 * 44.74 * 48.08 * 47.22 * 46.52 * 46.52 * 45.12 * 45.88	" \$ 46.28 \$ 47.12 \$ 46.82 46.74	" 1 45°12 1 45°90 1 46°34 45°79	* 2 45 °04 2 46 °56 2 47 °54 2 46 °84 46 °50	$M = 46^{\omega} \cdot 63$ $\omega = 13 \cdot 01$ $\frac{1}{w} = 0 \cdot 08$ $C = 86^{\circ} 52' 46^{\omega} \cdot 62$

#### EASTERN SIND MERIDIONAL SERIES.

At XXXVII (Morgich)—(Continued).										
Angle between	0° 0′ 180'	Circle read 0′79°12′	lings, telescope 259°12′158°2	being set o 5' 338° 25'	on XXXI 237° 37′	[V (Koli 57°36'	u) 316° 49'	136° 48′	M - Mean of Groups so - Relative Weight C - Concluded Angle	
XXXVI (Kháro) and XXXVIII (Trisingh)	" h 60 · 62 h 59 h 60 · 30 h 59 h 60 · 20 h 58 h 59 · 92 60 · 26 59	*44     h 58*20       68     h 59*70       82     h 58*32       h 59*20       *31     58*86	* * * * * * * * * * * * * * * * * * *	" 96 h 59°12 20 h 59°50 90 h 58°76 35 59°13	" h 59·24 h 58·22 h 59·00 58·82	* 1 57.52 1 58.42 1 58.22 58.05	" 2 58.52 2 59.12 2 59.48 59.04	" 1 59°30 1 59°96 1 58°78 59°35	$M = 58'' \cdot 96$ $w = 21 \cdot 90$ $\frac{1}{w} = 0 \cdot 05$ $C = 59^{\circ} 51' 58'' \cdot 97$	

## At XXXVIII (Trisingh)

\*March 1880; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2. †December 1880; observed by Lieut.-Colonel B. R. Branfill, with Troughton and Simms' 24-inch Theodolite No. 1.

Angle hotwoon		Circl	le readin	gs, teles	cope bein	ng set on	XXXV	II (More	gich)		M = Mean of Groups
Angle Detween	813° 13′	133° 13′	<b>32° 26'</b>	212° 25'	111° <b>38′</b>	<b>2</b> 91° <b>38</b> ′	190° 50′	10° 49′	270° 2′	90° 2′	C = Concluded Angle
	"	"	"	<i>N</i> 7 0	<i>"</i>	"	"	<i>n</i> 7 - 0	"	*	26
•	h 50°44	h 50°02 h 57°84	h 57.48	h 57.54	h 57.78	h 50.44	h 56.94	1 58.12	1 57 24	l 58.80 l 57.82	$M = 57^{-1} \cdot 45$
XXXVII (Morgich)	h 60.80 h 57.44	<b>h</b> 56.28	h 56.78 h 56.94	h 57.80	h 57°58	h 57°04	h 57.18	\$ 57.40	1 58.68	h 57.92	$w = 18 \cdot 87$
and XXXVI (Kháro)	h 56 · 20 h 57 · 80										$\frac{1}{w} = 0.05$
,	57.62	56.81	56.60	57.71	57.67	56.23	57.34	58.04	57.91	58.18	$C = 46^{\circ} 46' 57'' \cdot 44$
•	1 7.38	1 7.88	h 6.74	h 7.88	h 6.88	h 7.38	h 5.68	1 7.06	1 7.88	1 7.58	$M = 7'' \cdot 28$
XXXVI (Kháro)	1 7.00	l 7.34 l 8.70	h 6.34	h 7.32	h 6.24	h 8'42 h 7'34	h 7.28	17.82	1 8.94	1 6.84	$w = 28 \cdot 87$
and							h 6.38				$\frac{1}{w} = 0.03$
XXXV (Chauki)	7.04	7.97	6.61	7.20	6.88	7.71	6.91	7.29	7`97	6.91	$C = 54^{\circ}33' 7'' \cdot 28$
	1 27.16	1 26.14	h 26.02	h 23.54	h 26.44	h 26.30	h 26.92	1 26.96	1 27.84	1 26.16	
	1 25.44	<i>1</i> 27 28 <i>1</i> 25 40	h 24.08 h 25.10	h 25.56	h 20°22 h 27°20	h 25.88	n 25.80 l 26.06	<i>l</i> 25.18 <i>l</i> 25.50	l 20·32 l 26·32	l 25°94 l 26°94	
XXXV (Chauki)			h 26.12 h 26.38	h 24°52 h 25°94							
and XL (Kiraríwáro)				h 26°14 h 27°16							
											$M = 26'' \cdot 16$
	20 13	20 27	*5 54	25 30	20 02	20 30	20 20	25'00	20-83	20-35	w = 25.88
		Cir	cle read	ings, tele	escope be	ing set o	n XXX	V (Chau	ki)		
	102° 48′	282° 48′	182°0′	2° 0′	261° 12′	81° 12′	840° 25'	160° <b>25'</b>	59° 86'	239° 86′	w = 35.73
	, "	"	"	*		"	*	*	"	•	$\frac{1}{2} = 0.03$
+	h 27.11	h 25.28	1 25.98	1 28.23	h 24.14	h 25°32	1 27.08	1 28.13	<i>l</i> 26.69	h 27°15	$C = 51^{\circ} 2' 26'' \cdot 21$
XXXV (Chauki) and	1 25.57	h 27 · 20	l 27.12 l 26.79	1 27.50	h 24.28	h 25.31	1 27.99	l 25.19	h 25.95	h 27.32	
XL (Kiraríwáro)	26.39	26.37	26.99	27.85	24.96	25.38	27.46	26.23	25.79	27.12	$M = 26'' \cdot 44$ to = 9 \cdot 85

At XXXVIII (Trisingh)—(Continued).											
Angle between	102° 48′	Circle readings, telescope being set on XXXV (Chauki) 102°48′ 282°48′ 182°0′ 2°0′ 261°12′ 81°12′ 840°25′ 160°25′ 59°36′ 239°36′									
† XL (Kiraríwáro) and XLIII (Núrpír)	<i>k</i> 14.89 <i>k</i> 17.35 <i>k</i> 16.92 16.39	" h 14°95 h 15°11 h 15°02	" l 15.69 l 14.56 l 14.12 14.79	" l 13·40 l 14·49 l 14·80 I 4·23	" h 17 · 16 h 15 · 07 h 16 · 24 16 · 16	k 15.69 k 14.56 k 15.92 15.39	<i>l</i> 15·13 <i>l</i> 14·65 <i>l</i> 14·11 14·63	" l 13·87 l 14·57 l 15·53 14·66	" h 16 · 27 h 14 · 91 l 14 · 74	* h 15.89 h 15.86 h 16.36 16.04	$M = 15'' \cdot 26$ $w = 14 \cdot 90$ $\frac{1}{w} = 0 \cdot 07$ $C = 51^{\circ}45' \cdot 15'' \cdot 26$

### At XXXIX (Thar Muhári)

December 1880; observed by Lieut.-Colonel B. R. Branfill, with Troughton and Simms' 24-inch Theodolite No. 1.

Angle between	104° 50'	284° 50′	Circle re 184° 2'	adings, 4°1'	telescope 263° 14′	being se 83° 14'	ot on XI 342° 26′	LI (Mári) 162° 25'	) 61° 38′	<b>24</b> 1° 88′	M – Mean of Groups w – Relative Weight C – Concluded Angle
XLI (Mári) and XL (Kiraríwáro)	* \$ 39.29 \$ 36.97 \$ 38.44 38.23	h 38.04 h 37.57 h 37.52 37.71	" l 38·43 l 37·17 l 39·02 38·21	1 36·94 1 37·56 1 37·95 37·48	" h 37·38 h 36·78 h 37·48 37·21	n h 37 · 63 h 35 · 99 h 36 · 32 36 · 65	" 1 38.85 1 38.41 1 38.54 38.60	" 1 36·96 1 38·05 1 36·88 37·30	n h 37 ° 95 h 37 ° 40 h 37 ° 05 37 ° 47	* \$ 36.84 \$ 36.99 \$ 37.61 37.15	$M = 37'' \cdot 60$ $w = 22 \cdot 20$ $\frac{1}{w} = 0 \cdot 05$ $C = 46^{\circ} 27' 37'' \cdot 60$
XL (Kiraríwáro) and XXXV (Chauki)	k 12.92 k 14.03 k 13.60	h 12.50 h 13.16 h 13.61	l 14.17 l 14.56 l 14.68 14.47	l 15·27 l 14·40 l 14·37 14·68	k 13.92 k 15.37 k 14.73 14.67	h 13·39 h 13·56 h 14·43 13·79	l 14.62 l 14.04 l 13.42 14.03	l 14°75 l 13°76 l 14°24 14°25	h 12.85 h 12.66 h 13.21	k 14.38 l 13.71 l 13.79 13.96	$M = 13''.94$ $w = 22 \cdot 70$ $\frac{1}{w} = 0 \cdot 04$ $C = 58^{\circ} 21' 13'' \cdot 94$

### At XL (Kiraríwáro)

December 1880; observed by Lieut.-Colonel B. R. Branfill, with Troughton and Simms' 24-inch Theodolite No. 1.

Angle between	0° 1′	( 180° 1′	Circle rea 79° 12'	dings, to 259° 12'	elescope 158° 25′	being set 338° 25'	t on XL1 237° 37′	[I (Yáru 57° 37'	.) 816° 48′	136° 48′	M = Meen of Groups w = Relative Weight C = Concluded Angle
XLII (Yáru) and XLIII (Núrpír)	" h 14.01 l 12.89 h 14.18	" l 13·20 l 10·99 l 12·50	h 11 · 19 h 12 · 32 h 12 · 88	<i>h</i> 13·24 <i>l</i> 12·96 <i>l</i> 13·23	<i>l</i> 12·30 <i>l</i> 13·49 <i>l</i> 12·19 12·66	<i>h</i> 12·32 <i>h</i> 12·91 <i>l</i> 12·77 12·67	<i>l</i> 11 · 95 <i>l</i> 12 · 23 <i>l</i> 10 · 26	<i>l</i> 12·29 <i>l</i> 11·57 <i>l</i> 13·77	<i>n</i> <i>h</i> 12 · 76 <i>h</i> 12 · 30 <i>l</i> 12 · 06 12 · 37	<pre>     l 12 · 94     l 11 · 70     l 12 · 17     l2 · 27 </pre>	$M = 12'' \cdot 52$ $w = 20 \cdot 40$ $\frac{1}{w} = 0 \cdot 05$ $C = 51^{\circ} c' 10'' \cdot 50$
XLIII (Núrpír) and XXXVIII (Trisingh)	<i>k</i> 40°41 <i>k</i> 41°93 <i>l</i> 42°80 41°71	l 42.68 l 42.14 l 41.04 41.95	h 41 · 54 h 40 · 32 h 39 · 23 40 · 36	h 39.52 l 40.07 l 41.22 40.27	l 41 · 84 l 40 · 45 l 41 · 74 41 · 34	h 42 · 53 h 41 · 15 l 40 · 70 41 · 46	l 41.05 l 41.34 l 42.26 41.55	l 40.34 l 40.78 l 39.85 40.32	h 42°57 l 41°67 h 40°79 41°68	l 40.52 l 41.73 l 41.61 41.29	$M = 41'' \cdot 19$ $M = 41'' \cdot 19$ $w = 17 \cdot 50$ $\frac{1}{w} = 0 \cdot 06$ $C = 59^{\circ} 49' 41'' \cdot 19$

At XL (Kiraríwáro)—(Continued).

Angle between	Circle readings, telescope being set on XLII (Yáru) 0° 1′ 180° 1′ 79° 12′ 259° 12′ 158° 25′ 838° 25′ 237° 87′ 57° 37′ 316° 48′ 136° 48′	M = Mean of Groups w = Relative Weight C = Concluded Angle
XXXVIII (Trisingh) and XXXV (Chauki)	*       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *	$M = 50'' \cdot 01$ $w = 15 \cdot 20$ $\frac{1}{w} = 0 \cdot 07$ $C = 61^{\circ} 8' 50'' \cdot 01$
XXXV (Chauki) and XXXIX (Thar Muhári)	k 8.95 l 12.14 k 11.54 k 9.08 l 10.49 k 10.92 l 9.01 l 9.02 k 10.65 l 9.82 k 10.24 l 10.73 k 9.76 l 10.80 l 8.64 k 12.54 l 8.35 l 8.69 k 11.40 l 11.44 l 8.89 k 9.90 k 10.39 l 9.53 l 9.28 l 10.07 l 8.80 l 8.82 l 10.27 l 10.53 9.36 10.92 10.56 9.80 9.47 11.18 8.72 8.84 10.77 10.60	$M = 10" \cdot 02$ $w = 10' \cdot 40$ $\frac{1}{w} = 0' \cdot 10$ $C = 77^{\circ} 53' 10" \cdot 02$
XXXIX (Thar Muhári) and XLI (Mári)	$\begin{array}{c} h \ 34 \cdot 81 \ l \ 33 \cdot 57 \ h \ 33 \cdot 04 \ h \ 34 \cdot 32 \ l \ 35 \cdot 15 \ h \ 33 \cdot 46 \ l \ 34 \cdot 50 \ l \ 35 \cdot 29 \ h \ 33 \cdot 00 \ l \ 32 \cdot 76 \\ h \ 33 \cdot 26 \ l \ 34 \cdot 80 \ h \ 33 \cdot 68 \ l \ 33 \cdot 21 \ l \ 34 \cdot 33 \ l \ 34 \cdot 83 \ l \ 34 \cdot 87 \ l \ 34 \cdot 58 \ l \ 34 \cdot 35 \ l \ 33 \cdot 65 \\ l \ 34 \cdot 99 \ l \ 34 \cdot 19 \ h \ 33 \cdot 55 \ l \ 34 \cdot 74 \ l \ 34 \cdot 75 \ h \ 34 \cdot 38 \ l \ 34 \cdot 48 \ l \ 34 \cdot 76 \ h \ 34 \cdot 93 \ l \ 32 \cdot 18 \\ \hline \\ 34 \cdot 35 \ \ 34 \cdot 19 \ \ 33 \cdot 42 \ \ 34 \cdot 09 \ \ 34 \cdot 74 \ \ 34 \cdot 75 \ \ 34 \cdot 22 \ \ 34 \cdot 62 \ \ 34 \cdot 88 \ \ 34 \cdot 09 \ \ 32 \cdot 86 \end{array}$	$M = 34'' \cdot 15$ $w = 21 \cdot 30$ $\frac{1}{w} = 0 \cdot 05$ $C = 69^{\circ} 17' 34'' \cdot 15$
XLI (Mári) and XLII (Yáru)	h 31 · 44 l 29 · 04 h 32 · 90 h 31 · 62 l 30 · 75 h 31 · 60 l 31 · 52 l 32 · 00 h 30 · 91 l 34 · 28 h 30 · 96 l 30 · 16 h 32 · 59 l 31 · 37 l 32 · 37 h 32 · 73 l 32 · 01 l 32 · 10 h 31 · 78 l 34 · 23 l 31 · 14 l 29 · 98 h 32 · 58 l 31 · 24 l 32 · 20 l 31 · 49 l 31 · 85 l 31 · 96 l 31 · 80 h 32 · 65 31 · 18 29 · 73 32 · 69 31 · 41 31 · 77 31 · 94 31 · 79 32 · 02 31 · 50 33 · 72	$M = 31'' \cdot 78$ $w = 8 \cdot 90$ $\frac{1}{w} = 0 \cdot 11$ $C = 40^{\circ} 47' 31'' \cdot 78$

## At XLI (Mári)

December 1880; observed by Lieut.-Colonel B. R. Branfill, with Troughton and Simms' 24-inch Theodolite No. 1.

Angle between	Circle readings, telescope being set on XLII (Yáru) 0°1′ 180°0′ 79°18′ 259°12′ 158°24′ 338°24′ 227°37′ 47°37′ 316°49′ 186°49′	M - Mean of Groups w - Relative Weight C = Concluded Angle
XLII (Yáru) and XL (Kiraríwáro)	h 55.07       l 56.16       h 56.19       h 57.01       l 57.08       l 55.99       l 56.93       h 55.50       h 56.82       l 55.93         l 56.48       l 55.33       h 56.62       h 56.15       l 54.42       l 56.75       h 56.51       h 56.09       l 55.87         l 55.57       l 54.82       h 56.29       h 56.44       h 55.44       l 55.88       h 56.06       h 56.27       l 55.32         55.71       55.44       55.65       56.21       55.98       55.87       56.39       55.71	$M = 55^{\circ} \cdot 99$ $w = 41 \cdot 70$ $\frac{1}{w} = 0 \cdot 02$ $C = 77^{\circ} 3' 55'' \cdot 99$
XL (Kiraríwáro) and XXXIX (Thar Muhári)	$\begin{array}{c} h \ 49^{\circ}89 \ l \ 48^{\circ}81 \ h \ 50^{\circ}28 \ h \ 47^{\circ}75 \ l \ 49^{\circ}85 \ l \ 48^{\circ}45 \ l \ 48^{\circ}95 \ h \ 49^{\circ}52 \ h \ 48^{\circ}11 \ l \ 47^{\circ}43 \\ l \ 49^{\circ}45 \ l \ 46^{\circ}72 \ h \ 48^{\circ}25 \ h \ 48^{\circ}84 \ l \ 49^{\circ}74 \ l \ 47^{\circ}99 \ l \ 50^{\circ}00 \ h \ 50^{\circ}25 \ h \ 48^{\circ}71 \ l \ 49^{\circ}99 \\ l \ 48^{\circ}62 \ l \ 47^{\circ}69 \ h \ 48^{\circ}84 \ l \ 48^{\circ}22 \ h \ 49^{\circ}63 \ h \ 49^{\circ}49 \ h \ 49^{\circ}22 \ h \ 49^{\circ}33 \ l \ 47^{\circ}28 \ l \ 48^{\circ}63 \\ \hline 49^{\circ}32 \ \ 47^{\circ}74 \ \ 49^{\circ}12 \ \ 48^{\circ}27 \ \ 49^{\circ}74 \ \ 48^{\circ}64 \ \ 49^{\circ}39 \ \ 49^{\circ}70 \ \ 48^{\circ}03 \ \ 48^{\circ}68 \end{array}$	$M = 48'' \cdot 86$ $w = 15 \cdot 90$ $\frac{1}{w} = 0 \cdot 06$ $C = 64^{\circ} 14' 48'' \cdot 86$
# At XLII (Yáru)

# December 1880; observed by Lieut.-Colonel B. R. Branfill with Troughton and Simms' 24-inch Theodolite No. 1.

Angle between	Circle readings, telescope being set on XLIV (Vijnot) 224° 10′ 44° 10′ 303° 21′ 123° 21′ 22° 34′ 202° 34′ 101° 46′ 281° 45′ 180° 58′ 0° 57′	M - Mean of Groups $\infty$ - Relative Weight C - Concluded Angle
XLIV (Vijnot) and XLV (Longwáli)	h 45 · 49 h 48 · 56 l 46 · 68 h 49 · 84 h 48 · 04 l 47 · 19 h 48 · 52 h 49 · 77 l 47 · 72 l 47 · 45         h 45 · 49 h 48 · 56 l 46 · 68 h 49 · 84 h 48 · 04 l 47 · 19 h 48 · 52 h 49 · 77 l 47 · 72 l 47 · 45         h 48 · 13 l 49 · 09 l 49 · 14 h 49 · 21 l 47 · 36 l 48 · 30 h 49 · 38 h 48 · 92 l 48 · 19 l 47 · 76         h 47 · 28 l 49 · 00 l 48 · 42 h 49 · 50 l 47 · 48 l 46 · 66 h 47 · 90 l 48 · 48 l 47 · 44 l 48 · 43         46 · 97 48 · 88 48 · 08 49 · 52 47 · 63 47 · 38 48 · 60 49 · 06 47 · 78 47 · 88	$M = 48'' \cdot 18$ $w = 12 \cdot 70$ $\frac{1}{w} = 0 \cdot 08$ $C = 39^{\circ} 23' 48'' \cdot 18$
XLV (Longwáli) and XLIII (Núrpír)	k 16 · 22 k 15 · 38 l 16 · 36 k 13 · 67 k 17 · 40 l 14 · 61 k 14 · 05 k 15 · 42 l 15 · 31 l 17 · 02 h 17 · 42 l 15 · 44 l 15 · 66 k 14 · 80 l 15 · 91 l 15 · 74 k 14 · 83 k 17 · 09 l 15 · 55 l 15 · 49 k 16 · 29 l 16 · 29 l 14 · 22 k 14 · 90 l 18 · 43 l 15 · 96 k 14 · 91 l 16 · 34 l 16 · 90 l 16 · 09 16 · 64 15 · 70 15 · 41 14 · 46 17 · 25 15 · 44 14 · 60 16 · 28 15 · 92 16 · 20	$M = 15'' \cdot 79$ $w = 11 \cdot 00$ $\frac{1}{w} = 0 \cdot 09$ $C = 39^{\circ} 4' 15'' \cdot 79$
XLIII (Núrpír) and XL (Kiraríwáro)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$M = 2^{"} \cdot 50$ $w = 13 \cdot 58$ $\frac{1}{w} = 0 \cdot 07$ $C = 80^{\circ} 20^{\prime} \cdot 2^{"} \cdot 52$
XL (Kiraríwáro) and XLI (Mári)	$\begin{array}{c} \begin{array}{c} \begin{array}{c} 3 & 5 & 4 & 2 & 7 & 4 & 1 & 4 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 3 & 1 & 2 & 0 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 3 & 1 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 3 & 1 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 3 & 1 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 3 & 1 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 3 & 1 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 3 & 1 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 3 & 1 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 3 & 1 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 3 & 1 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \end{array} \\ \begin{array}{c} 3 & 2 & 5 & 5 \end{array} \\ \begin{array}{c} 3 & 2 & 5 \end{array} \\ \end{array} \\ \begin{array}{c} 3 & 2 & 5 \end{array} \\ \end{array} \end{array} $ \\ \begin{array}{c} 3 & 2 & 5 \end{array} \\ \begin{array}{c} 3 & 2 & 5 \end{array} \\ \end{array} \end{array}  \\ \begin{array}{c} 3 & 2 & 5 \end{array} \\ \begin{array}{c} 3 & 2 & 5 \end{array} \\ \end{array} \end{array}  \\ \begin{array}{c} 3 & 2 & 5 \end{array} \end{array} \\ \begin{array}{c} 3 & 2 & 5 \end{array} \\ \end{array} \end{array}  \\ \begin{array}{c} 3 & 2 & 5 \end{array} \end{array}  \\ \begin{array}{c} 3 & 2 & 5 \end{array} \end{array} \\ \end{array}  \\ \begin{array}{c} 3 & 2 & 5 \end{array} \end{array}  \\ \begin{array}{c} 3 & 2 & 5 \end{array} \end{array} \end{array}  \\ \begin{array}{c} 3 & 2 & 5 \end{array} \end{array} \end{array} \end{array}  \\ \begin{array}{c} 3 & 2 & 5 \end{array} \end{array} \end{array} \end{array} \\ \end{array}  \\ \begin{array}{c} 3 & 2 & 5 \end{array} \end{array} \end{array} \end{array} \\	$C = 83^{\circ} 32^{\circ} 2^{\circ} \cdot 51$ $M = 32^{\circ} \cdot 59$ $w = 10 \cdot 00$ $\frac{1}{w} = 0 \cdot 10$
	32.00 31.80 32.93 32.91 32.42 32.09 31.86 34.77 32.20 32.89	$C = 62^{\circ} 8' 32'' \cdot 59$

# At XLIII (Núrpír)

December 1880; observed by Lieut.-Colonel B. R. Branfill with Troughton and Simms' 24-inch Theodolite No. 1.

Angle between	0° 1′	Circle 180° 1′	• reading 79° 18'	78, telesc 259° 12'	ope being 158° 24'	g set on 838° 24'	XXXVI 237° 87'	II (Trie 57° 37'	ingh) 816°49′	136° 48′	M - Mean of Groups v = Relative Weight C = Concluded Angle
XXXVIII (Trisingh) and	k 5.47 k 3.60 k 5.01	k 5°28 k 5°07 l 5°90	" l 4·41 l 4·25 l 3·27	k 5.53 k 4.90 k 4.84	h 4°02 l 3°94 l 4°06	" 1 3.66 1 4.01 1 4.79	h 4·45 h 3·82 h 4·55	h 4°20 h 3°97 h 3°87	* 2 4·93 2 4·39 2 4·41	k 5.90 k 5.53 k 4.58	$M = 4^{"} \cdot 55$ $w = 27 \cdot 00$ $\frac{1}{w} = 0 \cdot 04$
XL (Kiraríwáro)	4.69	5.42	3.98	5.09	4.01	4.12	4*27	4.01	4.28	5°34	$\begin{bmatrix} ~~\\ C = 68^{\circ} 25' 4'' \cdot 55 \end{bmatrix}$

At XLIII (Núrpír)—(Continued).										
Angle between	Circle readings, telescope being set on XXXVIII (Trisingh) 0°1' 180°1' 79°13' 259°12' 158°24' 338°24' 237°37' 57°37' 316°49' 136°48'	M = Mean of Groups w = Relative Weight C = Concluded Angle								
XL (Kiraríwáro) and XLII (Yáru)	k 43 · 27       k 43 · 41       l 43 · 20       k 44 · 69       k 43 · 75       l 44 · 62       k 43 · 15       k 43 · 82       l 44 · 73       l 45 · 38         k 44 · 09       k 44 · 31       l 42 · 54       k 43 · 67       l 43 · 43       l 43 · 52       k 44 · 20       k 45 · 32       l 44 · 26       k 44 · 10         k 43 · 72       l 44 · 85       l 43 · 75       l 42 · 97       l 45 · 55       k 43 · 37       l 44 · 21       k 43 · 53         43 · 69       44 · 19       43 · 16       44 · 37       43 · 38       44 · 56       43 · 57       44 · 50       44 · 40       44 · 34	$M = 44'' \cdot 02$ $w = 27 \cdot 80$ $\frac{1}{w} = 0 \cdot 04$ $C = 45^{\circ} 24' 44'' \cdot 02$								
XLII (Yárn) and XLIV (Vijnot)	h 50.29 h 51.00 l 51.20 h 49.62 h 49.55 l 48.76 h 51.05 h 50.94 l 49.94 l 50.22 h 50.97 h 50.90 l 50.92 h 51.16 l 51.14 l 49.67 h 50.55 h 50.37 l 50.51 h 50.34 h 50.90 l 49.66 l 50.25 h 49.73 l 49.52 l 49.94 h 51.19 h 50.46 l 50.86 h 50.30 h 50.48	$M = 50'' \cdot 40$ $w = 40 \cdot 17$ $\frac{1}{w} = 0 \cdot 02$ $C = 42^{\circ} 10'_{\circ} 50''' \cdot 40$								
XLIV (Vijnot) and XLV (Longwáli)	h 49 °01 h 48 °47 l 48 °56 h 48 °23 h 48 °17 l 51 °10 h 48 °80 h 49 °57 l 47 °55 l 49 °70 h 49 °34 h 47 °59 l 49 °13 h 49 °03 l 48 °52 l 49 °43 h 47 °71 h 49 °41 l 48 °21 h 48 °40 h 48 °66 l 47 °81 l 49 °07 h 49 °43 l 48 °33 l 48 °73 h 48 °85 l 49 °54 l 49 °10 h 49 °20									
XLV (Longwáli)	49'00 47'96 48'92 48'90 48'34 49'75 48'45 49'51 48'29 49'10	$C = 47^{\circ} 46' 48'' \cdot 82$								

# At XLIV (Vijnot)

December 1880 and January 1881; observed by Lieut.-Colonel B. R. Branfill with Troughton and Simms' 24-inch Theodolite No. 1.

Angle between	Circle readings, telescope being set on XLVIII (Dewari) 0°1′ 180°1′ 79°18′ 259°13′ 158°24′ 838°25′ 237°36′ 57°37′ 316°49′ 136°49′	M = Mean of Groups w = Relative Weight C = Concluded Angle
XLVIII (Dewari) and R. M.	k 48.26       k 48.67       k 47.53       k 48.13       k 49.15       k 49.70       k 48.98       k 48.45       k 49.81       k 49.32         k 46.48       l 49.23       k 48.09       l 49.34       k 47.60       k 50.10       k 48.15       l 46.85       k 49.31       l 47.25         k 47.24       k 47.97       k 46.05       k 47.83       l 47.87       l 48.51       k 48.34       k 50.47       l 48.81         k 46.47	$M = 48'' \cdot 34$ $w = 11 \cdot 06$ $\frac{1}{w} = 0 \cdot 09$ $C = 36^{\circ} 31' \cdot 48'' \cdot 33$
XLVIII (Dewari) and XLVI (Vín)	h 39 93 h 39 13 h 39 86 h 38 75 h 41 19 h 40 35 h 40 14 h 39 15 h 39 61 h 39 70 h 38 96 l 39 15 h 40 46 l 42 05 h 38 12 h 41 72 h 40 10 h 38 31 h 40 09 l 41 98 h 39 47 h 39 19 h 38 55 l 40 18 h 38 99 l 39 47 h 39 62 h 38 28 h 40 13 h 39 16 h 40 34 39 68 39 16 39 62 40 33 39 16 40 51 39 95 38 58 39 94 40 28	$M = 39'' \cdot 72$ $w = 16 \cdot 76$ $\frac{1}{w} = 0 \cdot 06$ $C = 61^{\circ} 37' 39'' \cdot 71$

Nore.-R. M. denotes Referring Mark.

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At XLIV (Vijnot)—(Continued).									
Angle between	Circle readings, telescope being set on XLVIII (Dewari) 0°1' 180°1' 79°13' 259°13' 158°24' 838°25' 237°36' 57°37' 816°49' 136°49'	M = Mean  of Groups w = Relative Weight C = Concluded Angle							
XLVI (Vín) and XLV (Longwáli)	k 27.66 k 27.07 k 26.52 k 27.71 k 26.53 k 27.91 k 27.57 k 27.19 k 29.38 k 28.36 k 26.72 l 27.63 k 26.36 l 27.42 k 26.74 k 27.06 k 27.16 l 30.09 k 28.58 k 29.19 k 26.07 k 28.60 k 25.87 k 28.06 k 27.60 l 28.70 k 26.69 k 27.52 k 28.30 k 30.15 26.82 27.77 26.25 27.73 26.96 27.89 27.14 28.27 28.75 29.23	$M = 27'' \cdot 68$ $w = 10 \cdot 20$ $\frac{1}{w} = 0 \cdot 10$ $C = 46^{\circ} 16' 27'' \cdot 68$							
XLV (Longwáli) and XLIII (Núrpír)	h 32 · 42 h 31 · 77 h 32 · 52 h 29 · 61 h 30 · 42 h 29 · 24 h 30 · 93 h 31 · 95 h 29 · 85 h 30 · 63 h 30 · 39 h 30 · 59 h 30 · 43 l 29 · 49 h 31 · 39 h 31 · 37 h 31 · 11 l 30 · 17 h 29 · 73 l 29 · 44 h 31 · 30 h 31 · 08 h 31 · 85 h 28 · 62 h 30 · 62 h 31 · 94 h 29 · 63 h 30 · 09 h 29 · 54 h 29 · 48 h 31 · 82 31 · 37 31 · 32 31 · 60 29 · 24 30 · 81 30 · 85 30 · 56 30 · 74 29 · 71 29 · 85	$M = 30'' \cdot 61$ $w = 13 \cdot 07$ $\frac{1}{w} = 0 \cdot 08$ $C = 45^{\circ} 33' 30'' \cdot 60$							
XLIII (Núrpír) and XLII (Yáru)	$ \begin{array}{c} h \ 5 \cdot 26 \ h \ 4 \cdot 73 \ h \ 7 \cdot 35 \ h \ 8 \cdot 27 \ h \ 5 \cdot 66 \ h \ 6 \cdot 55 \ h \ 5 \cdot 93 \ h \ 5 \cdot 26 \ h \ 6 \cdot 55 \ h \ 6 \cdot 55 \ h \ 6 \cdot 50 \\ h \ 8 \cdot 26 \ h \ 4 \cdot 72 \ h \ 7 \cdot 90 \ l \ 7 \cdot 02 \ h \ 5 \cdot 71 \ h \ 5 \cdot 32 \ h \ 6 \cdot 43 \ l \ 8 \cdot 45 \ h \ 5 \cdot 84 \ l \ 6 \cdot 82 \\ h \ 5 \cdot 34 \ h \ 4 \cdot 29 \ h \ 7 \cdot 23 \ h \ 6 \cdot 96 \ h \ 5 \cdot 94 \ l \ 7 \cdot 62 \ h \ 8 \cdot 01 \ h \ 6 \cdot 90 \ h \ 6 \cdot 75 \ l \ 5 \cdot 77 \\ h \ 5 \cdot 25 \end{array} $	$M = 6'' \cdot 40$ $w = 10 \cdot 86$ $\frac{1}{w} = 0 \cdot 09$ $C = 58^{\circ} 21' 6'' \cdot 40$							

# At XLV (Longwáli)

# January 1881; observed by Lieut.-Colonel B. R. Branfill with Troughton and Simms' 24-inch Theodolite No. 1.

Angle between	185°6′ 5°6′	Circle readings, tel 264°18′84°18′	escope being set on XLIII 843°80′ 163°29′ 62°42′	(Nárpír) 242° 42′ 141° 54′ 821° 54′	M - Mean of Groups = Relative Weight C = Concluded Angle
XLIII (Núrpír) and XLII (Yáru)	k       7.44       k       6.00         k       6.82       l       6.11         l       6.28       l       5.8         l       5.4       l       5.4	5 h 3.88 h 5.16 0 h 5.87 h 4.32 4 h 4.44 h 4.38 2 5 4.73 4.6	l 6.98 k 4.49 k 6.54 k l 7.03 l 5.03 k 4.09 k l 6.17 l 3.80 k 6.09 l 6.73 4.44 5.57	4.47 5.69 7.25	$M = 5'' \cdot 62$ $w = 8 \cdot 12$ $\frac{1}{w} = 0 \cdot 12$ $C = 49^{\circ} 58' 5'' \cdot 62$
XLII (Yárn) and XLIV (Vijnot)	1 h 35.14 h 35.1 h 35.36 l 35.9 l 34.01 l 36.9 l 36.2 34.84 36.0	2 h 34 · 43 h 34 · 78 6 h 34 · 88 h 34 · 98 1 h 33 · 29 h 34 · 92 4 6 34 · 80 34 · 89	1 34.59 1 38.14 k 34.94 k 1 35.36 1 38.17 k 34.60 k 1 35.34 k 36.99 k 34.46 l 35.10 37.77 34.67	37.14 1 37.06 1 35.95 36.13 1 35.30 1 34.92 36.50 1 36.29 1 33.60 36.59 36.22 34.82	$M = 35'' \cdot 52$ $w = 7 \cdot 51$ $\frac{1}{w} = 0 \cdot 13$ $C = 36^{\circ} 41' 35'' \cdot 52$

At XLV (Longwáli)-(Continued).

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Angle between	185° 6'	Cin 5° 6′	rcle read 264° 18'	ings, tel 84°18'	escope be 343° 30'	əing set o 163° 29'	on XLII 62° 42'	I (Núrp 242° 42'	oír) 141°54	321° 54′	M = Mean of Groups to = Relative Weight C = Concluded Angle
XLIV (Vijnot) and XLVI (Vín)	ћ 44 · 22 / ћ 44 · 13 / l 45 · 56 /	44 ° 93 1 46 ° 16 1 44 ° 95 1 44 ° 97	n h 45 ° 47 h 45 ° 94 h 45 ° 33	* h 45 · 32 h 45 · 33 h 46 · 19	7 l 46.06 l 45.52 l 45.82	• l 44 • 97 l 45 • 36 l 44 • 72	* h 44 · 77 h 45 · 81 h 44 · 49	*	• l 44·67 l 45·31 l 45·49	r l 44.09 h 44.12 h 45.35	$M = 45'' \cdot 10$ $w = 33 \cdot 54$ $\frac{1}{w} = 0 \cdot 03$
	44.64	45°25	45*58	45.61	45.80	45.03	45.03	44 * 43	45.16	44.23	$C = 47^{\circ} 39' 45'' \cdot 10$
XLVI (Vín) and XLVII (Got Mír Muhammad)	k 53·32 k 53·19 k 54·17	k 52°58 l 53°13 l 52°47	h 52°98 h 53°98 h 52°81	ћ 53°57 ћ 53°53 ћ 51°93	l 52.01 l 51.98 l 51.76	l 51 °07 l 52 °68 l 52 °62	h 52°60 h 53°18 h 53°71	h 52.88 h 54.52 l 55.48	l 52.69 l 52.90 l 53.19	l 53°80 h 53°32 h 53°42	$M = 53'' \cdot 05$ $w = 16 \cdot 90$ $\frac{1}{m} = 0 \cdot 06$
	53.26	52.73	53.36	53.01	51.93	52.13	53 · 16	54.39	52.93	53.21	$C = 50^{\circ} 45' 53'' \cdot 05$
At XLVI (Vín) January 1881; observed by LieutColonel B. R. Branfill with Troughton and Simms' 24-inch Theodolite No. 1.											
Angle between	0° 1′	Cir 180° 1′	cle readi 79°12′	ings, tele 259° 13′	жсоре be 158° 25′	ing set o 838° 25'	n XLV 237°37'	(Longwá 57° 37'	11i) 316° 48′	186° 49′	M - Mean of Groups • - Relative Weight C - Concluded Angle
XLV (Longwáli) and XLIV (Vijnot)	k 46 · 86 1 k 47 · 45 k 47 · 79 j	46 · 19 46 · 76 51 · 20 49 · 62	n h 48 · 32 h 47 · 56 h 48 · 24	n h 47 · 26 l 45 · 67 l 47 · 20	h 46.65 h 46.75 d 47.63	h 46 · 93 l 45 · 07 l 45 · 27	l 45°31 l 46°84 l 47°27	k 50 · 52 k 47 · 37 k 46 · 00	h 47 · 86 h 48 · 16 h 48 · 41	k 50°70 l 47°75 l 48°13 k 47°74	$M = 47'' \cdot 45$ $w = 7 \cdot 74$ $\frac{1}{w} = 0 \cdot 13$
	47`37	48.44	48.04	46.21	47.01	45.76	46 • 47	47 • 96	48.14	48.28	$C = 86^{\circ} 3' 47'' \cdot 47$
XLIV (Vijnot) and XLVIII (Dewari)	k 4.86 h 6.01 h 5.85	l 3°54 l 2°84 h 3°02	h 5.07 h 3.16 h 2.48 h 3.48	h 5.26 l 2.22 h 5.00	k 5.28 k 5.64 l 5.02	k 5°47 k 5°91 k 6°33	1 5.85 1 3.80 1 2.76 h 5.97	k 2·34 k 5·74 k 1·81 d 5·28	k 5.94 k 5.16 k 4.58	h 5.74 h 3.63 h 3.68	$M = 4'' \cdot 56$ $w = 8 \cdot 48$ $\frac{1}{w} = 0 \cdot 12$
	5.22	3.13	3.22	4.16	5.31	5.90	4.60	3.29	5.33	4*35	$C = 71^{\circ}45' 4'' \cdot 55$
XLVIII (Dewari) and XLIX (Kot Sabzal)	k 24 · 75 k 23 · 13 k 22 · 67	l 24°37 l 25°16 l 24°02	h 24 · 42 h 25 · 08 h 23 · 97	h 24°93 l 25°23 l 24°93	<b>k</b> 23·33 k 23·92 k 24·14	h 23 · 78 h 24 · 15 h 23 · 92	l 24°13 l 25°44 h 23°87	k 25°94 k 23°77 k 23°77	h 23°47 h 23°55 h 24°20	l 25.69 h 23.29 h 24.51 h 24.18 h 25.22	$M = 24'' \cdot 26$ $w = 28 \cdot 25$ $\frac{1}{w} = 0 \cdot 04$
	23.22	24.22	24.49	25.03	23.80	23.95	24 · 48	24.49	23.74	<b>24</b> •58	$C = 54^\circ 51' 24'' \cdot 27$

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At XLVI (Vin)—(Continued).									
Angle between	Circle readings, telescope being set on XLV (Longwáli) 0°1′ 180°1′ 79°12′ 259°13′ 158°25′ 838°25′ 237°37′ 57°37′ 816°48′ 136°49′	M - Mean of Groups w - Relative Weight C - Concluded Angle							
XLIX (Kot Sabzal) and XLVII (Got Mír Muhammad)	*       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *       *	$M = 52w \cdot 73$ $w = 5 \cdot 03$ $\frac{1}{w} = 0 \cdot 20$ $C = 80^{\circ} 34' 52'' \cdot 73$							
XLVII (Got Mír Muhammad) and XLV (Longwáli)	k 49.81 l 51.06 k 52.58 k 50.85 k 51.35 k 48.96 l 48.64 k 51.67 k 50.98 k 49.98 k 51.25 l 49.49 k 51.96 l 51.12 k 51.17 k 49.97 l 49.85 k 52.89 k 50.29 l 47.89 k 49.96 l 50.98 k 50.69 l 52.62 k 50.91 k 47.97 d 52.53 k 50.55 k 51.79 k 54.73 d 51.53	$M = 50'' \cdot 83$ $w = 8 \cdot 40$ $\frac{1}{w} = 0 \cdot 12$							
	50.34 50.21 51.24 51.23 51.14 48.97 50.34 51.20 51.02 51.03	$C = 66^{\circ} 44' 50'' \cdot 83$							

## At XLVII (Got Mír Muhammad)

January 1881; observed by Lieut.-Colonel B. R. Branfill with Troughton and Simms' 24-inch Theodolite No. 1.

Angle between	0°1′	Ci 180° 1'	rcle read 79°13′	ings, tele 259°13′	escope be 158° 24'	oing set o 838° 24'	on XLV 237° 37'	(Longwa 57° 37'	áli) 816° 49′	136° 49′	M = Mean of Groups w = Relative Weight C = Concluded Angle
XLV (Longwáli) and XLVI (Vín)	<i>k</i> 15.65 <i>k</i> 15.79 <i>k</i> 13.80 15.08	k 16 · 72 h 14 · 37 k 16 · 20 15 · 76	<i>k</i> 15.82 <i>l</i> 18.10 <i>l</i> 17.70 17.21	<i>l</i> 18.01 <i>l</i> 16.36 <i>l</i> 17.73 17.37	<i>k</i> 15°35 <i>h</i> 14°29 <i>k</i> 16°01 15°22	" h 16 · 50 h 16 · 06 h 16 · 67 16 · 41	k 16.90 k 17.14 l 15.80 16.61	" 18.10 16.40 17.28 17.26	<i>t</i> <i>i</i> <i>i</i> <i>i</i> <i>i</i> <i>i</i> <i>i</i> <i>i</i> <i>i</i> <i>i</i> <i>i</i>	* h 15.06 h 15.52 h 16.46 15.68	$M = 16'' \cdot 15$ $w = 9 \cdot 20$ $\frac{1}{w} = 0 \cdot 11$ $C = 62^{\circ} 29' 16'' \cdot 15$
XLVI (Vín) and XLIX (Kot Sabzal)	k 48 · 82 k 49 · 48 k 49 · 07 49 · 12	h 52.81 h 50.33 h 50.98	h 48 · 27 l 45 · 48 h 51 · 62 48 · 46	l 46 · 26 l 46 · 56 h 51 · 68 48 · 17	h 48.62 h 48.73 h 47.38 48.24	h 48.85 h 50.93 h 50.80 50.19	h 48 · 27 h 48 · 05 l 48 · 86 48 · 39	2 49.61 2 48.38 3 51.58 49.86	l 49.05 l 49.93 l 49.38 49.45	h 51 · 60 h 50 · 23 h 51 · 79 51 · 21	$M = 49'' \cdot 45$ $w = 5 \cdot 00$ $\frac{1}{w} = 0 \cdot 20$ $C = 55^{\circ} 49' \cdot 49'' \cdot 45$

## At XLVIII (Dewari)

January 1881; observed by Lieut.-Colonel B. R. Branfill with Troughton and Simms' 24-inch Theodolite No. 1.

Angle between	<b>224°</b> 17′	<b>44°</b> 17′	Circle 1 803° 29'	readings, 123° 30′	telescop 22° 42'	e being a 202° 42'	et on L 101° 54′	(Kubba) 281° 54'	181° 5′	1°5′	M - Mean of Groups w - Relative Weight C - Concluded Angle
L (Kubba) and LI (Ghundi)	h 35 · 89 h 35 · 58 h 36 · 85	n h 36·61 h 37·79 h 37·09	" l 37·02 h 36·95 h 36·69	h 38·35 h 37·35 h 38·12	" h 38 · 00 l 35 · 80 h 36 · 34 d 35 · 86	* l 37·22 l 36·78 h 36·55	* h 35 · 93 h 37 · 13 h 37 · 06	" h 36 · 43 l 33 · 79 l 32 · 49 d 34 · 48	" h 33 · 55 h 37 · 40 h 36 · 49 h 36 · 91	h 36 · 21 h 37 · 22 h 37 · 73	$M = 36'' \cdot 56$ $w = 8 \cdot 62$ $\frac{1}{w} = 0 \cdot 12$ $G = 66^{3} \cdot 66'' \cdot 12$
	36.11	37.16	36.89	37.94	36.20	36.85	36.21	34.30	36.09	37.02	$C = 63^{\circ} 42^{\circ} 36^{\circ} \cdot 55$

At XLVIII (Dewari)—(Continued).									
Angle between	Circle readings, telescope being set on L (Kubba) 234°17′44°17′803°29′123°30′22°42′202°42′101°54′281°54′181°5′1°5′	M - Mean of Groups so - Relative Weight C - Concluded Angle							
LI (Ghundi) and XLIX (Kot Sabzal)	h 14.99 h 14.28 h 12.34 h 14.57 h 13.13 l 18.21 h 15.23 h 14.50 h 19.16 h 14.95 h 14.37 h 15.73 h 12.85 h 15.45 l 15.38 l 16.13 h 14.03 l 15.61 h 17.01 h 14.80 h 14.16 h 15.60 h 16.39 h 14.44 h 17.02 h 16.08 h 14.98 l 18.07 h 15.22 h 15.41 d 15.26 d 15.42 d 17.80 h 16.23	$M = 15'' \cdot 40$ $w = 7 \cdot 48$ $\frac{1}{w} = 0 \cdot 13$							
	14·51 15·22 14·25 14·82 15·18 16·81 14·75 16·50 16·91 15·05	$C = 00^{\circ} 29  15^{\circ}  41$							
XLIX (Kot Sabzal) and	h 37 99 h 39 69 h 40 03 h 37 42 h 41 92 l 39 97 h 39 75 h 40 82 h 42 82 h 37 58 h 40 60 h 38 88 h 38 28 h 40 31 h 41 88 l 39 01 h 39 56 h 39 64 h 40 15 h 37 77 h 39 09 l 41 45 h 37 91 h 37 41 l 40 83 l 39 86 h 39 88 l 39 45 h 39 76 h 36 92 d 38 41 h 39 51 h 41 55 h 40 14 h 39 95	$M = 39'' \cdot 59$ $w = 6 \cdot 60$ $\frac{1}{w} = 0 \cdot 15$							
	39.02 39.88 38.74 39.17 41.54 39.75 39.73 39.97 40.67 37.42	$C = 53^{\circ} 27' 39'' \cdot 59$							
XLVI (Vín) and XLIV (Vijnot)	h 17.73 h 15.54 h 16.38 h 15.96 h 15.96 l 12.98 h 17.13 h 16.03 h 12.13 h 18.73 h 17.91 h 14.54 h 17.26 h 17.81 h 15.89 l 13.83 h 18.48 h 17.91 h 18.49 h 17.50 h 17.59 l 14.85 h 16.07 h 17.76 l 15.47 l 16.79 h 12.94 l 13.37 h 18.29 h 18.16 h 13.35 h 17.11 l 16.80 d 14.06 h 16.53	$M = 16'' \cdot 32$ $w = 5 \cdot 15$ $\frac{1}{w} = 0 \cdot 19$							
	17.74 14.57 16.57 17.18 15.77 15.18 16.34 15.34 16.36 18.13	$C = 46^{\circ} 37' 16'' \cdot 28$							

At XLIX (Kot Sabzal)

January 1881; observed by Lieut.-Colonel B. R. Branfill with Troughton and Simms' 24-inch Theodolite No. 1.

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Angle between	Cir 216° 24′ 3	cle rea 86° 24'	dings, te 295° 36'	lescope ł 115° 36'	being set 14°48'	on XLV 194°48'	7II (Got 94°0'	; Mír Mu 274°0′	173°12	353° 12′	M - Mean of Groups to - Relative Weight C - Concluded Angle
XLVII (Got Mír Muhammad) and XLVI (Vín)	" h 18·32 h h 17·27 l l 16·98 l 17·52	" 17.69 17.76 18.96 18.14	* \$ 17.82 \$ 16.97 \$ 18.13 17.64	n h 18.79 h 20.03 l 18.52	1 16 · 76 1 15 · 68 1 17 · 17 16 · 54	* \$ 19.40 \$ 19.61 \$ 18.11 19.04	" h 17·32 h 17·48 h 18·32 17·71	" h 16 · 21 l 17 · 82 l 17 · 17 17 · 07	* \$ 18.15 \$ 16.93 \$ 16.85 17.31	4 17.03 h 17.71 h 16.77	$M = 17'' \cdot 73$ $w = 12 \cdot 50$ $\frac{1}{w} = 0 \cdot 08$ $C = 43^{\circ}35' \cdot 17'' \cdot 73$
XLVI (Vín) and XLVIII (Dewari)	h 57 · 36 h h 57 · 10 l h 59 · 11 l 57 · 86	57°98 58°74 59°41 58°71	k 56 · 08 k 56 · 10 k 54 · 88	k 53 °75 k 54 °93 l 54 °70 54 °46	2 56 92 2 58 37 3 56 98 57 42	<b>h</b> 58 · 12 h 54 · 84 h 56 · 33 56 · 43	k 54 · 58 k 55 · 07 k 54 · 99 l 55 · 33 54 · 99	1 57.08 1 57.63 1 56.43 57.05	k 57°23 k 57°61 k 57°98	k 57°79 k 56°85 l 57°76	$M = 56'' \cdot 77$ $w = 5 \cdot 10$ $\frac{1}{w} = 0 \cdot 20$ $C = 71^{\circ} 40' 56'' \cdot 77$

At XLIX (Kot Sabzal)—(Continued).										
Angle between	Circle readings, telescope being set on XLVII (Got Mír Muhammad) 216°24′ 36°24′ 295°36′ 115°36′ 14°48′ 194°48′ 94°0′ 274°0′ 173°12′ 353°12′	M - Mean of Groups $\omega$ - Relative Weight C - Concluded Angle								
XLVIII (Dewari) and LI (Ghundi)	h 53 · 20 h 52 · 27 h 55 · 03 h 55 · 12 l 52 · 52 h 54 · 47 h 54 · 80 h 51 · 39 l 52 · 21 h 52 · 63 h 52 · 67 l 52 · 12 h 53 · 91 h 54 · 28 l 51 · 40 h 54 · 87 h 54 · 49 l 50 · 79 h 57 · 73 h 54 · 29 h 53 · 46 h 53 · 49 h 55 · 75 l 54 · 29 h 54 · 15 h 53 · 97 h 53 · 54 l 52 · 82 h 54 · 10 d 52 · 93 h 51 · 87	$M = 53'' \cdot 55$ $w = 6 \cdot 94$ $\frac{1}{w} = 0 \cdot 14$								
	53.11 52.63 54.90 54.56 52.69 54.44 54.28 51.67 53.98 53.28	$C = 55^{\circ} 24' 53'' \cdot 55$								
LI (Ghundi) and	h 27 · 45 h 26 · 01 h 28 · 93 h 25 · 87 l 27 · 81 h 27 · 36 h 26 · 98 h 26 · 25 l 26 · 82 h 28 · 08 h 26 · 41 l 24 · 04 h 29 · 05 h 27 · 11 l 27 · 99 h 26 · 42 h 27 · 83 l 26 · 41 h 25 · 74 h 27 · 34 h 26 · 55 l 26 · 35 h 27 · 05 l 25 · 30 h 27 · 86 h 27 · 09 h 26 · 88 l 27 · 88 h 27 · 75 h 27 · 62	$M = 27'' \cdot 01$ $w = 11 \cdot 60$ $\frac{1}{m} = 0 \cdot 09$								
LAII (Daowala)	26.80 25.47 28.34 26.09 27.89 26.96 27.23 26.85 26.77 27.68	$C = 45^{\circ} 42' 27'' \cdot 01$								
January and Feb	At L (Kubba) January and February 1881; observed by LieutColonel B. R. Branfill with Troughton and Simms' 24-inch Theodolite No. 1.									
Angle between	Circle readings, telescope being set on LIX (Máchka) 0°1′ 180°1′ 79°13′ 259°13′ 158°25′ 338°25′ 237°37′ 57°37′ 316°49′ 136°49′	M = Mean of Groups $\infty$ = Relative Weight C = Concluded Angle								
LIX (Máchka) and LI (Ghundi)	h 13.49 h 15.76 l 14.61 l 15.29 h 15.21 h 13.53 h 14.03 l 14.36 l 16.62 l 14.11 h 13.63 h 14.98 l 16.38 h 14.46 h 14.56 h 15.31 h 12.76 l 14.10 l 12.40 h 13.00 l 16.08 l 14.87 h 13.43 h 12.75 h 14.77 h 14.96 h 13.26 l 14.76 h 13.14 h 13.70 l 16.34	$M = 14'' \cdot 38$ $w = 14 \cdot 66$ $\frac{1}{w} = 0 \cdot 07$								
<u></u>	14.40 15.20 15.19 14.17 14.85 14.60 13.35 14.41 14.05 13.60	$C = 71^{\circ} 50' 14'' \cdot 39$								
LI (Ghundi) and XLVIII (Dewari)	h 45 · 47 h 43 · 75 h 44 · 04 l 39 · 63 h 42 · 76 h 45 · 74 h 46 · 18 l 44 · 53 l 42 · 91 l 44 · 35 h 45 · 08 h 44 · 75 h 40 · 05 h 44 · 76 h 43 · 98 h 44 · 33 h 46 · 77 l 44 · 33 l 42 · 81 h 44 · 97 l 44 · 04 h 46 · 95 l 40 · 79 h 46 · 01 h 43 · 79 h 46 · 31 h 45 · 57 l 44 · 56 l 42 · 15 h 45 · 64 h 44 · 71 h 44 · 60	$M = 44'' \cdot 34$ $w = 4 \cdot 88$ $\frac{1}{m} = 0 \cdot 20$								
	44.86 45.15 42.40 43.75 43.51 45.46 46.17 44.47 42.62 44.99	$C = 57^{\circ} 5' 44'' \cdot 32$								
February 1881	At LI (Ghundi) February 1881; observed by LieutColonel B. R. Branfill with Troughton and Simms' 24-inch Theodolite No. 1.									
Angle between	Circle readings, telescope being set on XLVIII (Dewari) 0° 1′ 180° 1′ 79° 13′ 259° 13′ 158° 25′ 338° 25′ 237° 37′ 57° 37′ 316° 49′ 136° 49′	M - Mean of Groups $\omega$ - Relative Weight C - Concluded Angle								
XLVIII (Dewari) and L (Kubba)	#       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #       #	$M = 39w \cdot 58$ $w = 13 \cdot 53$ $\frac{1}{w} = 0 \cdot 07$								
	40.67 39.16 39.84 38.56 40.29 39.58 38.96 38.62 40.28 39.79	$C = 59^{\circ} 11' 39'' \cdot 57$								

Nore.-Stations LIX and LXII appertain to the Great Indus Series.

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	At LI (Ghundi)—(Continued).										
Angle between	n Circle readings, telescope being set on XLVIII (Dewari) 0° 1' 180° 1' 79° 13' 259° 13' 158° 25' 338° 25' 237° 37' 57° 37' 816° 49' 136° 49'										
L (Kubba) and LIX (Máchka)	*	l 42·13 l 40·72 k 44·34 l 46·02	k 43 · 12 k 43 · 61 l 44 · 64	h 45.68 h 44.98 l 42.62	<i>k</i> 43 · 86 <i>h</i> 42 · 59 <i>l</i> 40 · 83	<i>k</i> 41 · 53 <i>k</i> 43 · 21 <i>l</i> 42 · 61	*	* h 44 * 84 h 45 * 80 h 44 * 23	l 44·74 l 43·35 l 43·74	" h 43 · 39 h 45 · 35 h 44 · 47	$M = 43'' \cdot 63$ $w = 8 \cdot 88$ $\frac{1}{w} = 0 \cdot 11$ $G = 6 \cdot 8 \cdot 8' \cdot 10'' \cdot 60'$
	42.87 h 59.70	43.30	43.79 262.38	44 · 43	42.43 . \$ 59.00	42.45 \$63.80	43.72 h60.39	44 90 161 · 38	43 <sup>•</sup> 94 <i>l</i> 59 <sup>•</sup> 81	44.40 263.20	$C = 64^{\circ} 36^{\circ} 43^{\circ} \cdot 63$ $M = 66^{\circ} \cdot 61$
LIX (Máchka) and LXII (Dáowála)	<i>h</i> 61 · 98 <i>h</i> 59 · 36 <i>l</i> 59 · 53	l 60°31 h 59°87	h 59.66 h 61.20 l 63.51	<i>h</i> 59°95 <i>h</i> 59°56	k 56 · 97 k 60 · 08 l 65 · 03	k 61 · 14 l 62 · 62	h 58°29 l 62°00	h 59°82 h 61°81 h 59°84	l 61 °05 l 59 °97	h 61 · 64 h 58 · 57 h 58 · 63	$w = 6 \cdot 85$ $\frac{1}{w} = 0 \cdot 15$
	60.14	60°24	61.69	59.45	60.32	62.52	60.23	60.71	60°28	60.29	$C = 85^{\circ}58' \circ 0'' \cdot 62$
LXII (Dáowála) and	h 45.82 h 46.35 l 46.02	l 45°91 k 44°11 k 44°90	h 42.53 h 42.98 h 43.23	h 45°20 h 43°92 l 45°31	h 45 · 46 h 46 · 01 h 46 · 17	h 42.76 h 43.93 l 43.42	k 44 °68 k 46 °67 l 45 °84	h 43°25 h 44°67 h 43°24	l 45.78 l 45.11 l 44.87	k 44°51 k 44°11 k 44°52	$M = 44'' \cdot 71$ $w = 7 \cdot 80$ $\frac{1}{m} = 0 \cdot 13$
ALIA (AU Dauzai)	46.06	44 • 97	42.91	44.81	45.88	43`37	45.73	43.72	45°25	44.38	$C = 86^{\circ} 5' 44'' \cdot 71$
XLIX (Kot Sabzal) and XLVIII (Dewari)	k 51 · 39 h 51 · 03 l 51 · 25 d 52 · 27	l 52.73 h 52.48 h 50.16 d 52.27	k 52.76 k 51.35 k 52.37	\$ 50°56 \$ 51°98 \$ 50°17 \$ 53°37	h 51°92 h 50°26 h 52°46	h 52·21 h 50·95 l 49·54	h 52.82 h 54.70 h 51.49 l 50.02	k 51 · 73 k 52 · 65 k 51 · 28	2 49 44 2 49 31 2 50 95	k 51 · 83 k 51 · 22 k 50 · 77	$M = 51'' \cdot 49$ $w = 12 \cdot 72$ $\frac{1}{w} = 0 \cdot 08$
	51.49	51.91	52.16	51.22	51.22	50.90	52.36	51.89	49.90	51.27	$C = 64^{\circ} 5' 51'' \cdot 49$

February 1881; observed by Lieut.-Colonel B. R. Branfill with Troughton and Simms' 24-inch Theodolite No. 1.

Angle between	Circle readings telescope being set on LXII (Dáowála) 79°21' 259°21' 158°33' 338°33' 237°45' 57°45' 316°58' 136°58' 86°10' 216°10'	M = Mean of Groups w = Relative Weight C = Concluded Angle
LXII (Dáowála) and LI (Ghundi)	n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n       n	$M = 55'' \cdot 28$ $w = 7 \cdot 96$ $\frac{1}{w} = 0 \cdot 13$ $C = 35'' \cdot 49' \cdot 55''' \cdot 28$
LI (Ghundi) and L (Kubba)	k62.43       k59.82       k64.22       k60.64       k61.76       k59.71       k63.28       k61.01       k61.80       l64.65         k62.43       k59.82       k64.22       k60.64       k61.76       k59.71       k63.28       k61.01       k61.80       l64.65         k62.62       k60.05       k63.97       k59.56       l63.09       k59.57       k62.40       k64.24       l64.32       k64.80         k61.25       k62.45       k61.48       k63.01       k63.78       k59.52       k61.84       k62.09       l64.70       k61.91         d62.31       d62.31       d64.31       d64.31       d64.31       d64.37       d64.37	$M = 62'' \cdot 25$ $w = 4 \cdot 64$ $\frac{1}{w} = 0 \cdot 22$ $C = 43^{\circ}31'  2'' \cdot 25$

Nore.-Stations LIX and LXII appertain to the Great Indus Series.



February 1881	At LXII (Dáowála) February 1881; observed by LieutColonel B. R. Branfill with Troughton and Simms' 24-inch Theodolite No. 1.										
Angle between	Angle between 0°1' 180°0' 79°13' 259°13' 158°25' 338°25' 237°37' 57°37' 816°49' 136°49'										
XLIX (Kot Sabzal) and LI (Ghundi)	k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k       k	$M = 48'' \cdot 63$ $w = 11 \cdot 90$ $\frac{1}{w} = 0 \cdot 08$ $C = 48^{\circ} 11' \cdot 48'' \cdot 63$									
LI (Ghundi) and LIX (Máchka)	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$M = 4'' \cdot 50$ $w = 15 \cdot 70$ $\frac{1}{w} = 0 \cdot 06$ $C = 58^{\circ} 12' 4'' \cdot 50$									
LI (Ghundi) and B. M.	l 21.54 k 22.09 k 24.87 k 21.65 k 23.49 k 22.94 k 22.32 k 22.87 k 23.12 k 23.67 k 22.39 k 22.64 k 23.68 l 21.87 k 22.23 k 23.10 k 22.01 k 23.14 k 21.22 k 23.47 k 23.28 k 23.21 k 23.84 k 22.18 l 22.33 k 21.94 k 22.28 l 22.83 k 23.82 l 21.87 22.40 22.65 24.13 21.90 22.68 22.66 22.20 22.95 22.72 23.00	$M = 22w \cdot 73$ $w = 21 \cdot 30$ $\frac{1}{w} = 0 \cdot 05$ $C = 0^{\circ} 5' 22w \cdot 73$									

Norzs.-Stations LIX (Máchka) and LXII (Dáowála) appertain to the Great Indus Series. R. M. denotes Referring Mark.

February, 1885.

W. H. COLE,

In charge of Computing Office.



Sums of	Squares of	Apparent	Errors	of	Single	Observations,	and of	Apparent	Errors of	Single Zero	8.
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Station of Observation.	Observed Angle.	Number of Observa- tions.	Sum of Squares of Errors of single Observations	Number of Zeros.	Sum of Squares of Errors of single Zeros.	Remarks.
LXXV	I & LXXVIII	40	50.79	IO	1.92	201 sufficiences
**	LXXVIII & V	38	39.61	IO	8.66	
LXXVIII	LXXV & I	38	34.80	IO	3.53	AND ADDRESS OF
33	I & II	33	20.22	10	3.23	
39	II & III	37	26.75	10	8.41	
33	III & IV	38	23.64	IO	2.97	
>>	IV & V	37	30.27	10	2.31	
33	V & LXXV	38	29.61	10	1.36	
I	II & LXXVIII	30	5.68	ю	2.12	
- 33	LXXVIII & LXXV	31	8.98	10	1.92	
II	III & LXXVIII	34	25.68	10	1.80	Barran's 94 inch No. 9
33	LXXVIII & I	31	9.84	10	1.35	S Barrows 24-inch No. 2.
III	IV & LXXVIII	35	25.63	10	4.10	1000
22	LXXVIII & II	30	8.95	IO	3.80	
IV	VI & VII	41	60.08	10	7.18	
>>	VII & V	36	20.56	10	2.61	
>>	V & LXXVIII	34	22.64	ю	3.44	
>>	LXXVIII & III	34	15.84	10	3.21	
V	LXXV & LXXVIII	35	24.40	10	2.57	
>>	LXXVIII & IV	35	13.58	IO	0.62	
33	IV & VII	38	25.26	10	2.98	
"	VII & VIII	40	42.68	10	2.72	J

Note.-Stations LXXV and LXXVIII appertain to the Karáchi Longitudinal Series.

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## SUMS OF SQUARES OF APPARENT ERRORS.

Station of Observation.	Observed Angle.	Number of Observa- tions.	Sum of Squares of Errors of single Observations.	Number of Zeros.	Sum of Squares of Errors of single Zeros.	Bemadks.
VI	IX & VII	40	43.83	10	5.28	h
"	VII & IV	36	18.70	10	2.52	
VII	VI & IX	37	31.37	10	1.78	
<b>3</b> 7	IX & X	36	21.42	10	3.03	
,,	X & VIII	34	25.67	10	3.22	
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	VIII & V	34	11.22	10	3.88	
"	V & IV	36	33.03	10	1.06	
,,	IV & VI	36	32.68	10	4.34	
VIII	V & VII	33	17.84	10	4.06	
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	VII & X	36	28.36	10	4.34	
IX	XI & XII	35	24.69	10	5.29	2
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	XII & X	39	<b>26</b> •48	10	2.82	
>>	X & VII	38	29.21	10	2.12	
<b>&gt;</b> >	VII & VI	33	10.14	10	1.13	
X	VIII & VII	31	7.38	10	1.82	
>>	VII & IX	36	16.33	10	<b>2</b> ·98	
,,,	IX & XI	35	16.10	10	1.89	
"	XI & XII	33	10.00	10	1.11	
XI	ΧΙΙΙ & ΧΙV	34	19.38	10	5.36	
32	XIV & XII	31	12.21	10	2.16	
"	XII & X	32	8.38	10	I ° 20	Barrow's 24-inch No. 2.
32	X & IX	30	7.70	10	2.38	
XII	. X & IX	39	31.02	10	2.41	
"	IX & XI	38	54.56	10	4.03	
"	XI & XIV	39	38.93	10	6.37	
"	XIV & XV	40	44 * 20	10	6.72	
XIII	XVI & XIV	35	20.91	10	5.02	
"	XIV & XI	31	8.40	10	2.77	
XIV	XVI & XVII	39	33.75	10	3.52	
"	XVII & XV	41	41.24	10	4.03	
"	XV & XII	31	11.62	10	0.85	
"	XII & XI	35	19.42	10	2 · 17	
"	XI & XIII	32	21.06	10	<b>2</b> ·98	
"	XIII & XVI	30	5.62	10	2.70	
,,	XVI & R. M.	32	14.28	ю	3.23	
xv	XII & XIV	31	6.34	10	2 · 32	
"	XIV & XVII	33	15.94	10	1 • 48	
XVI	XVIII & XIX	31	11.92	10	1 · 82	
"	XIX & XVII	33	8.08	10	4·68	
"	XVII & XIV	32	11.95	ю	1.06	
"	XIV & XIII	30	7.57	IO	1.72	j

NOTE.-R. M. denotes Referring Mark.

Station of Observation.	Observed Angle.	Number of Observa- tions.	Sum of Squares of Error of single Observations.	Number of Zeros.	Sum of Squares of Error of single Zeros.	Remarks.
XVII	XV & XIV	31	10'14	ю	1.23	1
**	XIV & XVI	31	12.65	10	3.92	
,,	XVI & XIX	34	16.72	10	1.42	
"	XIX & XX	33	18.99	IO	2.67	· ·
XVIII	XXI & XIX	44	60.20	10	10.48	
,,	XIX & XVI	35	25.93	10	1.48	
XIX	XXI & XXII	33	<b>2</b> 0.90	10	0.81	
"	XXII & XX	34	18.49	10	1.24	
>>	XX & XVII	38	44.29	10 .	3.32	
,,	XVII & XVI	35	16.36	10	0.01	
,,	XVI & XVIII	33	14.41	10	4.13	
,,	XVIII & XXI	34	24.24	10	5.13	
XX	XVII & XIX	35	27.81	IO	1.20	
"	XIX & XXII	32	12.11	10	<b>3.</b> 91	
XXI	XXIII & XXIV	39	41.24	10	5.14	
"	XXIV & XXII	35	33.38	IO	I.43	
"	XXII & XIX	34	16.03	10	1.04	
"	XIX & XVIII	33	8.04	IO	1.23	
XXII	XX & XIX	32	13.62	IO	1.10	
37	XIX & XXI	39	43.43	10	1.31	
"	XXI & XXIII	32	12.05	10	3.22	Barrow's 24-inch No. 2.
"	XXIII & XXIV	34	<b>2</b> 5·89	10	2 · 27	
XXIII	XXV & XXVI	34	12.11	10	7.21	
"	XXVI & XXIV	34	20.54	10	6.62	
"	XXIV & XXII	33	16.42	10	1.96	
"	XXII & XXI	30	5.09	10	0.33	
XXIV	XXII & XXI	33	14.00	10	1.43	
"	XXI & XXIII	34	19.13	10	1.89	
,,	XXIII & XXVI	30	<b>3</b> .87	10	1.83	
"	XXVI & XXIX	35	32.22	10	3.00	
XXV	XXVII & XXVIII	35	16.81	10	1.68	
,,	XXVIII & XXVI	35	21.09	10	4.11	
>>	XXVI & XXIII	35	24.11	10	2.20	
XXVI	XXV & XXVIII	36	26.12	10	8.19	
"	XXVIII & XXIX	<b>3</b> 5	27.43	10	2.29	
>>	XXIX & XXIV	32	11.64	10	5.09	
>>	XXIV & XXIII	31	5.03	10	0.99	
<b>39</b>	XXIII & XXV	33	19.37	IO	2.36	
XXVII	XXX & XXVIII	37	28.33	10	2.94	
<b>3</b> 7	XXVIII & XXV	43	54.43	10	6.71	
XXVIII	XXIX & XXVI	31	7.62	10	1 · 26	J

## SUMS OF SQUARES OF APPARENT ERRORS.

Station of Observation.	Observed Angle.	Number of Observa- tions.	Sum of Squares of Errors of single Observations.	Number of Zeros.	Sum of Squares of Errors of single Zeros.	Remarks.
XXVIII	XXVI & XXV	32	16.32	10	4.75	<u>ר</u>
"	XXV & XXVII	34	22.68	10	5.12	
"	XXVII & XXX	39	39.60	10	3.02	
"	XXX & XXXI	41	30.77	10	4.15	
"	XXXI & XXIX	37	29.40	10	4.84	
XXIX	XXIV & XXVI	30	8.46	10	6.49	
,,	XXVI & XXVIII	32	14.42	10	5.11	
,,	XXVIII & XXXI	32	14.68	10	1.83	
XXX	XXXII & XXXIII	38	32.79	10	7.12	
"	XXXIII & XXXI	40	43.32	10	4.83	
"	XXXI & XXVIII	33	9*38	10	3.29	
,,	XXVIII & XXVII	32	14.20	10	4.34	
XXXI	XXIX & XXVIII	42	42.18	IO	7.81	
**	XXVIII & XXX	36	19.67	IO	2.62	
,,	XXX & XXXIII	34	12.29	10	2.06	Barrow's 24-inch No. 2.
33	XXXIII & XXXIV	40	40.60	10	6.64	
,,	XXXIV & R. M.	33	21.23	10	2.93	
XXXII	XXXV & XXXVI	32	14.54	10	3.21	
"	XXXVI & XXXIII	34	19.91	10	2.20	
"	XXXIII & XXX	39	43.93	10	2.26	
XXXIII	XXXVI & XXXIV	36	24.44	10	6 • 98	
"	XXXIV & XXXI	36	29.66	10	I · 32	
>>	XXXI & XXX	37	22.16	10	1.28	
"	XXX & XXXII	38	49.36	10	1.26	
57	XXXII & XXXVI	41	46.43	ю	8.08	
XXXIV	XXXI & XXXIII	36	31.22	10	7.99	
>>	XXXIII & XXXVI	34	15.36	10	4.80	
37	XXXVI & XXXVII	36	24.29	10	I · 48	J
XXXV	XXXIX & XL	30	2.76	10	4.78	Troughton and Simms' 24-inch No. 1.
33	XL & XXXVIII	30	10.63	10	2.69	h
"	XXXVIII & XXXVI	31	6 · 16	10	1.40	
"	XXXVI & XXXII	30	3.40	10	2.69	
XXXVI	XXXIII & XXXII	35	18.49	10	I · 37	
33	XXXII & XXXV	37	23.09	10	3.83	
<b>33</b>	XXXV & XXXVIII	36	24.85	10	3.84	Barrow's 24 inch No 9
"	XXXVIII & XXXVII	38	35.67	10	3.26	Dallow 6 23-1101 100. 2.
37	XXXVII & XXXIV	34	22.35	10	1.03	
"	XXXIV & XXXIII	33	12.75	10	0.40	
XXXVII	XXXIV & XXXVI	35	28.33	10	4.67	
>>	XXXVI & XXXVIII	32	6.29	10	3.22	
XXXVIII	XXXVII & XXXVI	34	21.35	10	2.93	J

Norg.-R. M. denotes Referring Mark.

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Station of Observation.	Observed Angle.	Number of Observa- tions.	Sum of Squares of Errors of single Observations.	Number of Zeros. Sum of Squares of Errors of single Zeros.		Remarks.
XXXVIII	XXXVI & XXXV	31	9.20	10	2.14	Bernet Stind No. 9
"	XXXV & XL	36	21.47	10	1.86	$\int \frac{\text{Darrow B } 24\text{-lifen No. 2.}}{24}$
,,	XXXV & XL	31	15.85	10	7.28	ר
"	XL & XLIII	30	12.28	10	4.81	
XXXIX	XLI & XL	30	8 · 73	10	3.12	
"	XL & XXXV	30	5.32	10	3.42	
XL	XLII & XLIII	30	12.10	10	3.18	
"	XLIII & XXXVIII	30	15.30	10	3.62	
"	XXXVIII & XXXV	30	13.99	10	4.20	
"	XXXV & XXXIX	30	14.13	10	7 * 2 2	
"	XXXIX & XLI	30	8.77	10	3.33	
"	XLI & XLII	30	5.85	10	9.46	
XLI	XLII & XL	30	8.24	10	1.53	
>>	XL & XXXIX	30	12.36	10	4.41	
XLII	XLIV & XLV	30	11.01	10	5.90	
<b>37</b>	XLV & XLIII	30	13.20	10	6.24	
"	XLIII & XL	31	14.64	10	5.34	
"	XL & XLI	30	19.13	10	6.99	
XLIII	XXXVIII & XL	30	5.47	10	<b>2</b> .83	
**	XL & XLII	30	8.94	10	2.37	
"	XLII & XLIV	31	6.67	10	· 1·62	
"	XLIV & XLV	30	7 <sup>•</sup> 54	10	<b>2</b> ·86	Troughton and Simms' 24-inch
XLIV	XLVIII & B. M.	31	12.11	10	6.64	No. 1.
"	XLVIII & XLVI	32	22.26	10	3.33	
**	XLVI & XLV	30	12.26	10	7.23	
"	XLV & XLIII	31	15.01	10	5.43	
"	XLIII & XLII	31	19.31	10	6.20	
XLV	XLIII & XLII	31	11.03	10	9.92	
,,	XLII & XLIV	31	10.32	10	10.92	
**	XLIV & XLVI	31	7.01	10	2.03	
**	XLVI & XLVII	30	9.40	10	4.31	
XLVI	XLV & XLIV	32	41.09	10	7.92	
<b>39</b>	XLIV & XLVIII	33	34.19	10	7.68	
"	XLVIII & XLIX	32	12.49	10	2.04	
**	XLIX & XLVII	31	35.89	10	14.33	
"	XLVII & XLV	31	45 * 27	10	6.30	
XLVII	XLV & XLVI	30	16.72	10	8.10	
,,	XLVI & XLIX	30	52.23	10	12.82	
XLVIII	L & LI	33	24.82	10	8.24	
"	LI & XLIX	34	42 . 72	10	8.22	
"	XLIX & XLVI	35	32.26	10	11.12	Ų

Norg.-R. M. denotes Referring Mark.

## SUMS OF SQUARES OF APPARENT ERRORS.

Station of Observation.	Observed Angle.	Number of Observa- tions.	Sum of Squares of Errors of single Observations.	Number of Zeros. Sum of Squares of Errors of single Zeros.		Remarks.
XLVIII	XLVI & XLIV	35	75.18	10	11.72	 ר
XLIX	XLVII & XLVI	30	9°93	10	6.19	
**	XLVI & XLVIII	31	13.77	10	16.42	
33	XLVIII & LI	31	34.09	10	9.72	
39	LI & LXII	30	12.89	10	6.39	
$\mathbf{L}$	LIX & LI	31	28.02	10	3.42	
33	LI & XLVIII	32	51.32	10	13.23	
LI	XLVIII & L	33	21.88	10	4.81	
"	L & LIX	31	32.01	10	<b>6</b> .66	Froughton and Simms' 24-inch
<b>33</b>	LIX & LXII	35	80.86	10	6.91	No. 1.
>>	LXII & XLIX	30	8.04	ю	10.23	
>>	XLIX & XLVIII	34	33.77	10	4.30	
LIX	LXII & LI	31	33.66	10	8.03	
<b>33</b>	LI & L	32	36.21	10	16.12	
LXII	XLIX & LI	30	10.23	10	6 • 48	
<b>&gt;</b> >	LI & LIX	31	13.42	10	4.41	
"	LI & R. M.	30	10.22	10	3.12	ز

Notes.-Stations LIX and LXII appertain to the Great Indus Series.

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B. M. denotes Referring Mark.



From the preceding data of the sums of squares of apparent errors, in the measurement of each angle, we may ascertain the e.m.s. (error of mean square) of observation of a single measure of an angle, and the e.m.s. of graduation and observation, of the mean of the measures on a single zero, for each group of angles, measured with the same instrument, by the same observer, and under similar circumstances.

The instruments employed were Barrow's 24-inch Theodolite No. 2 and Troughton and Simms' 24-inch No. 1, both having 5 microscopes to read the azimuthal circle; observations were taken on 5 pairs of zeros (face right and face left) giving circle readings at 7° 12' apart.

The e.m.s. of observation of a single measure of an angle

 $= \sqrt{\frac{\text{Sum of squares of apparent errors of observations.}}{\text{No. of observations} - \text{No. of angle } \times \text{No. of changes of zero.}}}$ 

The e.m.s. of graduation and observation of the mean of the  $\left\{ = \sqrt{\frac{\text{Sum of squares of apparent errors of zero.}}{\text{No. of angles } \times (\text{No. of changes of zero-1})} \right\}$ 

			ط 880 880	Number of						
Group	Instrument and Observer	Position of stati	Interval betwee microscope readii of circle	Measures on each zero (average)	Angles	Single messures	Single zeros	s. m. s. of observation of a single measure	e. m. s. of graduation and observation of a single zero	
I	Barrow's 24-inch Theodolite No. 2; Capt. M. W. Rogers, B.E.	Hills	。 , 7 1 <b>2</b>	8.48	146	5082	1460	$\left\{\frac{3294\cdot84}{5082-1460}\right\}^{\frac{1}{2}} = \pm 0''\cdot964$	$\left\{\frac{475\cdot83}{1460-146}\right\}^{\frac{1}{2}} = \pm 0^{"}\cdot602$	
п	Troughton and Simms' 24-inch Theodolite No. 1; LieutCol. B. R. Branfill.	22	7 12	8.03	27	816	<b>2</b> 70	$\left\{\frac{330\cdot 27}{816-270}\right\}^{\frac{1}{2}} = \pm 0 \cdot 778$	$\left\{\frac{143\cdot44}{270-27}\right\}^{\frac{1}{2}} = \pm 0.768$	
ш	∕ Ditto.	Plains	7 12	<b>8·18</b>	80	953	800	$\left\{\frac{-863\cdot55}{953-300}\right\}^{\frac{1}{2}} = \pm 1.150$	$\left\{\frac{234\cdot93}{300-30}\right\}^{\frac{1}{2}} = \pm 0.933$	

February, 1885.

W. H. COLE, In charge of Computing Office.

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PRINCIPAL TRIANGULATION. REDUCTION OF FIGURES.

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Figure	No.	1.
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	Observed Angles					Е	quations t	to be sat	tisfied			Factor
	<u> </u>			<b>x</b> <sub>1</sub> +	<b>x<sub>2</sub> +</b> :	K <sub>8</sub>		•	••	$= e_1 =$	= — 0.267,	λ,
		ocal ht		- x₄ +	x, +:	Γ <sub>ε</sub>	•••		••	= e, =	= - 0.591,	λ
No.	Value	sipro /eig]		- x, +	x. +:					= e. =	= - 0.400,	λ.
		Rec		-, . X., +	<b>x</b> +:	<b>K</b>				= e, =	= - 0.760.	λ.
			-		- <u>11</u>	-13 ···		•		= e. =	= - 0.284	λ.
	o / <i>"</i>			~13 i	~ <u>14</u> 1.		•••	• •	••	- °5 -	- + 0.000	, <i>n</i> 5
	68 39 56.66	•04		A16 T	<b>-</b> 17 <b>-</b> 1		- 1 -	· ·	-		0.090,	~6
2	60 25 37.49	•13		× <sub>1</sub> +	×4 T	<u>⊷</u> 7 ⊤ 2	- · · ·	-18 -	▲16	- c <sub>7</sub> -	0 04,	4
8	50 54 27.65	•05	17	$x_{8} - 12$	x <sub>2</sub> +11	$x_6 - 10$	к <sub>5</sub> + ох	<b>9</b> — 9	x <sub>8</sub>	= e <sub>8</sub> =	= -88.0,	λ <sub>8</sub>
4	66 39 2.43	•05	+ 2	$x_{12} - 30$	$x_{11} + 20$	$x_{15} - 122$	K <sub>14</sub> + 20 X	( <sub>18</sub> — 0	x <sub>17</sub> J			
5	49 53 30.63	•02				Fan	ations had	moon th	. Factor		•	
6	63 27 28.30	•06				Equ	ations bet	ween ti	le ractor		_	
7	38 25 36.68	•05						Co-e	fficients	of		
8	67 53 28.01	•06	No. of	Value of								
9	73 40 56.00	•07	е	е	2	ኢ	λ.	λ	λε	$\lambda_{\epsilon}$	$\lambda_7$	λ,
10	60 I 8·78	•11						•				
11	35 12 13.27	•05	1	- 0.26	+0.23	•••	•••	•••	•••	•••	+0.04	- 0.71
12	84 46 38.03	•04	2	- 0.59	r l	+0.13	•••	•••	•••	•••	+0.05	+ 0.30
13	81 16 52.98	•06	8	- 0.400		-	<b>+0.18</b>	•••	•••	•••	+0.05	- 0.13
14	59 29 14.07	•03	4	- 0.76	<b>,</b>			+0.30	•••	•••	+0.11	- 1.43
15	30 13 53.43	.03	5	- 0.28					+0.13		+0.06	+ 0.43
16	33 · 5 33 +3	•06	6	+ 0.00				*		+0.12	+0.00	+ 1.30
17	88 14 51.00	•02	7	- 0.64	1					10-5	+0.27	
19	46 47 48.10	••5	, g	- 88:0							10 37	 + 148.05
10	40 47 48 19	•00	0	-00.0								T 140 05
	Values of the Factor	:8				А	ngular er	rors in	seconds			
	$\lambda_1 = - 3.0634$			<b>.</b> .	:08	8		0		<b>.</b> .	- + .060	
	$\lambda_1 = -3.4885$			×1 -	6c	5	×7 —	_ 0,	/ 4	<u>~18</u> -		
	$h_{g} = -3.0144$			x <sub>2</sub> =	+ ·05	9	x <sub>8</sub> =	+ 2	13	×14	= + 252	
	$n_{g} = -32144$			x <sub>3</sub> =	= •83	0 C	x <sub>9</sub> =	- ·5	41	<b>X</b> 15 :	=005	
	$\lambda_4 = -10  1593$			x <sub>4</sub> =	· - • • • • •	0	$x_{10} =$	- •9	23	<b>x</b> <sub>16</sub> :	= + '401	
	$\lambda_5 = -0.0154$			$x_{5} =$	= + •20	I	$x_{11} =$	+ •6	21	X <sub>17</sub> :	= + .177	
	$h_6 = + 5.9143$			<b>x</b> <sub>6</sub> =	=70	6	x <sub>12</sub> =	- '4	67	<b>x</b> <sub>18</sub>	= - • 548	
	$\lambda_7 = + 1.7656$						۳۵	C.	~~			
	$\lambda_8 = - 0.7526$						[wx*]	= 78.	03			

\* In the tables of the equations between the factors the co-efficients of the terms below the diagonal are omitted for convenience, the co-efficient of the *ptk* term in the *qtk* line being always the same as the co-efficient of the *qtk* term in the *ptk* line.

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## PRINCIPAL TRIANGULATION. REDUCTION OF FIGURES.

	Obse	ervec	I Angles						Equatio	ons to be	satisfied	l				Factor
					3	x <sub>1</sub> + x	2	+ x <sub>8</sub>	•••		•••	. :	= e <sub>1</sub> =	— 0·897	2	λ <sub>1</sub>
				ocal		ĸ₄ + x	5	+ x <sub>6</sub>	•••	•••	•••	. :	= e <sub>9</sub> =	- 0.728	وأ	λ
No.		Val	ue	cipr. Veig		к <sub>7</sub> + х	8	+ x <sub>9</sub>	•••	•••	•••	, :	= e <sub>s</sub> =	- 0.559	) 9	λ
				Re		x <sub>10</sub> + x	11	+ x <sub>19</sub>	•••	•••		. :	= e4 =	- 0.313	5	λ,
					2	x <sub>18</sub> + x	14	+ <b>x</b> <sub>15</sub>	•••	•••	•••	. :	= e <sub>5</sub> =	- 0.323	5	$\lambda_5$
1	0 73	<b>२</b> 0	" 41.75	•04		x <sub>16</sub> + x	17	+ x <sub>18</sub>	•••	•••	•••	. :	= e <sub>6</sub> =	- 0.205	, ,,	λ <sub>6</sub>
2	54	30	56.98	•05		x <sub>1</sub> + x	4	+ x7	+ x <sub>10</sub>	+ x <sub>13</sub>	, +x	16 <sup>1</sup>	= e <sub>7</sub> =	+ 0.10,		$\lambda_{\gamma}$
3	51	- 49	22.12	•05	17:	x <sub>3</sub> — 15x	s +	9x8	-21 X <sub>5</sub>	+12X9	— 7×	·• )	_ 0 _	- 1 710		
4	68	56	56.45	•05	+ 13	x <sub>19</sub> — 10x	11 +	5 x <sub>15</sub>	-15x <sub>14</sub>	$+18x_{18}$	— 8x	<sub>17</sub> 5	= c <sub>8</sub>	+ 7 9,		~8
5	45	- 29	6.30	•06		<u> </u>										
6	65	33	58.00	•06					Equat	ions betv	veen the	Factors	6			
7	48	43	- 50.52	•06							Co.off	isionte o	£			
8	71	47	46.93	•07	No. of	Value of					C0-61		·L			
9	59	28	22.95	•03	e	e		λ	λ	$\lambda_{3}$	ኢ	λ	ኢ	$\lambda_7$		λ
10	58	5	34.22	•05				•								
11	64	39	21.44	•05	1	-0.897	+0	0.14	•••	•••	•••	•••	•••	+0.04	+	0.10
12	57	15	5.31	•05	2	-0.728			+0.12	•••	•••	•••	•••	+0.02	-	0.72
13	48	34	37:32	•04	8	-0.229				+0.19	•••	•••	•••	+0.02	-	0.13
14	55	23	49.26	•02	4	-0.313					+0.12	•••	•••	+0.02	+	0.12
15	76	I	33.83	.09	5	-0.333						+0.12	•••	+0.04	+	0.12
16	61	59	19.84	•07	6	-0.302				*			+0.33	+0.02	+	1.84
17	68	36	34.62	•04	7	+0.10								+0.31		
18	49	24	6.60	.13	8	+7.9									+1	26.01
7	Values	of	the Facto	rs					Ang	gular erre	ors in se	conds				
	λ <sub>1</sub> =		• 7.9057			$\mathbf{x}_1 =$	_	•115	•	x <sub>7</sub> =	013	7	x <sub>13</sub> =	= + .028		
	$\lambda_{g} =$	= -	· 5·3922			x <sub>2</sub> =	-	•461		<b>x</b> <sub>8</sub> =	414	•	<b>x</b> <sub>14</sub> =	دوه· — =		
	λ, =	=	5.3082			$x_3 =$	_	.321		x, =	- 128	3	<b>x</b> <sub>15</sub> =	= - • 283		
	λ <sub>4</sub> =	= -	· 3·8495			x <sub>4</sub> =	-	•018		$x_{10} =$	+ •059	)	<b>x</b> <sub>16</sub> =	= + .133		
	λ <sub>δ</sub> =	= -	- 3.2810			x <sub>5</sub> =	-	•433		$x_{11} =$	- • 230	5	<b>x</b> <sub>17</sub> =	=152		
	λ <sub>6</sub> =	=	3.1177			x <sub>6</sub> =	-	• 277		x <sub>12</sub> =	136	5	<b>x</b> <sub>18</sub> =	= - 186		
	λη =	= +	5.0272							[	- 18.1	8				
	λ <sub>8</sub> =	= +	· 0 <b>·</b> 0871							[wx-]	= 10'1	0				

Figure No. 2.

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	Observed Angles				Equations to	o he satisfied		Factor
		7		x <sub>1</sub> + x	$\mathbf{x}_{2} + \mathbf{x}_{3}$	+ X4	$= e_1 = -$	0.022, λ
No.	Value	leciproce Weight		- x <sub>8</sub> + x		+ x <sub>6</sub>	$= e_{2} = -$	0.021, λ <sup>8</sup>
		<b>H</b>		x <sub>5</sub> + x	<sup>4</sup> 6 + <b>x</b> <sub>7</sub>	+ <b>x</b> <sub>8</sub>	$= e_8 = +$	0°299, λ <sub>8</sub>
	0 / //			- 161	x <sub>1</sub> + 3 x <sub>3</sub>	-21 x <sub>3</sub>		8.0
1	54 21 17.01	•05		+ 171	<i>x</i> <sub>6</sub> −3 <i>x</i> <sub>7</sub>	+19x <sub>8</sub> 5	= e <sub>4</sub> = +	0°0, A <sub>4</sub>
2	41 19 30.08	•02						
8	41 12 40.19	•04			Equations	between the Fa	ctors	
4	43 6 33.84	•05				Co off	isionte of	
5	49 41 17.86	•09	No. of	Value of		00-611	icients of	
6	45 59 29°37	·03	e	e	_	_		
7	36 15 22.25	•02			λ <sub>1</sub>	λ	λ	λ4
8	48 3 52.04	•09	1	- 0:075	+0.16		······	
				- 0 0/3	-010	+0°09	•••	- 1.20
			z	- 0.021		+0.31	+0.13	— o.33
	•••		3	+ 0.399		*	+0.33	+ 2.16
			4	+ 8.8				+ 71.96
77	alves of the Frater					· ·		
•	ardes of the factor	8			Angula	r errors in secon	ds.	
	$\lambda_1 = + 1.3492$			x <sub>1</sub>	=032	X	4₅ = − .034	
	$\lambda_3 = - 0.9344$			xs	= + .032	x	k <sub>6</sub> = + ∙056	
	$\lambda_8 = + 0.5584$			x <sub>3</sub>	=093	ĸ	$x_7 = + \cdot 003$	
	$\lambda_{4} = + 0.1309$			x4	= + '020	x	$x_8 = + \cdot 274$	
					ני	w1 <sup>8</sup> ] = 1·27		

Figure No. 3.

																-	
		Obs	erve	d Angles						Equ	ations to	be sati	sfied			]	Factor
	· <u> </u>						x <sub>1</sub>	+ x,	+ x <sub>3</sub>		•••	•		$= e_1 =$	+ 0.045	,	λ <sub>1</sub>
					ocal cht		x4	+ x,	. + x <sub>6</sub>			•••		= e <sub>2</sub> =	- 0.102	,	λ
	No.		Val	lue	cipr Veig		<b>x</b> 7	+ <b>x</b> ,	3 + x <sub>9</sub>	•••		•••		= e <sub>3</sub> =	- 0.418	,	λ <sub>3</sub>
					Re		<b>x</b> <sub>10</sub>	+ x	11 + X <sub>12</sub>	•••	•••	•••		= e <sub>4</sub> =	+ 0.080	,	λ4
ŀ							<b>x</b> 13	+ x	$+ x_{15}$			•••		= e <sub>6</sub> =	- 0.253	,	λ5
	1	51	47	32.12	•04		<b>x</b> 16	+ x	$x_{17} + x_{18}$	•••	•••	•••		= e <sub>6</sub> =	- 0.813	,	λ <sub>6</sub>
	2	60	4T	0.00	•04		x <sub>1</sub>	<b>+ x</b> ,	+ x <sub>7</sub>	+ x <sub>10</sub>	) + x <sub>18</sub>	+ x	16	= e <sub>7</sub> =	- 0.94,		λη
	3	67	31	28.32	•10	8	3 x <sub>3</sub>	— I I X	$+12x_{6}$	-13 x <sub>5</sub>	+ 1 2 X <sub>9</sub>	— 14 x	8 }	_ ^ _			
	4	62	44	34.36	•02	+ 9	x <sub>12</sub>	—14x	11 + 1 1 x <sub>15</sub>	— 1 2 X <sub>14</sub>	$+20x_{18}$	-10x	<sub>17</sub> §	= e <sub>8</sub> =	+21.9,		~8
	5	57	3	26.65	•11												
	6	60	12	0.22	•03					Equat	tions betw	veen the	Factors				
1	7	64	I	50.19	•07							Co-eff	icients of				
	8	55	49	5 <sup>6</sup> ·45	•03	No. of	Va	lue of									
	9	60	8	14.19	•03	Ē		e	λ	λ	λ <sub>3</sub>	λ4	$\lambda_{\delta}$	λ <sub>6</sub>	λη		λ <sub>8</sub>
	10	56	8	31.22	•06		-						<u> </u>				
	11	57	21	1.82	•06	1	+	0.042	+0.18	•••	•••	•••	•••	•••	+0.04	+	0.36
	12	66	30	27.72	•02	2	-	0.102		+0.10	•••	•••	•••	•••	+0.03	-	1.02
	13	58	28	38.10	•04	3	-	0.418			+0.13	•••	•••	•••	+0.01	-	0.06
	14	60	19	55°97	•03	4	+	0.080				+0.14	•••	•••	+0.06	-	0.96
	15	61	1 [	26.56	•07	5	-	0.223					+0.14	•••	+0.04	+	0.41
	16	66	48	52.68	•05	6	-	0.813			+	ĸ		+0.12	+0.02	+	1 • 20
	17	66	32	20.74	•04	7	-	0.94							+0.38		•••
	18	46	38	47.04	•08	8	+:	21.9								+1	06.22
	1	Values	of	the Facto	rs					An	gular erro	ors in se	conds				
		λ <sub>1</sub> =	= +	- 0.1021				$\mathbf{x}_1 =$	- •086		x <sub>7</sub> =	- • 287	,	x <sub>13</sub> =	— ·174		
		λ <sub>g</sub> =	= +	- 1.7638		1		$x_g =$	- • 137		<b>x</b> <sub>8</sub> =	191	ſ	$x_{14} =$	- 179		
		λ <sub>3</sub> =	=	- 1.8585				$\mathbf{x}_{s} =$	+ • 268		x, =	+ •060	þ	$x_{15} =$	+ .100		
		λ <sub>4</sub> =	= +	- 3.0203				<b>x</b> <sub>4</sub> =	009		$x_{10} =$	+ .048	3	<b>x</b> <sub>16</sub> =	432		
		λ <sub>5</sub> =	= -	- 2.1084				$\mathbf{x}_{5} =$	<u> </u>		$\mathbf{x}_{11} =$	083	7	<b>x</b> <sub>17</sub> =	- '384		
		λ <sub>6</sub> =	= -	- 6.3938				x <sub>6</sub> =	+ .108		x <sub>13</sub> =	+ .11ð	)	x <sub>18</sub> =	+ .003		
		λ <sub>7</sub> =	= -	- 2.2441													
		λ <sub>8</sub> =	= +	- 0.3218		ľ					[wx <sup>2</sup> ] :	= 15.7	3				
						1											

Figure No. 4.

	Observed Angles					Equatio	ns to be s	atisfied				Factor
No.	Value	Reciprocal Weight	ג ג ג	$+ x_{1} + x_{2}$ $+ x_{1} + x_{2}$ $+ x_{1} + x_{2}$ $+ x_{2} + x_{3}$	$x_{11} + x_{2} + x_{3}$ $x_{5} + x_{6} + x_{9}$ $x_{11} + x_{19}$	  	  	·· ·· ··	• • •	$= e_1 =$ $= e_3 =$ $= e_3 =$ $= e_4 =$	+ 0.202 + 0.546 - 0.790 + 0.444	, λ <sub>1</sub> , λ <sub>2</sub> , λ <sub>3</sub> , λ <sub>4</sub>
1 2 8 4	0       ,       "         47       16       16.06         77       11       25.08         55       32       20.25         51       36       24.18	•02 •06 •04 •07	3 3 153 + 103	$x_{13} + x_{16} + x_{16} + x_{16} + x_{11} + x_{11} + x_{12} + x_{13} - 5x_{23} + 5x$	$ \begin{array}{rcrr}  & + x_{16} \\  & + x_{17} \\  & + x_{7} \\  & + x_{6} \\  & + x_{6} \\  & & + x_{5} \\  & & & \\ \end{array} $	 + x <sub>10</sub> - 24 x <sub>5</sub> - 16 x <sub>14</sub>	 + $x_{13}$ + 15 $x_9$ + 21 $x_{18}$	 + 1 - 143	<sup>4</sup> 16 <sup>4</sup> 8 <sup>4</sup> 8	$= e_{5} =$ $= e_{6} =$ $= e_{7} =$ $= e_{8} =$	+ 0.316 - 0.239 - 0.44, + 38.0,	, λ <sub>5</sub> , λ <sub>8</sub> λ <sub>7</sub> λ <sub>8</sub>
6 7	41 55 1 10 86 28 36·21 69 3 7·07	•05 •04 •03				Equat	tions betw	reen the Co-effi	Factors cients of			
8 9 10	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	•05 •03 •03	No. of e	Value of e	λ <sub>1</sub>	λ	λ	λ,	$\lambda_5$	λ <sub>6</sub>	λ <sub>7</sub>	λ <sub>8</sub>
11 12 13	58 6 12.03 64 48 46.30 72 36 6.18	•04 •03 •08	1 2 8	+ 0·202 + 0·546 - 0·790	+0.13	 +0.16	+0.11 	•••	••••	···· ····	+0.02 +0.02 +0.03	+ 0.30 - 1.16 - 0.25
14 15 16	52 40 28.36 54 43 26.53 62 23 3.23	·02 ·15 ·06	4, 5 6	+ 0·444 + 0·316 - 0·239			•	<del>*</del> +0.10	 +0·25	  +0 <sup>.</sup> 13	+0.03 +0.08 +0.06	- 0.22 + 1.93 + 0.35
17 18	72 4 57 <sup>.12</sup> 45 32 0.32	•04 •03	7 8	- 0:44 +38:0							+0.30	 + 119.71
	Values of the Facto	)rs				Ang	gular erro	ors in se	conds 		· ,	
	$\lambda_{1} = + 1.1502$ $\lambda_{2} = + 7.6600$ $\lambda_{3} = - 5.4526$ $\lambda_{4} = + 6.2195$ $\lambda_{5} = - 0.9534$ $\lambda_{6} = - 1.5852$ $\lambda_{7} = - 2.9337$ $\lambda_{3} = + 0.4088$			$x_1 = x_2 = x_3 = x_4 = x_5 = x_6 = x_6 = x_6$	$ \begin{array}{r} - & \cdot 036 \\ - & \cdot 053 \\ + & \cdot 291 \\ + & \cdot 331 \\ - & \cdot 108 \\ + & \cdot 323 \end{array} $		$x_7 = -x_8 = -x_9 = -x_{10} = -x_{11} = -x_{13} = -x_{$	- ·252 - ·558 + ·020 + ·099 + ·036 + ·309 = 28·39	)	$x_{13} = x_{14} = x_{16} = x_{16} = x_{17} = x_{18} = x_{18} = x_{18}$	$ \begin{array}{r} - & \cdot 311 \\ - & \cdot 150 \\ + & \cdot 777 \\ - & \cdot 271 \\ - & \cdot 178 \\ + & \cdot 210 \\ \end{array} $	

Figure No. 5.

	Obs	erved	d Angles				Equation	us to be satisfied		Factor
				ocal at		x <sub>1</sub> + x	s +x	s + x <sub>4</sub>	$= e_1 = -$	+ 0·060, λ <sub>1</sub>
No.		Val	ue	lecipro Weigl		x <sub>3</sub> + x	4 + X	5 + X <sub>6</sub>	= e <sub>2</sub> = -	- 0·481, λ <sub>2</sub>
				<u>н</u>		x <sub>5</sub> + x	6 + X		= e <sub>8</sub> = -	+ 0·108, λ <sub>8</sub>
1	。 37	, 39	<i>"</i> 28·64	•03		— 27 x + 25 x	-3x	$\begin{array}{c} -27 \mathbf{x}_{3} \\ -27 \mathbf{x}_{3} \\ +24 \mathbf{x}_{8} \end{array}$	= e <sub>4</sub> = -	-14·3, λ4
2	54	26	24 · 25	•05						
8	42	21	28.16	•05			Equation	ons between the l	Factors	
4	45	32	39.93	•04				Co-	efficients of	
5	53	51	39.98	•09	No. of	Value of				
6	38	14	12.30	.01	e	e	$\lambda_1$	λ <sub>3</sub>	· λ <sub>3</sub>	$\lambda_{4}$
7	46	6	10.37	•04						
8	41	47	58.29	•04	1	+ 0.060	+0.12	+0.09		- 2.31
					2	- 0.481		+0.13	+0.10	- 1.10
					3	+ 0.108		*	+0.18	+ 1.13
					4	-14.3				+ 88.22
	Value	s of 1	the Factor	rs			Ang	ular errors in sec	onds	
	λ <sub>1</sub> =	=	• 0.0841			<b>x</b> <sub>1</sub>	= + .300		<b>x</b> ₅ = − •086	
	λ <sub>3</sub> =	=	· 8·7066			Xg	= + .022		$x_6 =103$	
	λ <sub>3</sub> :	= +	· 7·8154			<b>X</b> <sub>3</sub>	= + .003		$x_7 = + .343$	
	λ <sub>4</sub> :		• • • 37 <b>37</b>			X4	=354		$x_8 = - \cdot 046$	
$\lambda_4 = -0.3737$								$[wx^2] = 10.40$		

Figure No. 6.

Figure	No.	7.
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						Obser	ved Angle	8				
No.		Value		Reciprocal Weight	No.		Value	Reciprocal Weight	No.		Value	Reciprocal Weight
1	° 76 2	· // 27 7 · 4	14	•02	10	° 66 1	<i>, ,</i> 17 20.54	11	19	· 0 55	, " 22 30·20	•07
2	, 53	5 46.	 26	·00	11	63	33 27.48	•07	20	56	34 38.80	·05
3	50 2	27 7.1	10	•02	12	50	9 3.74	•06	21	68	2 51.68	•05
4	81 4	47 19°4	<b>1</b> 6	·07	13	70 s	28 51.83	•04	22	68	17 21.80	•06
5	50	52 6.2	74	·06	14	49 4	49 14.54	•05	23	60	32 33.34	·o6
6	47 2	20 34.0	95	·08	15	59 4	41 54.06	.10	24	51	10 6.30	•06
7	64	59 12.0	56	·05	16	56 1	11 39.26	·08	25	53	38 48.78	·08
8	52	4 36.2	26	•07	17	<b>7</b> 0 1	1 35.95	•04	26	56	10 39.23	• 11
9	62	56 12.1	<b>18</b>	·02	18	53 3	36 45.02	11	27	70	10 32.52	·03
					Equa	tions to 1	be satisfied	1				Factor
x <sub>1</sub>	+ x <sub>s</sub>	+ x <sub>3</sub>	•••	•••	•••	•••	•••			$= e_1$	= + 0.025,	λ
x4	+ x <sub>5</sub>	+ x <sub>6</sub>	•••	•••	. <b></b>	•••						
<b>x</b> 7	⊥ .							•••	•••	= e <sub>9</sub>	= + 0.176,	λ
		+ x9		•••	•••			•••	••••	$= e_{g}$ $= e_{g}$	= + 0.176, = - 0.333,	λ <sub>3</sub> λ <sub>3</sub>
<b>x</b> <sub>10</sub>	+ <b>x</b> <sub>11</sub>	+ x <sub>9</sub> + x <sub>13</sub>	•••	•••	••••	••••	••••	 	····	$= e_{g}$ $= e_{g}$ $= e_{4}$	= + 0.176, = - 0.333, = - 0.110,	λ <sub>3</sub> λ <sub>3</sub> λ4
x <sub>10</sub> x <sub>13</sub>	$+x_{8}$ $+x_{11}$ $+x_{14}$	+ x <sub>9</sub> + x <sub>13</sub> + x <sub>15</sub>	 		••••	 	•••	 	··· .	$= e_{3}$ $= e_{3}$ $= e_{4}$ $= e_{5}$	= + 0.176, = - 0.333, = - 0.110, = - 0.494,	λ₃ λ₅ λ₄ λ₅
x <sub>10</sub> x <sub>13</sub> x <sub>16</sub>	$+ x_{11}$ $+ x_{14}$ $+ x_{17}$	$+ x_9$ $+ x_{12}$ $+ x_{15}$ $+ x_{18}$	  	···· ····	•  	  	···· ····	···· ··· ···	··· ·	$= e_{g}$ $= e_{3}$ $= e_{4}$ $= e_{5}$ $= e_{6}$	= + 0.176, = - 0.333, = - 0.110, = - 0.494, = - 0.814,	$\lambda_3$ $\lambda_5$ $\lambda_6$ $\lambda_6$
x <sub>10</sub> x <sub>13</sub> x <sub>16</sub> x <sub>19</sub>	$+ x_{8}$ + $x_{11}$ + $x_{14}$ + $x_{17}$ + $x_{20}$	$+ x_9$ $+ x_{19}$ $+ x_{15}$ $+ x_{18}$ $+ x_{21}$	  		••• ••• •••	  	···· ···· ····	···· ···· ····	··· · · · · · · · · · · · · · · · · ·	$= e_{g}$ $= e_{3}$ $= e_{4}$ $= e_{5}$ $= e_{6}$ $= e_{7}$	= + 0.176, $= - 0.333,$ $= - 0.110,$ $= - 0.494,$ $= - 0.814,$ $= - 0.407,$	$\lambda_3$ $\lambda_5$ $\lambda_6$ $\lambda_7$
x <sub>10</sub> x <sub>13</sub> x <sub>16</sub> x <sub>19</sub> x <sub>22</sub>	$+ x_{8}$ + $x_{11}$ + $x_{14}$ + $x_{17}$ + $x_{20}$ + $x_{23}$	$+ x_9$ $+ x_{19}$ $+ x_{15}$ $+ x_{18}$ $+ x_{21}$	  	··· ··· ···	••• ••• •••	··· ··· ···	···· ···· ····	···· ···· ····	··· · · · · · · · · · · · · · · · · ·	$= e_{g}$ $= e_{3}$ $= e_{4}$ $= e_{5}$ $= e_{6}$ $= e_{7}$ $= e_{8}$	= + 0.176, $= - 0.333,$ $= - 0.110,$ $= - 0.494,$ $= - 0.814,$ $= - 0.407,$ $= + 0.205,$	$\lambda_3$ $\lambda_5$ $\lambda_6$ $\lambda_7$ $\lambda_8$
x <sub>10</sub> x <sub>13</sub> x <sub>16</sub> x <sub>19</sub> x <sub>99</sub> x <sub>92</sub>	$+ x_{8}$ + $x_{11}$ + $x_{14}$ + $x_{17}$ + $x_{20}$ + $x_{23}$ + $x_{26}$	$+ x_9$ $+ x_{19}$ $+ x_{15}$ $+ x_{18}$ $+ x_{21}$ $+ x_{24}$ $+ x_{27}$	   	··· ··· ··· ···	••• ••• ••• •••	··· ··· ··· ···	···· ···· ···· ···• ···•	···· ···· ····	··· · · · · · · · · · · · · · · · · ·	$= e_{g}$ $= e_{3}$ $= e_{4}$ $= e_{5}$ $= e_{6}$ $= e_{7}$ $= e_{8}$ $= e_{9}$	= + 0.176, $= - 0.333,$ $= - 0.110,$ $= - 0.494,$ $= - 0.814,$ $= - 0.407,$ $= + 0.205,$ $= - 0.527,$	$\lambda_3$ $\lambda_5$ $\lambda_6$ $\lambda_7$ $\lambda_8$ $\lambda_9$
x <sub>10</sub> x <sub>13</sub> x <sub>16</sub> x <sub>19</sub> x <sub>22</sub> x <sub>25</sub> x <sub>1</sub>	$+ x_{8}$ $+ x_{11}$ $+ x_{14}$ $+ x_{17}$ $+ x_{20}$ $+ x_{23}$ $+ x_{26}$ $+ x_{4}$	$+ x_9$ $+ x_{19}$ $+ x_{15}$ $+ x_{18}$ $+ x_{21}$ $+ x_{24}$ $+ x_{37}$ $+ x_7$	    + x <sub>10</sub>	   + x <sub>13</sub>	··· ··· ··· ···	··· ··· ··· ···	···· ···· ···· ··· ···	···· ···· ···· ····	····	$= e_{g}$ $= e_{3}$ $= e_{4}$ $= e_{5}$ $= e_{6}$ $= e_{7}$ $= e_{8}$ $= e_{9}$ $= e_{10}$	= + 0.176, $= - 0.333,$ $= - 0.110,$ $= - 0.494,$ $= - 0.814,$ $= - 0.407,$ $= + 0.205,$ $= - 0.527,$ $= + 0.33,$	$\lambda_3$ $\lambda_5$ $\lambda_6$ $\lambda_7$ $\lambda_8$ $\lambda_9$ $\lambda_{10}$
x <sub>10</sub> x <sub>13</sub> x <sub>16</sub> x <sub>19</sub> x <sub>22</sub> x <sub>25</sub> x <sub>1</sub> x <sub>9</sub>	$+ x_{8}$ $+ x_{11}$ $+ x_{14}$ $+ x_{17}$ $+ x_{20}$ $- x_{23}$ $+ x_{26}$ $+ x_{4}$	$+ x_9$ $+ x_{19}$ $+ x_{15}$ $+ x_{18}$ $+ x_{31}$ $+ x_{32}$ $+ x_{37}$ $+ x_7$ $+ x_{16}$	    + x <sub>10</sub>	   + x <sub>13</sub>	···· ··· ··· ··· ··· ··· ··· ···	··· ··· ··· ··· ···	···· ···· ···· ··· ··· ···	···· ···· ···· ····	····	$= e_{g}$ $= e_{3}$ $= e_{4}$ $= e_{5}$ $= e_{6}$ $= e_{7}$ $= e_{8}$ $= e_{9}$ $= e_{10}$ $= e_{11}$	= + 0.176, $= - 0.333,$ $= - 0.110,$ $= - 0.494,$ $= - 0.814,$ $= - 0.407,$ $= + 0.205,$ $= - 0.527,$ $= + 0.33,$ $= - 0.30,$	$\lambda_{3}$ $\lambda_{5}$ $\lambda_{6}$ $\lambda_{7}$ $\lambda_{8}$ $\lambda_{9}$ $\lambda_{10}$ $\lambda_{11}$
x <sub>10</sub> x <sub>13</sub> x <sub>16</sub> x <sub>19</sub> x <sub>22</sub> x <sub>25</sub> x <sub>1</sub> x <sub>9</sub> 17x <sub>3</sub>	$+ x_{8} + x_{11} + x_{14} + x_{14} + x_{17} + x_{20} + x_{23} + x_{23} + x_{26} + x_{4} + x_{11} - 16 x_{9}$	$+ x_9$ $+ x_{19}$ $+ x_{15}$ $+ x_{18}$ $+ x_{31}$ $+ x_{34}$ $+ x_{37}$ $+ x_7$ $+ x_{16}$ $+ 19 x_6$	   + x <sub>10</sub> - 17 x <sub>5</sub>	   + x <sub>13</sub> + x <sub>22</sub>	    + x <sub>25</sub> - 16 x <sub>8</sub>	    + 18 x <sub>13</sub>	···· ···· ···· ··· ··· ··· ···	     + 1 2 x <sub>15</sub> -	···· ···· ··· ··· ··· ··· ··· ··· ···	$= e_{g}$ $= e_{3}$ $= e_{4}$ $= e_{5}$ $= e_{6}$ $= e_{7}$ $= e_{8}$ $= e_{9}$ $= e_{10}$ $= e_{11}$ $= e_{13}$	= + 0.176, $= - 0.333,$ $= - 0.110,$ $= - 0.494,$ $= - 0.814,$ $= - 0.407,$ $= + 0.205,$ $= - 0.527,$ $= + 0.33,$ $= - 0.30,$ $= - 15.4,$	$\lambda_{3}$ $\lambda_{5}$ $\lambda_{6}$ $\lambda_{7}$ $\lambda_{8}$ $\lambda_{9}$ $\lambda_{10}$ $\lambda_{11}$ $\lambda_{12}$

	Equations between the Factors														•	
No. of	Value of						(	Co-efficie	ents of							
е	e	λ <sub>1</sub>	$\lambda_2$	λ <sub>8</sub>	λ4	$\lambda_5$	λ <sub>6</sub>	λ <sub>7</sub>	λ <sub>8</sub>	λ	λ <sub>10</sub>	λ <sub>11</sub>		λ <sub>12</sub>		λ <sub>18</sub>
1	+ 0.025	+0.13	•••	•••	•••	•••		•••	•••		+0.02	•••	_	1.10		
2	+ 0.176		+0.31					•••			+0.02	•••	+	0.20		
8	- 0.333			+0.14	•••	•••	•••		•••	•••	+0.02	+0.03	-	0.92	+	0.63
4	- 0.110				+0.34	••••	•••	•••	•••	•••	+0.11	+0.02	+	0.31	-	0.09
5	- 0.494					+0.19		•••		•••	+0.04	•••	+	0.30		
6,	- 0.814						+0.33		•••	•••	•••	+0.08		•••	+	1.33
7	- 0.407							+0.12	•••	•••		+0.02		•••	-	0.30
8	+ 0.302					*			+0.18	•••	•••	+0.06		•••	+	<b>o.3</b> 0
9	- 0.227									+0.33	•••	+0.08		•••		1.30
10	+ 0.33										+0.39	•••		•••	+	0.46
11	- 0.30											+0.38		0.22		
12	-15.4												+1	53.47	-	37:36
13	+ 49 • 8														+ 1	41.04
	Values of	f the Fac	ctors					Ang	ular err	ors in se	conds					
	$\lambda_1 =$	- 0.36	48											<u></u>		
	λ <sub>2</sub> =	+ 0.01	45			$\mathbf{x}_1 =$	+ •045		<b>x</b> <sub>10</sub> =	+ •475		<b>x</b> <sub>19</sub> =	-	•042		
	λ <sub>8</sub> =	- 5.22	20			x <sub>2</sub> =	006		$x_{11} =$	+ .002		x <sub>20</sub> =	-	•410		
	$\lambda_4 =$	- 2.00	43			<b>x</b> <sub>8</sub> =	014	•	x <sub>19</sub> =	— ·5 <sup>8</sup> 7		x <sub>21</sub> =	+	•045		
	$\lambda_{5} =$	- 3.11	88			x, =	+ •183		<b>x</b> <sub>18</sub> =	021		x <sub>23</sub> =	+	• 100		
	λ <sub>6</sub> =	- 6.56	50			x <sub>5</sub> =	+ .020		<b>x</b> <sub>14</sub> =	- •139		x <sub>23</sub> =		• 307		
	$\lambda_7 =$	- 2.41	52			x <sub>6</sub> =	027		x <sub>15</sub> =	334		x <sub>24</sub> =	+	•412		
	λ <sub>8</sub> =	- 0.12	83			<b>x</b> <sub>7</sub> =	- •353		<b>x</b> <sub>16</sub> =	379		x <sub>25</sub> =	+	•097		
	λ <sub>9</sub> =	- 0.61	48			x, =	+ .098		$x_{17} =$	- • 395		x <sub>26</sub> =	-	• 705		
	$\lambda_{10} =$	+ 2.60	31			x, =	078		x <sub>18</sub> =	040		x <sub>27</sub> =	+	·081		
	$\lambda_{11} =$	+ 1.82	37													-
	$\lambda_{13} =$	- 0.01	85						[wx <sup>9</sup> ]	= 31.41	I					
	$\lambda_{13} =$	+ 0.41	36													

.

Figure No. 7-(Continued).

Figure No. 8.

						Obset	rved A	Angles									
No.	٦	Value	F	Keciprocal Weight	No.		Value	9	Reciprocal	Weight	No.			Va	lue		Reciprocal Weight
1	0	· //	, <u> </u>		10	ہ 8 ج	,	"	• 1		10		0	,		<i>"</i>	:07
2	39 67 A	0 " 90	) 7 ·		10	0j	/ J	0.45	•		20		/3 50	#L 51	: وج	3.07	•05
8	0/ 4 50 I	H 37 7	/ • •		19	40	30 2	40 75 a.ta	•••	3	20 91		29 46	31 46	5.	, y/	
0 A	53 1	10 20 3. 18 <b>5</b> 81 <i>0</i>	4 - ·	03	12	54	14 - 9	3 13	•0		99 20		40 80	40 F 4	57	· 44	•05
5	04 3 40	50 <u>5</u> 0 20			10	50	50 26	7 21		5	~~ 92		00 F 4	54	55		00
5	43	0 11·5;	/ < .		19	73	20 4 05 1	11.03			20 94		54	33	ز س		103
7	52 1	4 51 8	, .	12	10	49	35 1		1		~1 05		44	31	54	1.03	-03
0	74 1	14.0	5	10	10	54	13 1	14'11	•0	23	~U		57 60	35	22	1.30	-00
•	52 3	32 40°90	· ·	.07	17	30	53 5	59.05	•0	.0	20			15	40		-03
9	53 1	.0 58.92	+ ·	02	19	80	52 4	40-02	-0	00	21		53	o	50	0.09	-05
		-															
					Equa	tions to	be sat	isfied									Factor
x <sub>1</sub>	+ x <sub>2</sub>	+ x <sub>3</sub>			Equa 	tions to	be sat	isfied		•••		=	e <sub>1</sub>	= ·	ł	0.042	Factor
X1 X4	+ x <sub>2</sub> + x <sub>5</sub>	+ x <sub>3</sub> + x <sub>6</sub>	•••	•••	Equa 	tions to	be sat 	isfied 				=	e <sub>1</sub> e <sub>2</sub>	= ·	+ +	0°042 0°473	Factor 1, $\lambda_1$ 1, $\lambda_3$
X1 X4 X7	+ x <sub>2</sub> + x <sub>5</sub> + x <sub>8</sub>	+ x <sub>8</sub> + x <sub>6</sub> + x <sub>9</sub>	··· ···	 	Equa  	tions to  	be sat  	isfied · ·	···· ···	 		-	e <sub>1</sub> e <sub>2</sub> e <sub>3</sub>	= · = ·	+ + -	0.042 0.473 0.267	Factor 1, λ <sub>1</sub> 1, λ <sub>3</sub> 1, λ <sub>3</sub>
X <sub>1</sub> X4 X7 X10	+ x <sub>2</sub> + x <sub>5</sub> + x <sub>8</sub> + x <sub>11</sub>	+ x <sub>3</sub> + x <sub>6</sub> + x <sub>9</sub> + x <sub>19</sub>	··· ··· ···	  	Equa   	tions to   	be sat   		···· ··· ···	  			e <sub>1</sub> e <sub>2</sub> e <sub>8</sub> e <sub>4</sub>		+ + -	0.042 0.473 0.267 0.668	Factor 1, $\lambda_1$ 1, $\lambda_3$ 1, $\lambda_3$ 1, $\lambda_4$
X <sub>1</sub> X4 X7 X10 X13	$+ x_{2}$ $+ x_{5}$ $+ x_{8}$ $+ x_{11}$ $+ x_{14}$	+ x <sub>3</sub> + x <sub>6</sub> + x <sub>9</sub> + x <sub>12</sub> + x <sub>15</sub>	  	  	Equa   	tions to   	be sat   	isfied  	···· ··· ···	  			e <sub>1</sub> e <sub>2</sub> e <sub>8</sub> e <sub>4</sub>		+ +  +	0.042 0.473 0.267 0.668 0.400	Factor 1, $\lambda_1$ 3, $\lambda_3$ 1, $\lambda_3$ 1, $\lambda_4$ 1, $\lambda_5$
X <sub>1</sub> X <sub>6</sub> X <sub>7</sub> X <sub>10</sub> X <sub>18</sub> X <sub>16</sub>	$+ x_{9}$ $+ x_{5}$ $+ x_{8}$ $+ x_{11}$ $+ x_{14}$ $+ x_{17}$	+ x <sub>3</sub> + x <sub>6</sub> + x <sub>9</sub> + x <sub>12</sub> + x <sub>15</sub> + x <sub>18</sub>	···· ··· ···	  	Equa   	tions to   	be sat    	isfied  	···· ··· ···	  			e <sub>1</sub> e <sub>2</sub> e <sub>5</sub> e <sub>5</sub> e <sub>6</sub>		+ + - + -	0.042 0.473 0.267 0.668 0.400 0.158	Factor 1, $\lambda_1$ 3, $\lambda_3$ 1, $\lambda_3$ 3, $\lambda_4$ 3, $\lambda_5$ 4, $\lambda_8$
X <sub>1</sub> X <sub>6</sub> X <sub>7</sub> X <sub>10</sub> X <sub>18</sub> X <sub>16</sub> X <sub>19</sub>	$+ x_{9}$ $+ x_{5}$ $+ x_{8}$ $+ x_{11}$ $+ x_{14}$ $+ x_{17}$ $+ x_{90}$	$+ x_{3}$ $+ x_{6}$ $+ x_{9}$ $+ x_{19}$ $+ x_{15}$ $+ x_{18}$ $+ x_{91}$	···· ··· ··· ···	   	Equa   	tions to '	be sat    	isfied 	···· ··· ··· ···	··· ··· ··· ···			e <sub>1</sub> e <sub>9</sub> e <sub>5</sub> e <sub>6</sub> e <sub>7</sub>		+ + +	0.042 0.473 0.267 0.668 0.400 0.158 0.491	Factor         λ <sub>1</sub> λ <sub>2</sub> λ <sub>3</sub> λ <sub>3</sub> λ <sub>3</sub> λ <sub>3</sub> λ <sub>4</sub> λ <sub>5</sub> λ <sub>5</sub> λ <sub>6</sub> λ <sub>7</sub> λ <sub>7</sub>
X <sub>1</sub> X <sub>4</sub> X <sub>7</sub> X <sub>10</sub> X <sub>13</sub> X <sub>16</sub> X <sub>19</sub> X <sub>28</sub>	$+ x_{9}$ $+ x_{5}$ $+ x_{8}$ $+ x_{11}$ $+ x_{14}$ $+ x_{17}$ $+ x_{90}$ $+ x_{93}$	$+ x_{3}$ $+ x_{6}$ $+ x_{9}$ $+ x_{19}$ $+ x_{15}$ $+ x_{18}$ $+ x_{91}$ $+ x_{94}$	···· ··· ··· ···	   	Equa    	tions to '	be sat     	isfied 	···· ···· ····	··· ··· ··· ···			e <sub>1</sub> e <sub>2</sub> e <sub>3</sub> e <sub>5</sub> e <sub>6</sub> e <sub>7</sub> e <sub>8</sub>		+ + - + - +	0.042 0.473 0.267 0.668 0.400 0.158 0.491 0.245	Factor 1, $\lambda_1$ 3, $\lambda_3$ 7, $\lambda_3$ 3, $\lambda_4$ 3, $\lambda_5$ 4, $\lambda_5$ 5, $\lambda_7$ 5, $\lambda_7$ 6, $\lambda_7$ 6, $\lambda_8$
X1 X4 X7 X10 X13 X16 X19 X28 X25	$+ x_{9}$ $+ x_{5}$ $+ x_{8}$ $+ x_{11}$ $+ x_{14}$ $+ x_{17}$ $+ x_{90}$ $+ x_{93}$ $+ x_{98}$	$+ x_{3}$ $+ x_{6}$ $+ x_{9}$ $+ x_{19}$ $+ x_{15}$ $+ x_{18}$ $+ x_{91}$ $+ x_{94}$ $+ x_{97}$	···· ··· ··· ···	   	Equa    	tions to '	be sat     	isfied  	···· ···· ···· ····	   			e <sub>1</sub> e <sub>2</sub> e <sub>5</sub> e <sub>6</sub> e <sub>7</sub> e <sub>8</sub> e <sub>9</sub>		+ + + - + +	0.042 0.473 0.267 0.668 0.400 0.158 0.491 0.245 0.297	Factor         λ <sub>1</sub> λ <sub>2</sub> λ <sub>3</sub> λ <sub>3</sub> λ <sub>3</sub> λ <sub>4</sub> λ <sub>5</sub> λ <sub>5</sub> λ <sub>6</sub> λ <sub>7</sub> λ <sub>8</sub> λ <sub>7</sub> λ <sub>8</sub> λ <sub>7</sub> λ <sub>8</sub> λ <sub>9</sub> λ <sub>8</sub> λ <sub>9</sub> λ <sub>8</sub> λ <sub>9</sub>
X1 X4 X7 X10 X13 X16 X19 X92 X92 X95 X1	$+ x_{9}$ $+ x_{5}$ $+ x_{8}$ $+ x_{11}$ $+ x_{14}$ $+ x_{17}$ $+ x_{30}$ $+ x_{33}$ $+ x_{98}$ $+ x_{4}$	$+ x_{3}$ $+ x_{6}$ $+ x_{9}$ $+ x_{19}$ $+ x_{15}$ $+ x_{18}$ $+ x_{21}$ $+ x_{24}$ $+ x_{27}$ $+ x_{7}$	···· ··· ··· ··· ··· ··· ··· + x <sub>10</sub>	     + <b>x</b> <sub>18</sub>	Equa:    	tions to '	be sat      	isfied   	···· ···· ···· ····	··· ··· ··· ··· ···			e <sub>1</sub> e <sub>2</sub> e <sub>3</sub> e <sub>5</sub> e <sub>6</sub> e <sub>7</sub> e <sub>8</sub> e <sub>9</sub> e <sub>10</sub>		+ + + - + + -	0.042 0.473 0.267 0.668 0.400 0.158 0.491 0.245 0.297 0.55,	Factor 1, $\lambda_1$ 3, $\lambda_3$ 7, $\lambda_3$ 3, $\lambda_4$ 3, $\lambda_5$ 4, $\lambda_5$ 5, $\lambda_7$ 5, $\lambda_8$ 5, $\lambda_9$ 5, $\lambda_9$
X1 X4 X7 X10 X13 X16 X19 X92 X92 X92 X1 X9	$+ x_{9}$ + $x_{5}$ + $x_{8}$ + $x_{11}$ + $x_{14}$ + $x_{17}$ + $x_{90}$ + $x_{93}$ + $x_{98}$ + $x_{4}$	$+ x_{3}$ $+ x_{6}$ $+ x_{9}$ $+ x_{19}$ $+ x_{15}$ $+ x_{18}$ $+ x_{91}$ $+ x_{94}$ $+ x_{97}$ $+ x_{7}$ $+ x_{16}$	    + x <sub>10</sub>	     + x <sub>13</sub> + x <sub>29</sub>	Equa       + x <sub>25</sub>	tions to '	be sat     	isfied   	···· ···· ···· ····	··· ··· ··· ··· ··· ···			$e_1$ $e_2$ $e_3$ $e_5$ $e_7$ $e_8$ $e_7$ $e_8$ $e_7$ $e_8$ $e_9$ $e_{10}$ $e_{11}$		+ + + - + + - +	0.042 0.473 0.267 0.668 0.400 0.158 0.491 0.245 0.297 0.55, 0.99,	Factor $\lambda_1$ $\lambda_2$ $\lambda_3$ $\lambda_3$ $\lambda_3$ $\lambda_3$ $\lambda_4$ $\lambda_5$ $\lambda_6$ $\lambda_7$ $\lambda_8$ $\lambda_7$ $\lambda_8$ $\lambda_7$ $\lambda_8$ $\lambda_7$ $\lambda_8$ $\lambda_7$ $\lambda_8$ $\lambda_7$ $\lambda_8$ $\lambda_{10}$ $\lambda_{11}$
X1 X4 X7 X10 X13 X16 X19 X22 X25 X1 X9 16 X8	$+ x_{9} + x_{5} + x_{8} + x_{11} + x_{14} + x_{17} + x_{90} + x_{93} + x_{94} + x_{4} + x_{11} - 9 x_{9}$	$+ x_{3}$ $+ x_{6}$ $+ x_{9}$ $+ x_{19}$ $+ x_{15}$ $+ x_{18}$ $+ x_{21}$ $+ x_{24}$ $+ x_{27}$ $+ x_{7}$ $+ x_{16}$	    + x <sub>10</sub> + x <sub>19</sub> - 22 x <sub>5</sub>	     + X <sub>13</sub> + X <sub>22</sub> + 16 X <sub>9</sub>	Equa         	tions to      + 15x <sub>18</sub>	be sat       	isfied	···· ···· ···· ···· ··· ···	··· ··· ··· ··· ··· ··· ··· ··· ···	4		$e_1$ $e_2$ $e_3$ $e_4$ $e_5$ $e_7$ $e_8$ $e_7$ $e_8$ $e_9$ $e_{11}$ $e_{12}$		+ + + + - + + + + + + + + + + + + +	0.042 0.473 0.267 0.668 0.400 0.158 0.491 0.245 0.297 0.55, 0.99, 55.6,	Factor $\lambda_1$ $\lambda_1$ $\lambda_2$ $\lambda_3$ $\lambda_3$ $\lambda_3$ $\lambda_3$ $\lambda_3$ $\lambda_3$ $\lambda_4$ $\lambda_5$ $\lambda_6$ $\lambda_7$ $\lambda_6$ $\lambda_7$ $\lambda_8$ $\lambda_7$ $\lambda_8$ $\lambda_7$ $\lambda_8$ $\lambda_{10}$ $\lambda_{11}$ $\lambda_{19}$

	Equations between the Factors															
No. of	Value of			<u> </u>			(	Co-efficie	nts of							
е	е	λ <sub>1</sub>	λ	λ <sub>3</sub>	λ4	$\lambda_{5}$	λ <sub>6</sub>	λ <sub>7</sub>	λ <sub>8</sub>	λ <sub>9</sub>	λ <sub>10</sub>	λ <sub>11</sub>		λ <sub>12</sub>	λ	18
1	+ 0.042	+0.12	•••	•••					•••	•••	+0.04			0.24		•••
2	+ 0.473		+0.36	•••	•••	•••		•••		•••	+0.04	•••	-	0.16		
8	- 0.267			+0.19	•••			•••		•••	+0.10	+0.03		0.80	+	0.22
4	– o·668				+0.19	•••	•••	•••	•••	•••	+0.13	+0.03		0.12	-	0.36
5	+ 0.400					+0.31	•••	•••	•••	•••	+0.02	•••	+	1.38		•••
6	- 0.128						+0.12	•••	•••	•••	•••	+0.03		•••	-	0.96
7	- 0.491							+0.12	•••	•••	•••	+0.02		•••	+	0.40
8	+ 0.245					*			+0.13	•••	•••	+0.06		•••	+	0.31
9	+ 0.297									+0.14	•••	+0.00		•••	+	0.21
10	- o·55										+0.32	•••		•••		0.36
11	+ 0.99											+0.32	-	o.43		•••
12	+55.6												+ 1	183.37		26.92
13	+ 53 • 4														+ 1	19.76
	Values of	the Fac	etors					Ang	ular erro	ors in se	conds					
	$\lambda_1 =$	+ 0.63	70													
	$\lambda_{g} = $	+ 1.900	56			$\mathbf{x}_1 = \mathbf{x}_1$	+ 0.069	)	$x_{10} =$	216	i	x <sub>19</sub> =	+	•045		
	$\lambda_s = -$	- 2.780	51			x <sub>2</sub> = -	- 0.241		<b>x</b> <sub>11</sub> =	175	;	x <sub>20</sub> =	_	•744		
	$\lambda_4 = -$	- 4.078	87			x <sub>3</sub> = ·	+ 0.214		x <sub>19</sub> =	277	,	<b>x</b> <sub>21</sub> =	+	• 208		
	$\lambda_{5} = -$	- 1.016	61			x <sub>4</sub> = -	+ 0.130	)	x <sub>13</sub> =	+ .004	ł	x <sub>29</sub> =	+	.311		
	$\lambda_6 =$	+ 1.087	<b>4</b> I			$x_{5} = -$	- 0.701		x <sub>14</sub> =	231		x <sub>23</sub> =	-	• 364		
	$\lambda_7 = -$	- 7.73	7 <b>7</b>			$x_6 = -$	+ 1.054		$x_{15} =$	+ .627	,	x <sub>24</sub> =	+	• 298		
	λ <sub>8</sub> =	- 3.18	76			$x_7 = -$	- 0.527		$x_{16} =$	+ • 284	ł	x <sub>25</sub> =	+	· 284		
	λ <sub>9</sub> =	- 3.63	71			<b>x</b> <sub>8</sub> = -	+ 0.019	1	<b>x</b> <sub>17</sub> =	576	<b>i</b>	x <sub>26</sub> =	_	· 252		
	$\lambda_{10} =$	+ 1.09	10			x, = ·	+ 0.241		x <sub>18</sub> =	+ • 134		x <sub>27</sub> =	+	• 265		
	$\lambda_{11} = \cdot$	+ 8.373	36													
	$\lambda_{13} = $	+ 0.40	19						[wx <sup>2</sup> ] =	= 67.77	,					
	$\lambda_{13} = $	+ 0.295	57													

Figure No. 8-(Continued).

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Figure No. 9.

	Observed Angles			Equations to be satisfied Factor											
		<u> </u>	-]	x <sub>1</sub>	+ x,	, +x,	<b>,</b>			•••	= e <sub>1</sub> =	= — 0.014	, λ <sub>1</sub>		
		ocal ht		X4	+ x,	+x,				•••	= e <sub>2</sub> =	= — 0.304	., λ <sub>2</sub>		
No.	Value	cipr Veig		X7	+ x <sub>s</sub>	+ x,				•••	= e <sub>8</sub> =	= - 1.660	, λ <sub>3</sub>		
		Re		<b>x</b> <sub>10</sub>	+ <b>x</b> 1	1 + x <sub>1</sub>	<u> </u>			•••	= e <sub>4</sub> =	= — 0.028	, λ,		
			-	<b>x</b> <sub>18</sub>	+ x <sub>1</sub>	• + x <sub>1</sub>				•••	= e <sub>5</sub> =	= — 0.016	, λ <sub>5</sub>		
1	° ' " 61 8 50.01	•07		<b>x</b> <sub>16</sub>	+ <b>x</b> <sub>1</sub>	$7 + x_1$	.8				= e <sub>6</sub> =	= — 0.131	, λ <sub>6</sub>		
2	67 48 45.08	•04		x <sub>1</sub>	+ x,	, + <b>x</b> ,	, +x	x <sub>10</sub> + x	13 +	- x <sub>16</sub>	$= e_{7} =$	= — 0°33,	λη		
8	51 2 26.21	•03	17	x <sub>8</sub> -	- 8 x <sub>9</sub>	$+ 8x_{0}$	3 — 17 1	x <sub>5</sub> + 2 x	9 - 21	x <sub>8</sub> )					
4	50 40 41.10	·06	+ 5	; x <sub>12</sub> -	-11 x <sub>1</sub>	$1 + 20 x_1$	5 - 10 1	$x_{14} + 21 x$	<sub>18</sub> — 13	$\{x_{17}\}$	= e <sub>8</sub> =	= +33.6,	λ <sub>8</sub>		
5	51 45 15.26	•07													
6	68 25 4.55	•04					Equi	ations bet	ween tł	ne Factor	<b>19</b>				
7	51 3 12.52	.02			<u> </u>							<b></b>			
8	45 24 44.02	•04	No. of	Valu	e of				Со-е	fficients	of				
9	83 32 2.51	•07	e	e	-	<u> </u>	>		<u> </u>						
10	40 47 31.78	.11				~1	~3	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	~4	~5	~6	~7	~8		
11	62 8 32.59	• 10	1	- o·	014	+0.14		•••			•••	+0.02	+ 0.10		
12	77 3 55.99	•02	2	– o·	304		+0.12	•••		•••		+0.06	- 0.87		
13	69 17 34.15	.05	8	– I.	660			40.16				+0.02	- 0.70		
14	64 14 48.86	·06	4	– o·	028				+0.33			+0.11	- 1.00		
15	46 27 37.60	·05	5	- 0.	016					+0.16	•••	+0.02	+ 0.40		
16	77 53 10.02	.10	6	- o·	131				*		+0.30	+0.10	+ 0 <sup>.</sup> 74		
17	58 21 13.94	•04	7	- 0.	33							+0.44			
18	43 45 36.91	·o6	8	+ 33.	6								+123.76		
۲	Values of the Factor						Aı	gular err	ors in s	seconds					
	h = - 0.0050														
	$\lambda_{1} = -1.0381$			x <sub>1</sub>	=	+ .013		$\mathbf{x}_{7} =$	- '42	28	<b>x</b> <sub>18</sub> =	= + •∞7			
	$\lambda_{1} = -0.7278$			Xg		113		$\mathbf{x}_8 =$	- • 58	52	<b>x</b> <sub>14</sub> =	= - • 200			
	$\lambda_{1} = + 0.3157$			X3		+ .082		x <sub>9</sub> =	05	50	<b>x</b> <sub>15</sub> =	= + 177			
	$\lambda_{c} = -1.0278$			X4		+ .009		$x_{10} =$	+ •10	23	<b>x</b> <sub>16</sub> =	=092			
	$\lambda_{a} = -2.0868$			<b>X</b> 5	. = .	- '344		x <sub>11</sub> =	- · 22	20	<b>x</b> <sub>17</sub> =	=203			
	$\lambda_7 = + 1.1682$			x <sub>6</sub>	. = .	+ .033		x <sub>19</sub> ==	+ '0	29	<b>x</b> <sub>18</sub> =	= + '104			
	$\lambda_{0} = + 0.2201$							[wx <sup>2</sup> ]	= 24.0	09					
									•	-					

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## PRINCIPAL TRIANGULATION. REDUCTION OF FIGURES.

	Observed Angles				Equations to	be satisfied		Factor		
	<u> </u>	t al		x <sub>1</sub> + 3	- x <sub>2</sub> + x <sub>8</sub>	+ x4	$= e_1 = -$	- 0.012, λ1		
No.	Value	leciproc Weight	• •	x <sub>s</sub> + 3	x <sub>4</sub> + x <sub>5</sub>	+ x <sub>6</sub>	-= e <sub>s</sub> = +	- 0·155, λ <sub>8</sub>		
	· .	<u> </u>		x <sub>5</sub> + 3	x <sub>6</sub> + x <sub>7</sub>	+ <b>x</b> <sub>8</sub>	= e <sub>8</sub> = +	-0.180, λ <sub>8</sub>		
1	o <i>' "</i> 49 58 5.62	• 12		- 172 + 183	$x_1 - ox_3$	$-23x_{3}$	-18·3, λ <sub>4</sub>			
2	47 46 48.82	•04		1202	-6 - 5-7	-/ · · · · · · · · · · · · · · · · · · ·				
8	43 10 50.40	•02			Equations between the Factors					
4	39 4 15.79	•09				Co-effic	cients of			
5	39 23 48.18	•08	No. of	Value of						
6	58 21 6.40	.09	e	e	λ <sub>1</sub>	λ <sub>3</sub>	λ <sub>3</sub>	λ,		
7	45 33 30.60	•08								
. <b>8</b>	36 41 35 <b>·52</b>	•13	1	- 0.013	+0.32	+0.11	••••	- 2.20		
			2	+ 0.122		+0.38	+0.12	+ 1.12		
			8	+ 0.180		#	+0.38	+ 5.79		
· · ·	. ·		4	+18.3				+ 185.75		
V	alues of the Facto	rs			Angular	Angular errors in seconds				
	$\lambda_1 = + 1.5041$			<b>x</b> 1	=255	X,	<sub>5</sub> = - ·176			
	$\lambda_{3} = + 1.0513$			x <sub>s</sub>	= + ·o60	x	s = + ·148			
	$\lambda_3 = -3.2499$			X3	=042	X	r =174			
	$\lambda_4 = + 0.2135$			X4	= + ·230	= + ·230 x <sub>8</sub>				
	••••				[1	$\mathbf{w}\mathbf{x}^{3}] = 3.47$	•	•		

Figure No. 10.

	Observed Angles			Equations to be satisfied										
	<u> </u>		·	x <sub>1</sub>	+ x <sub>8</sub>	+ <b>x</b> <sub>3</sub>	•••	•••	=	e <sub>1</sub> =	- 0.02	55, λ <sub>1</sub>		
No	Velue	rocal ight		x,	+ x <sub>5</sub>	+ <b>x</b> 6	•••	•••		e <sub>3</sub> =	- 0.31	ο, λ <sub>s</sub>		
110.	V ALUC	Recip Wei		x <sub>7</sub>	+ <b>x</b> <sub>8</sub>	+ x <sub>9</sub>				e <sub>8</sub> =	- 0.36	ίο, λ <sub>8</sub>		
				<b>x</b> <sub>10</sub>	+ <b>x</b> <sub>11</sub>	+ x <sub>19</sub>	•••	•••	=	e <sub>4</sub> =	+ 0.31	3, λ		
	o / <i>W</i>			<b>x</b> 18	+ x <sub>14</sub>	+ x <sub>15</sub>			=	e <sub>5</sub> =	+ 0.18	βι, λ <sub>5</sub>		
	80 3 47.47	•13		x <sub>1</sub>	+ x <sub>4</sub>	+ x <sub>7</sub>	+ x <sub>10</sub>	+ x <sub>18</sub>	=	e <sub>6</sub> =	- 0.15	5, λ <sub>6</sub>		
2	46 16 27.68	•10	1	9x <sub>8</sub> —	20x <sub>9</sub> +	1 I X <sub>6</sub>	— 17 x <sub>5</sub>	+22x9		•				
8	47 39 45.10	•03	-1	4x <sub>8</sub> +	15x <sub>18</sub> —	~ 7 x <sub>11</sub>	+ 1 2 X <sub>15</sub>	-20X14	=	e <sub>7</sub> =	- 25.0,	~		
4	66 44 50.83	•12			<u></u>					<u> </u>				
5	50 45 53.05	•06		Equations between the Factors										
6	62 29 16.15	•11						Co-eff	icients of					
7	80 34 52.73	• 20	No. of	Value of e	f									
8	55 49 49 45	• 20			λ	λ	, 7	<b>1</b> 8 7	λ <sub>4</sub> λ	·5	λ <sub>6</sub>	λη		
9	43 35 17.73	•08			-	6			<del>.</del>					
10	54 51 24.27	•04		- 0.05	5 +0.2		•••	•• •	•• •	• •	+0.13	- 1.43		
11	71 40 56.77	• 20		- 0.31	0	+0'	' <b>29</b> .		•••		+0.13	+ 0.19		
12	53 27 39 <sup>.</sup> 59	• 15	8	- o·30	0		+0	. 48	•••	••••	+0.30	- 1.04		
13	<b>71 45 4</b> .55	•12	4	+ 0.31	3			+ 4	o <b>·3</b> 9 ··		+0.04	+ 0.82		
14	46 37 16.28	•19	5	+ 0.18	I		*		+0	• 37	+0.13	- 3.08		
15	61 37 39.71	•06	6	- 0.12						-	+0.01	•••		
			7	-25.6								+ 287 . 59		
	Values of the Fact	Drs					Angular e	errors in se	conds					
	$\lambda_1 = - 1 \cdot 1279$	)		<b>.</b> .	06						- · • • •	-		
	$\lambda_3 = -0.0100$	)		• <u>1</u> -	00	5	<u>~</u> 6 -	232	•		T 34	.) 		
	$\lambda_{3} = -1.252$	5		x <sub>8</sub> =		5	x <sub>7</sub> =	= - ·122		x <sub>12</sub> =	- •09	7		
	$\lambda_{1} = + 0.0720$	)		<b>x</b> <sub>8</sub> =	= •09.	5	<b>x</b> 8 =	= + •052		x <sub>18</sub> =	+ •00	3		
	$\lambda_{r} = -0.0102$	1		x <sub>4</sub> =	=03	3	<b>x</b> 9 =	= - • 290		x <sub>14</sub> =	+ •29	3		
	$\lambda_{n} = \pm 0.6442$	1		<b>x</b> <sub>5</sub> =	= + •05	5	<b>x</b> <sub>10</sub> =	= + •o6 <u>;</u>	5	<b>x</b> <sub>15</sub> =	11	5		
	$\lambda_7 = -0.1080$	)					[wx	<sup>s</sup> ] = 3.5%	7					

Figure No. 11.

	Observed Angles					Eq	uations t	o be sati	sfied			Factor
				<b>x</b> 1 -	+ x <sub>s</sub>	+ x <sub>8</sub>	•••	•	•••	= e <sub>1</sub> =	= + 0'179,	λ
		ocal	ļ	x	+ x5	+ x <sub>6</sub>		•	•••	= e <sub>3</sub> =	= + 0.045,	λ
No.	Value	ecipr Weig		x <sub>7</sub> -	+ x <sub>8</sub>	+ x <sub>9</sub>		•	•••	= e <sub>s</sub> =	= — 0.024,	λ <sub>s</sub>
		<b>Å</b> .		<b>x</b> <sub>10</sub> -	+ <b>x</b> 11	+ x <sub>19</sub>	<b>.</b>	•		= e <sub>4</sub> =	= — 0.135,	λ4
	0 / //			<b>x</b> <sub>18</sub> -	+ x <sub>16</sub>	+ x <sub>18</sub>	; ··	•	•••	= e <sub>s</sub> =	= + 0.179,	$\lambda_{5}$
1	64 5 51.49	•08		<b>x</b> 1 ·	+ x4	+ x <sub>7</sub>	+ <b>x</b>	- 10 +	- x <sub>18</sub>	= e <sub>6</sub> =	= + 0.02,	λ <sub>6</sub>
2	60 29 15.41	.13	I	4 <b>x</b> <sub>8</sub> — 1	1 Xg	+ 19x6	- 213	x <sub>5</sub> + 2	9x, )	_		
8	55 <b>24</b> 53°55	•14	-1	3x <sub>8</sub> +	7 <b>x</b> 19	-22 x <sub>11</sub>	+ 103	a <sub>15</sub> — 1.	4 x <sub>14</sub> 5	= e <sub>7</sub> =	= + 8'7,	۲۸
4	86 5 44.71	.13					Equatio	ns betwe	en the Fac	tors		
5	45 42 27.01	•09					-1					
6	48 11 48.63	•08	No. of	Value of					Co-efficient:	s of		
7	85 58 0·62	•15	e	е	,	λ,	λ	λ	λ,	λ,	λ	λ <sub>7</sub>
8	58 12 4.50	•06										
9	35 49 55.28	.13	1	+0.129	+0	.35	•••	•••	•••	•••	+0.08 4	- 0.23
10	64 38 43.63	.11	2	+0.042		+	-0.30	•••	•••	•••	+0.13 -	- 0.32
11	43 31 2.25	• 22	8	-0.034				+0.34	•••	•••	+0.12 4	- 2.99
12	71 50 14.39	•07	4	-0.132					+0.40	•••	+0.11 -	- 4.35
18	59 11 39.57	•07	5	+0.128				*		+0.39	+0.02 -	- 1.60
14	57 5 44.32	• 20	6	+0.03							+0.24	•••
15	<b>63 42 3</b> 6·55	.13	7	+8.2							-	- 392 • 32
	Values of the Factor	8			ł		Angul	ar errors	s in seconds	•		
	$\lambda_1 = + 0.4918$									_	_ ``	
	$\lambda_3 = + 0.3183$			<b>1</b> 1 =	+ '0	533	×.	, = +	057	±11	= - 132	
	$\lambda_3 = - 0.3590$			x <sub>3</sub> =	+ •	027	X,	, = -	-052	x <sub>19</sub>	= + .010	
	$\lambda_4 = - 0.0353$			<b>x</b> <sub>s</sub> =	+ •	119	X,	, = -	-035	<b>X</b> 13	= + '035	
	$\lambda_{5} = + \circ \cdot 5794$			x4 =	+ •	017	x,	) = +	•003	<b>x</b> <sub>14</sub>	= + •044	
	$\lambda_6 = -0.0843$			x, =		029	<b>x</b> j	10 = -	.013	<b>x</b> 15	= + .100	
	$\lambda_{\gamma} = + 0.0257$						[	wx <sup>9</sup> ] =	0.43			

Figure No. 12.

May, 1885.

W. H. COLE, In charge of Computing Office.

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# PRINCIPAL TRIANGULATION. TRIANGLES.

No. of 1	riangle	Number and Name of Station	rica. ess	Corre	ections to	Observed .	Angle	Corrected Plane		Distance	
Circuit	Non- circuit		Sphe Exc	Figure	Circuit	Non- circuit	Total	Angle	Log. feet	Feet	Miles
1		LXXV (Rojhra) LXXVIII (Sandohar) V (Bhádi)	" •689 •689 •689	" - •659 + •088 + •838	" + '880 + '090 - '970	"	+ ·221 + ·178 - ·132	0 / " 60 25 37.022 68 39 56.149 50 54 26.829	5:0107656,2 5:0405528,1 4:9613162,0	102509*86 109787*48 91477*90	19°415 20°793 17°325
2		LXXVIII (Sandohar) V (Bhádi) IV (Narithal)	2·067 •651 •650 •650	+ .086 201 + .706	+ ·484 + ·112 - ·596		+ ·267 + ·570 - ·089 + ·110	180 0 0.000 66 39 2.349 49 53 29.891 63 27 27.760	5'0220268,9 4'9426977,8 5'0107656,2	105202°71 87639°08 102509°86	19°925 16°598 19°415
	40	LXXV (Rojhra) LXXVIII (Sandohar) I (Fulrár)	1.951 .340 .340 .340	+ ·548 - ·461 - ·177		+ '336 - '272 - '064	$+ \cdot 591$ + $\cdot 884$ - $\cdot 733$ - $\cdot 241$	46 47 48 734 44 57 20 757 88 14 50 509	4 <sup>.8</sup> 242059,7 4 <sup>.8106688,9</sup> 4 <sup>.</sup> 9613162,0	66712·30 64664·94 91477·90	12.635 12.247 17.325
	41	I (Fulrár) LXXVIII (Sandohar) II (Chánga)	· 254 · 255 · 255	+ •605 - •069 - •252		+ '497 - '232 - '265	+1.102 -301 -517	39 13 54·278 81 16 52·424 59 29 13·298	4.6899756,1 4.8838957,4 4.8242059,7	48975 • 14 76541 • 29 66712 • 30	9°276 14°496 12°635
	42	II (Chánga) LXXVIII (Sandohar) III (Patatonk)	·704 ·283 ·283 ·283 ·849	$+ \cdot 467 + \cdot 923 - \cdot 621$		+ ·296 + ·049 - ·345	$\begin{array}{r} + & \cdot 284 \\ + & \cdot 763 \\ + & \cdot 972 \\ - & \cdot 966 \\ + & \cdot 769 \end{array}$	180       0       0.000         84       46       38.510         60       1       9.469         35       12       12.021         180       0       0.000	4`9273847,5 4`8668065,1 4`6899756,1	84602 · 80 73587 · 92 48975 · 14	16°023 13°937 9°276

NOTES.—1. The values of the side are given in the same line with the opposite angle.
2. Stations LXXV (Rojhra) and LXXVIII (Sandohar) appertain to the Karáchi Longitudinal Series.

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## PRINCIPAL TRIANGULATION. TRIANGLES.

No. of t	riangle		ical	Corre	ctions to	Observed	Angle	Corrected Plang		Distance	
Circuit	Non- circuit	Number and Name of Station	Spher Exce	Figure	Circuit	Non- circuit	Total	Angle	Log. feet	Feet	Miles
	43	III (Patatonk) LXXVIII (Sandohar) IV (Narithal)	" • 364 • 363 • 363	+ ·541 + ·072 - ·213	<b>W</b> :	+ '209 - '118 - '091	" + '750 - '046 - '304	° , " 73 40 56.386 38 25 36.271 67 53 27.343	4·9426977,7 4·7540043,7 4·9273847,5	87639°07 56755°04 84602°80	16.598 10.749 16.023
<b>8</b>		IV (Narithal) V (Bhádi) VII (Rupihar)	1°090 •582 •582 •583	+ •461 + •321 + •115	+ ·637 - ·077 - ·560		$+ \cdot 400$ + 1 \cdot 098 + \cdot 244 - \cdot 445	180 0 0.000 54 30 57.496 51 49 21.782 73 39 40.722	4`9507019,2 4`9354085,1 5`0220268,9	89269°25 86180°40 105202°71	16°907 16°322 19°925
4		V (Bhádi) VII (Rupihar) VIII (Kanakotri)	1.747 .459 .460 .459 1.378	+ •433 + •018 + •277	+ ·876 - ·230 - ·646		$+ \frac{100}{100} $	183         0         0         0         0000           45         29         7         050         68         56         55         778         65         33         57         172           180         0         0         0         0000         0         0000	4 <sup>.</sup> 8445842,7 4 <sup>.</sup> 9614543,9 4 <sup>.</sup> 9507019,2	69917°24 91507°02 89269°25	13°242 17°331 16°907
5		VIII (Kanakotri) VII (Rupihar) X (Bhitala)	· 320 · 319 · 320	+ '414 + '017 + '128	+ '450 + '062 - '512		+ .864 + .079 384	71 47 47 474 48 43 50 280 59 28 22 246	4 <sup>.</sup> 8870873,0 4 <sup>.</sup> 7853817,0 4 <sup>.</sup> 8445842,7	77105 · 84 61007 · 28 69917 · 24	14 <sup>.603</sup> 11 <sup>.554</sup> 13 <sup>.242</sup>
6		VII (Rupihar) X (Bhitala) IX (Mangtor)	<u>959</u> ·428 ·428 ·427	- '059 + '236 + '136	+ ·564 + ·079 - ·643		+ 559 + 505 + 315 - 507	58 5 34 297 64 39 21 327 57 15 4 376	4 8911247,0 4 9183152,4 4 8870873,0	77826.00 82854.33 77105.84	14°740 15°692 14°603
	44	IV (Narithal) VII (Rupihar) VI (Hatodan)	1 283 421 422 422	$+ \cdot 186$ $- \cdot 133$ $+ \cdot 152$		+ 1 · 331 - · 230 - 1 · 101	+ 313 +1.517 - 363 - 949	49 24 7.696 61 59 19.055 68 36 33.249	4 <sup>.</sup> 8468162,4 4 <sup>.</sup> 9122944,5 4 <sup>.</sup> 9354085,1	70277°49 81713°61 86180°40	13·310 15·476 16·322
	45	VI (Hatodan) VII (Rupihar) IX (Mangtor)	1 · 205 · 345 · 344 · 344	+ ·283 - ·058 + ·098	. <u> </u>	+ '738 + '394 -1'132	$+ \cdot 205$ + 1 \cdot 021 + \cdot 336 - 1 \cdot 034	180       0       0       0       0         76       1       34       506         48       34       37       312         55       23       48       182	4`9183152,4 4`8063335,8 4`8468162,4	82854 · 33 64022 · 64 70277 · 49	15°692 12°126 13°310
7		X (Bhitala) IX (Mangtor) XII (Thakur)	1.033 (399 (398 (398) (398)	+ ·058 - ·020 + ·037	+ ·314 + ·223 - ·537		+ 323 + 372 + 203 - 500	82 32 10°243 43 6 33°645 54 21 16°112	4°9775321,9 4°8158980,4 4°8911247,0	94958 • 13 65448 • 25 77826 • 00	17°984 12°396 14°740
8		IX (Mangtor) XII (Thakur) XI (Narhar)	*407 *407 *407 *407	+ °034 - °274 - °059	+ '482 - '144 - '338		+ .516 418 397	49 41 17.969 48 3 51.215 82 14 50.816	4 <sup>.86</sup> 37805,9 4 <sup>.8530312,6</sup> 4 <sup>.9775321,9</sup>	73076 · 98 71290 · 44 94958 · 13	13°840 13°502 17°984
	46	IX (Mangtor) X (Bhitala) XI (Narhar)	*437 *437 *437	+ .014 + .093 056		+ '705 - '143 - '562	+ .719 050 618 + .051	92 47 51 982 41 12 39 703 45 59 28 315	5 <sup>.0</sup> 337370,7 4 <sup>.8</sup> 530312,6 4 <sup>.8</sup> 911247,0	108077°95 71290`44 77826`00	20°469 13°502 14°740
9		XI (Narhar) XII (Thakur) XIV (Malar)	· 432 · 432 · 432 · 431	+ ·137 - ·268 + ·086	+ ·484 + ·130 - ·614		+ .621 138 528	60 41 1.089 67 31 27.750 51 47 31.161	4`9089662,3 4`9341767,2 4`8637805,9	81089·80 85936·32 73076·98	15°358 16°276 13°840
10		XII (Thakur) XIV (Malar) XV (Badhor)	1 295 445 446 446 1 337	+ ·266 + ·009 - ·168	+ ·424 - ·034 - ·390	5	$- \frac{.045}{.025}$ $- \frac{.025}{.025}$ $- \frac{.558}{.07}$	160         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0	4 8944387,3 4 9194465,6 4 9089662,3	78422°15 83070°45 . 81089°80	14.853 15.733 15.358

NOTE.-Station LXXVIII (Sandohar) appertains to the Karáchi Longitudinal Series.

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No. of t	riangle		rical eas	Corre	octions to	Observed .	Angle	Corrected Plane		Distance	
Circuit	Non- circuit	Number and Name of Station	Sphei Kro	Figure	Circuit	Non- circuit	Total	Angle	Log. feet	Feet	Miles
11		XV (Badhor) XIV (Malar) XVII (Sinaba)	" • 416 • 416 • 416	" + '191 + '287 - '060	" + *450 - *045 - *405	η	" + •641 + •242 - •465	0 / 7 55 49 56 675 64 1 50 016 60 8 13 309	4 <sup>.8</sup> 740247,1 4 <sup>.</sup> 9100831,8 4 <sup>.8</sup> 944387,3	74821 · 21 81298 · 62 78422 · 15	14°171 15°397 14°853
12		XIV (Malar) XVII (Sinaba) XVI (Ramsar)	1 · 248 · 336 · 337 · 337	- ·048 + ·087 - ·119	+ ·303 + ·025 - ·328		$+ \cdot 418$ + $\cdot 255$ + $\cdot 112$ - $\cdot 447$	180 0 0.000 56 8 31.469 57 21 1.595 66 30 26.936	4 <sup>.</sup> 8309009,3 4 <sup>.</sup> 8369072,0 4 <sup>.</sup> 8740247,1	67748-69 68692-16 74821-21	12 · 831 13 · 010 14 · 171
	47	XI (Narhar) XIV (Malar) XIII (Jeysulmere)	1.010 .424 .425 .424	- ·003 + ·432 + ·384		+ ·556 + ·120 - ·676	080 + .553 + .552 292	180 0 0.000 46 38 47.169 66 48 52.807 66 32 20.024	4 <sup>.</sup> 8332637,4 4 <sup>.</sup> 9350780,3 4 <sup>.</sup> 9341767,2	68118°29 86114°85 85936°32	12°901 16°310 16°276
	48	XIII (Jeysulmere) XIV (Malar) XVI (Ramsar)	·315 ·314 ·314	- ·100 + ·174 + ·179		+ ·338 + ·270 - ·608	$+ \cdot 813$ + $\cdot 238$ + $\cdot 444$ - $\cdot 429$	180         0         0.000           61         11         26.483           58         28         38.290           60         19         55.227	4 <sup>.8</sup> 369072,0 4 <sup>.8</sup> 249501,5 4 <sup>.8</sup> 332637,4	68692 · 16 66826 · 72 681 18 · 29	13°010 12°657 12°901
18		XVI (Bamsar) XVII (Sinaba) XIX (Joganali)	·943 ·396 ·396 ·396	+ .053 291 + .036	+ ·231 + ·198 - ·429		+ 253 + 284 - 093 - 393	180         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0         0	4`95 <b>39220,0</b> 4`8810634,6 4`8 <b>309009,3</b>	89933-60 76043-73 67748-69	17°033 14°402 12°831
14		XVII (Sinaba) XIX (Joganali) XX (Kardo)	1.188 .334 .335 .335	$+ \cdot 108$ $- \cdot 331$ $- \cdot 323$	+ ·345 - ·171 - ·174		$\frac{-202}{+453}$ -502 -497	180         0         0.000           41         55         1.279           51         36         23.343           86         28         35.378	4°7795551,0 4°8489289,4 4°9539220,0	60194°26 70620°20 89933°60	11°400 13°375 17°033
15		XX (Kardo) XIX (Joganali) XXII (Arrabhit)	1.004 277 277 277 276	+ ·558 + ·252 - ·020	+ ·303 - ·004 - ·299		$\frac{-546}{+861}$ + 248 - 319	180 0 0.000 56 58 45.874 69 3 7.041 53 58 7.085	4 <b>.7952602,9</b> 4.8420730,0 4.7795551,0	62410-88 69514-11 60194-26	11.820 13.166 11.400
16		XIX (Joganali) XXII (Arrabhit) XXI (Sanahu)	·830 ·242 ·242 ·242	- ·099 - ·036 - ·309	+ '168 + '032 - '200		+ .790 + .069 004 509	180 0 0.000 57 5 2.667 58 6 11.784 64 48 45.549	4 <sup>.</sup> 7626542,1 4.7675582,6 4 7952602,9	57896 • 75 58554 • 22 62410 • 88	10°965 11°090 11°820
	49	XVI (Ramsar) XIX (Joganali) XVIII (Potanawári)	· 720 · 303 · 303 · 303	- ·210 + ·271 + ·178		+ 217 + 165 - 382	$\frac{- \cdot 444}{+ \cdot 007} \\ + \cdot 436 \\ - \cdot 204$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	4 <sup>.</sup> 7561449,8 4 <sup>.</sup> 8501258,3 4 <sup>.</sup> 8810634,6	57035°46 70815°09 76043°73	10°802 13°412 14°402
	50	XVIII (Potanawári) XIX (Joganali) XXI (Sanahu)	· 909 · 251 · 252 · 251	- '777 + '311 + '150		+ ·196 + ·271 - ·467	+ 239 - 581 + 582 - 317	180         0         0.000           54         43         25.698           72         36         6.510           52         40         27.792	4`7675582,6 4`8353292,7 4`7561449,8	58554°22 68443°04 57035°46	11.090 12.963 10.802
17		XXII (Arrabhit) XXI (Sanahu) XXIV (Dhanono)	- 754 • 307 • 307 • 306	- '114 + '354 - '300	+ ·113 + ·181 - ·294		$- \frac{310}{- 001}$ + $\frac{535}{- 594}$	96 47 52.102 45 32 40.158 37 39 27.740	4`9735898,1 4`8302268,6 4`7626542,1	94100°05 67643°62 57896°75	17°822 12°811 10°965
18		XXI (Sanahu) XXIV (Dhanono) XXIII (Harnáo)	<u>920</u> 377 377 378 1.132	+ '086 + '046 - '240	+ '086 + '005 - '091		$ \begin{array}{r} - & \cdot & 060 \\ + & \cdot & 172 \\ + & \cdot & 051 \\ - & \cdot & 331 \\ - & \cdot & 108 \\ \end{array} $	180 0 0.000 53 51 39.775 41 47 58.264 84 20 21.961 180 0 0.000	4 <sup>.</sup> 8829031,8 4 <sup>.</sup> 7995299,5 4 <sup>.</sup> 9735898,1	76366 • 56 63027 • 49 94100 • 05	14°463 11°937 17°822

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# PRINCIPAL TRIANGULATION. TRIANGLES.

No. of T	riangle		rical ess	Corre	ctions to	Observed .	Angle	Corrected Plane	•	Distance           Log. feet         Feet         Miles           9651481,1         92288.62         17.474           7995299,4         63027.48         11.933           7626542,1         57896.75         10.96		
Circuit	Non- circuit	Number and Name of Station	Bpher Exc	Figure	Circuit	Non- circuit	Total	Angle	Log. feet	Feet	Miles	
	51	XXI (Sanahu) XXII (Arrabhit) XXIII (Harnáo)	* * 284 * 284 * 283	" + '440 - '062 + '103	77	* + *267 + *018 - *285	" + '707 - '044 - '182	0 / 7 99 24 20'333 42 21 27'832 38 14 11'835	4'9651481,1 4'7995299,4 4'7626542,1	92288.62 63027.48 57896.75	17°479 11°937 10°965	
19		XXIII (Harnáo) XXIV (Dhanono) XXVI (Ráviláhu)	•851 •292 •291 •292	+ ·006 + ·014 - ·045	+ °104 + °012 - °116		$+ \cdot 481 \\+ \cdot 110 \\+ \cdot 026 \\- \cdot 161 \\- \cdot 025$	180 0 0.000 53 5 46.178 50 27 6.835 76 27 6.987	4'7980561,7 4'7822645,1 4'8829031,8	62813 · 95 60570 · 97 76366 · 56	11 · 897 11 · 472 14 · 463	
20		XXIV (Dhanono) XXVI (Ráviláhu) XXIX (Máringra)	325 325 324	- °020 - °183 + °027	+ '117 + '011 - '128		- 025 + 097 - 172 - 101	50 52 6.512 81 47 18.963 47 20 34.525	4 <sup>.</sup> 8212126,4 4 <sup>.</sup> 9270438,6 4 <sup>.</sup> 7980561,7	66254°08 84536°42 62813°95	12.548 16.011 11.897	
21		XXVI (Ráviláhu) XXIX (Máringra) XXVIII (Girája)	• 278 • 277 • 278 • 822	+ '353 - '098 + '078	+ '005 + '054 - '059		+ .358 044 + .019 + .222	64 59 12.140 52 4 35.939 62 56 11.921	4 <sup>.</sup> 8288055,6 4 <sup>.</sup> 7685622,2 4 <sup>.</sup> 8212126,4	67422°61 58689°75 66254°08	12.769 11.115 12.548	
22		XXIX (Máringra) XXVIII (Girája) XXXI (Asu)	348 348 348 348	+ '395 + '379 + '040	+ '010 + '031 - '041		$+ \cdot 405$ + $\cdot 410$ - $\cdot 001$	70 11 36 007 56 11 39 322 53 36 44 671	4 <sup>.</sup> 8965140,6 4 <sup>.</sup> 8425614,0 4 <sup>.</sup> 8288055,6	78797 · 79 69592 · 33 67422 · 61	14°924 13°180 12°769	
23		XXVIII (Girája) XXXI (Asu) XXX (Singra)	· 362 · 362 · 363	+ '042 + '410 - '045	- '052 + '044 + '008		- 014 - 010 + 454 - 037	55 22 29 828 56 34 38 892 68 2 51 280	4`8445434,0 4`8506972,9 4`8965140,6	69910-66 70908-34 78797-79	13°241 13°430 14°924	
	52	XXIII (Harnáo) XXVI (Ráviláhu) XXV (Bándri)	· 308 · 308 · 308	+ '334 + '021 + '139		+ ·120 + ·078 - ·198	+ .454 + .099 059	59 41 54 206 70 28 51 621 49 49 14 173	4 <sup>.8</sup> 353578,7 4 <sup>.8</sup> 734507,3 4 <sup>.</sup> 7822645,1	68447`54 74722`38 60570`97	12.964 14.152 11.472	
	53	XXVI (Báviláhu) XXV (Bándri) XXVIII (Girája)	924 *290 *290 *290	- '475 + '587 - '002		+ '021 + '060 - '081	$+ \frac{494}{- \cdot 454}$ + $\cdot 647$ $- \cdot 083$	180         0         0         0         0         0           66         17         28.796         50         9         4.097         63         33         27.107           180         0         0.0000         0.0000         0.0000         0.0000         0.0000	4 <sup>.</sup> 8450561,7 4 <sup>.</sup> 7685622,2 4 <sup>.</sup> 8353578,7	69993°25 58689°75 68447°54	13·256 11·115 12·964	
	54	XXV (Bándri) XXVIII (Girája) XXVII (Máhu)	353 352 352	- '081 - '097 + '705		- °019 + °084 - °065	- '100 - '013 + '640	70 10 32 067 53 38 48 415 56 10 39 518	4 <sup>.</sup> 8990445,9 4 <sup>.</sup> 8315765,0 4 <sup>.</sup> 8450561,7	79258·27 67854·16 69993·25	15°011 12°851 13°256	
	55	XXVII (Máhu) XXVIII (Girája) XXX (Singra)	·411 ·412 ·412	- ·412 - ·100 + ·307		- •008 + •077 - •069	- '420 - '023 + '238	51 10 5.469 68 17 21.365 60 32 33.166	4 <sup>.</sup> 8506972,9 4 <sup>.</sup> 9272107,8 4 <sup>.</sup> 8990445,9	70908 · 34 84568 · 92 79258 · 27	13.430 16.017 15.011	
.24		XXXI (Asu) XXX (Singra) XXXIII (Parethal)	· 235 · 332 · 333 · 333 · 333	- ·214 + ·241 - ·069	- ·082 + ·047 + ·035		- ·296 + ·288 - ·034	53 10 19.692 67 44 37.725 59 5 2.583	4 <sup>.8</sup> 144244,5 4 <sup>.8</sup> 774718,9 4 <sup>.8</sup> 445434,0	65226·56 75417·45 69910·66	12°354 14°284 13°241	
25		XXX (Singra) XXXIII (Parethal) XXXII (Bitri)	993 223 223 224 .670	627 004 + .231	- ·123 + ·033 + ·090		$ \begin{array}{r} - & \cdot & 750 \\ + & \cdot & 029 \\ + & \cdot & 321 \\ - & \cdot & 400 \end{array} $	49 35 11.257 56 58 7.016 73 26 41.727 180 0 0.000	4`7144157,0 4`7562481,6 4`8144244,5	51810°25 57049°02 65226°56	9°813 10°805 12°354	

No.of T	riangle		rical	Corre	ctions to (	Observed A	Angle	Corrected Plane		Distance	
Circuit	Non- circuit	Number and Name of Station	Spher	Figure	Circuit	Non- circuit	Total	Angle	Log. feet	Feet	Miles
26	~	XXXIII (Parethal) XXXII (Bitri) XXXVI (Kháro)	* • 263 • 263 • 262	" + '216 + '277 + '175	" - 'í04 - '010 + '114	4	$+ \cdot 112$ + $267$ + $289$ + $3668$	85 7 36.089 54 14 3.134 40 38 20.777	4 <sup>.</sup> 8990669,7 4 <sup>.</sup> 8098816,6 4 <sup>.</sup> 7144157,0	79262 ° 36 64547 ° 83 51810 ° 25	15°012 12°225 9°813
27		XXXII (Bitri) XXXVI (Kháro) XXXV (Chauki)	· 357 · 358 · 358	- ·265 - ·284 + ·252	- ·173 + ·030 + ·143	-	- · 438 - · 254 + · 395	53 8 55 885 57 35 23 768 69 15 40 347	4·8313570,1 4·8546230,9 4·8990669,7	67819 88 71552 22 79262 36	12.845 13.552 15.012
28		XXXVI (Kháro) XXXV (Chauki) XXXVIII (Trisingh)	1.073 .309 .308 .308	- ·311 - ·298 + ·364	- °154 + °034 + °120		<u>- ·297</u> - ·465 - ·264 + ·484	180 0 0.000 80 54 58.286 44 31 54.258 54 33 7.456	4`9149085,4 4`7662962,0 4`8313570,1	82206 · 95 58384 · 32 67819 · 88	15,569 11,058 12,845
	56	XXXI (Asu) XXXIII (Parethal) XXXIV (Kolu)	•925 •385 •386 •386	+ '701 - '120 -1'054		- 167 + 046 + 121	$\frac{-245}{+534}$	180 0 0.000 43 6 11.719 84 38 57.740 52 14 50.541	4 <sup>.8</sup> 141024,0 4 <sup>.</sup> 9775 <sup>8</sup> 48,7 4 <sup>.8</sup> 774718,9	65178°21 94969°66 75417°45	12°344 17°987 14°284
	57	XXXIII (Parethal) XXXIV (Kolu) XXXVI (Kháro)	319 319 319 319	+ ·527 - ·019 - ·241		- ·010 - ·037 + ·047	$- \frac{473}{- 517}$ $- \frac{056}{- 194}$	74 10 15.048 52 32 46.525 53 16 58.427	4 <sup>.</sup> 8933571,5 4.8098816,6 4.8141024,0	78227 ° 08 64547 ° 83 65178 ° 21	14.816 12.225 12.344
	58	XXXIV (Kolu) XXXVI (Kháro) XXXVII (Morgich)	<u>957</u> •246 •246 •246	+ ·576 - ·284 - ·134		- ·093 + ·016 + ·077	+ 207 + 483 - 268 - 057	38 54 0.087 54 13 13.596 86 52 46.317	4 6919358,5 4 8031682,7 4 8933571,5	49196°69 63557°72 78227°08	9·318 12·037 14·816
	59	XXXVII (Morgich) XXXVI (Kháro) XXXVIII (Trisingh)	- 738 - 217 - 217 - 217 - 217 - 651	+ ·744 - ·045 - ·208		- ·079 - ·053 + ·132	+	180         0         0         0         000           59         51         59         418           73         21         3         435           46         46         57         147           180         0         0         0000	4`7662962,0 4`8107520,6 4`6919358,5	58384 · 32 64677 · 32 49196 · 69	11.058 12.249 9.318
29		XXXV (Chauki) XXXVIII (Trisingh) XL (Kiraríwáro)	·438 ·438 ·438	+ •113 - •087 - •012	- ·173 - ·033 + ·206		060 120 + .194	67 48 44 582 51 2 25 652 61 8 49 766	4`9390613,9 4`8632235,3 4`9149085,4	86908 · 32 72983 · 31 82206 · 95	16 · 460 13 · 823 15 · 569
<b>30</b>		XXXVIII (Trisingh) XI. (Kiraríwáro) XLIII (Núrpír)	434 435 435	$+ \cdot 344$ $- \cdot 008$ $- \cdot 032$	- ·324 + ·168 + ·156		+ 014 + 020 + 160 + 124	51 45 14.846 59 49 40.915 68 25 4.239	4 <sup>.</sup> 8656989,4 4 <sup>.</sup> 9074047,9 4 <sup>.</sup> 9390613,9	73400 · 48 80798 · 78 86908 · 32	13.902 15.303 16.460
31		XL (Kiraríwáro) XLIII (Núrpír) XLII (Yáru)	· 237 · 236 · 237	+ ·428 + ·582 + ·650	- ·272 + ·069 + ·203		$+ \cdot 304$ + $\cdot 156$ + $\cdot 651$ + $\cdot 853$	51 3 12 439 45 24 44 435 83 32 3 120	4`7593005,6 4`7210583,2 4`8656989,4	57451°39 52608°80 73400°48	10.881 9.964 13.902
	60	XXXV (Chauki) XL (Kiraríwáro) XXXIX (Thar Muhári)	333 334 334	$   \begin{array}{r} - & \cdot & 164 \\    + & \cdot & 092 \\    + & \cdot & 203   \end{array} $		- ·087 - ·026 + ·113	- 251 + 000 + 000 + 000 + 000	43 45 36.326 77 53 9.752 58 21 13.922	4'7730187,1 4'9233583,3 4'8632235,3	59295°08 83822°06 72983°31	11°230 15°875 13°823
	61	XXXIX (Thar Muhári) XL (Kiraríwáro) XLI (Mári)	· 208 · 209 · 209 · 626	- · 177 - ·007 + ·200		- ·077 - ·022 + ·099	$ \begin{array}{r} + & \cdot 131 \\ - & \cdot 254 \\ - & \cdot 029 \\ + & \cdot 299 \\ + & \cdot 016 \end{array} $	180         0         0         000           46         27         37         138           69         17         33         912           64         14         48         950           180         0         0         00000	4 <sup>.</sup> 6787272,4 4 <sup>.</sup> 7894476,9 4 <sup>.</sup> 7730187,1	47722°95 61581°14 59295°08	9.038 11.663 11.230

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#### PRINCIPAL TRIANGULATION. TRIANGLES.

No. of t	triangle	Number and Name of Station	rical	Corre	ctions to	Observed .	Angle	Corrected Plane		Distance	
Circuit	Non- Circuit	Number and Name or Station	Sphe Exc	Figure	Circuit	Non- Circuit	Total	Angle	Log. feet	Feet	Miles
	62	XLI (Mári) XL (Kiraríwáro) XLII (Yáru)	* * 130 * 129 * 129	- ·029 - ·163 + ·220	*	- °020 - °054 + °074	" - '049 - '217 + '294	0 / 7 77 3 55 811 40 47 31 434 62 8 32 755	4 <sup>.</sup> 7210583,2 4 <sup>.</sup> 5473431,5 4 <sup>.</sup> 6787272,4	52608.80 35264.94 47722.95	9°964 6°679 9°038
82		XLIII (Núrpír) XLII (Yáru) XLV (Longwáli)	· 388 · 214 · 214 · 214 · 214	- °013 - °230 + °255	- 185 - 022 + 207			180 0 0.000 90 57 38.808 39 4 15.324 49 58 5.868	4 <sup>.</sup> 8751873,0 4 <sup>.</sup> 674783 <b>2,2</b> 4 <sup>.</sup> 7593005,6	75021 · 78 47291 · 51 57451 · 39	14.209 8.957 10.881
33		XLII (Yáru) XLV (Longwáli) XLIV (Vijnot)	·642 ·173 ·173 ·174	+ ·176 - ·382 + ·026	- ·423 + ·239 + ·184		$\frac{+ \cdot 012}{- \cdot 247}$ - \cdot 143 + \cdot 210	180 0 0.000 39 23 47 760 36 41 35 204 103 54 37 036	4 <b>·6906722,2</b> 4·6644730,1 4·8751873,0	49053 75 46182 03 75021 78	9°290 8°747 14°209
	63	XLII (Yáru) XLIII (Núrpír) XLIV (Vijnot)	· 205 · 205 · 205 · 205	- °054 + °047 - °148		- ·445 + ·287 + ·158	499 + .334 + .010	78 28 3 266 43 10 50 529 58 21 6 205	4 <sup>.</sup> 8203681,0 4 <sup>.</sup> 6644730,1 4 <sup>.</sup> 7593005,6	66125·36 46182·03 57451·39	12°524 8°747 10°881
34		XLV (Longwáli) XLIV (Vijnot) XLVI (Vín)	· 102 · 101 · 102 · 305	+ °095 - °103 + °063	- •459 + •289 + •170		364 + .186 + .233 + .055	47 39 44 634 46 16 27 765 86 3 47 601	4`5604538,0 4`5506311,3 4`6906722,2	36345°76 35532°94 49053°75	6 · 884 6 · 730 9 · 290
35		- $\cdot 305$ -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -       -<		$ \begin{array}{r} - & 293 \\ - & 176 \\ + & 288 \\ - & 181 \\ \end{array} $	61 37 39 297 71 45 4 254 46 37 16 449	4 <b>·6434435,6</b> 4·676610 <b>3,8</b> 4 <b>·5604538,</b> 0	43999 <sup>.08</sup> 4749 <sup>0.90</sup> 36345.76	8·333 8·994 6·884			
36		XLVI (Vín) XLVIII (Dewari) XLIX (Kot Sabzal)	· 106 • 105 • 106	- °065 + °097 - °345	- ·443 + ·212 + ·231		508 + .309 114	54 51 23 656 53 27 39 794 71 40 56 550	4`5786281,5 4`5709869,6 4`6434435,6	37899°03 37238°06 43999°08	7 · 178 7 · 053 8 · 333
	64	XLV (Longwáli) XLVI (Vín) XLVII (Got Mír Muhammad)	·080 ·080 ·080	- °055 + °033 + °232		- • 542 + • 289 + • 253	$ \begin{array}{r} 313 \\ - & 597 \\ + & 322 \\ + & 485 \\ + & 340 \end{array} $	50 45 52 373 66 44 51 072 62 29 16 555	4`4918011,5 4`5659585,8 4`5506311,3	31031 · 38 36809 · 39 35532 · 94	5 <sup>.877</sup> 6.971 6.730
	65	XLVII (Got Mír Muhammad) XLVI (Vín) XLIX (Kot Sabzal)	·090 ·090 ·090	052 + .122 + .290		- • 590 + • 157 + • 433	642 + .279 + .723	55 49 48 718 80 34 52 919 43 35 18 363	4`5709869,6 4`6473891,2 4`4918011,5	37238.06 44400.62 31031.38	7°053 8°409 5°877
87		XLVIII (Dewari) XLIX (Kot Sabzal) LI (Ghundi)	·090 ·090 ·091	027 119 033	- '310 - '092 + '402		-337 -211 +369 -170	60 29 14 983 55 24 53 249 64 5 51 768	4`5642506,6 4`5401566,3 4`5786281,5	36664°91 34686°19 37899°03	6°944 6°569 7°178
88		XLIX (Kot Sabzal) LI (Ghundi) LXII (Dáowála)	· 101 · 102 · 102	+ '029 - '017 - '057	- ·788 + ·170 + ·618		- .759 + .153 + .561	45 42 26 150 86 5 44 761 48 11 49 089	4`5466178,2 4`6908284,5 4`5642506,6	35206°09 49071°40 36664°91	6·668 9·294 6·944
<b>89</b>		LI (Ghundi) LXII (Dáowála) LIX (Máchka)	305 142 141 141 .141 .424	+ °052 + °035 - °063	- ·354 - ·466 + ·820		$ \begin{array}{r} - & \cdot & 302 \\ - & \cdot & 431 \\ + & \cdot & 757 \\ + & \cdot & 024 \end{array} $	85 58 0.176 58 12 3.928 35 49 55 896 180 0 0.000	4`7780782,6 4`7085244,3 4`5466178,2	59989 · 91 51112 · 18 35206 · 09	11.362 9.680 6.668

NOTE.-Stations LIX (Máchka) and LXII (Dáowála) appertain to the Great Indus Series.

No. of triangle			ne of Station			Observed .	Angle	Corrected Plane		Distance	
Circuit	Non- Circuit	Number and Name or Station	Sphe. Exc	Figure	Circuit	Non- Circuit	Total	Angle .	Log. Feet	Feet	Miles
	66	XLVIII (Dewari) LI (Ghundi) L (Kubba)	" •087 •087 •087	" 	"	" - ·991 + ·042 + ·949	" - 1 · 091 + · 007 + · 905	63 42 35°372 59 11 39°490 57 5 45°138	4`5686746,6 4`5500412,9 4`5401566,3	37040 · 31 35484 · 71 34686 · 19	7.015 6.721 6.569
	67	L (Kubba) LI (Ghundi) LIX (Máchka)	· 261 · 135 · 135 · 135 · 135 · 405	- ·010 + ·013 + ·132		- 1 ° 046 - ° 260 + 1 ° 306	$\frac{-1.056}{-1.438}$ +1.438 +.135	180       0       0.0000         71       50       13.199         64       38       43.248         43       31       3.553         180       0       0.0000	4`7085244,3 4`6867335,4 4`5686746,6	51112°18 48610°88 37040°31	9°680 9°207 7°015

None.-Station LIX (Máchka) appertains to the Great Indus Series.

May, 1885.

W. H. COLE, In charge of Computing Office.



# PRINCIPAL TRIANGULATION. LATITUDES, LONGITUDES AND AZIMUTHS.

	Station A				Side AB		Station B
Circuit No.	Number and Name of Station	Latitude North	Longitude East of Greenwich	Azimuth at A	Log. feet	Azimuth at <b>B</b>	Number and Name of Station
1	LXXV (Roibre)	0 1 1	0 / 4	0 / 4	4:06121620	o , ,	LXXVIII (Sendoher)
•		24 37 20 20	/0 10 45 00	65 7 48:01	4 901 3102,0	245 2 10°54	I (Fulner)
"	37 77	<b>3</b> 3	<b>3</b> 2	172 21 14.80	4 0100000,9	ata an mag	$\nabla$ (Bhédi)
"	" " LXXVIII (Sendahar)	» ar a a:80	" 70 1 22118	226 46 28:00	5.0405520,1	352 20 7 20	(Enlact)
	HAAVIII (Sandonar)	*5 5 5 09	/0 1 44 10	330 40 20 UY	4 0242059.7	150 40 40 09	I (Fullar)
	22 23	"	>>	50 3 20.77	4 0099750,1	230 0 970	II (Changa)
				118 4 30.23	4.0272847.5	207 58 45.76	III (Patatonk)
		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	,,	156 30 7.15	4.0426077.8	336 27 25.28	IV (Narithal)
		,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	223 0 10.15	5.0107656.2	43 14 34.80	$\nabla$ (Bhádi)
	I (Fulrár)	24 52 56.48	70 6 7.00	117 34 34.16	4.8828057.4	207 20 23.31	II (Chánga)
	II (Chánga)	24 58 47.00	69 53 50.47	153 13 30.96	4.8668065,1	333 10 58.06	III (Patatonk)
		•					
	III (Patatonk)	25 9 37 . 71	69 47 49 · 63	224 17 49.01	4.7540043,7	44 20 52.99	IV (Narithal)
	IV (Narithal)	25 16 19.94	69 55 1.47	272 59 56.87	5.0220268,9	93 8 5.34	V (Bhádi)
	37 39	>>	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	169 4 50.68	4.9122944,5	349 3 38.26	VI (Hatodan)
	<b>3</b> 7 <b>3</b> 9	,,	,,	218 28 58.80	4.9354085,1	38 33 9.48	VII (Rupihar)
2	V (Bhádi)	25 15 24 . 18	70 14 5.95	144 57 27.70	4.9507019,2	324 53 28.17	13 33
"	<b>23 23</b>	"	"	190 26 35.31	4.9614543,9	10 27 52.82	VIII (Kanakotri)
	VI (Hatodan)	25 29 34 72	69 52 12.52	280 27 4.59	4.8468162,4	100 32 28.96	VII (Rupihar)
	23 23	"	<b>,</b> ,	204 25 29.73	4.8063335,8	24 27 34.63	IX (Mangtor)
	VII (Rupihar)	25 27 27 90	70 4 46 . 65	255 56 31.94	4'8445842,7	76 I 50 <sup>.</sup> 45	VIII (Kanakotri)
	9 <b>9</b> >>	<b>9</b> 9	"	149 7 6.61	4.9183152,4	329 3 46.11	IX (Mangtor)

NOTE.-Stations LXXV (Rojhrs) and LXXVIII (Sandohar) appertain to the Karáchi Longitudinal Series.

	Station A				Side AB		Station B
Circuit No.	Number and Name of Station	Latitude North	Longitude East of Greenwich	Azimuth at A	Log. Feet	Asimuth at B	Number and Name of Station
3	VII (Rupihar) VIII (Kanakotri) IX (Mangtor) " "	o / * 25 27 27 90 25 30 15 61 25 39 12 08 "	°, 7 70 4 46.65 70 17 7.01 69 57 1.86 "	0 , " 207 12 41.34 147 49 38.24 271 48 41.30 179 0 48.89	4·8870873,0 4·7853817,0 4·8911247,0 4·8530312,6	o / * 27 15 27 54 327 47 4 98 91 54 49 30 359 0 43 05	X (Bhitala) """ XI (Narhar)
<b>4</b> "	""" X (Bhitala)	" 25 38 47 · O2	" 70 11 11 · 99	228 42 7.26 133 7 29.44 174 26 59.94	4'9775321,9 5'0337370,7 4'8158980,4	48 47 46.37 313 1 14.30 354 26 29.86	XII (Thakur) XI (Narhar) XII (Thakur)
5	XI (Narhar) """"""""""""""""""""""""""""""""""""	<sup>2</sup> 5 50 58 · 14 "	69 56 48·43 "	276 45 51.83 169 26 2.71 216 4 50.30	4.8637805,9 4.9350780,3 4.9341767 2	96 51 37.99 349 24 46.87 36 8 53.10	"" XIII (Jeysulmere) XIV (Malar)
"	XIII (Inakur) """"""""""""""""""""""""""""""""""""	25 49 32 28 " 26 4 56 64 " 26 2 25 80	70 IO 2.71 , 69 53 55 22 , 70 6 3.37	104 23 0'17 221 26 33'51 282 52 26'43 221 40 59'63 281 36 47'17	4`9089002,3 4`9194465,6 4`8332637,4 4`8249501,5 4`8944387,3	344 21 21 50 41 30 56 86 102 57 46 33 41 44 34 73 101 42 56 52	" " XV (Badhor) XIV (Malar) XVI (Ramsar) XV (Badhor)
6	""" XV (Badhor) XVI (Ramsar)	" 25 59 48 · 75 26 13 10 · 75	" 70 20 5 37 70 2 3 26	161 26 24.93 217 34 56.74 157 32 53.61 274 54 11.91	4·8369072,0 4·8740247,1 4·9100831,8 4·8309009,3 4·8501258 2	341 24 39'19 37 38 37'35 337 30 23'63 94 59 39'28	XVI (Ramsar) XVII (Sinaba) """ XVIII (Potanawári)
7 `,,		" 26 12 12 · 87 " 26 23 30 · 96	" 70 14 24 45 " 69 55 59 78	197 42 46·55 150 31 59·44 192 27 1·05 260 3 8·22	4·8810634,6 4·9539220,0 4·8489289,4 4·7561449,8	17 44 39 39 330 28 23 73 12 28 15 24 80 7 43 06	XIX (Joganali) "" XX (Kardo) XIX (Joganali)
8	""" XIX (Joganali) "" XX (Kardo)	" 26 25 8·18 " 26 23 35·87	" 70 6 17 · 78 " 70 17 11 · 90	205 19 42.27 278 52 0.05 152 43 49.82 209 48 52.73 155 55 37.11	4.8353292,7 4.7795551,0 4.7675582,6 4.7952602,9 4.8420730,0	25 22 6.06 98 56 50.96 332 41 38.02 29 51 25.20 335 53 17.84	XXI (Sanahu) XX (Kardo) XXI (Sanahu) XXII (Arrabhit) """
9 "	XXII (Janahu) """ XXII (Arrabhit) XXIII (Harnáo)	20 33 43 59 " 26 34 4 4 0 "	70 1 22 28 " 70 11 59 57	168 28 31.61 222 20 11.76 130 19 5.35 184 45 29.64	4 7020542,1 4 7095299,5 4 9735898,1 4 9651481,1 4 8302268,6 4 8820022 8	67 57 37 23 348 27 29 31 42 25 25 46 310 13 17 19 4 45 57 42	" " XXIII (Harnáo) XXIV (Dhanono) XXIII (Harnáo) XXIV (Dhanono)
10 "	""""""""""""""""""""""""""""""""""""""	26 54 44 36	70 I3 I · 48 09 52 27 · 24	151 19 25.99 211 1 20.50 134 40 31.23 185 32 38.07 281 27 12.76	4·8734507.3 4·7822645,1 4·7980561,7 4·9270438,6 4·8353578,7	331 16 27 24 31 3 55 97 314 36 48 69 5 33 18 87 101 32 47 90	" " XXV (Bándri) XXVI (Ráviláhu) " " XXIX (Máringra) XXVI (Ráviláhu)

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## PRINCIPAL TRIANGULATION. LATITUDES, LONGITUDES AND AZIMUTHS.

	Station A	· · · · ·			Side AB		Station <b>B</b>
Circuit No.	Number and Name of Station	Latitude North	Longitude East of Greenwich	Azimuth at A	Log. Feet	Azimuth at B	Number and Name of Station
	XXV (Bándri) """ XXVI (Báviláhu)	° ' " 26 54 44 36 "	69 52 27 · 24 "	° , <b>°</b> 161 7 35.95 231 18 8.37 167 50 16.00	4·8315765,0 4·8450561,7	<ul> <li><i>v</i></li> <li><i>v</i></li></ul>	XXVII (Máhu) XXVIII (Girája)
	XXVII (Máhu)	" 27 5 20°19	, , , , , , , , , , , , , , , , , , ,	232 49 29 40 284 55 5 81	4 <sup>,005,022,2</sup> 4 <sup>,8212126,4</sup> 4 <sup>,8990445,9</sup>	52 53 53.72 105 I 31.16	" " XXIX (Máringra) XXVIII (Girája)
11	" " XXVIII (Girája) " " XXIX (Máringra)	" 27 I 57.40 " 26 59 5.37	,, 70 2 31 40 ,, 70 14 31 76	233 44 59 93 284 53 2.80 173 18.52 94 228 41 23 13 175 10 6 29	4.9272107,8 4.8288055,6 4.8506972,9 4.8965140,6 4.8425614,0	53 50 44 <sup>.</sup> 81 104 58 29 <sup>.</sup> 94 353 18 11 <sup>.</sup> 24 48 46 21 <sup>.</sup> 76 355 9 36 <sup>.</sup> 74	XXX (Singra) XXIX (Máringra) XXX (Singra) XXXI (Asu) """
12 "	XXX (Singra) """ XXXI (Asu) ""	27 13 34 · 87 " 27 10 32 · 14 "	70 0 59 95 " 70 13 26 85 "	285 15 19:59 167 55 30:06 217 30 41:54 158 31 21:04 201 37 33:14	4·8445434,0 4·7562481,6 4·8144244,5 4·8774718,9 4·9775848,7	105 21 1.01 347 54 29.32 37 34 3.60 338 29 0.68 21 40 31.28	" " XXXII (Bitri) XXXIII (Parethal) " " XXXIV (Kolu)
13 "	XXXII (Bitri) """" XXXIII (Parethal) """	27 22 47 · 33 " 27 22 7 · 08 "	69 58 47 · 55 ,, 70 8 20 · 54 ,,	274 27 47 37 167 4 47 73 220 13 43 98 253 50 2 55 179 39 47 19	4.7144157,0 4.8546230,9 4.8990669,7 4.8141024,0 4.8098816,6	94 32 10.83 347 3 25.70 40 18 6.28 73 55 22.21 359 39 45.24	XXXIII (Parethal) XXXV (Chauki) XXXVI (Kháro) XXXIV (Kolu) XXXVI (Kháro)
	XXXIV (Kolu) """ XXXV (Chauki) """""	27 25 6·31 ,, 27 34 17·96 ,, ,,	70 19 55 29 " 69 55 49 75 "	126 28 9.05 165 22 9.38 277 47 45.00 233 15 50.43 121 41 28.75	4 <sup>.8</sup> 933571,5 4 <sup>.8</sup> 031682,7 4 <sup>.8</sup> 313570,1 4 <sup>.</sup> 9149085,4 4 <sup>.</sup> 9233583,3	306 22 46.50 345 20 46.98 97 53 30.41 53 21 30.50 301 35 20.72	"" XXXVII (Morgich) XXXVI (Kháro) XXXVIII (Trisingh) XXXIX (Thar Muhári)
14 " 15	" " XXXVI (Kháro) " " XXXVII (Morgich) XXXVIII (Trisingh)	" 27 32 46·30 " 27 35 15·29 27 42 24·35	,, 70 8 16 32 ,, 70 16 56 85 70 8 2 81	165 27 5.41 252 9 32.65 178 48 29.00 132 5 33.18 104 23 56.59	4.8632235,3 4.6919358,5 4.7662962,0 4.8107520,6 4.9390613,9	345 25 30.63 72 13 33.54 358 48 22.74 312 1 25.37 284 16 40.43	XL (Kiraríwáro) XXXVII (Morgich) XXXVIII (Trisingh) """ XL (Kiraríwáro)
"	,, , , , , , , , , , , , , , , , , , ,	" 27 41 33 40 " 27 45 57 48 "	" 69 42 36 · 23 " 69 52 25 · 64 "	156 9 11 <sup>.87</sup> 243 14 6 <sup>.47</sup> 196 46 29 <sup>.12</sup> 132 36 14 <sup>.84</sup> 173 23 46 <sup>.40</sup>	4`9074047,9 4`7730187,1 4`7894476,9 4`6787272,4 4`7210583,2	336 6 21.98 63 18 40.72 16 48 1.40 312 33 12.24 353 23 14.91	XLIII (Núrpír) XL (Kiraríwáro) XLI (Mári) "" XLII (Yáru)
	", " XLI (Mári) XLII (Yáru) ", ", ", ",	" 27 51 17 · 24 27 54 34 · 99 "	" 69 45 54 · 26 69 51 18 · 20 "	224 26 59.08 235 29 16.30 269 51 11.54 191 23 8.07 230 46 56.01	4·8656989,4 4·5473431,5 4·7593005,6 4·6644730,1 4·8751873,0	44 31 26.66 55 31 47.79 89 56 11.33 11 23 55.80 50 52 0.31	XLIII (Núrpír) XLII (Yáru) XLIII (Núrpír) XLIV (Vijnot) XLV (Longwáli)

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	Station A				Side AB		Station B
Circuit No.	Number and Name of Station	Latitude North	Longitude East of Greenwich	Azimuth at A	Log. Feet	Azimuth at B	Number and Name of Station
16 " 17 "	XLIII (Núrpír) " XLIV (Vijnot) " " " " XLV (Longwáli) " XLVI (Vín)	<ul> <li>, , , , , , , , , , , , , , , , , , ,</li></ul>	0 / * 70 I 58.65 69 52 59.95 " 70 2 6.92 69 57 27.40	0       ,       *         133       7       2:06         180       53       50:35         267       29       18:59         221       12       50:72         159       35       11:30         135       13       20:42         185       59       13:88         248       26       17:72	4.8203681,0 4.6747832,2 4.6906722,2 4.5604538,0 4.6766103,8 4.5506311,3 4.5559585,8 4.4918011,5	<ul> <li>313 2 49'39</li> <li>53 54'23</li> <li>87 33 35'69</li> <li>41 14 56'58</li> <li>339 33 44'14</li> <li>315 11 8'88</li> <li>5 59 34'07</li> <li>68 28 50'71</li> </ul>	XLIV (Vijnot) XLV (Longwáli) "" XLVI (Vín) XLVIII (Dewari) XLVI (Vín) XLVII (Got Mír Muhammad)
" "	)) )) ))	9) 93	>> *>	113 0 0.95 167 51 <b>24</b> .71	4 <sup>.</sup> 0434435,0 4 <sup>.</sup> 5709869,6	292 50 27.57 347 50 43.39	XLVIII (Dewari) XLIX (Kot Sabzal)
19	XLVII (Got Mír Muhammad) XLVIII (Dewari) """ XLIX (Kot Sabzal)	28 8 26 79 28 9 24 00 " 28 12 34 44	70 2 49 <sup>.8</sup> 1 69 49 54 <sup>.8</sup> 7 " 69 55 59 <sup>.8</sup> 3	124 18 39 52 239 28 47 68 115 16 57 14 178 59 32 60 114 56 33 38	4.6473891,2 4.5786281,5 4.5500412,9 4.5401566,3 4.5642506,6	304 15 24 94 59 31 40 05 295 14 7.79 358 59 29 38 294 53 37 52	""" L (Kubba) LI (Ghundi) ""
"	" " L (Kubba) " " LI (Ghundi) " " LIX (Máchka) LXII (Dáowála)	" 28 11 53 93 " 28 15 7 41 " 28 19 41 57 28 20 12 87	" 69 43 56 23 " 69 49 48 05 " 69 41 47 41 69 52 57 86	160 38 59'64 238 8 22'57 166 18 9'23 122 49 52'34 208 47 52'66 266 56 8'51	4.6908284,5 4.5686746,6 4.6867335,4 4.7085244,3 4.5466178,2 4.7780782,6	340 37 33 44 58 11 8 96 346 17 8 23 302 46 4 55 28 49 22 63 87 1 26 70	LXII (Dáowála) LI (Ghundi) LIX (Máchka) """ LXII (Dáowála) """

NOTE.-Stations LIX (Máchka) and LXII (Dáowála) appertain to the Great Indus Series.

June, 1885.

W. H. COLE, In charge of Computing Office.



#### PRINCIPAL TRIANGULATION. HEIGHTS ABOVE MEAN SEA LEVEL.

The following table gives, first, the usual data of the observed vertical angles and the heights of the signal and instrument, &c., in pairs of horizontal lines, the first line of which gives the data for the 1st or the fixed station, and the second line the data for the 2nd or the deduced station. This is followed by the arc contained between the two stations, and then by the terrestrial refraction, and the height of the 2nd station above or below the 1st, as computed from the vertical angles in the usual manner. This difference of height applied to the given height above mean sea level of the fixed station, gives that of the deduced station. Usually there are two or three independent values of the height of the deduced station; the details are so arranged as to show these consecutively and their mean in the columns of "Trigonometrical Results." The mean results thus obtained are however liable to receive corrections for the errors generated in the trigonometrical operations, which are shown up by the spirit leveling operations, whenever a junction between the two has been effected. The spirit leveled determinations, when available, are always accepted as final, and the trigonometrical heights of stations, lying between other stations fixed by the leveling operations, are adjusted—usually by simple proportion—to accord with the latter.

The heights of Eastern Sind Meridional Series have been adjusted between the values of Rojhra H.S. and Sandohar H.S. of the Karáchi Longitudinal Series, and those of Máchka T.S. and Dáowála T.S. of the Great Indus Series as finally determined in connection with the general reduction of the North-West Quadrilateral. The fixed heights are as follows :--

LXXV ( LXXVIII (	(Kojhra) (Sandohar	···· 51 ···· 40	$\binom{8}{8}$ feet above	e Mean Sea	Level at	Karáchi from	<b>Karáchi Longit</b> udi	inal Series.
LIX ( LXII (	Máchka) Dáowála)	· 27 28	$\begin{bmatrix} 3\\2 \end{bmatrix}$	,,,	"	from	Great Indus Serie	8.

The trigonometrical heights always refer to the upper mark-stone, or to the upper surface of the pillar on which the theodolite stood. When the pillar of the station is perforated, the height given in the last column, is that between the upper surface of pillar and ground level mark-stone in floor of passage; otherwise it is the approximate height of the structure above the ground at the base of the station.

Astronomical Date		Date			ations	Height	in feet	2	Terre Refr	estrial action	Station	Heigh Statio	t in feet on above Sea Leve	of 2nd Mean l	r Tower
187	3	Mean of Times	Number and Name of Station	Observed Vertical Angle	of observ	لعمر	ument	ntained A	sconds	nals of ned Aro	Height of ion — 1st in feet	Trigono Res	metrical ults	77. 1	f Pillar o
	-	of obser- vation			Number	Sig	Instr	වී	In se	Decir Contai	2nd Stati	By each deduc- tion	Mean	Final Result	Height o
		h. m.		0 1 11				"							feet
No <b>v</b> . Dec.	26 4, 5	2 24 2 25	LXXV (Rojhra) I (Fulrár)	Do 7 10.9 Do 2 42.8	12 16	2°5 2°7	5°3 5°3	638	32	·050	- 41.9	476 · 1	475.4	475	<b>0</b> +
)) ))	1 5	2 16 2 20	LXXVIII (Sandohar) I (Fulrár)	Do 130.9 Do 823.0	12 12	2·6 2·8	5·3 5·3	659	41	·062	+ 66.7	474.7	475 4	4/5	
Nov. Dec.	80 7	2 18 2 22	LXXVIII (Sandohar) II (Chánga)	Do 742.9 E o 020.1	12	2·6 2·7	5.3	484	33	·068	- 57.2	350.8			
													351.3	351	0†

NOTE.-Stations LXXV (Rojhrs) and LXXVIII (Sandohar) appertain to the Karáchi Longitudinal Series.

+ The pillar is sunk having its upper surface flush with the ground.

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Astro	nomical	Date			tions	Height	in feet		Terre Refre	strial ction	ation	Heigh Static	t in feet on above	of 2nd Mean	[ower
187	76	Mean of Times	Number and Name of Station	Observed Vertical Angle	of observa	lan	ument	ntained Arc	sconds	nals of ned Arc	Height of ion — 1st St in feet	f Trigono Res	Sea Leve metrical ulte	L 	f Pillar or '
		of obser- vation			Number	Sig	Instr	Ğ	In 96	Decir Contai	] 2nd Stat	By each deduc- tion	Mean	Final Result	Height o
															foot
Dec. "	<b>4</b> 7	h. m. 2 45 2 43	I (Fulrár) II (Chánga)	Do 11 15.4 Do 0 8.4	12 12	2·6 2·6	5°3 5°3	756	43	·057	-123.8	351.6			
Nov. Dec.	<b>3</b> 0 10	2 34 2 34	LXXVIII (Sandohar) III (Patatonk)	Do 945.6 Do 237.4	I 2 I 2	2·8 2·7	5·3 5·3	836	53	·063	- 87.9	320.1	22014		
29 23	7 10	2 31 2 31	II (Chánga) III (Patatonk)	Do 654.0 Do 44.0	I 2 I 2	2·8 2·6	5°3 5°3	727	42	·058	- 30.4	320.8	320 4	320	or
Nov. Dec.	80 12	2 54 2 35	LXXVIII (Sandoh <b>ar)</b> IV (Narithal)	Do 944.2 Do 313.9	I 2 I 2	2.6 2.7	5°3 5°3	866	50	·058	— 82·8	325.2			
" " 1	10 12, 18	2 42 2 43	III (Patatonk) IV (Narithal)	Do 358.7 Do 443.4	12 16	2.6 2.6	5·3 5·3	561	30	·053	+ 6.3	326.6	326.4	326	ot
>> >>	21 13	2 I 2 2 I I	V (Bhádi) IV (Narithal)	Do 12 11.4 Do 3 15.5	I 2 I 2	2·6 2·6	5°3 5°3	1040	62	·060	—136·6	327.3			
Nov. Dec.	22 20	2 35 2 35	LXXV (Rojhra) V (Bhádi)	Do 923.9 Do 617.5	I 2 I 2	2·6 2·7	5°3 5°3	1084	76	·070	- 49.2	468.5			
Nov. Dec.	30 20	3 13 3 13	LXXVIII (Sandohar) V (Bhádi)	Do 551.6 Do 916.1	I 2 I 2	2·6 3·3	5°3 5°3	1013	58	<sup>.</sup> 057	+ 51.3	459°2	463.4	463	ot
27 77	13 21	2 II 2 I2	IV (Narithal) V (Bhádi)	Do 315.5 Do 1211.4	I 2 I 2	2·6 2·6	5°3 5°3	1040	62	•0 <b>6</b> 0	+136.6	462.5			
" " 2	13 26, 27	2 52 2 52	IV (Narithal) VII (Rupihar)	Do 636.9	I 2 I 2	2·6 2·6	5°3 5°3	851	50	·059	+ 5.6	332.0	220.8	220	
"2 "2	20, 21 26, 27	2 33 2 36	V (Bhádi) VII (Rupih <b>ar)</b>	Do1143.1 Do124.7	16 12	2·7 2·7	5°3 5°3	882	53	·060	-133.8	329.6	330 0	330	
39 32	12 30	3 7 2 4 2	IV (Narithal) VI (Hatodan)	Do 711.9 Do 50.6	12 12	2·6 2·6	5°3 5°3	807	45	·056	- 26.0	300.4	200.7	200	
,, 2 ,,	26, 27 30	2 22 2 23	VII (Rupihar) VI (Hatodan)	Do 643.4 Do 335.5	I 2 I 2	2·6 2·7	5°3 5°3	694	46	•06 <b>6</b>	- 31.9	298.9	*yy /	299	
>> >>	20 24	2 55 2 54	V (Bhádi) VIII (Kanakotri)	Do 7 1.4 Do 619.8	I 2 I 2	2·6 2·7	5°3 5°3	<u>9</u> 04	57	·063	- 9.1	454.3	454.7	454	
»	26, 27 24	2 53 2 53	VII (Rupihar) VIII (Kanakotri)	E 0 0 56 5 D 0 11 15 8	12 12	2·6 2·7	5°3 5°3	691	44	·064	+124.2	455.0	+J <b>+ /</b>	434	
Dec. Jan.	30, 31 4, 5	2 45 2 45	VI (Hatodan) IX (Mangtor)	Do 510.3 Do 421.4	I 2 I 2	2·7 2·6	5°3 5°3	633	40	·063	- 7.7	292.0			
Dec. Jan.	26, 27 8, 4	2 17 2 17	VII (Rupihar) IX (Mangtor)	Do 749.4 Do 423.7	12 12	2·7 2·7	5°3 5°3	818	49	•060	- 41.3	289.5	290.8	290	ot

NOTE.—Stations LXXV (Rojhra) and LXXVIII (Sandohar) appertain to the Karáchi Longitudinal Series. † The pillar is sunk having its upper surface flush with the ground.

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## PRINCIPAL TRIANGULATION. HEIGHTS ABOVE MEAN SEA LEVEL.

Astronomical	Date			tions	Height	in feet		Terre Refre	strial	<b>tation</b>	Heigh Statio	t in feet on above	of 2nd Mean	Lower
1877	Mean of Times of obser- vation	Number and Name of Station	Observed Vertical Angle	Number of observa	Bignal	Instrument	Contained Arc	In seconds	Decimals of Contained Arc	Height of 2nd Station - 1st F in feet	Trigono Ree By each deduc- tion	Mean	l Final Result	Height of Pillar or '
														feet
Jan. 7,8,9 ,, 5	h.m. 236 236	X (Bhitala) IX (Mangtor)	Do 851.5 Do 231.7	I 2 I 2	2·6 2·7	5°3 5°3	769	50	·065	- 71.5	291.0			
1876-77 Dec. 26, 27 Jan. 8, 9	2 46 2 47	VII (Rupih <b>ar)</b> X (Bhitala)	Do 421.3 Do 711.3	12 16	2·6 2·8	5·3 5·3	762	42	·055	+ 31.9	362.7			
Dec. 24 Jan. 7.9	<b>2</b> 40 <b>2</b> 40	VIII (Kanakotri) X (Bhitala)	Do 946.7 Eo 037.2	I 2 I 2	2.6	5.3	602	35	·058	- 92.3	362.4	362.5	362	ot
1877 Jan. 5 7.8.9	2 36 2 36	IX (Mangtor) X (Bhitala)	Do 231.7	12	2.7	5.3	769	50	·065	+ 71.5	362.3			
,, 1, 3, 3 ,, 4, 5 ., 17, 18	2 36 2 36	IX (Mangtor) XI (Narhar)	Do 618.3	12	2.7	5.3	704	34	·048	- 18.3	272.5			
" 8, 9 " 17, 18	2 3I 2 35	X (Bhitala) XI (Narhar)	Do 10 53.8	16 12	2.7	5.3	1068	54	·051	- 88.7	273.8	272.8	272	ot
" 12, 13 " 17	2 44 2 41	XII (Thakur) XI (Narhar)	Do 9 0.2 Do 1 23.1	12	2·7 2·8	5.3	722	42	·058	- 75.8	272 . 1			
,, <b>4</b> , 5 ,, 12, 18	3 I 3 2	IX (Mangtor) XII (Thakur)	Do 452.2 Do 9 1.9	16 16	2·7 2·6	5.3	938	58	·062	+ 57.4	348.2			
,, 8,9 ,, <b>12</b> ,13	2 33 2 33	X (Bhitala) XII (Thakur)	Do 538.6 Do 45.8	12 12	2·7 2·6	5.3	647	41	·063	- 14.8	347.7	348.3	348	ot
" 17 " <b>12,</b> 18	2 41 2 44	XI (Narhar) XII (Thakur)	Do 152.1 Do 9 0.2	I 2 I 2	2·8 2·7	5.3	722	42	·058	+ 75.8	348.9			
" 17, 18 " 26, 28	2 55 2 55	XI (Narhar) XIV (Malar)	Do 434.6 Do 9 0.3	I 2 I 2	2.6 2.6	5°3 5°3	849	25	·029	+ 55.4	328.2			
" 12, 18 " 26, 27	2 44 2 44	XII (Thakur) XIV (Malar)	Do 651.9 Do 515.1	I 2 I 2	2·6 2·6	5°3 5°3	801	44	·055	- 19.0	329.3	328.8	328	o <del>t</del>
"17,18,19 "22	2 39 2 39	XI (Narhar) XIII (Jeysulmere)	Do 4 57.1 Do 8 11.3	16 16	2·8 2·6	5°3 5°3	851	38	·045	+ 40.4	313.3			
,, 26, 27, 28 ,, 22	2 25 2 24	XIV (Malar) XIII (Jeysulmere)	Do 550.4 Do 419.9	16 12	2·7 2·6	5°3 5°3	673	40	·059	- 15.1	313.7	313.4	313	OT
,, 13,15 Feb. 4	2 23 2 37	XII (Thakur) XV (Badhor)	Do 037.1 Do 12 4.5	16 12	2.6 2.6	5°3 5°3	821	37	·045	+138.4	486.7	48	18-	~*
Jan. 26, 27, 30 Feb. 8	2 40 2 40	XIV (Malar) XV (Badhor)	E 0 1 1.5 D 0 12 36.2	16 16	2·6 2·8	5·3 5·3	<b>7</b> 75	48	·062	+155.6	484.4	. + · · · ·	402	
Jan. 22 Feb. 10, 11	2 34 2 34	XIII (Jeysulmere) XVI (Ramsar)	Do 429.5 Do 541.1	I 2 I 2	2·7 2·6	5°3 5°3	660	33	·050	+ 11.2	324.9			-

 $\ensuremath{\uparrow}$  The pillar is sunk having its upper surface flush with the ground.

Astronomical	Date			tions	Height	in feet		Terre Refre	etrial ction	ation	Height Static	t in feet o on above	of 2nd Mean	
1877	Mean of Times	Number and Name of Station	Observed Vertical Angle	эг of observa	ignal	trument	ontained Arc	seconds	imals of ained Arc	Height of ation – 1st St in feet	f Trigono Res	Sea Level metrical ults	Final	of Pillar or '
	vation			Numbe	20	Inst	Ö	In	Dec Conte	2nd Ste	By each deduc- tion	Mean	Result	Height
	1		9 1 11				4							foct
Jan. 25, 26, 27 Feb. 10, 11	<i>n. m.</i> 2 32 2 32	XIV (Malar) XVI (Ramsar)	Do 531.1 Do 53.3	12 12	2·7 2·8	5°3 5°3	679	30	·044	- 4.2	324.3	324.5	324	ot
" 7, 8 " 10, 11	2 42 2 41	XVII (Sinaba) XVI (Ramsar)	Do 924.4 Do 048.2	I 2 I 2	2·8 2·6	5°3 5°3	669	37	<sup>.</sup> 055	- 84.9	324 . 2			
Jan. 25, 26, 27, 28 Feb. 7, 8	2 56 2 49	XIV (Malar) XVII (Sinaba)	Do 212.2 Do 926.8	20 16	2·6 2·8	5°3 5'3	739	28	·0 <b>3</b> 8	+ 78.9	407.7			
" 8 " 7,8	2 51 2 48	XV (Badhor) XVII (Sinaba)	Do 918.8 Do 258.2	I 2 I 2	2·6	5.3	80 <b>3</b>	40	·050	- 75.0	410.2	409 · 2	408	ot
" 10, 11 " 7, 8	2 41	XVI (Ramsar) XVII (Sinaba)	$D \circ \circ 48.2$ $D \circ \circ 24.4$	12	2·6 2·8	5.3	669	37	·055	+ 84.9	409.5			
" 10, 11 " 17, 18	2 45	XVI (Ramsar) XIX (Joganali)	Do 2 53.6	16	5.9	5.3	751	2 I	·028	+ 66.3	390.8			
" 7,8 " 7,18	2 39	XVII (Sinaba) XIX (Joganali)	Do 734.7	16	2.7	5.3	888	40	<sup>.</sup> 045	- 19.7	389.5	390.2	389	ot
,, 10, 11 ., 14	- 39 2 59 2 58	XVI (Ramsar) XVIII (Potanawári)	$D \circ 5 38.6$ $D \circ 5 8.8$	12	2.7	5.3	699	33	<sup>.</sup> 047	- 5.0	319.2			
,, 17 ,, 14	2 27	XIX (Joganali) XVIII (Potanawári)	Do 8 42.7	12	2.7	5.3	563	27	·048	- 71.6	318.6	319.0	318	ot
,, 7,8 , 22	2 45	XVII (Sinaba) XX (Kardo)	Do 1 34.5	12	2.6	5.3	698	36	·052	+ 77.7	486 · 9			
,, 18 ,, 18	2 48 2 48	XIX (Joganali) XX (Kando)	$E \circ \circ 59^{\circ}6$	12	2.6	5.3	595	36	.061	+ 96.4	486 • 6	486·8	486	ot
,, 14 ,, 14	2 49 2 49	XVIII (Potanawári)	Do 4 28.4	12 16	2.6	53	676	19	·028	+ 19.4	338.4			
" 18 " 18	2 50 2 43	XIX (Joganali)	Do 724.7	10 12	2.6	5°3 5°3	578	28	·050	- 49.4	340.8	339.5	338	ot
" 27 " 24	<sup>2</sup> 43 2 58	XXII (Sanahu) XXII (Arrabhit)	Do 130.4 Do 931.0	I 2 I 2	2·7 2·8	5°3 5°3	572	21	.037	- 83.6	330.3			
,, 27 ,, 17	2 59 3 14	XXI (Sanahu) XIX (Joganali)	E 0 0 23.9 D 0 3 10.2	I 2 I 2	2.0 3.0	5°3 5°3	6							
" 24	3 15	XXII (Arrabhit)	Do 644.4	I 2	2.7	5.3	017	ZI	° <b>0</b> 34	+ 32-5	422.7			
,, 22 ,, 24	2 18 2 18	AA (Kardo) XXII (Arrabhit)	DO 212.9	I 2 I 2	2.0 2.0	5°3 5°3	68 <del>7</del>	30	·044	- 63.8	423.0	423.0	422	ot
,, 27 ,, 24	2 59 2 58	XXI (Sanahu) XXII (Arrabhit)	E 0 0 23.9 D 0 9 31.0	I 2 I 2	2.6 2.8	5°3 5°3	572	21	<sup>.</sup> 0 <b>3</b> 7	+ 83.6	423.2			

**†** The pillar is sunk having its upper surface flush with the ground.

#### PRINCIPAL TRIANGULATION. HEIGHTS ABOVE MEAN SEA LEVEL.

Astronomica	l Date			tions	Height	t in feet		Terre Refr	strial action	tation	Heigh Stati	it in feet on above	of 2nd Mean	Tower
1877	Mean of Times of obser- vation	Number and Name of Station	Observed Vertical Angle	Number of observe	Signal	Instrument	Contained Arr	In seconds	Decimals of Contained Arc	Height of 2nd Station – 1st S in feet	Trigono Rea By each deduc- tion	Sea Level	Final Result	Height of Pillar or
	!	/	<u> </u> !	'		¦'	   .				<u> </u>			feet
Feb. 27 Mar. 4	h. m. 2 13 2 39	XXI (Sanahu) XXIII (Harnáo)	°'' Do 4 1.4 Do 5 59.6	I 2 I 2	2·6 2·7	5°3 5°3	623	20	·032	+ 18.2	357.7			J
Feb. 25 Mar. 3, 4	2 40 2 45	XXII (Arrabhit) XXIII (Harnáo)	Do 941.3 Do 447.0	12 16	5 <sup>•</sup> 4 5 <sup>•</sup> 4	5°3 5°3	912	22	·024	- 65.9	357.1	356.9	356	ot
" 15 " 3	3 2 3 1	XXIV (Dhanono) XXIII (Harnáo)	Do 926.5 Do 210.6	12 12	2·6 2·6	5·3 5·3	754	35	·046	) — 80°7	355.8			
" 1 " 15	2 23	XXI (Sanahu) XXIV (Dhanono)	Do 4 6.2 Do 11 12.0	12	2·6 5·9	5.3	930	8	· 000 g	) + 98.8	438.3			
Feb. 24 Mar. 15	2 41 2 45	XXII (Arrabhit) XXIV (Dhanono)	Do 5 0.0 Do 6 11.2	I 2 I 2	2·6 2·6	5.3	668	6	و∞٠	) + 11.7	434.7	437 .0	436	ot
" 3 " 15	3 I 3 2	XXIII (Harnáo) XXIV (Dhanono)	Do 2 10.6 Do 9 26.5	12 12	2·6 2·6	5·3 5·3	754	35	·046	5 + 80·7	438.1			
,, 3 ,, 10	2 48 2 48	XXIII (Harnáo) XXVI (Ráviláhu)	Do 3 9.8 Do 6 25.5	I 2 I 2	2.7	5°3 5°3	598	20	.033	3 + 28.6	385.5			
,, 15 ,, 10	2 35 2 32	XXIV (Dhanono) XXVI (Ráviláhu)	Do 748.5 Do 29.4	I 2 I 2	2.7	5·3 5·3	621	21	·034	ı — 51.7	385.3	385.4	384	ot
" 3 " 7	3 15 3 15	XXIII (Harnáo) XXV (Bándri)	Do 717.5 Do 416.6	I 2 I 2	2.6 2.6	5·3 5·3	738	30	·041	- 32·8	324 · I			
(1) (2)	3 I 3 I	XXVI (Ráviláhu) XXV (Bándri)	Do 815.6 Do 26.0	8 12	2·6 2·6	5°3 5°3	676	35	·052	- 61.3	324.1	324.1	323	ot
1877 Mar. 15 1890 Feb. 12, 13	2 40 2 56	XXIV (Dhanono) XXIX (Máringra)	Do 534.3 Do 748.6	16 16	2.6	5·3 5·3	835	24	·029	) + 27.6	464.6			
(3) 1890 Feb. 12	258 30	XXVI (Ráviláhu) XXIX (Máringra)	Do 052.6 Do 919.3	24 12	2·0 2·6	5·3 5·3	655	31	·047	+ 81.7	467.1	465.9	405	OT
Jan. 30, 31 Feb. 8	2 53 2 54	XXV (Bándri) XXVIII (Girája)	Do 3 8·1 Do 739·1	I 2 I 2	2·7 2·6	5·3 5·3	692	30	·043	; + 45 <sup>.</sup> 9	370.0			
Jan. 27,28 Feb. 8	2 30 2 30	XXVI (Ráviláhu) XXVIII (Girája)	Do 527.6 Do 335.6	12 12	2·7 2·6	5·3 5·3	580	28	·048	- 16.0	369.4	369.7	368	ot
" 12,13 " 8	3 I 3 O	XXIX (Máringra) XXVIII (Girája)	D o 10 6.5 D o 016.9	I 2 I 2	2·6 2·7	5°3 5°3	666	29	·044	, - 96·3	369.6			
Jan. 30, 31 Feb. 2, 4	2 38 2 38	XXV (Bándri) XXVII (Máhu)	Do 5 8.7 Do 5 18.2	12 12	2·5 2·6	5°3 5°3	670	30	·045	; + 1·7	325.8	-		
" 8 " 2	2 49 2 48	XXVIII (Girája) XXVII (Máhu)	Do 8 0.2 Do 4 3.9	I 2 I 2	2·6 2·7	5·3 5·3	783	37	·047	/ — 45°3	324.4	325 1	324	ОТ
						'		'				'		

† The pillar is sunk having its upper surface flush with the ground. (1). The mean of observations taken on 10th March 1877 and 27th January 1880. (2). The mean of observations taken on 7th March 1877 and 30th, 31st January 1880. (3). The mean of observations taken on 11th March 1877 and 27th, 28th January 1880.

Ast	ronomical	Date			tions	Height	; in feet		Terre Refr	strial action	tation	Heigh Statie	it in feet on above	of 2nd Mean	lower
	890	Mean of Times	Number and Name of Station	Observed Vertical Angle	of observa	nal	ument	itained Arc	conde	ned Arc	Ieight of ion – 1st S <sup>'</sup> in feet	Trigono Rea	Sea Leve 		Pillar or
		of obser- vation			Number	Sig	Instr	Cor	In se	Decir Contai	E 2nd Stati	By each deduc- tion	Mean	Final Result	Height of
		h m.		0 1 "											feet
Feb. "	2 24	2 5 2 4	XXVII (Máhu) XXX (Singra)	Do 346.6 Do 94.0	I 2 I 2	2·6 2·6	5·3 5·3	835	40	·048	+ 65.1	390.2			
"	8 24	2 55 2 55	XXVIII (Girája) XXX (Singra)	Do 426.8	12	2·6 2·6	5.3	<b>7</b> 00	28	·040	+ 21.9	391.6	390.9	389	ot
,,	18, 19 94	2 31	XXXI (Asu)	Do 937.0	12	2.6	5.3	690	41	·059	- 89.7	390.9			
»» »»	8	2 31 2 59	XXX (Singra) XXVIII (Girája)	Do 0473 Do 1141	I 2 I 2	2·7 2·7	5.3	778	22	.042	+ 110.4	480.1			
"	18 13	3 O 2 30	XXXI (Asu) XXIX (Márin <i>o</i> ra)	$D \circ 10 52.4$ $D \circ 40.4$	12	2.6	5.3		33	042		400			
"	19, 20	2 45	XXXI (Asu)	Do 611.0	12	2.7	5.3	687	25	·036	+ 15.3	481.2	480.6	479	ot
") ")	24 18, 19	2 31 2 31	XXX (Singra) XXXI (Asu)	D o o 47·3 D o 9 37·0	12 12	2·7 2·6	5°3 5°3	690	41	·059	+ 89.7	480.6			
,, Mar.	24 1	2 33 2 34	XXX (Singra) XXXIII (Parethal)	Do 221.8 Do 84.2	12	2.7	5·3	644	18	·028	+ 54.0	444.9			
Feb. Mar.	18, 20 1, 2	2 II 2 I3	XXXI (Asu) XXXIII (Parethal)	D o 7 31 · 7 D o 4 3 · 4	12	2.7	5°3 5°3	745	32	·043	- 38.1	442.5	443'7	442	ot
Feb. "	24 27	2 34 2 34	XXX (Sing <b>ra)</b> XXXII (Bitri)	Do 550.2 Do 37.0	12 12	2·6 2·6	5·3 5·3	563	23	·041	- 22.6	368.3	-68.17	-64	
Mar. Feb.	1 27	159 158	XXXIII (Parethal) XXXII (Bitri)	Do 9 0.3 Eo 0 52.8	I 2 I 2	2.6 2.5	5°3 5°3	512	23	<sup>.</sup> 045	- 74.6	369 . 1	300 7	307	от
,, 18 Mar.	, 20, 21 4	2 30 2 31	XXXI (Asu) XXXIV (Kolu)	Do 844.0 Do 717.0	16 12	2·7 2·8	5°3 5°3	938	-7	.007	- 19.9	460.7			
" "	1 4	2 43 2 44	XXXIII (Parethal) XXXIV (Kolu)	Do 4 8·4 Do 6 0·3	12 12	2·7 2·6	5°3 5°3	644	27	·042	+ 17.6	461.3	461.0	459	ot
Feb. Mar.	27 9, 10	I 4I I 4I	XXXII (Bitri) XXXVI (Kháro)	Do 3 1.8 Do 9 22.6	12 12	2·7 2·6	5°3 5°3	783	27	·034	+ 73'1	441.8			
23 23	1 8,9	2 IO 2 I2	XXXIII (Parethal) XXXVI (Kháro)	Do 515.2 Do 452.2	I 2 I 2	2·7 2·5	5°3 5°3	637	24	·0 <b>3</b> 8	- 3.7	440'0	440.0	438	ot
>> >>	4 9, 10	157 158	XXXIV (Kolu) XXXVI (Kháro)	Do 7 4.0 Do 5 4.0	I 2 I 2	2·7 2·7	5°3 5°3	773	30	· <b>•3</b> 9	- 22.8	438.2			
>> >>	<b>4</b> 6	2 51 2 51	XXXIV (Kolu) XXXVII (Morgich)	Do 429.3 Do 553.7	I 2 I 2	2·7 2·8	5·3 5·3	628	10	·016	+ 13.1	474 • 1			
»» »	9, 10 6	I 54 I 53	XXXVI (Kháro) XXXVII (Morgich)	Do 134.9 Do 637.2	I 2 I 2	2.7	5°3	486	7	·014	+ 36.1	476 • 1	475 ' 1	473	ot
		ļ													

† The pillar is sunk having its upper surface flush with the ground.

## PRINCIPAL TRIANGULATION. HEIGHTS ABOVE MEAN SEA LEVEL.

Astronomical	Date			tions	Height	in feet		Terre Refr	strial action	tation	Heigh Statio	t in feet on above	of 2nd Mean	<b>Lower</b>
1880	Mean of Times of obser- vation	Number and Name of Station	Observed Vertical Angle	Number of observa	Signal	Instrument	Contained Arc	In seconds	Decimals of Contained Arc	Height of ind Station – 1st E in feet	Trigono Rea By each deduc- tion	Sea Leve metrical pults Mean	l Final Result	Ieight of Pillar or
										~~~~				feet
Feb. 27 Mar. 15	h. m. 121 121	XXXII (Bitri) XXXV (Chauki)	o''" Do 630.9 Do 454.4	12 12	2·6 2·6	5°3 5°3	" 70 <b>7</b>	19	·027	- 16.8	351.9			Jeer
" 8 " 15	2 30 2 29	XXXVI (Kháro) XXXV (Chauki)	Do 10 2.7 Do 1 0.9	I 2 I 2	2·6 2·6	5·3 5·3	670	11	.019	- 89.1	350.9	320.1	348	ot
" 13 " 15	4 23 4 24	XXXVIII (Trisingh) XXXV (Chauki)	Do 926.1 Do 255.8	I 2 I 2	5°5 5°4	5°3 5°3	812	34	·042	- 77.9	347.6			
" 15 " 18	4 24 4 23	XXXV (Chauki) XXXVIII (Trisingh)	Do 255.8 Do 926.1	I 2 I 2	5°4 5°5	5°3 5°3	812	34	·042	+ 77'9	429.3			
" 8 " 11	2 47 2 47	XXXVI (Kháro) XXXVIII (Trisingh)	Do 526.2 Do 354.6	12 12	2.6 2.6	5°3 5°3	577	19	·033	- 13.0	427.0	426.8	425	ot
"6 "12,18	I 25 I 41	XXXVII (Morgich) XXXVIII (Trisingh)	Do 755.4 Do 229.0	12 12	2·6 2·7	5.3	639	17	·027	- 51.1	424.0			
Dec. 9, 10, 11 " 15, 16	I 37 I 39	XXXV (Chauki) XL (Kiraríwáro)	Do 751.2 Do 324.8	12 8	2·5 9·8	5·2 5·2	721	20	·028	- 43.4	306.7			
" 17, 18, 19 " 14, 15, 16	128 127	XXXVIII (Trisingh) XL (Kiraríwáro)	Do 11 32.4 Do 154.0	16 12	2.5	5°2 5°2	858	33	·038	-121.8	305.0	305.9	304	ot
"9,10,11 "6,7,8	I 27 I 27	XXXV (Chauki) XXXIX (Thar Muhári)	Do 7 59.6 Do 4 56.5	I 2 I 2	2.5	5.2	828	33	·040	- 37 · 2	312.9			
$\begin{array}{cccccccccccccccccccccccccccccccccccc$	I 20 I 19	XL (Kiraríwáro) XXXIX (Thar Muhári)	Do 412.0 Do 510.6	16 12	2.5	5°2 5°2	586	22	·038	+ 8.4	314.3	313.6	312	0†
,, 6, 7, 8   ,, 2, 4, 5	1 10 1 11	XXXIX (Thar Muhári) XLI (Mári)	Do 626.4 Do 320.3	I 2 I 2	2.5	5·2 5·2	608	20	·033	- 27.8	285.8			
"13, 15, 16 "2, 4, 5	137 136	XL (Kiraríwáro) XLI (Mári)	Do 516.2 Do 230.7	I 2 I 2	2.5	5°2	471	15	·032	- 19.3	286 · 7	286 • 2	284	0†
,, <b>12, 13, 14,</b> 15, 16 ,, <b>25, 26, 27, 28</b>	1 16 1 15	XL (Kiraríwáro) XLII (Yáru)	Do 5 2.0 Do 3 51.4	20 16	6·1 2·4	5·2 8·6	519	4	•008	- 12.6	293.3			
" 2, 4, 5 " 25, 26, 27, 28	I 23 I 22	XLI (Mári) XLII (Yáru)	Do 217.1 Do 357.7	12 16	6·1 2·5	5·2 8·6	348	2	·006	+ 5'1	291.3	291.8	290	ot
,, 21, 22, 23, 24 ,, 25, 26, 27,	I I2 I I2	XLIII (Núrpír) XLII (Yáru)	Do 739.3 Do 057.1	16 16	7 <sup>.</sup> 4 7 <sup>.</sup> 7	5°2 8°6	567	23	·041	- 57.6	290.9			
28 ,, 17, 18, 19 ,, 21, 22, 23, 24	I 20 I 27	XXXVIII (Trisingh) XLIII (Núrpír)	Do 931'I Do 241'I	12 16	2·5 6·0	5°2 5°2	798	36	<sup>.</sup> 045	- 78.5	348.3			
,, 13, 15, 16 ,, 21, 22, 23, 24	136 136	XL (Kiraríwáro) XLIII (Núrpír)	Do 349.0 Do 749.8	12 16	2·5 2·4	5°2 5°2	725	22	• <b>03</b> 0	+ 42.7	348.6	348.9	347	ot
					-	-								

**†** The pillar is sunk having its upper surface flush with the ground.

Astronomical Date				sions	Height	in feet		Terre Refra	strial	ation	Height Statio	t in feet	of 2nd Mean	OWER
	Mean of	Number and Name	Observed	f observat		aent	ined Arc	nds	ls of d Arc	ight of 1 – 1st St. 1 feet	frigono	Sea Level		Pillar or T
1880-81	of obser-		Vertical Angle	er o:	ligna	trun	Jonta	Beco	cima	Batior ir	Kes		Final	-
	vation			l umb		In		In	Cont	2nd St	By each deduc- tion	Mean	Result	Height
	h m		o i //				"							feet
Dec. 25, 26, 27, 28 ,, 21, 22, 23, 24	I I 2 I I 2	XLII (Yáru) XLIII (Núrpír)	Do 057'1 Do 739'3	16 16	7 <sup>.</sup> 7 7 <sup>.</sup> 4	8·6 5°2	567	23	·04 I	+ 57.6	349.9			
" 25, 26, 27, 28 " 30, 31.	130	XLÍI (Yáru)	Do 448.6	16	11.1	8.6	456	- 6	.013	- 14.7	277 · 1		1	
Jan. 4, 5	1 32	XLIV (Vijnot)	Do 215.7	16	12.2	5.3				.,				
24 ,, 30, Jan. 4, 5	I 28 I 28	XLIII (Núrpír) XLIV (Vijnot)	Do 838.3 Do 130.0	16 12	11.3 8.0	5°2 5°2	653	9	·014	- 70'3	278.6	277·9	276	13
Jan. 8, 9, 10, 11 Dec. 30, 31, Jan. 4, 5	1 44 1 43	XLV (Longwáli) XLIV (Vijnot)	Do 714.1 Do 035.0	16 16	9°0 2°5	5°2 5°2	484	5	.010	- 50.8	277.9	1		
Dec. 25, 26, 27, 28 Jan. 8, 9, 10, 11	I 22 I 22	XLII (Yáru) XLV (Longwáli)	Do 451'I Do 726'7	16 16	2·5 12·8	8·6 5°2	741	0	.000	+ 35°2	327.0			
Dec. 21, 22, 23, 24 Jan. 9, 10, 11	139 139	XLIII (Núrpír) XLV (Longwáli)	Do 518.7 Do 214.0	16 12	2°5 8°0	5°2	467	8	·017	- 18.4	330.2	328.7	326	10
Dec. 30, 31, Jan. 4, 5 ., 8, 9, 10, 11	I 43 I 44	XLIV (Vijnot) XLV (Longwáli)	Do 035.0 Do 714.1	16 16	2·5	5.2	484	5	.010	+ 50.8	328.6			
Dec. 30, 31, Jan. 4, 5 ,, 12, 13, 14, 15, 16	1 13 1 13	XLIV (Vijnot) XLVI (Vin)	Do 522°0 Do 250°6	16 20	3.0 2.5	5°2 5°2	359	- 52	• 145	- 13.6	264.3		~ 6 -	
,, 8, 9, 10, 11 ,, 12, 13, 14, 15, 16	I 14 I 15	XLV (Longwáli) XLVI (Vín)	Do 936.2 Eo 337.5	16 20	2·9 7·7	5°2 5°2	351	- 3	•009	— 66·o	262.7	203.2	201	12.2
,, 8, 9, 10, 11 ,, 18, 19, 20	I 23 I 22	XLV (Longwáli) XLVII (Got Mír Muhammad)	Do 826.0 Eo 227.4	16 12	3.0 3.0	5°2 5°2	364	I	.003	— 55·8	272.9	050.0	470	
,, 12, 13, 14, 15, 16 ,, 18, 19, 20	130 130	XLVI (Vín) XLVII (Got Mír Muhammad)	Do 237.5 Do 31.1	20 1 2	2.5 15.2	5°2 5°2	<u>3</u> 07	-39	· I 27	+ 8.3	271 . 7	2/2 3	2/0	
Dec. 30, 31, Jan. 4, 5 ,, 25, 26, 27, 28	I 34 I 35	XLIV (Vijnot) XLVIII (Dewari)	Do 525.0 Do 42.3	16 16	2°5 9'7	5°2 5°2	469	-53	.113	- 5.9	272.0			
,, 15, 16, 17 ,, 25, 26, 27, 28	I 42 I 42	XLVI (Vín) XLVIII (Dewari)	Do 314.7 Do 438.2	20 16	13.3 12.0	5°2 5°2	434	-61	.141	+ 9.8	273.3	272.0	<b>2</b> 70	16
"21, 22, 23, 24 "26, 27, 28	1 17 1 17	XLIX (Kot Sabzal) XLVIII (Dewari)	Do 330.4 Do 222.8	16 12	9.7 12.1	5°2 5°2	374	-21	·056	- 5.0	270.6			
$\begin{array}{c} , 12, 13, 14, \\ 15, 16 \\ , 21, 22, 23, \\ 24 \end{array}$	130 130	XLVI (Vín) XLIX (Kot Sabzal)	Do 328.5 Do 411.0	20 16	2°5 14°7	5°2 5°2	368	-65	• 177	+ 9.9	273.4			
,, 18, 19, 20 ,, 21, 22, 23, 24	I 37 I 37	XLVII (Got Mír Muhammad) XLIX (Kot Sabzal)	Do 344.6 Do 412.5	12 16	9°9 14°6	5°2 5°2	439	-52	. 1 18	+ 5°4	277.7	276 · 2	274	28
,, 26, 27, 28 ,, 21, 22, 23, 24	I 17 I 17	XLVIII (Dewari) XLIX (Kot Sabzal)	Do 222.8 Do 330.4	12 16	12°1 9°7	5°2 5°2	374	-21	·056	+ 5.0	277 . 6			

**†** The pillar is sunk having its upper surface flush with the ground.

#### PRINCIPAL TRIANGULATION. HEIGHTS ABOVE MEAN SEA LEVEL.

Astronomica	l Date			tions	Height	in feet		Terre Refra	strial	tation	Heigh Static	t in feet on above	of 2nd Mean	Lower
1881	Mean of Times	Number and Name of Station	Observed Vertical Angle	r of observa	gnal	rument	ntained Arc	econds	mals of ined Arc	Height of tion – 1st St in feet	Trigono Ree	Sea Level metrical pults	Final	f Pillar or '
	of obser- vation			Numbe		Inst	ပိ	Ine	Decin Conta	2nd Stat	By each deduc- tion	Mean	Result	Height o
	h m		01 "	-			"							feet
Jan. 25, 26, 27, 28 Feb. 3, 4, 5, 6	I 25 I 26	XLVIII (Dewari) LI (Ghundi)	Do 234.8 Do 230.0	16 16	8·7 14·0	5°2 5°2	343	- 17	·0 <b>5</b> 0	+ 2.3	274.3			
Jan. 21, 22, 23, 24 Feb. 3, 4, 5, 6	I 23 I 23	XLIX (Kot Sabzal) LI (Ghundi)	Do 313.3 Do 227.4	16 16	8·7 12·1	5·2 5·2	362	- 18	·050	- 3.4	273.8	274.0	271	18.8
Jan. 25, 26, 27, 28 ,, 30, 31, Feb. 2	I 23 I 23	XLVIII (Dewari) L (Kubba)	Do 256.6 Do 156.6	16 12	9·6 13·8	5°2 5°2	351	- 9	·026	- 3.1	268.9	260.1	267	20:0
Feb. 3, 4, 5, 6 Jan. 30, 81, Feb. 2	I 20 I 20	LI (Ghundi) L (Kubba)	Do 312.4 Do 242.3	16 12	12·8 8·7	5·2 5·2	366	- 25	•068	- 4.8	269 · 2	209 1	207	20 9
,, 30, 31, Feb. 2 Feb. 8, 9, 10	1 33 1 35	L (Kubba) LIX (Máchka)	Do 336.5 Do 450.8	16 20	12·8 13·4	5°2 5°2	480	- 48	. 100	+ 9.1	278 · 2	278.0	273	23.8
,, <b>3, 4, 5,</b> 6 ,, 8, 9, 10	I 28 I 28	LI (Ghundi) LIX (Máchka)	Do 425.0 Do 442.4	28 24	12·8 16·0	5·2 5·2	505	- 58	• 1 1 5	+ 3.8	277.8			
Jan. 21, 22, 23, 24 Feb. 14, 15, 16, 17	I 44 I 44	XLIX (Kot Sabzal) LXII (Dáowála)	Do 321.2 Do 430.7	16 16	14°1 12°1	5·2 5·2	484	- 27	•056	+ 7.3	283.5		- 9 -	
,, <b>3, 4, 5,</b> 6 ,, <b>14, 15,</b> 16, 17	1 30 1 30	LI (Ghundi) LXII (Dáowála)	Do 124.4 Do 248.0	16 16	15·9 16·0	5°2 5°2	348	- 15	•043	+ 7.2	281.3	282.3	282	23.4

Norz.-Stations LIX (Máchka) and LXII (Dáowála) appertain to the Great Indus Series.

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June, 1885.

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W. H. COLE, In charge of Computing Office.



#### PRINCIPAL TRIANGULATION. AZIMUTHAL OBSERVATIONS.

## At XIV (Malar)

Lat. N. 26° 2′ 25″ 80; Long. E. 70° 6′ 3″ 87 = 440242; Height above Mean Sea Level, 328 feet. January 1877; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Stars observed Mean Right Ascension 1877.0 Mean North Polar Distance 1877.0 Local Mean Times of Elongation, January 25

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a Ursæ 1	Mino	ris (	West)	and No. 1	1612 <sup>.</sup>	† (Eas	t)
	1 <sup>h</sup>	1 3 <sup>m</sup>	41 <sup>s</sup>	1 3 <sup>h</sup>	<b>4</b> 5 <sup>m</sup>	56 <b>°</b>	
	1°	20'	48" . 11	6°	37′	50" . 8	34
Western	10 <sup>h</sup>	50 <sup>m</sup>		Eastern	<b>I</b> 1 <sup>h</sup>	3 <sup>8m</sup>	

l Date on ngs of lark)				FAC	CE LEFT		FACE BIGHT						
Astronomical I	Elongation	Zeros (Circle Reading Referring Maı	Observed Horizontal Angle : Diff. of Readings Ref. Mark-Star	Interval in Time from Elongation	Reduction in Arc to Time of Elongation	Reduced Observation Ref. Mark – Star at Elongation	Observed Horizontal Angle : Diff. of Readings Ref. Mark – Star	H BO B B B B B B B B B B C B C B C B C C C C C C C C C C C C C C C C C C C C	Reduced Observation Ref. Mark – Star at Elongation				
Jan. 25	W.	• 1 209 16 29 16	• / " + 12 10 33 26 10 32 08 10 13 46 10 4 42 9 32 30	m 8 I 47 4 57 21 15 23 19 35 44	+ 0 0°16 0 1°25 0 23°04 0 27°70 1 4°95	• / " + 12 10 33 42 33 33 36 50 32 12 37 25	$\begin{array}{c} \circ & , & " \\ + & 12 & 10 & 27 \cdot 24 \\ & 10 & 25 \cdot 64 \\ & 10 & 22 \cdot 40 \\ & 10 & 19 \cdot 78 \\ & 9 & 41 \cdot 30 \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{array}{r}             0 & i & i \\             + 12 & 10 & 31 \cdot 56 \\             27 \cdot 90 \\             28 \cdot 31 \\             31 \cdot 14 \\             32 \cdot 90 \\         \end{array} $				
" 25	E.	209 16 & 29 16	+ 3 17 34 92 17 35 42 18 58 70 19 16 10 21 31 66	0 5 2 25 17 59 20 16 30 28	- 0 0.00 0 1.48 1 21.58 1 43.72 3 54.69	+ 3 17 34 92 33 94 37 12 32 38 36 97	+ 3 17 46.88 17 37.02 17 48.00 17 55.40 20 31.78	7       55        0       15.74         5       53       0       8.69         8       21       0       17.58         10       31       0       27.83         26       48       3       1.58	+ 3 17 31 · 14 28 · 33 30 · 42 27 · 57 30 · 20				
"26	W.	288 28 & 108 28	+ 12 10 31.78 10 33.88 10 24.08 10 19.84 9 57.12	5 45 I 10 I3 45 I6 5 27 22	+ 0 1.69 0 0.07 0 9.65 0 13.19 0 38.18	+ 12 10 33 47 33 95 33 73 33 03 35 30	+ 12 10 15.04 10 15.22 10 29.54 10 24.06 10 $6.94$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	+ 12 10 32 34 28 48 30 63 27 70 30 82				
" 28	E.	288 28 & 108 28	$\begin{array}{rrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrrr$	8 50 3 53 10 34 13 52 25 43	- 0 19 54 0 3 78 0 28 18 0 48 48 2 47 10	+ 3 17 33 62 32 58 37 06 30 84 38 34	+ 3 18 30.28 18 16.28 17 31.14 17 33.88 19 19.66	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{r} + 3 17 30.19 \\ 27.15 \\ 28.82 \\ 28.30 \\ 25.97 \end{array}$				

† Of Greenwich New Seven-year Catalogue of 2,760 Stars for 1864.

### PRINCIPAL TRIANGULATION. AZIMUTHAL OBSERVATIONS.

	3		ts of t)		FACE LE	T		FACE BIGHT				
	T INTITATION	Elongation	Zeros (Circle Reading Referring Mar	Observed Horizontal Angle: Diff. of Readings Ref. Mark – Star	Interval Time from Elon Flor Flor	ction in Time of gation	Reduced Observation Ref. Mark – Star at Elongation	Observed Horizontal Angle : Diff. of Readings Ref. Mark – Star	Interval in Time from Elongstion	Reduction in Arc to Time of Elongation	Reduced Observation Ref. Mark – Star at Elongation	
Jan	. 29	w.	~ , 7 39 & 39 187 39	• / * + 12 10 27 · 96 10 28 · 26 10 33 · 60 10 24 · 92	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	" 4 · 33 2 · 62 4 · 21 7 · 41	$ \begin{array}{r}  & & & & & & \\  & + & 12 & 10 & 32 \cdot 29 \\  & & & 30 \cdot 88 \\  & & & 37 \cdot 81 \\  & & & 32 \cdot 33 \\ \end{array} $	• / " + 12 10 11 • 42 10 14 • 20 10 32 • 00 10 31 • 16	<i>m</i> 8 19 41 17 13 0 43 2 50	, " + 0 19·80 0 15·13 0 0·03 0 0·41	• / # + 12 10 31 · 22 29 · 33 32 · 03 31 · 57	
"	29	Е	7 39 & 39 187 39	10 1 · 14 + 3 18 26 · 84 17 34 · 30 17 29 · 24 18 28 · 50	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	31.95 48.31 1.46 0.06 56.77	$\begin{array}{r} 33.09 \\ + 31738.53 \\ 32.84 \\ 29.18 \\ 31.73 \end{array}$	10 11 44 + 3 17 53 44 17 42 58 17 43 16 17 47 88	20 I 8 54 7 5 7 21 9 0	0 20.45 - 0 19.83 0 12.61 0 13.60 0 20.42	31.89 + 31733.61 29.97 29.56 27.46	
"	80	w	86 51 & 266 51	18 42 00 + 12 10 24 40 10 33 70 10 32 58 10 23 66	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	11.13 12.32 0.36 0.03 10.95	$31.53 + 12 10 36.72 \\ 34.06 \\ 32.61 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 \\ 34.58 $	19 37 02 + 12 10 28 16 10 25 72 10 31 08 10 28 74	22 20 9 50 8 6 5 52 7 35 22 12	2 7.17 + 0 4.94 0 3.35 0 1.75 0 2.94	30°45 + 12 10 33°10 29°07 32°83 31°68 30°48	
"	80	Е	86 51 & 266 51	+ 3 18 45 92 17 38 84 17 31 64 18 27 72 18 38 70	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	10.68 3.48 0.70 54.81 7.69	+ 3 17 35 · 24 35 · 36 30 · 94 32 · 91 31 · 01	+ 3 18 8.98 17 53.12 17 48.74 17 55.56 19 34.26	12 28 10 7 8 40 10 14 22 13	- 0 38.91 0 25.69 0 18.89 0 26.37 2 4.61	+ 3 17 30.07 27.43 29.85 29.19 29.65	
"	81	w	166 4 & 346 4	+ 12 10 21.54 10 34.62 10 33.88 10 21.94 10 16.38	$\begin{array}{c} 17 & 25 \\ 1 & 34 \\ 0 & 5 \\ 13 & 59 \\ 15 & 46 \\ \end{array}$	15°51 0°12 0°00 9°97 12°68	$\begin{array}{r} + 12 & 10 & 37 \cdot 05 \\ & 34 \cdot 74 \\ & 33 \cdot 88 \\ & 31 \cdot 91 \\ & 29 \cdot 06 \end{array}$	+ 12 10 24 96 10 23 90 10 31 92 10 25 96 10 8 54	12 35 10 46 5 52 7 53 22 5	+ 0 8.08 0 5.93 0 1.76 0 3.17 0 24.87	+ 12 10 33 04 29 83 33 68 29 13 33 41	
"	81	E	166 4 & 346 4	+ 3 18 59 74 17 37 68 17 26 96 18 11 30 18 23 68	18 35 - 1 4 38 0 2 21 0 12 20 0 14 24 0	26 · 39 5 · 39 1 · 38 38 · 31 52 · 29	$\begin{array}{r} + 3 17 33 \cdot 35 \\ 32 \cdot 29 \\ 25 \cdot 58 \\ 32 \cdot 99 \\ 31 \cdot 39 \end{array}$	+ 3 18 16 76 17 57 34 17 33 72 17 34 88 19 35 90	13 45 10 57 3 13 5 10 22 23	- 0 47 40 0 30 05 0 2 61 0 6 74 2 6 60	$\begin{array}{r} + 3 17 29.36 \\ 27.29 \\ 31.11 \\ 28.14 \\ 29.30 \end{array}$	

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## Abstract of Astronomical Azimuth observed at XIV (Malar) 1877.

Face	L R	L R	L R	L R	L R
Zero	209° 29°	<b>2</b> 88° 108°	8° 188°	87° 267°	166° 346°
Date	January 25	January 28	January 29	January 30	January 31
Observed difference of Circle-Readiugs, Ref. M.—Star reduced to Elongation	34.92 31.14 33.94 28.33 37.12 30.42 32.38 27.57 36.97 30.20	33.62 30.19 32.58 27.15 37.06 28.82 30.84 28.30 38.34 25.97	38.53 33.61 32.84 29.97 29.18 29.56 31.73 27.46 31.53 30.45	35°24 30°07 35°36 27°43 30°94 29°85 32°91 29°19 31°01 29°65	33·35 29·36 32·29 27·29 25·58 31·11 32·99 28·14 31·39 29·30
Means	35.07 29.53	34.49 28.09	32.76 30.21	33.09 29.24	31.12 29.04
Means of both faces Level Corrections Corrected Means Az. of Star fr. S., by W. Az. of Ref. M. "	+ 3 17 32.30  - 0.52  + 3 17 31.78  187 23 32.74  190 41 4.52	31 · 29 - 0 · 89 30 · 40 32 · 70 3 · 10	$ \begin{array}{r}                                     $	$ \begin{array}{r} 31 \cdot 17 \\ + 1 \cdot 10 \\ 32 \cdot 27 \\ 32 \cdot 68 \\ 4 \cdot 95 \end{array} $	$ \begin{array}{c}                                     $

1. By Eastern Elongation of No. 1612<sup>+</sup>.

2.	By	Western	Elongation	of	a	Ursæ	Minoris.
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Face	L	R	L	R	L	R	L	R		L	B	2
Zero	209°	<b>29°</b>	<b>2</b> 88°	108°	8°	188°	87°	267°	:	166°	34(	6°
Date	Janua	ry 25	Januar	ту 26 ″	Janua	ry 29	Janus	ary 30		Janua	ary 3.	1
Observed difference of Circle-Readings, Ref. M. – Star reduced to Elongation	33 · 42 33 · 33 36 · 50 32 · 12 37 · 25	31 · 56 27 · 90 28 · 31 31 · 14 32 · 90	33 47 33 95 33 73 33 03 35 30	32 · 34 28 · 48 30 · 63 27 · 70 30 · 82	32 · 29 30 · 88 37 · 81 32 · 33 33 · 09	31 · 22 29 · 33 32 · 03 31 · 57 31 · 89	36 · 72 34 · 06 32 · 61 34 · 61 34 · 58	33 · 10 29 · 07 32 · 83 31 · 68 30 · 48	3 3 3 2	7 ° 05 4 ° 74 3 ° 88 1 ° 91 9 ° 06	33 · 0 29 · 1 33 · 0 29 · 1 33 · 0	04 83 68 13 41
Means	34.52	30.36	33.90	29.99	33 · 28	31.31	34.52	31.43	3:	3.33	31 . {	82
Means of both faces Level Corrections Corrected Means Az. of Star fr S., by W. Az. of Ref. M. "	+ 12 10 32 - 0 + 12 10 32 178 30 32 190 41 4	44 10 34 29 63	31 · - 0· 31 · 32 · 3 ·	95 86 09 18 27	$3^{2}$ + 0 $3^{2}$ $3^{2}$ 4	* * 25 * 11 * 36 * 07 * 43	32 + 0 33 31 5	" • 98 • 36 • 34 • 96 • 30		$+ \begin{array}{c} 3^{2} \\ + \begin{array}{c} 0 \\ 3^{2} \\ 3^{1} \\ 4 \end{array}$	* 58 *08 *66 *74 *40	
			(hv	Eastern	Elongat	ion				。 100	,	<i>"</i>
Astronomical Azimuth	of Referrin	g Mark	by	Western	Mea	n	•	••	•••	,,		4.41
Angle Referring Mark	and XVI (1	Ramsar)	see naae	144 ant	<i>e</i>	•••	••••	••	···-	" - 20	, 14	4 30
Astronomical Azimuth	of Ramsar	hv obser	vation							161	26	22.07
Geodetical Azimuth	of	h <b>v c</b> alcu	lation fro	om that	adopted	(Vol. I	. nage 1	41) at				1
Kaliánpur, see	page 204 a	nte					· · · · · · · ·		•••	161	26	24.93
Astronomical – Geodetic	cal Azimuth	at XIV	(Malar)		•••			••		-		2.86

† Of Greenwich New Seven-Year Catalogue of 2760 Stars for 1864.

# At XXXI (Asu)

Lat. N. 27° 10' 32"·14; Long. E. 70° 13'  $26''\cdot85 = 44053\cdot8$ ; Height above Mean Sea Level, 479 feet. February 1880; observed by Captain M. W. Rogers, R.E., with Barrow's 24-inch Theodolite No. 2.

Stars observed	a Ursæ Minoris (West)	and No. 1612+ (East).
Mean Right Ascension 1880.0	1 <sup>h</sup> 14 <sup>m</sup> 45 <sup>s</sup>	13 <sup>h</sup> 45 <sup>m</sup> 49 <sup>s</sup>
Mean North Polar Distance 1880.0	1° 19' 51".07	6° 38′ 44″·85
Local Mean Times of Elongation, February 17	Western 9 <sup>h</sup> 23 <sup>m</sup>	Eastern 10 <sup>h</sup> 11 <sup>m</sup>

ate	ta of	FA	CE LEFT	FACE BIGHT	
Astronomical I Elongation	Zeros (Circle Reading Referring Mar	Observed Horizontal Angle: Diff. of Readings Bef. Mark-Star	Reduction in Arc to Time of Elongation	Observed	on in ime of tion Ref. Mark – Star at Elongation
Feb. 17 W.	0 / 201 30 & 21 30	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccc} & & & & & & & \\ & & & & & & \\ + & 0 & 2 \cdot 86 & + & 44 & 39 & 43 \cdot 02 \\ & 0 & 4 \cdot 62 & & & & \\ 0 & 27 \cdot 87 & & & & & \\ 0 & 32 \cdot 97 & & & & & & \\ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c} * & \circ & , & * \\ 0.01 & + & 44 & 39 & 37^{\circ}13 \\ 0.06 & & & 36^{\circ}12 \\ 1.92 & & & 39^{\circ}88 \\ 4.90 & & & 40^{\circ}68 \end{array}$
"17 E.	201 30 & 21 30	+ 35 41 30°16 3 13 41 32°34 5 29 43 9°70 19 43 43 28°26 22 15	$\begin{array}{c ccccc} - & 0 & 2 \cdot 62 \\ & 0 & 7 \cdot 66 \\ & 1 & 39 \cdot 41 \\ & 2 & 6 \cdot 54 \end{array} \begin{array}{c} + & 35 & 41 & 27 \cdot 54 \\ & 24 \cdot 68 \\ & 30 \cdot 29 \\ & 21 \cdot 72 \end{array}$	$\begin{array}{c ccccc} + & 35 & 41 & 52 & 96 \\ & & 41 & 53 & 72 \\ & & 42 & 5 & 78 \\ & & & 42 & 5 & 78 \\ \end{array} \begin{array}{c} 11 & 28 & - & 0 & 3 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & & & 0 & 32 \\ & &$	3'34 + 35 41 19'62 3'93 19'79 8'17 17'61
" 18 W.	280 45 & 100 45	$\begin{array}{c ccccc} + & 44 & 39 & 40^{\circ} 44 & 10 & 50 \\ & 39 & 37^{\circ} 16 & 8 & 47 \\ & 39 & 44^{\circ} 40 & 5 & 24 \\ & 39 & 42^{\circ} 14 & 7 & 29 \end{array}$	$\begin{array}{c cccc} + & 0 & 5 \cdot 98 \\ 0 & 3 \cdot 94 \\ 0 & 1 \cdot 49 \\ 0 & 2 \cdot 86 \end{array} \begin{array}{c} + & 44 & 39 & 46 \cdot 42 \\ 41 \cdot 10 \\ 45 \cdot 89 \\ 45 \cdot \infty \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccc} 0.48 \\ + & 44 & 39 & 41 \cdot 32 \\ 0.04 & & 39 \cdot 44 \\ 9.45 & & 41 \cdot 47 \\ 2.44 & & 37 \cdot 60 \end{array}$
" 18 E.	280 45 & 100 45	$\begin{array}{c cccc} + & 35 & 41 & 57 \cdot 96 \\ & 41 & 42 \cdot 62 & 7 & 40 \\ & 41 & 38 \cdot 44 & 5 & 25 \\ & 41 & 39 \cdot 18 & 7 & 22 \end{array}$	$\begin{array}{c cccc} - & \circ & 24 \cdot 28 \\ \circ & 14 \cdot 89 \\ \circ & 13 \cdot 83 \end{array} + & 35 & 41 & 33 \cdot 68 \\ & 27 \cdot 73 \\ & 30 \cdot 98 \\ & 30 \cdot 98 \\ & 25 \cdot 35 \end{array}$	$\begin{array}{c ccccc} + & 35 & 41 & 22 \cdot 16 & 1 & 28 & - & 0 \\ & & 41 & 21 \cdot 60 & 0 & 16 & 0 \\ & & 42 & 3 \cdot 46 & 12 & 33 & 0 & 4 \\ & & & 42 & 11 \cdot 86 & 14 & 19 & 0 & 5 \end{array}$	0.54       + 35 41 21.62         0.02       21.58         0.18       23.28         2.35       19.51
" 20 W.	. 79 10 & 259 10	$\begin{array}{c ccccc} + & 44 & 39 & 30 \cdot 08 & 16 & 38 \\ & 39 & 34 \cdot 44 & 14 & 9 \\ & 39 & 48 \cdot 14 & 2 & 44 \\ & 39 & 41 \cdot 74 & 4 & 34 \end{array}$	$\begin{array}{c cccc} + & 0 & 14 \cdot 11 \\ 0 & 10 \cdot 20 \\ 0 & 0 \cdot 38 \\ 0 & 1 \cdot 06 \end{array} \begin{array}{c} + & 44 & 39 & 44 \cdot 19 \\ 44 \cdot 64 \\ 48 \cdot 52 \\ 42 \cdot 80 \end{array}$	$\begin{array}{c cccccc} + & 44 & 39 & 40 \cdot 32 & 7 & 52 & + & 0 \\ & & 39 & 38 \cdot 36 & 5 & 41 & 0 \\ & & 39 & 34 \cdot 50 & 10 & 26 & 0 \\ & & 39 & 32 \cdot 84 & 12 & 1 & 0 \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$
" <b>2</b> 0 E.	79 10 & 259 10	$\begin{array}{cccccc} + & 35 & 41 & 53 & 76 & 9 & 45 \\ & & 41 & 39 & 82 & 7 & 1 \\ & & 41 & 43 & 60 & 7 & 33 \\ & & & 41 & 50 & 52 & 9 & 32 \end{array}$	$\begin{array}{c cccc} -& 0 & 24 \cdot 11 \\ 0 & 12 \cdot 52 \\ 0 & 14 \cdot 54 \\ 0 & 23 \cdot 21 \end{array} \begin{array}{c} +& 35 & 41 & 29 \cdot 65 \\ 27 \cdot 30 \\ 29 \cdot 06 \\ 27 \cdot 31 \end{array}$	$\begin{array}{c cccccc} + & 35 & 42 & 33 & 78 \\ & 41 & 20 & 56 & 0 & 16 & 0 \\ & 41 & 17 & 02 & 1 & 58 & 0 \\ & 42 & 22 & 24 & 15 & 10 & 0 & 5 \end{array}$	1 * 31       + 35 41 22 * 47         5 02       20 * 54         5 '99       16 * 03         8 * 77       23 * 47
" 21 W.	158 20 & 338 20	+ 44 39 37 <sup>.</sup> 78 13 40 39 37 <sup>.</sup> 38 11 44 39 45 <sup>.</sup> 04 2 20 39 45 <sup>.</sup> 06 4 11	$\begin{array}{c cccc} + & 0 & 9 & 53 \\ 0 & 7 & 02 \\ 0 & 0 & 28 \\ 0 & 0 & 89 \end{array} \begin{array}{c} + & 44 & 39 & 47 & 31 \\ 44 & 40 \\ 45 & 32 \\ 45 & 95 \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccc} 1 \cdot 51 & + & 44 & 39 & 41 \cdot 79 \\ 5 \cdot 71 & & & 39 \cdot 33 \\ 5 \cdot 80 & & & 41 \cdot 92 \\ 8 \cdot 09 & & & 38 \cdot 61 \end{array}$

† Of Greenwich New Seven-Year Catalogue of 2760 Stars for 1864.

)ate		s of k)		FACE LEFT	FACE BIGHT				
Astronomical I	Elongation	Zeros (Circle Reading Referring Mar	Observed Horizontal Angle: Diff. of Readings Ref. Mark-Star	Reduction in Arc to Time of Elongation Ref. Mark – Star at Elongation	Dobserved Horizontal Angle: Diff. of Readings Ref. Mark-Star				
Feb. 21	E.	0 / 158 20 & 338 20	$\begin{array}{c ccccc} \circ & \prime & \prime & m & a \\ + & 35 & 41 & 57 & 98 & 10 & 37 \\ & 41 & 48 & 26 & 8 & 40 \\ & 41 & 35 & 98 & 5 & 32 \\ & 41 & 40 & 86 & 7 & 33 \end{array}$	$\begin{array}{c ccccc} , & " & & & & & & & \\ - & 0 & 28 \cdot 63 & & & + & 35 & 41 & 29 \cdot 35 \\ & 0 & 19 \cdot 07 & & & & 29 \cdot 19 \\ & 0 & 7 \cdot 82 & & & 28 \cdot 16 \\ & 0 & 14 \cdot 51 & & & 26 \cdot 35 \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				
" 22	W.	359 57 & 58	+ 44 39 36 16 13 47 39 37 70 11 42 39 45 20 1 22 39 45 74 3 15	$\begin{array}{c cccc} + & 0 & 9 & 70 \\ & 0 & 6 & 98 \\ \hline & 0 & 0 & 10 \\ & 0 & 0 & 54 \end{array} + \begin{array}{c} + & 44 & 39 & 45 & 86 \\ & 44 & 68 \\ & 44 & 68 \\ & 45 & 30 \\ & 46 & 28 \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				
" 22	E.	359 57 & 58	$\begin{array}{c cccccc} + & 35 & 42 & 22 \cdot 32 \\ & 42 & 8 \cdot 48 & 12 & 26 \\ & 41 & 29 \cdot 92 & 1 & 24 \\ & 43 & 10 \cdot 42 & 20 & 0 \end{array}$	$\begin{array}{c cccc} - & 0 & 53 \cdot 88 \\ & 0 & 39 \cdot 16 \\ & 0 & 0 \cdot 50 \\ & 1 & 42 \cdot 19 \end{array} + \begin{array}{c} 35 & 41 & 28 \cdot 44 \\ & 29 \cdot 32 \\ & 29 \cdot 32 \\ & 28 \cdot 23 \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				

## Abstract of Astronomical Azimuth observed at XXXI (Asu) 1880.

# 1. By Eastern Elongation of No. 1612<sup>+</sup>.

Face Zero	L R 202° 22°	L R 281° 101°	L R 79° 259°	L R 158° 838°	L R 0° 180°
Date	February 17	February 18	February 20	February 21	February 22
Observed difference of Circle-Readings, Ref. M.—Star reduced to Elongation	"" 27`54 19`62 24`68 19`79 30`29 17`61 21`72	33.68 21.62 27.73 21.58 30.98 23.28 25.35 19.51	" " 29 <sup>.65</sup> 22 <sup>.47</sup> 27 <sup>.30</sup> 20 <sup>.54</sup> 29 <sup>.06</sup> 16 <sup>.03</sup> 27 <sup>.</sup> 31 23 <sup>.47</sup>	" " 29`35 24`63 29`19 17`69 28`16 23`93 26`35 22`60	28.44 22.71 29.32 22.81 29.42 21.63 28.23 19.55
Means	26.06 19.01	29.44 21.20	28.33 20.63	. 28.26 22.21	28.85 21.68
Means of both faces Level Corrections Corrected Means Az. of Star fr. S., by W. Az. of Ref. M. "	• / * + 35 41 22.54 + 2.00 + 35 41 24.54 187 28 60.18 223 10 24.72	25°47 - 0°34 25°13 59°95 25°08	* 24.48 + 0.57 25.05 59.62 24.67	" + 0.40 25.64 59.50 25.14	" - 1'03 24'24 59'28 23'52

† Of Greenwich New Seven-Year Catalogue of 2760 Stars for 1864.



## Abstract of Astronomical Azimuth at XXXI (Asu) 1880-(Continued).

Face	L R	LR	L R	L R	LR
Zero	202° 22°	281° 101°	79° 259°	158° 338°	0° 180°
Date	February 17	February 18	February 20	February 21	February 22
	n	17 <b>4</b>	n n	n 4	
Observed. difference	43'02 37'1	46.42 41.32	44'19 43'47	47.31 41.70	45.86 41,26
of Circle-Readings,	40.24 30.1	41.10 39.44	44.64 40.01	44.40 39.33	44.68 37.31
Ref. MStar	47.49 39.8	45.89 41.47	48.52 40.04	45.32 41.92	45.30 40.14
reduced to Elongation	39.67 40.6	45.00 37.60	42.80 40.19	45.92 38.01	46.28 37.75
Means	42.61 38.4	44.60 39.96	45.04 40.93	45.75 40.41	45.23 39.13
	0 1 4	•	4	*	1
Means of both faces	+ 44 39 40.53	42.38	42.00	43.08	42.33
Level Corrections	+ 1.76	- 0.12	+ 0.23	+ 0.62	- 0·85
Corrected Means	+ 44 39 42.29	42.11	43.22	43.20	41 • 48
Az. of Star fr. S., by W.	178 30 42.48	42.26	41.81	41.28	41.36
Az. of Ref. M. "	223 10 24.77	24.37	25.03	25.28	22.84

# 2. By Western Elongation of a Ursæ Minoris.

	(by	Eastern El	ongation	•••	•••	•••	223	10	24.63
Astronomical Azimuth of Referring Mark	} by	Western	"	•••	•••	•••	,,		24.46
· · · ·	l		Mean	•••	•••	•••	,,		24.55
Angle Referring Mark and XXXIV (Kolu) &	ee pag	e 157 ante	•••	•••	•••	-	- 21	32	52.30
Astronomical Azimuth of Kolu by observation	n <sup>.</sup>	•••	•••	• • •	•••	•••	201	37	32.25
Geodetical Azimuth of ,, by calculation	ı from	that adopt	ed (Vol. ]	II, page	141) at				
Kaliánpur, see page 205 ante	•••	•••	•••	•••	•••	•••	201	37	33.14
Astronomical-Geodetical Azimuth at XXXI	(Asu)	)	•••	•••	•••	-	-		0.89
									• •

# At XLIV (Vijnot)

Lat. N. 28° 2' 3"·30; Long. E. 69° 52' 59"·95 =  $\overset{1}{4}$  39 32.0; Height above Mean Sea Level, 276 feet. December 1880 and January 1881; observed by Lt.-Colonel B. R. Branfill with Troughton and Simms' 24-inch Theodolite No. 1.

Stars observed	51 Cephei (East)	and $\lambda$ Ursæ Minoris (West).
Mean Right Ascension 1881.0	6 <sup>h</sup> 44 <sup>m</sup> 17 <sup>s</sup>	19 <sup>h</sup> 43 <sup>m</sup> 9 <sup>s</sup>
Mean North Polar Distance 1881.0	2° 46′ 18″ 96	1° 3′ 14″·33
Local Mean Times of Elongation, December 30	6 <sup>h</sup> 13 <sup>m</sup>	7 <sup>h</sup> 2 <sup>m</sup>

ate		rs of it)	74	ACE LEFT	FACE BIGHT			
Astronomical I	Elongation	Zeros (Circle Reading Referring Mar	Observed Horizontal Angle : Diff. of Readings Ref. Mark-Star	Reduction in Arc to Time of Elongation Elongation Ref. Mark – Star at Elongation	Observed	on in me of tion Ref. Mark – Star at Elongation		
Dec. 80	E.	0 7 323 29 & 143 29	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccc} & & & & & & & & & \\ \hline & & & & & & & \\ - & 2 & 32'77 & & & & & \\ 2 & 7'71 & & & & & & \\ 0 & 13'53 & & & & & & \\ 0 & 7'38 & & & & & & & \\ 0 & 7'38 & & & & & & & \\ 0 & 16'01 & & & & & & & \\ 0 & 48'01 & & & & & & & \\ 0 & 48'01 & & & & & & & \\ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\circ$ $\circ$ $\bullet$ 9.99     + 12 58 31.91 $8.42$ $30.67$ $\circ.00$ $32.05$ $\circ.69$ $29.71$ $5.20$ $30.20$ $1.85$ $31.89$		
" 80	w.	323 29 & 143 29	$\begin{array}{ccccccc} + & 17 & 17 & 46 \cdot 80 & 32 & 41 \\ & 17 & 55 \cdot 13 & 29 & 58 \\ \hline 18 & 31 \cdot 14 & 1 & 48 \\ \hline 18 & 30 \cdot 79 & 5 & 6 \\ \hline 18 & 0 \cdot 69 & 26 & 47 \\ \hline 17 & 57 \cdot 61 & 29 & 27 \end{array}$	$\begin{array}{c ccccc} + & 0 & 43 \cdot 55 \\ & 0 & 36 \cdot 62 \\ \hline & 0 & 0 \cdot 13 \\ & 0 & 1 \cdot 06 \\ & 0 & 29 \cdot 21 \\ & 0 & 35 \cdot 31 \\ \hline \end{array} \begin{array}{c} + & 17 & 18 & 30 \cdot 35 \\ & 31 \cdot 75 \\ & 31 \cdot 85 \\ & 31 \cdot 85 \\ & 29 \cdot 90 \\ & 35 \cdot 31 \\ \hline \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccc} 7'30 & + & 17 & 18 & 26 \cdot 83 \\ 4'60 & & 27 \cdot 74 \\ 8'32 & & 30 \cdot 47 \\ 1'51 & & 28 \cdot 03 \\ 1'99 & & 28 \cdot 18 \\ 2'41 & & 33' \cdot 00 \end{array}$		
" 81	E.	42 41 & 222 41	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccc} -& 0 & 54 \cdot 25 \\ 0 & 43 & 09 \\ 0 & 1 & 04 \\ 0 & 3 & 90 \\ 2 & 10 & 94 \\ 3 & 28 & 68 \\ \end{array} \begin{array}{c} + & 12 & 58 & 33 \cdot 67 \\ 3 & 0 & 06 \\ 3 & 5 & 08 \\ 3 & 5 & 08 \\ 3 & 3 & 36 \\ 3 & 3 & 36 \\ 3 & 3 & 69 \end{array}$	$\begin{array}{c cccccc} + & 12 & 60 & 39 \cdot 76 \\ & 60 & 16 \cdot 99 \\ & 58 & 44 \cdot 83 \\ & 58 & 36 \cdot 85 \\ & 59 & 5 \cdot 92 \\ & 59 & 5 \cdot 92 \\ & 59 & 41 \cdot 46 \end{array} \begin{array}{c ccccccc} - & 2 \\ & - & 2 \\ & 1 & 1 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & - & 2 \\ & -$	$\begin{array}{c ccccc} 4 \cdot 21 & + & 12 & 58 & 35 \cdot 55 \\ 4 \cdot 93 & & & 32 \cdot 06 \\ 1 \cdot 64 & & & 33 \cdot 19 \\ 6 \cdot 42 & & & 30 \cdot 43 \\ 1 \cdot 46 & & & 34 \cdot 46 \\ 9 \cdot 65 & & & & 31 \cdot 81 \end{array}$		
<b>" 81</b>	W.	42 41 & 222 41	$\begin{array}{c ccccc} + & 17 & 18 & 26 \cdot 15 \\ & 18 & 30 \cdot 29 & 7 & 8 \\ \hline & 18 & 15 \cdot 15 & 19 & 34 \\ & 18 & 5 \cdot 46 & 22 & 53 \\ & 16 & 57 \cdot 67 & 47 & 29 \\ & 16 & 45 \cdot 81 & 50 & 17 \end{array}$	$\begin{array}{c ccccc} + & 0 & 4 \cdot 52 \\ 0 & 2 \cdot 07 \\ 0 & 15 \cdot 60 \\ 0 & 21 \cdot 32 \\ 1 & 31 \cdot 50 \\ 1 & 42 \cdot 55 \end{array} \begin{array}{c} + & 17 & 18 & 30 \cdot 67 \\ 32 \cdot 36 \\ 30 \cdot 75 \\ 26 \cdot 78 \\ 29 \cdot 17 \\ 28 \cdot 36 \end{array}$	$\begin{array}{c cccccc} + & 17 & 17 & 58 \cdot 89 \\ & 18 & 1 \cdot 60 & 25 & 47 & 0 & 2 \\ \hline & 18 & 26 \cdot 64 & 5 & 39 & 0 \\ & 18 & 22 \cdot 88 & 9 & 22 & 0 \\ & 17 & 41 \cdot 98 & 33 & 7 & 0 & 4 \\ & 17 & 31 \cdot 76 & 35 & 59 & 0 & 5 \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$		
Jan. 1	E.	121 53 & 301 53	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	6.22       + 12 58 38.37         1.68       34.68         7.49       35.75         6.07       34.84         0.28       38.72         6.09       34.89		

### PRINCIPAL TRIANGULATION. AZIMUTHAL OBSERVATIONS.

<b>ate</b>			rs of it)		PACE	LBFT		FAOE BIGHT			
Astronomical I		Elongation	Zeros (Circle Reading Beferring Maı	Observed Horizontal Angle : Diff. of Readings Ref. Mark – Star	Interval in Time from Klongation	eduction in rc to Time of Elongation	Reduced Observation Ref. Mark – Star at Elongation	Observed Horizontal Angle : Diff. of Readings Ref. Mark – Star	H H H F F F F F F F F F F F F F F F F F	Reduced Observation Ref. Mark – Star at Elongation	
Jan.	1	W.	0 / 121 53 & 301 53	0 7 7 + 17 17 56 56 18 1.84 18 31.49 18 30.29 17 40.67 17 31.50	m 8 20 3 + 26 9 1 34 5 0 35 1 38 1	, " - 0 34 · 43 0 27 · 90 0 0 · 10 0 1 · 02 0 49 · 87 0 58 · 75	+ 17 18 30.99 29.74 31.59 31.31 30.54 30.25	+ 17 17 8.23 17 14.40 18 31.86 18 28.85 18 16.34 18 10.12	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	• / # + 17 18 35 • 97 32 • 13 37 • 59 31 • 97 32 • 09 30 • 19	
>>	2	E.	201 5 & 21 5	+ 12 59 19.29 59 5.27 58 35.10 58 34.58 59 34.67 60 26.14	20 17 - 16 42 0 46 1 24 23 34 32 8	- 0 44 · 10 0 29 · 91 0 0 · 06 0 0 · 21 0 59 · 78 1 51 · 19	+ 12 58 35.19 35.36 35.04 34.37 34.89 34.95	+ 12 60 8.16 59 54.71 58 45.72 58 40.03 58 41.82 59 3.39	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+ 12 58 36 38 35 98 35 55 34 85 34 10 34 28	
<b>3</b> 7	2	W.	201 5 & 21 5	+ 17 18 11.78 18 15.90 18 31.35 18 29.96 17 41.67 17 30.62	21 44 + 19 12 4 2 6 54 34 20 38 8	- 0 19 29 0 15 06 0 0 66 0 1 94 0 47 97 0 59 13	+ 17 18 31 .07 30 .96 32 .01 31 .90 29 .64 29 .75	+ 17 17 34 99 17 42 13 18 30 02 18 31 13 18 19 99 18 12 17	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{r} + 17 18 32.02 \\ 30.62 \\ 32.57 \\ 32.06 \\ 31.68 \\ 29.80 \end{array}$	
59	8	E.	280 17 & 100 17	+ 12 59 23.59 59 13.36 58 31.80 58 33.31 59 42.38 60 29.98	22 10 - 19 41 2 7 1 15 25 20 33 1	- 0 52 °64 0 41 °52 0 0 °48 0 0 °17 1 9 °10 1 57 °41	+ 12 58 30.94 31.84 31.32 33.14 33.28 32.57	+ 12 60 53 62 60 19 10 58 47 97 58 41 75 58 44 03 59 4 19	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{r} + 12 58 34.36 \\ 34.20 \\ 33.83 \\ 32.90 \\ 35.14 \\ 32.30 \end{array}$	
"	8	<b>w</b> .	280 17 & 100 17	+ 17 18 13 20 18 18 60 18 27 36 18 26 80 17 40 06 17 31 97	20 22 + 17 48 6 9 9 52 35 27 38 8	- 0 16 92 0 12 92 0 1 54 0 3 97 0 51 12 0 59 13	+ 17 18 30.12 31.52 28.90 30.77 31.18 31.10	+ 17 17 39 23 17 42 25 18 28 29 18 29 83 18 11 62 18 5 14	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	+ 17 18 33.07 28.90 29.90 30.27 30.72 30.23	

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# Abstract of Astronomical Azimuth observed at XLIV (Vijnot) 1880-81.

Face	T, R.	T, R	T, R	T, R	T, R
Zero	823° 143°	43° 223°	122° 802°	201° 21°	280° 100°
Date	December 30	December 31	January 1	January 2	January 3
Observed difference of Circle-Readings, Ref. M.—Star reduced to Elongation	36.01 31.91 35.27 30.67 32.73 32.05 33.52 29.71 32.09 30.20 34.50 31.89	33.67 35.55 30.06 32.06 35.08 33.19 35.28 30.43 33.36 34.46 33.69 31.81	34·28 38·37 32·72 34·68 35·46 35·75 33·73 34·84 34·35 38·72 32·60 34·89	35'19 36'38 35'36 35'98 35'04 35'55 34'37 34'85 34'89 34'10 34'95 34'28	30.94       34.36         31.84       34.20         31.32       33.83         33.14       32.90         33.28       35.14         32.57       32.30
Means	34.03 31.02	33.22 32.92	33.86 36.21	34.97 35.19	32.18 33.79 ,
Means of both faces Level Corrections Corrected Means Az. of Star fr. S., by W. Az. of Ref. M. "	$\begin{array}{c} & & & & & \\ & + & 12 & 58 & 32 \cdot 55 \\ & & - & 0 \cdot 36 \\ + & 12 & 58 & 32 \cdot 19 \\ & 183 & 8 & 30 \cdot 38 \\ & 196 & 7 & 2 \cdot 57 \end{array}$	" 33°22 	* - 0.60 34.44 31.06 5.50	35°08 	<b>32</b> .99 + 2.59 35.58 31.74 7.32

## 1. By Eastern Elongation of No. 51 Cephei.

2. By Western Elongation of  $\lambda$  Ursæ Minoris.

Face	L	R	L	R	L	R	L	R	L	R	
Zero	823°	143°	<b>4</b> 3°	223°	122°	<b>302°</b>	<b>2</b> 01°	<b>21°</b>	280	° 100	)°
Date	Decem	ber 30	Decen	nber 31	Janu ″	ary 1	Janu	ary 2	Ja	nuary 9	
Observed difference of Circle-Readings, Ref. MStar reduced to Elongation	30°35 31°75 31°27 31°85 29°90 32°92	26 · 83 27 · 74 30 · 47 28 · 03 28 · 18 33 · 00	30.67 32.36 30.75 26.78 29.17 28.36	32.02 28.72 27.94 26.45 26.59 24.41	30 · 99 29 · 74 31 · 59 31 · 31 30 · 54 30 · 25	35 · 97 32 · 13 37 · 59 31 · 97 32 · 09 30 · 19	31 ° 07 30 ° 96 32 ° 01 31 ° 90 29 ° 64 29 ° 75	32.02 30.62 32.57 32.06 31.68 29.80	30°1 31°5 28°9 30°7 31°1 31°1	2 33 0 2 28 0 0 29 0 7 30 0 8 30 0 0 30 0	07 90 27 72 23
Means	31.34	29.04	29.68	27.69	30.74	33.32	30.89	31.46	30.6	o 30.	52
Means of both faces Level Corrections Corrected Means Az. of Star fr S., by W. Az. of Ref. M. "	$ \begin{array}{r}                                     $	" • 50 • 69 • 59 • 28	21 	# 8.69 0.13 8.56 2.25 0.81	32 — c 31 31 3	" "03 "92 "11 "91 "02	31 	" 1 · 18 D · 03 1 · 15 1 · 46 B · 61	+	30°56 2°19 32°75 31°12 3°87	
Astronomical Azimuth	of Referrir	ng Mark	{ b b	y Eastern y Wester	n Elonga n ", Me	ation  an	•	•••	19	。, 96 7 "	" 4.81 2.52 3.67

Angle Referring Mark and XLVIII (Dewari) see page 166 ante	•••	- 36 31	48.33
Astronomical Azimuth of Dewari by observation	•••	159 35	15.34
Geodetical Azimuth of ,, by calculation from that adopted (Vol. II, page	141) at		
Kaliánpur, see page 206 ante	•••	159 35	11.30
Astronomical – Geodetical Azimuth at XLIV (Viinot)		+	4.01

### At LXII (Dáowála)\*

Lat. N. 28° 20' 12".87; Long. E. 69° 52' 57".86 = 43981.9; Height above Mean Sea Level, 282 feet. February 1881; observed by Lieut.-Colonel B. R. Branfill with Troughton and Simms' 24-inch Theodolite No. 1.

Stars observedδ Ursæ Minoris (East)and 51 Cephei (West).Mean Right Ascension 1881·018<sup>h</sup> 10<sup>m</sup> 43<sup>s</sup>6<sup>h</sup> 44<sup>m</sup> 17<sup>s</sup>Mean North Polar Distance 1881·03° 23' 26"·672° 46' 18"·96Local Mean Times of Elongation, February 18Eastern 14<sup>h</sup> 41<sup>m</sup>Western 15<sup>h</sup> 3<sup>m</sup>

ate		s of k)	FACE LEFT	FACE LEFT		
Astronomical I	Klongation	Zeros (Circle Reading Referring Mar	Observed Horizontal Angle:     .H     E     B     Reduction in Are to Time of E     Reduced Ol Ref. Mark       Diff. of Readings Ref. Mark – Star     .H     E     .H     E     .H     <	servation k — Star zation	Observed Horizontal Angle: Diff. of Readings Ref. Mark – Star	Reduction in Arc to Time of Elongation Ref. Mark-Star at Elongation
Feb. 13	E.	°' 30 55 & 210 56	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	, 34°26 37°10 32°42	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{vmatrix} & & & & \\ & & & & \\ & & & & \\ & & & &$
" 13	w.	30 55 & 210 56	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	24 · 57 23 · 76 24 · 17 23 · 59	$\begin{array}{c ccccc} - & 147 & 59 & 48 \cdot 09 \\ & 56 & 38 \cdot 58 & 10 & 58 \\ & 56 & 25 \cdot 34 & 2 & 21 \\ & 59 & 19 \cdot 90 & 40 & 25 \end{array}$	$\begin{array}{c cccc} + & 3 & 23 & 18 \\ \circ & 12 & 98 \\ \circ & 0 & 59 \\ 2 & 54 & 68 \end{array} \begin{array}{c} - & 147 & 56 & 24 & 91 \\ 25 & 560 \\ 24 & 75 \\ 25 & 25 & 22 \end{array}$
" 14	E.	110 8 & 290 8	$\begin{array}{c c c c c c c c c c c c c c c c c c c $	5 37 · 58 36 · 55 36 · 92 38 · 80	- 154 53 13.90 39 17 53 50.75 35 35 56 36.53 0 35 56 33.07 3 37	$ \begin{array}{ c c c c c c c c } -3&22\cdot07 & -154&56&35\cdot97 \\ 2&45\cdot94 & & 36\cdot69 \\ 0&0\cdot05 & & 36\cdot58 \\ 0&1\cdot73 & & 34\cdot80 \end{array} $
" 14	w.	110 8 & 290 8	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	5 23.78 23.11 25.53 26.29	- 147 57 26.97 24 8 56 44.54 14 31 56 56.70 17 18 58 1.64 30 5	$\begin{array}{c cccc} + & 1 & 2 \cdot 84 \\ & 0 & 22 \cdot 73 \\ & 0 & 32 & 17 \\ & 1 & 37 \cdot 02 \end{array} \begin{array}{c} - & 147 & 56 & 24 \cdot 13 \\ & 21 \cdot 81 \\ & 24 \cdot 53 \\ & 24 \cdot 62 \end{array}$
" 15	E.	189 20 & 9 20	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	5 37°26 38°76 39°12 37°64	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{vmatrix} -2 & 6.65 \\ 1 & 38.97 \\ 0 & 3.30 \\ 0 & 7.97 \end{vmatrix} - 154 56 37.19 \\ 35.89 \\ 37.60 \\ 36.18 $
" 15	<b>w</b> .	189 20 & 9 20	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	5 25.05 26.16 26.54 24.16	$\begin{array}{c ccccc} - & 147 & 57 & 6^{\cdot}42 & 19 & 19 \\ & 56 & 33^{\cdot}11 & 8 & 31 \\ & 57 & 15^{\cdot}84 & 21 & 25 \\ & 58 & 10^{\cdot}73 & 31 & 28 \end{array}$	$\begin{array}{c c c c c c c c c c c c c c c c c c c $
" 16	E.	268 32 & 88 32	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $	5 35°51 33°82 36°00 35°74	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$	$ \begin{vmatrix} -2 & 38 \cdot 09 \\ 2 & 7 \cdot 94 \\ 0 & 9 \cdot 68 \\ 0 & 17 \cdot 76 \end{vmatrix} - 154 & 56 & 37 \cdot 25 \\ 36 \cdot 41 \\ 34 \cdot 58 \\ 35 \cdot 76 \end{vmatrix} $

\* This station appertains to the Great Indus Series.

Date		rk) rk)	٦ د	ACE LEFT	FACE BIGHT				
Astronomical I	Elongation	Zeros (Circle Reading Referring Ma	Observed Horizontal Angle: Diff. of Readings Ref. Mark-Star	Reduction in Arc to Time of Elongation Ref. Mark-Star at Elongation	Diff. of Readings Ref. Mark-Star				
Feb. 16	w.	268 32 & - 88 32	$\begin{array}{cccccccccccccccccccccccccccccccccccc$	$\begin{array}{c ccccc} , & " & & & & & & \\ + & 2 & 28 \cdot 84 \\ & & 1 & 10 \cdot 64 \\ & & 0 & 1 \cdot 82 \\ & & 0 & 22 \cdot 19 \\ \end{array} \begin{array}{c} 0 & 1 \cdot 82 \\ & & 23 \cdot 34 \\ \end{array}$	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$				
" 17	E.	311 44 & 131 44	$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	$\begin{array}{c cccc} - & 0 & 2^{\cdot}13 \\ & 0 & 0^{\cdot}14 \\ & 3 & 8^{\cdot}67 \\ & 3 & 41^{\cdot}86 \end{array} \begin{array}{c} - & 154 & 56 & 38^{\cdot}48 \\ & 36^{\cdot}24 \\ & 36^{\cdot}20 \end{array}$	$ \begin{array}{c ccccccccccccccccccccccccccccccccccc$				
" 17	w	311 44 & 131 44	$\begin{array}{c cccc} - & 147 & 57 & 57 & 12 \\ & 57 & 2 & 32 \\ & 57 & 19 & 16 \\ \end{array} \begin{array}{c} 29 & 5 \\ 18 & 28 \\ 57 & 19 & 16 \end{array}$	$\begin{array}{c c} + & 1 & 31 \cdot 29 \\ & 0 & 36 \cdot 79 \\ & 0 & 54 \cdot 67 \end{array} - 147 & 56 & 25 \cdot 83 \\ & 25 \cdot 53 \\ & 24 \cdot 49 \end{array}$	$ \begin{array}{c c c c c c c c c c c c c c c c c c c $				

# Abstract of Astronomical Azimuth observed at LXII (Dáowála) 1881.

# 1. By Eastern Elongation of $\delta$ Ursæ Minoris.

Face	L	R	L	R	L	R	L	R	, <b>L</b>	R
Zero	81°	211°	110°	290°	189°	<b>9</b> °	269°	89°	812°	182°
Date	Februar	y 18	Febru	ary 14	Februa	ary 15	Februa	ury 16	Februa	ary 17
Observed difference of Circle-Readings, Ref. MStar reduced to Elongation	34·26 3 37·10 2 32·42	35°34 35°71	37 · 58 36 · 55 36 · 92 38 · 80	35°97 36°69 36°58 34°80	37 · 26 38 · 76 39 · 12 37 · 64	37 · 19 35 · 89 37 · 60 36 · 18	35°51 33°82 36°00 35°74	37°25 36°41 34°58 35°76	38.48 36.24 40.72 36.20	37 · 84 37 · 23 38 · 81 36 · 87
Means	34*59 :	35.23	37 . 46	36.01	38.20	36.72	35.27	36.00	37.91	37.69
Means of both faces Level Corrections Corrected Means Az. of Star fr. S., by W. Az. of Ref. M. "	- 154 56 35.0 - 0.3 - 154 56 35.3 - 154 56 35.3 183 51 27.3 28 54 51.9	)6 32 38 37 99	36 — 0 36 27 50	* * 06 * 80 * 59 > 79	37 + 0 36 27 51	• 46 • 71 • 75 • 82 • 07		* * 11 * 75 * 05 * 30		* *80 *01 *81 *28 *47

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#### PRINCIPAL TRIANGULATION. AZIMUTHAL OBSERVATIONS.

## Abstract of Astronomical Azimuth observed at LXII (Dáowála) 1881-(Continued).

Face	L 91°	R 911°	L 1109	<b>R</b> 2000	L 190°	<b>₽</b> o°	L 260°	R e0°	L 9199	<b>R</b>
		211		290	100		209		012	102
Date	Febru	ary 13	Febru	ary 14	Februa	ary 15	Februa	ury 16	Februs	ury 17
Observed difference of Circle-Readings Ref. M.—Star reduced to Elongation	24 · 57 23 · 76 24 · 17 23 · 59	" 24°91 25°60 24°75 25°22	" 23·78 23·11 25·53 26·29	" 24 · 13 21 · 81 24 · 53 24 · 62	* 25°05 26°16 26°54 24°16	" 26 · 20 25 · 31 26 · 63 24 · 67	" 20°76 21°98 24°73 23°34	* 21 ° 73 24 ° 03 24 ° 89 25 ° 88	" 25°83 25°53 24°49	# 27`44 25`51 23`20
Means	24.02	25.12	24.68	23.77	25.48	25.70	<b>32 · 7</b> 0	24.13	25.28	25.38
	0 1 11		"		17		"			
Means of both faces Level Corrections Corrected Means Az. of Star fr. S., by W. Az. of Ref. M. "	- 147 56 24 - 0 - 147 56 24 176 51 13 28 54 48	57 17 74 33 59	24 + 0 23 13 49	*23 *25 *98 *67 *69	25 + 0 24 13 48	· 59 · 66 · 93 · 90 · 97	23 - 0 23 14 50	•42 •08 •50 •12 •62	25 + 0 25 14 49	* 33 * 14 * 19 * 35 * 16

# 2. By Western Elongation of 51 Cephei.

	(by Eastern Elongation		1	•••	•••	28 54	51.32
Astronomical Azimuth of Referring Mark	by Western	,,	•••	•••	•••	"	49.41
	(	Mean	•••	•••	•••	"	50:37
Angle Referring Mark and LI (Ghundi) see 1	•••	•••		— o 5	22.73		
Astronomical Azimuth of Ghundi by observat	ion	•••	•••	•••	•••	28 49	27.64
Geodetical Azimuth of " by calculat	ion from that	adopted	(Vol. II,	p <b>age 141)</b>	at		
Kaliánpur: see page 206 ante	•••	•••	•••	•••	•••	28 49	22.63
Astronomical-Geodetical Azimuth at LXII (]	Dáowála)	•••	•••	•••	•••	+	5.01

July, 1885.

W. H. COLE, In charge of Computing Office.

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PLATE 2.

Fig. No. 10





Fig. No. 8 XXXVIII XXXV¢ 20 CONTRACTOR 10







C. F. Guthrie, Photo.

Photozincographed at the Office of the Trigonometrical Branch, Survey of India, Dehra Dún, July 1882.





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List of Published Works of the Great Trigonometrical Survey of India.

- An Account of the Measurement of an Arc of the meridian between the parallels of 18° 3' and 24° 7', being a continuation of the Grand Meridional Arc of India as detailed by the late Lieutenant-Colonel Lambton in the Volumes of the Asiatic Society of Calcutta. By Captain George Everest, of the Bengal Artillery, F.R.S., &c. London, 1830.
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- I. The Standards of Measure and the Base-Lines, also an Introductory Account of the early Operations of the Survey, during the period of 1800-1830. By Colonel J. T. Walker, R.E., F.R.S., &c., &c., Superintendent of the Survey. Dehra Dún, 1870.
- Do. II. History and General Description of the Principal Triangulation and of its Reduction. By Colonel J. T. Walker, C.B., R.E., F.R.S., &c., &c., Surveyor General of India and Superintendent of the Survey, and his Assistants. Dehra Dún, 1879.
- Do. III. The Principal Triangulation, the Base-Line Figures, the Karáchi Longitudinal, N.W. Himalaya, and the Great Indus Series of the North-West Quadrilateral. By Colonel J. T. Walker, R.E., F.R.S., &c., &c., Superintendent of the Survey, and his Assistants. Dehra Dún, 1873.
- Do. IV. The Principal Triangulation, the Great Arc (Section 24°-30°), Rahún, Gurhágarh and Jogí-Tíla Meridional Series, and the Sutlej Series of the North-West Quadrilateral. By Colonel J. T. Walker, R.E., F.R.S., &c., &c., Superintendent of the Survey, and his Assistants. Dehra Dún, 1876.
- Do. IVA. The Principal Triangulation of the North-West Quadrilateral, including the Reduction and Details of the Jodhpore and Eastern Sind Meridional Series. Prepared in the Office of the Trigonometrical Branch, Survey of India, Colonel C. T. Haig, R.E., Offg. Deputy Surveyor General, in charge, and published under the orders of Colonel G. C. DePrée, S.C., Surveyor General of India. Dehra Dún, 1886.
  - V. Details of the Pendulum Operations by Captains J. P. Basevi, R.E., and W. J. Heaviside, R.E., and of their Reduction. Prepared under the directions of Major-General J. T. Walker, C.B., R.E., F.R.S., &c., &c., Surveyor General of India and Superintendent of the Trigonometrical Survey. Dehra Dún and Calcutta, 1879.
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Account of the Operations of the Great Trigonometrical Survey of India—(Continued).

- Volume VI. The Principal Triangulation of the South-East Quadrilateral including the Great Arc-Section 18° to 24°, the East Coast Series, the Calcutta and the Bider Longitudinal Series, the Jabalpur and the Biláspur Meridional Series, and the Details of their Simultaneous Reduction. Prepared under the directions of Major-General J. T. Walker, C.B., R.E., F.R.S., &c., &c., Surveyor General of India and Superintendent of the Trigonometrical Survey. Dehra Dún, 1880.
  - VII. General Description of the Principal Triangulation of the North-East Quadrilateral including the Simultaneous Reduction and the Details of Five of the Component Series, the North-East Longitudinal, the Budhon Meridional. the Rangír Meridional, the Amua Meridional, and the Karára Meridional. Prepared under the directions of Lieutenant-General J. T. Walker, C.B., R.E., F.R.S., &c., &c., Surveyor General of India and Superintendent of the Trigonometrical Survey. Dehra Dún, 1882.
  - VIII. Details of the Principal Triangulation of Eleven of the Component Series Do. of the North-East Quadrilateral, including the following Series; the Gurwani Meridional, the Gora Meridional, the Hurílaong Meridional, the Chendwar Meridional, the North Parasnath Meridional, the North Malúncha Meridional, the Calcutta Meridional, the East Calcutta Longitudinal, the Brahmaputra Meridional, the Eastern Frontier-Section 23° to 26°, and the Assam Longitudinal. Prepared under the directions of Lieut.-General J. T. Walker, C.B., R.E., F.R.S., &c., &c., Surveyor General of India and Superintendent of the Trigonometrical Survey. Dehra Dún, 1882.
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- II. The Great Arc—Section  $24^{\circ}$  to  $30^{\circ}$ , or Series  $\varDelta$  of the North-West Quadrilateral. Do. By Colonel J. T. Walker, R.E., F.R.S., &c., &c., Superintendent of the Survey, and his Assistants. Dehra Dún, 1874.
- The Karáchi Longitudinal Series, or Series B of the North-West Quadrilateral. Do. III. By Colonel J. T. Walker, R.E., F.R.S., &c., &c., Superintendent of the Survey, and his Assistants. Dehra Dún, 1874.
- Do. IV. The Gurhágarh Meridional Series, or Series F of the North-West Quadrilateral. By Colonel J. T. Walker R.E., F.R.S., &c., &c., Superintendent of the Survey, and his Assistants, Dehra Dún, 1875.

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- V. The Rahún Meridional Series, or Series *E* of the North-West Quadrilateral. By Colonel J. T. Walker, R.E., F.R.S., &c., &c., Superintendent of the Survey, and his Assistants. Dehra Dún, 1875.
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- Do. XII. The Calcutta Longitudinal Series, or Series *B* of the South-East Quadrilateral. By Major-General J. T. Walker, C.B., R.E., F.R.S., &c., &c., Surveyor General of India and Superintendent of the Survey, and his Assistants. Dehra Dún, 1880.
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- Do. XIII A. The South Párasnáth Meridional Series and the South Malúncha Meridional Series of the South-East Quadrilateral. Prepared in the Office of the Trigonometrical Branch, Survey of India, Colonel C. T. Haig, R.E., Offg. Deputy Surveyor General, in charge, and published under the orders of Colonel G. C. DePrée, S.C., Surveyor General of India. Dehra Dún, 1885.
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- Do. XVIII. The Huríláong Meridional Series, or Series P, and the Chendwár Meridional Series, or Series Q of the North-East Quadrilateral. By Lieutenant-General J. T. Walker, C.B., R.E., F.R.S., &c., &c., Surveyor General of India and Superintendent of the Survey, and his Assistants. Dehra Dún, 1883.

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- Volume XIX. The North Párasnáth Meridional Series, or Series R, and the North Malúncha Meridional Series, or Series S of the North-East Quadrilateral. Prepared by J. B. N. Hennessey, Esq., M.A., F.R.S., &c., &c., Offg. Deputy Surveyor General, in charge of Trigonometrical Surveys, and his Assistants, and published under the orders of Colonel G. C. DePrée, S.C., Offg. Surveyor General of India. Dehra Dún, 1883.
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